PWGSC

Quality in Environmental Services VENUS MINE TAILINGS

SITE REHABILITATION

CONSTRUCTION MANAGEMENT REPORT



December 1995

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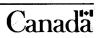
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VENUS MINE TAILINGS: SITE REHABILITATION

CONSTRUCTION MANAGEMENT REPORT

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EXECUTIVE SUMMARY

The work under this contract is the Site Rehabilitation of the Venus Mine Tailings located 22 km south of Carcross, Yukon. All work was completed as per the PWGSC specifications and drawings. The main components of the design includes the installation of a Waterloo Barrier sheet pile wall system, a cap over the tailings consisting of a geotextile, clay layer and a capillary break, the construction of a plug at the outlet of the asbestos decant pipe and a drainage discharge system.

Public Works and Government Services Canada (PWGSC) was retained by the Department of Indian Affairs (DIAND) to provide construction management and on-site supervision during the execution of the work. The prime contractor was the Carcross/Tagish Development Corporation (CTDC). The subcontractor for the installation of the Waterloo Barrier was C3 Environmental.

The work began on August 11, 1995 and was completed on October 20, 1995. Overall, the project proceeded as planned.

This report should be read in conjunction with thew C3 Environmental report entitled "Waterloo Barrier System - Sheet Pile & Sealant Installation Report, October 16th, 1995." The geotechnical information was not included in this report, however, should this information be required, a copy of the report can be obtained from Public Works and Government Services Canada.

The actual total cost of the project is \$1,198,880 excluding the engineering costs. The budget was \$1.2 million including \$100,000 for contingency. The project objectives were met, the total cost was under the allowed budget, and the work was completed on schedule.

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INTRODUCTION

The rehabilitation of the Old Venus Mine tailings pond was initiated by Indian Affairs and Northern Development(DIAND), Action on Waste, in collaboration with the Carcross/Tagish Development Corporation(CTDC) and Public Works and Government Services Canada (PWGSC). The project is funded by DIAND as part of their Action-on-Waste program and the contract is a contribution agreement between DIAND and the CTDC, the prime contractor for this project.

Two drilling programs were undertaken during the summer of 1995 by J.R.Paine and Associates. The first program took place between June 15th and 21st. The drilling program was design to confirm the tailings' volume quantity. Originally, the scope of work included the relocation of the tailings pond to a receiving gravel pit at km 97.5 along the Klondike highway. However, a reevaluation of the options was necessary due to public opposition. The containment of the tailings in-place became the reasonable option. At this point, a second drilling program was undertaken by J.R.Paine on July 19th and 20th. With this information, Public Work and Government Services Canada provided drawings and specifications.

The CTDC reviewed the PWGSC specs and provided an estimated cost of \$1,064,464.00. The cost estimate was approved and the work commenced on August 11th. The Contribution Agreement was signed on August 25, 1995 (see Annex A for details).

There are several components to the design which will reduce the release of contaminants into the environment and are as follows:

- 1. The Waterloo Barrier Sheet Pile Wall which minimizes the lateral migration of leachate from the tailings pond;
- 2. <u>The Capping Material</u> which ultimately serves multiple purposes. The cap consists of the following:
 - a Nilex nonwoven geotextile C24 immediately overlying the tailings;
 - 200 mm layer of silty clay cap; and
 - 300 mm layer of capillary break material.

The capping material eliminates the potential for erosion of the tailings surface, maintains the tailings in a saturated state and minimizes upward migration of contaminated water and tailing fines. The saturated state design is to minimize Acid Rock Drainage(ARD) which is a natural, chemical and biological oxidation of reactive sulphide mineral when exposed to air and water. The leaching and "flushing" of these chemical products is the cause of adverse effects to the environment.

3. The Asbestos Cement Decant pipe has been sealed at its upstream and downstream ends to prevent water and sediments from flowing into the lake environment. Originally, surface runoff ran across the tailings pond picking up fine tailing particles. The runoff would flow into the inlet of the decant pipe, discharging into Tagish Lake and depositing the suspended fines. The cap at the outlet prevents further discharge of tailings fines into the lake environment.

- 4. <u>Drainage Discharge System</u> controls the surface runoff level above the capping material.
- 5. <u>Underlying dense stiff clay</u>, although it is not man made, provides an excellent barrier below the tailing and minimizes any vertical migration of contaminated water.

J.R.Paine and Associated Ltd. and Underhill Professional Land Surveyors and Engineers provided the necessary engineering services. J.R.Paine provided construction management services during the initial phase of the work and conducted drilling and material testing programs. Underhill provided land surveying services including the layout of the Waterloo Barrier system and in-place volume quantities.

Pathway analysis was performed by Michael Goldstein of Soilcon Laboratories LTD. in Richmond, B.C. The report is entitled "Pathway Analysis and Reclamation Plan at the Old Venus Mine Tailings."

Some issues emerged during the execution of the work: highway culvert repair and settlement near the Waterloo Barrier. The highway culvert was damaged during the installation of the Waterloo Barrier. Additional costs were incurred by the contractor to performed the repairs. Additional concerns arose due to the sealing capabilities of the culvert. Several remedial options have been presented in this report. The settlement of the tailings near the Waterloo Barrier occurred at the completion of the work. Additional capillary break material was hauled to fill the settled area. An evaluation of the site will be required during the summer of 1996 to confirm the cause and effect of the settling tailings.

The work was completed on October 20, 1995.

PART A

1.0 WATERLOO BARRIER INSTALLATION

The Waterloo Barrier System is an low permeability interlocked steel sheet pile wall system. The wall is designed to provide containment of the tailings pond. From a plan view, the wall ties into the bedrock outcropping at the south west corner of the tailings pond, borders the south and east edges of the pond and ties into the bedrock outcrop at the north east corner of the site (see Diagram no.1 for details).

The contract for the installation of the Waterloo Barrier System was awarded to C3 Environmental, a division of Canadian Construction Controls Limited. Pile driving was subcontracted to a local company: R.C.Crane and Construction Ltd. of Whitehorse, Yukon. Quality control was performed by C3 Environmental engineers during the installation of the system.

The sheet pile joints are sealed with silica fume modified, thiotropic cementitious based grout WBS Type 301. The process of grouting begins by a "flushing stage". Flushing involves lowering a high water pressure hose into the wall joints and flushing accumulated soil. At the same time, the joint is checked for depth which indicates the condition of the sheet pile wall. Quality control of the cementious grout was also ongoing.

The installation of the Waterloo Barrier System commenced at the south section of the site on September 2nd. According to the geotechnical logs, a boulder stratum exists from 2.5 m to 3.5 m depth underlaid by stiff native clay. An attempt was made by the installation crew to drive the pile into the boulder stratum but was unsuccessful because the sheet pile could not penetrate passed the boulder stratum without damaging the top of the pile. This method was attempted from pile No. 19 to No. 56. From pile No. 57, a trench was excavated to remove the difficult boulder stratum. The sheet piles were placed into the trench, driven into the underlying clay and backfilled. This created an adequate seal between the bottom of the wall and the native clay.

From pile no. 200 to 341, the geotechnical logs from J.R.Paine and Associates Ltd indicated shallower bedrock. The pile were custom cut to follow the bedrock profile. Since trenching, rather that driving, had become the standard procedure, a trench was excavated. This enabled the inspection of the exposed bedrock for fissures and other characteristic hindering the proper seal of the wall/bedrock joint. The bedrock was inspected and appeared acceptable for our purposes. The piles were placed above the exposed bedrock and backfilled on both sides.

The PWGSC drawings indicate the design location of the Waterloo Barrier wall. However, circumstances dictated a slight offsetting from its intended location. The wall varied from the design for two reasons: lack of staging area for the installation equipment and shallow bedrock profile. The first reason for modifying the wall location was that the installation crew required a 5 m wide working area on both side of the wall for their heavy equipment.

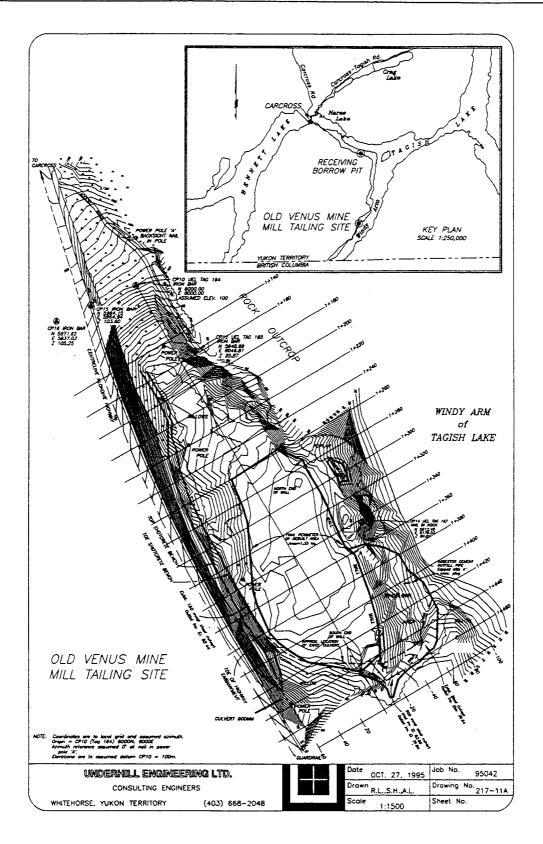


Diagram 1: Site Drawing

The design drawing show the Waterloo Barrier at the edge of the existing berm, leaving no work space on the east side of the wall. The wall location was therefore amended and offset inward by 5 m toward the tailings(see as-built drawings in Annex D). The second reason for altering the wall location was the shallow bedrock encountered near the outcrop at survey benchmark no. 166. Overburden was excavated at the west side of the outcrop during the levelling of the tailings. The ground elevation was lowered by approximately 2 m. A trench was dug at the intended location of the wall. The bedrock was found at a depth of 0.1 m to 0.5 m. Therefore, the wall was relocated farther around the outcrop to enable a deeper section of the wall to be installed, making it more stable (see annex D for details).

Various types of equipment were required during the installation of the Waterloo Barrier system. The heavy equipment was obtained through R.C.Crane and Construction Ltd. The following equipment was used by this contractor:

- Lewis 2500 lb Drop Hammer;
- Grove 20 Ton Telescopic Boom Crane;
- P&H 20 ton Lattice Boom Crawler Crane;
- P&H Track Backhoe; and
- Cat 950 Front End Loader.

C3 Environmental were responsible for grouting and sealing the joints. The following equipment was used:

- Colloidal Mixer;
- Grout Holding/Agitator Tanks;
- · Water Measuring Equipment;
- Viscosity Measuring Equipment;
- Portable Air Compressor;
- Moyno 3L4 Progressive Cavity Pump;
- Grout Volume Measuring Equipment; and
- Grout Lines and Pressure Control Valves.

Like the heavy equipment, the man power was divided into two crews: the sheet pile installation and grouting crew. The sheet pile installation crew consisted of 2 heavy equipment operators and one labourer from R.C.Crane. The cutting and welding of the wall's top sections was also performed by this contractor as required. The C3 Environmental crew consisted of a sheet pile installation quality control engineer and a labourer. The grouting crew consisted of a grouting quality control engineer and three labourers: two labourers were hired locally and the other was a C3 Environmental employee.

The construction of the Waterloo Barrier System began on September 2nd and was completed on September 21st. The pile driving took 16 days to complete and was completed on September 17th. The grouting of the joints commenced on September 13. The scheduled timeframe for this work had been 6 weeks commencing on August 28th. The work commenced slightly behind schedule, however, the installation crew worked 14-hour days and

7-day weeks to completed the work two weeks ahead of schedule.

C3 Environmental supplied a Quality Control Documentation entitled Waterloo Barrier System: Sheet Pile & Sealant Installation Report which includes the following information:

- 1. Pile identification number;
- 2. Date and time of driving;
- 3. Model of hammer and energy rating;
- 4. Elevation of top of pile;
- 5. Length of sheet pile in the ground when driving is complete;
- 6. Rate of penetration in feet per minutes;
- 7. Detailed remarks concerning alignment, obstruction, etc..;
- 8. Plumbness records of each joint installed; and
- 9. Joint flushing records for each joint.

The Waterloo Barrier System Quality Control document is not included in this report. However, should it be required, it may be obtained by contacting Public Works and Government Services Canada.

The total labour, equipment and material cost of this item was \$548,000. No cost overruns were incurred for this item of the contract.

2.0 SILTY CLAY CAP

This item of the contract includes supplying, loading, hauling, placing, grading and compacting a clay capping material. It consists of a 200 mm layer of silty clay material placed over the geotextile. The material was hauled from the old residential school site 2 km north of Carcross off highway 37 to Tagish. The purpose of the clay cap is to isolate the tailings pond and reduce potential contamination of surface runoff. An Atterberg Limit was performed and the results are as followed:

Liquid limit	23.1 %
Plastic Limit	19.0%
Plastic Index	4.1%
Unified Soil Classification	CL
T	

Permeability Range using

Standard Proctor Compaction 0.0004 to 0.00005 cm/hr

The hauling and placing of the clay material took approximately 11.5 days. A total of 880 loads were hauled with an average of 13 to 14 loads per truck per day. The hauling was performed during two periods: the first 480 loads were hauled and placed on the north third of the tailings and the remaining 400 were later hauled and placed at the south end.

During the construction, the tailing's pond final grade elevation was lowered from 82.5 m to 82.35 m. A mass balance calculation was performed to determine the final grade utilizing

the materials available on the tailings. Since the thickness of the silty clay is 200 mm, the final elevation of the clay was set at 82.55 m. Once the levelling of tailings at the north half was completed, the initial 480 loads of silty clay were hauled and placed. This work took place between September 18 and September 23, inclusively. Six trucks were used to haul the first 480 cu.m. of material.

At the west side of the north half, difficult conditions were encountered. The placement of clay was near impossible due to the tailings' extremely saturated condition. At this point, it was determined that a solid subbase was absolutely required to properly place the clay layer. To construct a solid subbase at the south half, additional dry material was relocated from the wind blown area. This raised the south tailings' final elevation to the original design elevation of 82.5 m. Consequently, the final elevation of the clay returned to 82.7 m across the entire site, hence requiring additional clay material at the north half of the tailings pond. The final clay thickness at the north half was therefore increased to 450 mm. Relocation of the wind blown tailings and final levelling of the south half of the tailings pond was completed on September 27. The following day, the hauling and placing of the remaining clay resumed and was completed on October 4.

The estimated in-place quantity of clay material was 2650 cu.m. This was based on the surface area of tailings of 13,300 sq.m. and the 200 mm layer of in-place clay material. However, the final clay volume exceeded the initial estimate by 1200 cu.m. and totalled 3850 cu.m. This increase in volume was due to consolidation, settlement and a change of tailing grade at the north portion of the tailings pond. The original item cost was estimated at \$50,100 based on a \$18.90/cu.m. unit rate.

	Expected	Actual
Volume	2650	3850
Cost	\$50,100	\$72,765

The equipment used for this task included haul trucks as described above, a Cat 950 front end loader, a Caterpillar D4 LGP and D6D. The D6D was used mainly for placing the clay along the east edge of the site where the tailing subbase was sufficiently stable. On the other hand, the D4 LGP was used where the tailings subbase was too saturated and unstable for the heavier D6D. The Caterpillar D4 LGP, being lighter that the D6, also had 30" wide pads(rather that 24" pads). This piece of equipment was necessary for placing the clay material over unstable tailings.

3.0 <u>COLLECT AND BURNING OF DEBRIS</u>

This item of the contract includes the collection and burning of wooden debris and brush located throughout the site. The burning of debris started on September 11, 1995 and was completed on September 12th. The work included cutting brush and small trees at the berm and wind blown tailings areas. It also included collecting the wooden debris located above the dike. All the combustible materials were collected onto the tailings area and set ablaze.

Also included under this item of the contract, a low permeability plug was constructed at the inlet and outlet of the asbestos cement decant pipe. The inlet was plugged with bentonite clay and capped with concrete as shown in Diagram no. 2. This work was performed on August 29th and 30th.

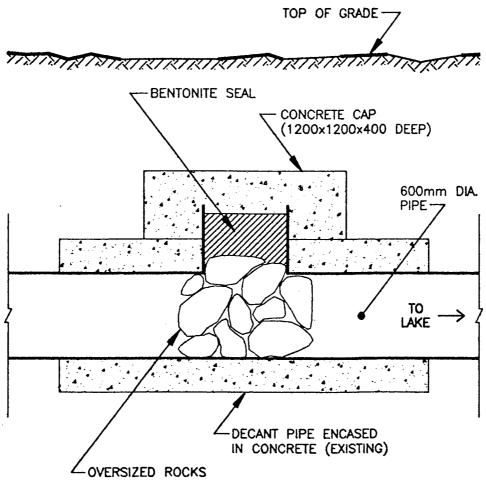


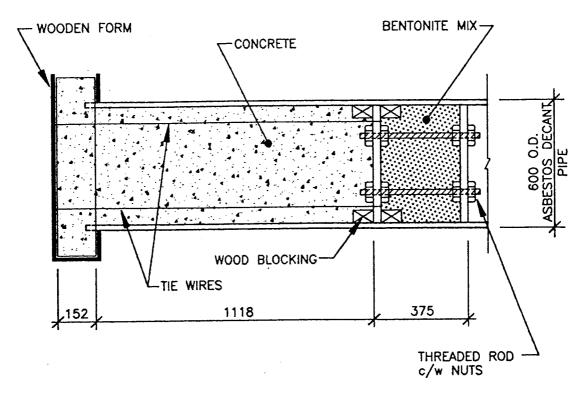
Diagram 2: Details of Decant Pipe Plug at Inlet

A concrete plug was also constructed at the outlet of the asbestos cement pipe at the lake shore. Three 12' asbestos pipe sections were removed at the outlet. A plug was constructed consisting of a 1.2 m concrete plug and a bentonite plug of 375 mm thick (see Diagram no.4 for details).

The work involved building circular wooden forms and placing them into the asbestos pipe. The concrete was poured on Saturday, October 14. Due to cool nights in October, a torch and a tarp were installed to maintain a warm environment for the curing process. On the following Monday, the bentonite plug was poured from the top of the asbestos pipe. J.R.Paine and Associates recommended using a 1:1:1 mix of PUREGOLD bentonite chips, X-tra Gel high yield bentonite and portland cement.

This portion of the project took approximately 5 days to complete. The total cost was \$4,032 as per the Contribution Agreement between DIAND, Arctic Environmental Strategy, and the Carcross/Tagish Development Corporation.

The only heavy equipment required for this activity was an excavator to remove the three sections of asbestos pipe.



SECTION

Diagram 3: Detail of Decant Pipe Plug at Outlet

4.0 EXCAVATING AND LEVELLING TAILINGS

4.1 Excavate and relocated wind blown tailings located outside the Waterloo Barrier

This part of the contract included excavating and placing wind blown tailing material originally located outside the original berm and consolidating them within the tailings pond area. In total, 3656 cu.m. were excavated from the wind blown tailings area. This work was accomplished in two sections: an initial 1120 cu.m. of wind blown tailings was excavated and completed on September 7 and an additional 2043 cu.m. of mainly native clayey material was excavated on September 25th and 26th and relocated onto the tailings pond area.

The initial 1120 cu.m. of windblown tailings were excavated as per the PWGSC specifications. However, the laboratory results from the confirmatory samples taken indicated that additional wind blown tailings would need to be excavated and relocated onto the tailings pond.

The dry condition of the wind blown tailings also assisted greatly in the levelling of the tailings: dry material placed above wet tailings made it easier for the levelling process. Once the 1120 cu.m. were relocated, a mass-balance calculation was conducted by Underhill. The results of this calculation indicated that an additional 1400 cu.m. was required to bring the level of the tailings to the design elevation of 82.5 m. This estimated volume did not account for consolidation and would most likely be in the order of 1600 cu.m. after consolidation and settlement. To avoid cost overruns for this item, the final elevation of the tailings was lowered from 82.50 m to 82.35 m (thus requiring no additional material to be hauled).

To achieve 82.35 m across the entire site, excessive handling of the tailings pond material was required. Through capillary forces, the pore water migrated upward. The top 500 mm layer of tailings quickly exceeded its liquid limit and became unstable and unworkable. Several attempts were made to let the tailings dry before resuming the levelling process. However, only a few passes were necessary before the D4 LGP dozer would get stuck. Levelling proceeded very slowly due to these saturated conditions. Consequently, the contractor tried a different approach. He placed the D6 dozer at the perimeter on stable ground and tied the winch cable to the back of the D4 LGP dozer. The D4 would crawl across the saturated tailings pulling the D6D's winch cable. Once he was far enough and almost stuck, the D4 LGP would get winched out as it backbladed. The D4 LGP would once again venture into the saturated tailings and get pulled out by the D6D and so on. This "Yo-Yo" method was much more effective for relocating saturated soil.

Finally, the saturated tailings final grade was achieved at 82.35 m. However, the moisture content was so high (exceeding the liquid limit), that the contractor was unable to place the textile and the clay without creating deep ruts with the dozer and damaging the geotextile material in the process. After covering the north half of the tailings pond, it became evident that a solid base would be required in order to properly place the geotextile and the clay. Several attempts were made to allow the tailings to dry and the pore water to settle. However, when there tailings appeared dry and stable, only a few passed with the dozer was required before saturated and unstable conditions would return. This meant that additional dry soil would be required, hence, the tailings final grade was reset to 82.5 m. The least expensive and most readily available dry material was located at the wind blown tailings area.

An additional 2043 cu.m. was excavated from this area. Little quantity was actually wind blown tailings material, but rather, the majority appeared to be native clayey silt. With a dozer, the contractor began near the Waterloo Barrier and pushed the top 300 mm of saturated tailings toward the west side of the pond as he filled in with native dry material. This provided a solid base for working as he continued to push the wet material further and further away from the wall. Within 4 days, the contractor had levelled the majority of the remaining south portion of tailings and had constructed a solid subbase for placing the geotextile and

the clay. The total excavated material from the wind blown tailings was 3656 cu.m. The original contract estimate was 1600 cu.m.. However, due to excessive consolidation, an additional 2043 cu.m. was required.

	Expected	Actual
Volume	1600 m ³	3656 m^3
Cost	\$9760	\$22,301.60

A estimated total of 7 days was required to relocate the wind blown tailings to the tailings pond. Equipment required to complete this work were a Northwest excavator, a Caterpillar D8, D6 and D4 LGP dozer. The Caterpillar D8 dozer was used to stockpile and the Northwest excavator to relocate the stockpile over the Waterloo Barrier.

4.2 Excavate and Relocate Tailings

The excavation and relocating of the tailings inside the Waterloo Barrier includes cutting the material at the perimeter located above the 82.5 m elevation grade, relocating it to low areas such as the center of the pond area. This activity was done concurrently with the excavating and relocating of the wind blown tailings. The work days for this activity was 34 days. The work was primarily done using the Cat D4 LGP dozer. The duration of this work was expected to take 2 weeks. Due to the saturated tailing conditions, this activity took an additional 3 weeks.

The initial phase of the levelling work included the construction of a temporary drainage ditch. Its function was to divert the spring water around the tailings. A filter dike was construction at its outlet to filter suspended tailings. The filter was maintain throughout the duration of the project.

The original estimate for the volume of the tailings to be excavated was 1700 cu.m. However, because the final elevation for the north third of the tailings pond was lowered 150 mm to 82.35, an additional 526 cu.m. was excavated. The circumstances for theses changes are included in the section 4.1 "Excavation and Relocation of wind Blown Tailings" of this report. The following table indicates the expected and actual cost incurred for this item of the contract at a unit cost \$8.82/cu.m.

	Expected	Actual
Volume	1700 m^3	2225 m^3
Cost	\$15,000	\$19,633.32

4.3 Final Shaping and Grading of Tailing Pond

The final shaping and grading was performed concurrently with the excavation and relocating of the tailings. Some backblading was required which took little time. Once the tailings were levelled, the dozer did the minimum amount of activity on the tailings to avoid activating the capillary forces and saturating the surface tailing. An estimated 80% of the tailing pond surface was very stable. The remaining 20% ranged from semi-saturated to extremely saturated. A 3000 sq.m. area of tailings at the west edge was covered with a second layer of geotextile above the clay cap. The textile also provided additional stability when placing the capillary break material.

This work was performed by backblading with either the cat D6D (or the D4 LGP in softer areas). The unit cost for this item of the contract was \$0.36/sq.m. for a 13,300 sq.m. area and a total cost of \$4655.

5.0 SUPPLY AND INSTALL GEOTEXTILE

This section of the contract includes the purchasing of a Nilex non-woven geotextile(C24) and installation as per the manufacturer requirements. The Nilex geotextile has two purposes. From a construction perspective, it provides stability during the placement of clay material. From a design point of view, the textile acts as a filter to prevent tailings fines from migrating upward to the surface.

The materials arrived on site on September 8. On September 18, the hauling and placing of the clay material commenced, hence, the geotextile was placed concurrently. The cloth was overlapped by 24" in areas where the tailings was very soft. A 12" overlap was used in areas of stable tailings. The entire levelled tailings pond was covered with the textile and overlaid by the silty cap. Additional textile was placed to cover a 3000 sq.m. area at the west edge of the tailings. Due to extremely saturated and unstable conditions, the textile may have been damaged when the clay was placed. Approximately 25 rolls of geotextile were placed below the clay and an additional 5 rolls to cover the 3000 sq.m. of wet clay.

Two labourers were required to place the textile and was accomplished by manually unrolling the rolls. A estimated 6 man-days were required to place the textile across the entire site. This item cost was on a unit price basis for a design surface area of 13,300 sq.m.. The contractor's unit rate for this item of the contract was \$3.38/sq.m. (supplied and installed). The total cost for this item was \$44,954.

6.0 CONSTRUCTING DRAINAGE DISCHARGE SYSTEM

The drainage discharge system is composed of a 600 m diameter corrugated galvanized culvert located at the south end of the tailings pond. This system drains excess surface runoff from the top half of the capillary break. The elevation of the outlet is 82.85 m, therefore maintaining a saturated condition for the bottom 150 mm of the capillary break, the clay cap

and the tailings. A dry condition is maintained for the top 150 mm of the capillary break.

A 120 cm x 25 cm notch was cut at the top of the wall. A flared end section was tack-welded to the wall and connected to the culvert. The culvert was installed at a 5% grade (approx) and runs southward perpendicular to the Waterloo Barrier for a distance of 60 ft to an 90° elbow. Then it runs eastward toward the outlet of the Highways Culvert for 80 feet (see as-built drawings for details). The culvert was backfilled at and near the elbow to provide structural stability. The outlet of the drainage system is composed of a second flared end section which discharges the runoff into a small ditch lined with gravel material.

The work commenced on October 17th. A welder cut a 120 cm x 25 cm notch into the top portion of the Waterloo Barrier. He tack-welded a flared end section to the wall. The area was then graded and prepared for the installation of the culvert. The next day, five 20' sections of 600 mm corrugated culvert and the 90° elbow were installed. On October 20th, three additional 20' sections were delivered to the site and installed along with the outlet flared end section.

This item was costed on a lump sum basis. However, since only 25 m of culvert was installed instead of 80 m, the item cost was reduces as follows:

	Expected	Actual
Length	80 m	25 m
Cost	\$15,053	\$4704.06

The installation of 25 m of culvert required 3 manhours of cutting and welding and an estimated 3 mandays for the installation of the discharge system. An excavator was used to handle the culvert sections into place. The D4 LGP dozer graded and prepared the area for the installation of the culvert.

7.0 CAPILLARY BREAK MATERIAL

The loading, hauling, placing, grading and compacting of 75 mm minus screened pitrun material is included in this item of the contract. The purpose of this material is to prevent erosion of the clay cap material and provide a break in the capillary forces. The idea behind the coarse gravel is to maintain the tailings saturated while providing a relatively dry and stable surface.

A grain size analysis was performed on the material and is enclosed in Annex F: J.R.Paine Construction Management report. The original cost estimate for this activity included the screening pitrun to meet the design gradation specification for 75 mm gravel. The cost was estimated at approximately \$13,000. To avoid delay of project, an arrangement was made between the CTDC and the Yukon Territorial Government(YTG) to purchase gravel material, at a cost of \$5.00/cu.m from their Kilometer 90 pit. This cost was estimated at \$25,000

rather that \$13,000 for screening; hence increasing the cost by \$12,000 for this item. The Carcross/Tagish Development Corporation reviewed their estimated costs taking into account the proximity of the pit(2.5 km) and the time frame for loading, hauling and placing of the material. In conclusion, the CTDC estimated that this additional cost would be absorbed into their original cost estimate of \$16.16/cu.m.

The hauling and placing of the pitrun commenced early afternoon of October 11. The work proceeded quickly and was completed on Sunday, October 15. The loading, hauling, placing and compacting of pitrun material at the outlet was also included under this item. Approximately 10 loads of unscreened pitrun material and 10 loads of 75 mm minus screened material was hauled concurrently with the hauling and placing of the capillary break material. Both items(item 7.2.7 and 7.2.8) were combined into this item because both were hauled from the same location, hence justifying having identical hauling costs. The material was placed in 300 mm lifts and compacted with the dozer to minimize potential settlement.

A total of approximately 550 loads of gravel was hauled. The first 400 loads were hauled in approximately 2.5 days using 8 haul trucks. The remaining 150 were hauled 3.5 days using 2 to 3 haul trucks. Approximately 4 loads were hauled per hour per truck. The work proceed extremely quickly during the first two and a half days, however, the pace was slowed down to enable the dozer to properly place and grade the gravel material.

The unit cost for the capillary break material was \$16.16/cu.m. Included in this cost is the \$5/cu.m. the YTG charged for the supply of the material. The costs are outlined in the following table:

	Expected	Actual	
Volume	4100 m^3	4725 m^3	
Cost	\$66,250	\$76,356	

The equipment used for hauling were band member haul trucks. The placing of the material was performed in combination by the D6 and the D4 LGP.

8.0 SUPPLY AND PLACE PITRUN AGGREGATE AT OUTFALL AREA

This item was deleted from the contract. Rather, pitrun material was hauled, place, compacted and included in the previous item(Capillary break Material). The material was taken from the same pit and therefore, justifies the consolidation of both items into one and costed at the same unit rate(see previous item).

9.0 COST TO COMPLETE

The cost to complete includes administration, supervision and other miscellaneous costs. This item was a fixed cost for \$344,779.

PART B

1.0 PROJECT COST REVIEW

This section reviews the construction costs for the project. Additional cost were incurred by the CTDC for work above and beyond the original items in the PWGSC specification document. This included additional labour, equipment and material costs incurred due to difficult working conditions during the levelling of the tailings pond and during the highway culvert repairs. Table 1 summaries and compares the itemized contract unit and lump sum costs and the actual cost.

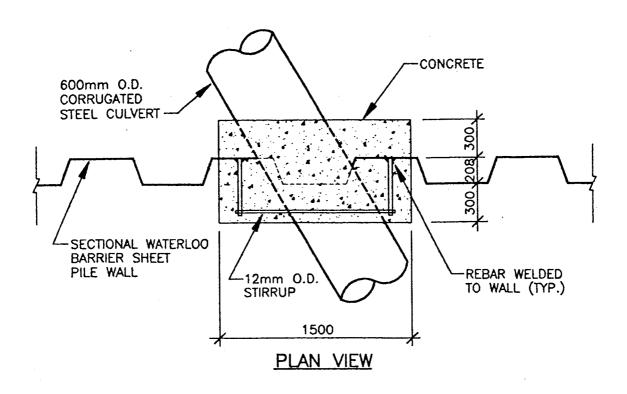
1.1 Additional Cost to the Contract

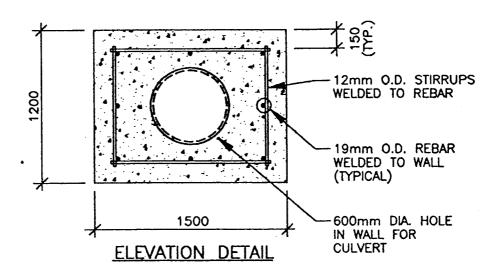
Due to unforseen circumstances, the project incurred some additional costs including the repair of the highway culvert, additional equipment time, labour and "cost to complete" costs. The extra costs incurred for the repair of the highway culvert were unexpected. No drawings are available indicating the location of this culvert. The costs include the labour, equipment and material costs are as follows:

Progress Claim No.3	
Highways Culvert Repair	\$12,000
Additional Equipment Time	\$20,000
Additional Labour	\$11,000
Progress Claim no.4	
Additional Cost to Complete	\$8700

Highway Culvert Repair

The work involved replacing a section of highway culvert located along the temporary drainage ditch and at the Waterloo Barrier. The culvert section located below the temporary ditch was damaged during the excavation and a 2 m section needed replacement. The YTG crew from Carcross were on site to perform these repairs. During the installation of the Waterloo Barrier, the sheet piles damaged the Highway culvert. Both sides of the Waterloo Barrier were excavated to a depth of approximately 5 m exposing the culvert. Approximately 5 m of culvert were removed from both side of the wall. A hole was cut into the wall in order to place the new section of culvert. The hole was cut as small as possible and a concrete plug was poured on both side to seal the Waterloo Barrier/wall intersection. The design for this plug was reviewed and approved by the Waterloo Barrier installer, C3 Environmental Ltd. The details are shown in Diagram no.4 on page no. 16. The excavation was then backfilled with tailings and native clay. The labour, equipment and materials costs claimed and approved for this additional work was \$12,000. This extra cost is claimed under Progress Claim no.3





HIGHWAY CULVERT REPAIR

Diagram no.4: Highway Culvert/Waterloo Barrier Intersection

Additional Equipment Time

The CTDC had estimated and budgeted 2 weeks of equipment time for the levelling of the tailings during their initial estimate of 1.1 million dollars. Due to the saturated and unstable conditions of the tailings, the work took 5 weeks to complete (see section 4.1 of this report for details). This doubled the expected rental cost of the equipment. An agreement was made that the CTDC would get compensated for this additional 2 weeks of equipment time, hence \$20,000. This extra cost is claimed under Progress Claim no.3 (see Annex C for details).

Additional Labour, Supervision and Surveyor Time

These extra costs were claimed for the increase in unit cost items. The claim was approved by the DIAND site representative for the amount of \$11,000. This extra cost is claimed under Progress Claim no.3 (see Annex C for details).

Additional "Cost to Complete Project" Cost

Under Item 9: "Costs to complete project", the CTDC included their profit, administration and accounting costs. These costs were based on percentages of the total cost of the project. Since the cost increased from \$1.11 MM to \$1.2 MM, the CTDC claimed for additional costs due to this increase in total project costs. The claim for this additional cost was \$8700. It was agreed to and approved by the DIAND site representative.

1.2 Overall Summary of Project Costs

The following table summaries the expected and the actual project costs:

ITEM	DESCRIPTION	Unit	EX	PECTED	AC	CTUAL
-		Cost	Quantity	Cost	Quantity	Cost
1	Waterloo Barrier	L.S.	n/a	\$548,000	n/a	\$548,000.00
2	Silty Clay Cap	\$18.90/m³	2650 m ³	\$50,100	3850 m ³	\$72,765.00
3	Dispose of Wood Debris	L.S.	n/a	\$4,032	n/a	\$4,032.00
4a	Excavate Wind Blown Tailings	\$18.90/m³	1600 m³	\$9,750	3656 m ³	\$22,301.60
4b	Excavate Tailings	\$6.10/m³	1700 m³	\$15,000	2226 m ³	\$19,633.32
4c	Final Grading	\$0.35/m ³	13,000 m²	\$4,600	13,300 m ²	\$4,655.00
5	Installation of Geotextile	n/a	13,300 m ²	\$45,000	13,300 m ²	\$44,954.00
6	Drainage Discharge System	L.S.	80 m	\$15,053	25	\$4704.06
7	Capillary Break Material	\$16.16/m³	4100 m ³	\$66,250	4725 m ³	\$76,356.00
8	Pitrun at Outfall Area		300 m ³	\$6,900	0	C
9	Costs to Complete	L.S.	n/a	\$344,779	n/a	\$344,77 9.00
	SUBTO	TAL		\$1,109,464.00		\$1,142,179.98
				Highway C	ulvert Repair	\$12,000
				Equ	ipment Time	\$20,000
				Labour , Su	pervision and Surveyor	\$11,000
				Additional "Costs	to Complete"	\$8,700
					SUBTOTAL	\$51,700
					TOTAL	\$1,193,879.98

Table no. 1: Project Cost Summary

2.0 <u>ADDITIONAL WORK FOR NEXT SUMMER</u>

2.1 Highway Culvert Upgrade

During the construction of the temporary drainage ditch, a 600 mm diameter corrugated culvert was discovered. The Yukon Highway Transportation department was asked to verify whether the culvert was installed during the construction of the Klondike Highway. However, no documents nor drawings identified the location of the culvert. Its purpose and ownership is therefore unknown. The highways culvert as shown on the as-built drawings in Annex D may have been installed prior to the construction of the Klondike Highway during the Venus Mine operation in the 1970's.

Because the culvert runs underneath the tailings pond from the highway embankment, a concern was raised concerning its structural integrity (life expectancy) and the possibility of infiltrating contaminated tailings water. To address these concerns, various options were proposed by PWGSC and are as follows:

Option

- 1. Status Quo (Do Nothing)
- 2. Insertion of a Culvert Sleeve
- 3. Installation of a Interior Water-proof liner
- 4. Remove and Replacement with New Culvert
- 5. Cap and Seal Outlet

Option 1: Status Quo (Do Nothing)

Currently, a "Do Nothing" approach is being followed. A monitoring program of the culvert effluent is underway by Renewable Resources, Indian and Norther Affairs Canada. If water concentrations of arsenic are found to be below federal and territorial guidelines, this option may be acceptable. However, a proactive options, as presented below, may reduce the risk potential future liabilities and provide a more adequate "care-free" long-term solution.

Option 2: Insertion of a Culvert Sleeve

This option consists of sliding a smaller plastic culvert inside the existing corrugated steel culvert and sealing the interstitial space with a bentonite slurry mix. The water presently running through the culvert may have to be diverted during the installation process. Physically, the new culvert can be pushed carefully, section by section, with a backhoe. The disadvantage of this option as that if any intersecting culverts merge with the main culvert along the sleeve, flow will be restricted. Any flow from these intersecting culverts shall not be restricted as it could potentially raise the soil's pore pressure and adversely affect the stability of the highway slope. If intersecting culverts are detected during the camera inspection, two options are available: excavate and expose joint and place a T-section or select a new option. The advantage is the lower cost and it is estimated that the labour, equipment and material costs will range between \$15,000-\$20,000.

Option 3: Installation of a Interior Water-proof liner

This option is a more highly technical solution to sealing the culvert. The technology involves coating the interior of the culvert, hence restricting potential tailing water from seeping into the culvert. The advantage of this technology is that, unlike option 2, holes can be cut into the liner at the intersecting culverts, hence not restricting the flow of water. Presently, there are no local contractors equipped to perform this type of work. A company from Vancouver or Edmonton would be required at an excessive mobilization cost. Bob White, a local contractor who performs TV inspection services, mentioned that next summer, he plans to purchase the necessary equipment to perform such work.

To properly install this liner, running water through the culvert needs to be diverted during the installation. The installer was not willing to provide a cost estimate until a remote camera inspection has been conducted. More information is required before assessing the feasibility of this option.

Option 4: Remove and Replacement with New Culvert

This option implies excavating 50 to 75 linear metres of culvert located below the tailings hence removing the capping material. Due to the saturated nature of the tailings, an extremaly wide trench would be required to excavate and remove the existing steel culvert. Our experience during the repair of the culvert dictates that the working condition would be similar. Hence it is anticipated that water will constantly fill the excavation and make the replacement of the culvert very difficult, time consuming and costly.

Option 5: Cap and Seal Outlet

This option involved constructing a seal plug at the outlet of the highways culvert to prevent the flow from running into the aquatic environment of Tagish Lake. It is recommended that this option not be selected because the function of the culvert is unknown. There are no drawings or documents available indicating the origin of the running water. It is assumed that the culvert drains pore water from the highway subbase. Constructing a plug could potentially prohibit the free draining of the soil and potentially jeopardize the stability of the highway slope. After the TV inspection is performed, sufficient information may be gathered to determine the culvert's function and the origin of the flow. However, without being absolutely certain of the function of the highway culvert, this option is not recommended.

Prior to evaluating the options, it is recommended that a visual inspection of the culvert be performed. The culvert interior inspection can be conducted through remote camera investigation. This method of inspection will provide the additional information necessary to adequately evaluate the viability and costs of the options above. The remote camera inspector is to provide the following information:

- 1. Physical condition and size of culvert;
- 2. Location and size of intersecting culverts;
- 3. Location and an angle of elbows and other obstructions; and
- 4. Any other information necessary to evaluate the remedial options.

The following is a local contractor equipped and experience in this field:

Yukon TV Inspection Services 9 Salter Pl. Whitehorse, Yukon

Phone no.: 403-633-5051

2.2 Drainage Discharge System Upgrade

The inlet of the discharge system, located at the wall, was constructed at a elevation of 82.85 m. If the tailings settles over the next year, this elevation may need to be lowered to allow free drainage of the top 150 mm of the gravel. These modifications are minor and less costly. However, the upgrades are critical to the control of an acceptable water level and the appearance of a dry condition.

2.3 Regrading of Capillary Break Material

Assuming that the tailing pond is stable, it is recommended that capillary break material be regraded. This work shall be accomplished in July or August, 1996, when the tailings have undergone a full freeze-thaw cycle and potentially settled.

Presently, the standing water covers approximately 50% to 70% of the tailings pond. To eliminate visible standing water, it is recommended that additional pitrun be hauled to the site and placed in the depressions (i.e. at the location of the standing water). The material is to be screened 75 mm minus and 25 mm plus pitrun: all particle sizes below 25 mm shall be screened out. The standing water will sit between the gravel particles and ensure a dry surface condition. If this work proceeds, lowering the outfall elevation may not be required as described in section 2.2 above.

2.4 Settlement Issue near the Waterloo Barrier

On October 20th, settlement of the capping material was noticed at the east side of the tailings pond immediately inside the Waterloo Barrier. The decant pipe may be located immediately below this settlement area. It is also possible that the decant pipe was punctured during the installation of the Waterloo Barrier. If this has occurred, the settlement may be caused by the soil filling the pipe cavity. Settlement did not occur until the outlet was capped and sealed. This indicates that the decant pipe may have filled up with water which allowed the soil to free-flow into the pipe. If the pipe has been filled with the settling tailings, no additional settlement will

be expected. However, further settlement may occur next summer when the tailings thaw out. If this is the case, additional material may need to be hauled to backfill the settled area. The settlement of the tailings should not cause an environmental concern. The settling tailings have no escape pathway because the tailings are confined by the concrete and bentonite cap at the outlet.

Next summer, after the soil has thawed and further settlement has occurred, an evaluation of the site will be required to determine the necessity for further work.

CONCLUDING REMARKS

The project was completed on schedule and under budget. The difficulties pertaining to the execution of the work were solved as the situations arose. The Carcross/Tagish Development Corporation (CTDC) manager and superintendent were very cooperative during this project. When extra costs were anticipated, Larry Whelan and Mel Jonhson reevaluated their operating costs and determined whether additional costs could be absorbed into the estimated costs. For example, the CTDC absorbed the additional \$5/cu.m. for the purchase the capillary break material into their \$16.16/cu.m unit cost.

Concerning the planning of the work, a preconstruction meetings was held with the CTDC before the start-up of the work. However, the C3 Environmental crew was not present causing some delays at the start-up of the job and some misunderstandings concerning their work plan. For example, the project manager was under the impression that the installation of the wall would begin at the north end of the tailings. However, the material for the south end section had already been ordered. It is recommended that next time, a pre-construction meeting be held with the prime contractor, the design and construction management engineers and all subcontractors. The purpose of this meeting would be as follows:

- Prepare a step-by-step work plan and schedule;
- · Discuss anticipated difficulties with the execution of the work; and
- Clarify ambiguities in the design specification document(if any).

The cost estimate provided by the Carcross/Tagish Development Corporation on August 4th was broken down into items as per the original PWGSC specification document. However, the original document was amended to alter the method of payment and replace the geomembrane specifications with a geotextile. The changes are included in a revised document entitled "Design of Venus Mine: Site Rehabilitation, July 1995 (Revised September, 1995)" in Annex B.

Overall, this project was good learning experience for all parties involved. The execution of the work was completed on schedule and under the allowed budget.

VENUS MINESITE

Followup Contracts

Following completion of the contract for installation of the Waterloo Barrier, and cover on the tailings, two items required follow up. These were as follows:

- 1. During installation of the Waterloo Barrier, it was discovered that there was an underground pipeline that angled across the site. The origin of the pipe could not be traced, nor could its present ownership. In a followup contract in 1996, Yukon TV Inspection cut into the pipe, lowered a video camera into the opening and provided a continous video tape of the condition of the pipe. An analysis of the video indicated that the pipe was corroding, joints were failing, and there were breaks in the pipe itself. Clearly there was a need to address the condition of the pipe. The cost of undertaking this inspection was \$4,300.00.
- 2. The original concept for the cover was based on creating a condition which would result in the tailings being submersed at all times, thus preventing ARD. A further design condition was that the final appearance of the surface would be dry, simply for appearance. It was known that water was entering the site from two sources, a steady flow from beneath the highway, and surface water resultant from rainfall and snow melting. What was not known at the design stage was the amount of water that would enter the site from beneath the highway, nor that this flow would continue unabated throughout the winter. While it was anticipated that there was sufficient water entering the site to ensure that the primary objective of submerging the tailings would be accomplished, it was not anticipated that this objective would be met within days of completing the Waterloo Barrier. Nevertheless the final surfacing of the tailings with a coarse material was expected to provide a medium for allowing water to run off the site via a laminar flow process. In hindsite, material utilized to provide the conduit for laminar flow contained too high a fines content to permit free flow of water and ponding resulted. To address the ponding issue remedial work was required.

As followup work, several contracts were prepared. The first contract which was undertaken was a contract to add additional coarse rock to the surface of the tailings pond in an attempt to reach the objective of a dry pond. Additional material was placed over the area which had ponded during the previous summer. While the depth of water ponding was reduced, the primary affect of adding additional material was that the area ponding was enlarged. As the work was undertaken during winter, over snow, no decision could be made on the effectiveness of the additional material at the time it was placed. This work was undertaken by Arctic Backhoe Services Ltd. for \$31,798.00.

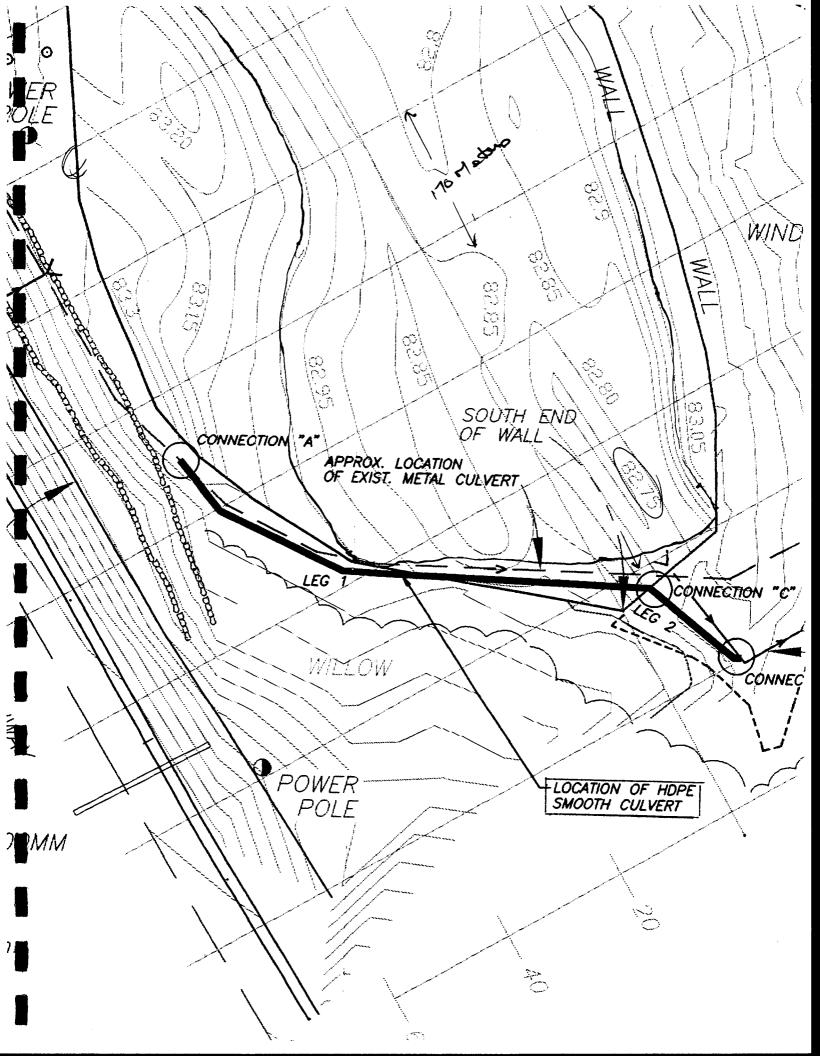
Shortly after the coarse material was placed, a second contract was undertaken by Yukon TV Inspections Ltd. This contract involved the installation of a new HDPE pipe to connect with the pipe which angled across the tailings, at a new location, and sealing the existing pipe at the wall location. This contract was in the amount of \$58,700.00. The new pipe was installed during winter months through the tailings and through the wall. Final cleanup of the backfilling was deferred until spring, as was the plugging of the old culvert. In spring, the contract amount was revised to \$67,931.00 to cover additional work. Yukon TV Inspections returned in spring and excavated along the south wall and exposed the old pipe. A hole was cut into this pipe and concrete pumped into it to form a seal at the wall. While on site, trenches from the previous year's

Venus Minesite Followup Contracts

work were cleaned up, and the new pipe buried at its exit location. The coarse rock which had been placed during the previous winter was regraded. In an attempt to improve the flow of water, the outlet at the south wall was lowered, and the discharge spout reattached.

It was planned to haul in an additional 10 loads of waste crushed gravel to fill in a void at the location outside the wall where excavation had taken place. The initial attempt to haul gravel was a failure as the loaded truck got stuct before it could dump its load. Further attempts at hauling were suspended to prevent damage to the tailings cap. As a result there remains a void at the south end of the wall. Should further attempts be made to fill in this void, they should be undertaken only under winter conditions.

There appears to be some evidence of erosion along the wall approximately midway along the east side. If material is hauled in to correct the depression along the south wall, the eroded areas should be filled in.



CONTRIBUTION AGREEMENT ARCTIC ENVIRONMENTAL STRATEGY ACTION ON WASTE PROGRAM

FOR THE PERIOD FROM August 1, 1995 to March 31, 1996.

This Agreemen	t made in triplicate the 25^{+1} day of 995
BETWEEN	Her Majesty the Queen in right of Canada, as represented by the Minister of Indian Affairs and Northern Development 345 - 300 Main Street WHITEHORSE, Yukon Y1A 2B5 (hereinafter referred to as "Canada")
	OF THE FIRST PART

AND

Carcross Tagish First Nation

Box 130

CARCROSS, Yukon

Y0B 1B0

(hereinafter referred to as the "Recipient")

OF THE SECOND PART

1. <u>INTRODUCTION</u>

- 1.1 Whereas the Minister has been authorized to establish and implement the Arctic Environmental Strategy, hereinafter referred to as the AES, throughout the Yukon Territory;
- 1.2 And whereas the Recipient has requested financial assistance from Canada to participate in the AES;
- 1.3 And whereas Canada has agreed to provide the Recipient with financial assistance to meet the said requirements;

1.4 Now therefore this agreement witnesses that the parties hereto, in consideration of the covenants and undertakings herein contained, covenant and agree as follows:

2. PURPOSE

- 2.1 The purpose of this Contribution Agreement is to enable the Recipient to participate in the Arctic Environmental Strategy, Action on Waste program in the Yukon Territory.
- 2.2 To enable the Recipient to clean up the mine tailings of the Old Venus mine in accordance with the plans and specifications outlined in Appendix "A" to this Contribution Agreements.

3. <u>DURATION</u>

3.1 This Agreement shall come into effect on the 1st day of August, 1995 and shall continue in effect until the 31st day of March, 1996, by which time the Recipient agrees to have fulfilled all of the terms and conditions of the Agreement. Funding under this Agreement shall terminate on the 31st day of March, 1996.

4. WORKPLAN

4.1 The Recipient agrees to undertake the Workplan in the manner and within the time set forth in Appendix "A" to this Contribution Agreement.

5. **FUNDING**

- 5.1 Subject to the terms and conditions herein described, and subject to funds being appropriated by Parliament for the purposes herein, Canada shall contribute to the Recipient an amount not to exceed One Million One Hundred Thousand Dollars (\$1,100,000.00).
- 5.2 An advance payment in the amount of Four Hundred Thirty Four Thousand Dollars (\$434,000.00) will be made upon signing of this contribution agreement.
- 5.3 Payment will be made upon receipt of progress claims for work satisfactorily completed as agreed between the Carcross Tagish First Nation's Project Manager and DIAND's Project Officer.

5.4 Final payment will be made upon receipt of a final report as required in Section 7.1.1.1.

6. DISBURSEMENT OF FUNDS

- 6.1 The disbursement of AES funds by the Recipient shall be in general accordance with plans and activities approved by the Director, Renewable Resources representing the Department of Indian Affairs and Northern Development.
- 6.2 The Recipient agrees that the Contribution or any part thereof shall not be disbursed for any purpose other than those contained in the Agreement. Failure to comply with the provisions of the Agreement entitles Canada to recover from the Recipient an amount equivalent to the sums disbursed for a purpose other than those contained herein, and the Recipient agrees that these amounts shall constitute disallowed expenses, which shall be due and payable by the Recipient to Canada within thirty (30) calendar days of so being requested in writing.
- 6.3 The Recipient agrees to repay any overpayment and unexpended balances, and that these amounts constitute an amount due and payable by the Recipient to Canada within thirty (30) calendar days of so being requested in writing.
- 6.4 The Recipient understands that this funding has been granted only until the 31st day of March, 1996. Acceptance of these funds by the Recipient does not guarantee that the Recipient will receive funding under Arctic Environmental Strategy Program in future years.

7. <u>REPORTS</u>

7.1 Activity Reports

- 7.1.1 The Recipient agrees to provide reports on the Workplan specified in Section 4.1 as follows:
 - 7.1.1.1 provide a final report no later than the 31st day of March, 1996, detailing the total expenditures and activities for the duration of the Agreement.

7.2 Financial Reports

- 7.2.1 The Recipient shall maintain a separate account for all receipts and expenditures pursuant to this Agreement, and shall maintain accounting records in a manner consistent with generally accepted accounting principles and practices as issued by the Canadian Institute of Chartered Accountants.
- 7.2.2 The Recipient agrees to provide an unaudited financial statement no later than the 31st day of March, 1996, detailing the recipients expenditures concerning the AES throughout the life of this agreement.
- 7.2.3 The Recipient agrees to forward the reports and financial statements to Director, Renewable Resources, DIAND, 345 300 Main Street, Whitehorse, Yukon Y1A 2B5, on behalf of Canada.

8. NON COMPLIANCE

8.1 Failure by the Recipient to fulfil any of the terms and conditions of this Agreement may result in no further funding being provided to the Recipient. In such an eventuality, the Recipient shall have thirty (30) calendar days from the date of so being requested in writing by Canada to take remedial action. Failure by the Recipient to do so may result in Canada terminating the Agreement, with the requirement that all funds not disbursed be returned to Canada within thirty (30) calendar days of so being requested in writing.

9. <u>AUDIT</u>

- 9.1 Canada reserves the right to audit the accounts and records of the Recipient to ensure compliance with the provisions of this agreement. Recipient shall make available in a timely manner any records, documents, information and explanation as the audit may reasonably require.
- 9.2 Canada agrees to inform Recipient of the financial results of any audit which it may initiate, providing general comments, information and explanation as the audit may reasonably require.

10. CONFLICT OF INTEREST

10.1 No former public office holder who is not in compliance with the post-employment provision of the Conflict of Interest and Post-Employment Code for Public Office Holder shall desire a direct benefit from this Agreement.

11. COMPLIANCE WITH ENVIRONMENTAL LEGISLATION

11.1 All activities undertaken pursuant to this Agreement shall conform to applicable environmental legislation and policies at the federal, territorial and local levels.

12. GENERAL

- 12.1 No member of the House of Commons of Canada shall be admitted to any share or part of the Agreement, or to any benefit to arise therefrom.
- 12.2 This Agreement supersedes all communications, negotiations and agreements, either written or oral, between the parties hereto in respect of matters pertaining to this agreement, prior to its execution and delivery.
- 12.3 The Recipient shall indemnify and save harmless Canada, its servants and agents from and against any damages, costs or expenses, or any claim, action, suit or other proceeding which they or any of them may at any time incur or suffer as a result of any injury to persons (including injury resulting in death) or loss of or damage to property which may be or be alleged to be caused by or suffered as a result of actions or omissions of the Recipient, its servants and agents.
- 12.4 The present Agreement shall be deemed to have been entered into at Whitehorse, in the Yukon Territory, and shall be governed by and interpreted in accordance with the laws of the Yukon Territory.
- 12.5 Any and all agreements entered into by the Recipient with third parties to fulfil its obligations under this Contribution Agreement shall include the following clause:

"The parties hereto agree and fully understand that the Carcross Tagish First Nation is not, and does not act as, the agent for Her Majesty the Queen in right of Canada in respect to this Agreement or any part thereof. The parties hereto further agree and acknowledge that each of them acts herein solely as its own Principal and on its own behalf."

- 12.6 This Agreement may be amended by mutual written consent of both parties hereto or their duly authorized representatives.
- 12.7 This Agreement may be terminated by either party with reasonable cause upon thirty (30) days written notice indicating the intent and reasons for such termination. All monies unaccounted for at that time shall be subject to an immediate audit as provided for under Article 9 of this Agreement. Any overpayment and unexpended balances shall be repaid and such other appropriate actions shall be taken by Canada or at its direction in these matters.
- 12.8 Any information released or announced to the public concerning the subject matter of this Agreement shall adequately acknowledge the contribution made by Canada on behalf of the federal government.

GOVERNMENT OF CANADA

SIGNED

24 August 1995.	Pomee Chamber
Date	Director, Renewable Resources DIAND
Bug, 25, 95 Date	Carcross Tagish First Nation

I certify that this Agreement meets Treasury Board requirements for the Arctic Environmental Strategy in the Yukon.

Date Director
Corporate Services
DIAND

APPENDIX A

WORKPLAN

PROJECT NAME: VENUS MINE TAILINGS SITE REHABILITATION

These Technical Terms and Conditions cover the "in place" environmental clean-up of the mine tailings of the old Venus Mine at Km 86.5 on the South Klondike Highway by the Carcross / Tagish First Nation during the time period from August 1, 1995 to MARCH 31, 1996. The total estimated cost of the project, one million and one hundred thousand dollars (\$1,100,000.00), will be provided by AES Action on Waste, Indian and Northern Affairs Canada.

CARCROSS / TAGISH FIRST NATION AGREE:

- To appoint the First Nation's Capital Project Manager to the project to ensure that the project is implemented in accordance with these Technical Terms and Conditions and this Contribution Agreement.
- 2. To advise DIAND by copy of a Band Council Resolution of the appointed Project Manager's authorized levels of authority (e.g. negotiating and signing Technical Terms and Conditions, approving changes in scope, signing contracts, etc..)
- 3. To carry out the following work:
 - a) The environmental clean-up of the mine tailings of the Old Venus in accordance with the Plans and Specifications prepared by Public Works and Government Services' Environmental Services Branch (Edmonton). The Plans and Specifications form a part of these Technical Terms and Conditions.
 - b) To ensure that an environmental screening is carried out prior to starting the project.
 - c) Recording, preparation and distribution of on-site project meeting and weekly meeting minutes.
- 4. To ensure that the supplier and installer of the Waterloo Barrier provide a one years warranty on the installation of the Waterloo Barrier.

- 5. That the First Lion's Project Manager will accor in DIAND's Project Officer or authorized designate on all inspections and will provide necessary site and construction project information.
- 6. That DIAND has the right to examine the project at any reasonable time and to engage its own or consulting inspection services to ensure conformity with the approved plans and specifications and to these Technical Terms and Conditions.
- 7. That it has the responsibility to undertake this project using sound project management practices that will ensure successful completion of this project.

DIAND AGREES:

- 8. To appoint a Project Officer and advise the First Nation in writing of this persons
- To appoint an on-site representative for the project officer and advise the First Nation in writing of this persons name.
- 10. To transfer funds in a timely and efficient manner for the implementation and completion of the project in compliance with these Technical Terms and Conditions.

Description of Work Completion of items in Sections 1,2, 3, 11 and 14 of these Technical Terms and Conditions and by signing these Technical Terms and Conditions.	<u>Percent</u> 39.4%	<u>Value</u> \$434,000.00
Progress payments for work satisfactorily completed as agreed between the First Nation's Project Manager and DIAND's Project Officer.	y 60.6%	\$666,000.00
Total Funds for the Project	100.0%	\$1,100,000.00

CARCROSS / TAGISH FIRST NATION AND DIAND AGREE:

- 11. That an environmental screening will be conducted prior to the first release of funds to the First Nation.
- 12. That a progress review will be held by DIAND in March of 1996 to determine the actual status of this project at which time any necessary decisions on future projects may be made.

- 13. Allocation of _ure year Capital Contributions __ dependent upon successful completion of current years projects.
- 14. An initial payment will be made to the First Nation to cover the up-front costs for the project as well as supply and delivery of the Waterloo Barrier. Subsequent progress payments will be based on satisfactorily completed work, as agreed upon between the First Nation's Project Manager and DIAND's Project Officer.
- 15. A 10% holdback will be retained on all progress payments.



Carcross/Tagish Development Corporation

Head Office: P.O. Box 130

Carcross, Yukon Y0B 1B0

Tel: (403) 821-4109 Fox: (403) 821-4811

August 04, 1995

D.I.A.N.D.
Technical Services
Department of Indian & Inuit Affairs
415 - D 300 Main Street
Whitehorse, Yukon

Attn: Mr. Art Dell P. Kng - Manager, Technical Services.

Dear Sir;

Re: Construction Cost Estimate Venus Mine Site Tailings - Site Rehabilitation.

Attached please find our estimated cost to undertake the work as outlined in P.W.G.S.C Construction Documents of July 1995. We acknowledge receipt of addendums changing earthwork quantities from tonnes to m3 where applicable and agree to survey measured quantities for final payment.

The geomembrane item 6 has not been included due to problems from supplier who is awaiting prices from the U.S. We should know today.

We hope the following to be to your satisfaction and look forward to working with you again.

Regards,

Larry Whelan, Manager

Lavy Whelan

cc. Mel Johnson - Construction Manager Mark Palmer - Action on Waste Management

CONTRIBUTION AGREEMENT ARCTIC ENVIRONMENTAL STRATEGY ACTION ON WASTE PROGRAM

AMENDMENT #1

Contribution Agreement entered into between "Canada" and the "Carcross/Tagish First Nation" for the period August 1, 1995 to March 31, 1996, to clean up the mine tailings of the Old Venus mine is hereby amended:

1. 5. FUNDING, page 2 of the Contribution Agreement

Under Section 5.1 - "Subject to the terms and conditions herein ... an amount not to exceed One Million One Hundred Thousand Dollars (\$1,100,000.00).

Should be amended to read "Subject to the terms and conditions herein ... an amount not to exceed One Million One Hundred Ninety Three Thousand Eight Hundred Eighty Dollars (\$1,193.880.00)."

2. All other terms and conditions of this contribution agreement remain the same.

SIGNED

27 October 1995

Date

Buce Chambers

Director, Renewable Resources, DIAND

Nov. 10, 95

Carcross Tagish First Nation

I certify that this amendment to this Agreement meets Treasury Board requirements for the Arctic Environmental Strategy in the Yukon.

A/Director, Corporate Services, DIAND

Yukon
MCHC
INVIRONMINIAL
STRAILGY



ACTION ON WASTE

#345, 300 Main Street-Whitehorse, Yukon Y1A 2B5

Phone: (403) 667-3270 Fex: (403) 667-3206

11 GY

November 30, 1995

Carcross Tagish First Nation P.O. Box 130 Carcross, Yukon YOB 180

ATTENTION: Mr. Larry Whelan

Dear Mr. Whelan:

RE: Contribution Agreement Amendment #2
Venus Mine Tailings Project

Please find enclosed three copies of the above amendment for the Venus Mine Tailings Project.

Would you please review and have Chief James sign all copies. Please return two original copies to us for our files.

if you have any questions, please call me at 667-3271.

Sincerely,

L. Dorothy McLeod/ Administrative Officer

Arctic Environmental Strategy

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Affaires Indiennes et du Nord Canadi **Canada**

CONTRIBUTION AGREEMENT ARCTIC ENVIRONMENTAL STRATEGY ACTION ON WASTE PROGRAM

AMENDMENT #2

Contribution Agreement entered into between "Canada" and the "Carcross/Tagish First Nation" for the period August 1, 1995 to March 31, 1996, to clean up the mine tailings of the Old Venus mine is hereby amended:

1. 5. <u>FUNDING</u>, page 2 of the Contribution Agreement

Under Section 5.1 - "Subject to the terms and conditions herein ... an amount not to exceed One Million One Hundred Ninety Three Thousand Eight Hundred Eighty Dollars (\$1,193,880.00).

Should be amended to read "Subject to the terms and conditions herein ... an amount not to exceed One Million One Hundred Ninety Eight Thousand Eight Hundred Eighty Dollars (\$1.198.880.00)."

2. All other terms and conditions of this contribution agreement remain the same.

Date

Date

Carcross Tagish First Nation

I certify that this amendment to this Agreement meets Treasury Board requirements for the Arctic Environmental Strategy in the Yukon.

Ww-24/65 Date

SIGNED

Director, Corporate Services, DIAND

1122 BBSS CARCROSS TAGISH 1-493-821-4892

This Looks

Good. We can

Come-up with

NEED TO: Federal Department Public Works

Edmonton, Alberta

DATE: October 27, 1995

ATTM: Mr. G. Strymadke - P. Ing. Ngr.

the \$ For ph this MocTaki

RE: Restoration Of Settlement Along Retaining Wall At Venus Mine Sito.

Dear Sir,

Pursuant to our telephone conversation on Wednesday October 25, 1995 and our subsequent site visit on October 37, 1995. The settlement is accurring in an area where the sheet piling had to be trenched into place due to large bolders. The beakfill in the area immediately adjacent to the sheet piling could not be completed for fear of damage to the pile finish.

Water from the piping and drainings system from the Skagway road is accumulating over the new fill and as the soils become saturated excesive settlement is accurring in the area.

To correct this and redirect the flow of Water away from the retaining wall we recommend placing approximately 15 loads of gravel in the area to refill the void and regrade the area adjacent away from the wall.

To do this the trenches and earth berns road has to be reopened and matereal hauled to the site.

The Work required and costs associated are as follows:

Loader 20hrs. \$ \$70.00 \$1,400.00 Tanden Truck 10hrs. \$ \$65.00 \$650.00 Supervisor 25hrs. # \$30.00 \$750.00 Pick-up and tamper \$300,00 \$3,100.00 Administration 10% 310.00

Total \$3,410.00

We hope the forgoing to be to your satisfaction. The work should be done before winter and monotored before spring run off as we feel the whole site will be in/undated with water from the highway following spring melt. Please call if you have questions.

Thanks

Manager

Add: 15 loads @ 11 met willed @ 5.00 royalty : 825.00

+ Admise 10%: \$2.50

1 403 821 4802 PAGE. 602

OCT 27 '95 12:27

DEC

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with Sec. 7 of the

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Cort. Pursuant to Sec. 34

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SPECIFICATION

FINAL DESIGN OF VENUS MINE TAILINGS SITE REHABILITATION

July, 1995 (Revised September, 1995)

DESIGN OF

VENUS MINE TAILINGS

SITE REHABILITATION



FINAL DESIGN

JULY 1995 (Revised September, 1995) Public Works and Govt. Services Canada Project No. 626483

LIST OF CONTENTS VENUS Mine Site

Page 1 September 7, 1995

This Specification is part of the document referred to as "Plans and Specifications" and marked "A" in the Articles of Agreement entered into

_
Officer)
· ,

INDEX TO SPECIFICATIONS

	SECTION	TITLE	<u>PAGES</u>
	DIVISION 0	GENERAL REQUIREMENTS	
	01005 01014 01410 01500 01545 01561	General Instructions Project Control Testing Laboratory Services Temporary Facilities Safety Requirements Environmental Protection	8 2 1 2 1 1
Waterloo Barrier			11
Collection and Disposal of Debris at the Venus Mine Tailings Site			
Excavate Wind Blown Tailings, Outfall Area Excavation and Level Existing Mine Site			

Public Works and Govt. Services Canada Project No. 626483	LIST OF CONTENTS VENUS Mine Site	Page 2 September 7, 1995
Supply and Placement of a	Silty Clay Cap	1
Non Woven Geotextile		10
Capillary Break Material		1
Miscellaneous Aggregates		1
Construct Drainage Outfall		1
Test Hole Logs		36
INDEX TO DRAWINGS		

Title:

VENUS Mine Tailings

Site Rehabilitation

Tailings Treatment Plan

Project No.: 626483

Date:

Revised September 7, 1995

1. <u>DESCRIPTION OF WORK</u>

- .1 Work under this Contract covers the "in place" environmental clean up of mine tailings, at the Venus Mine Tailings Site, and related works.
- The Venus Mine Tailings Site is located at approximate km 86.5 on the Skagway-Carcross Highway; granular material is located at Community and Transportation Services, Transportation Engineering Branch pit at Km 90 and capping material is located approximately 2 Km north of Carcross, and is currently being landfarmed.
- .3 Work under this Contract covers the following as indicated on the drawings and specifications:
 - .1 Installation of an impermeable wall (Waterloo Barrier) to contain the tailings pile at its current location.
 - .2 Loading, hauling, and placing a silty clay cap.
 - .3 Collecting and disposing wood debris, sealing pipes, and removing scrub brush.
 - .4 Excavating wind blown tailings and levelling the tailings site.
 - .5 Constructing a drainage discharge system.
 - .6 Supply and installation of a geotextile.
 - .7 Hauling, and placing granular capillary break material.
 - .8 Community consultation.
- .4 Related work associated with this Contract include:
 - .1 Provision of an on site construction office suitable for use by the Owner's site representative and the contractor's superintendent.
- .5 Testing services on this Contract will be provided as follows:
 - .1 The Owner will provide testing personnel to perform compaction testing (if specified), grain size analysis, sieve analysis, and testing for contaminants.

- .2 The tests performed by the Owner's testing personnel will form the basis for determining the depth and extent of materials to be removed, and will form the basis for acceptance of the work.
- .6 Items peculiar to this contract include:
 - .1 The Contractor is free to use his discretion on the selection and utilization of equipment for this project.
 - .2 To the extent indicated on the contract drawings and specifications, the Owner's intent is to have the bulk of the work completed prior to March 31, 1996.
 - .3 Test borings undertaken by Public Works in 1986 and 1987 and 1995 indicate the presence of high water tables. The selection of suitable equipment will be crucial on this project.

2. CODES

- .1 Perform work in accordance with National Building Code of Canada (NBC), and any other code of the Yukon Territory or local application, provided that in any case of conflict or discrepancy, the more stringent requirements shall apply.
- .2 Meet or exceed requirements of:
 - .1 Contract documents.
 - .2 Specified standards, codes and referenced documents.

3. **DOCUMENTS REQUIRED**

- .1 Maintain at job site, one copy of each of the following:
 - .1 Contract drawings.
 - .2 Specifications.
 - .3 Addenda.
 - .4 Change Orders.
 - .5 Field test reports.
 - .6 Copy of approved work schedule.
 - .7 Permits, licenses and land use regulations.
 - .8 Environmental assessment report.
 - .9 Labour and Materials Payment and Performance Bonds.

4. SITE CONDITIONS

- .1 Site information contained in these contract documents was derived from several sources listed below:
 - .1 Tailings Characterization was derived from a report prepared by Rock Group Consulting Engineers dated August 1994, titled "Tailings Characterization".
 - .2 Remedial Options, and anticipated volumes were derived from a report prepared by Klohn-Crippen, "Study of Remedial Options" dated March 1994.
 - .3 Subsurface information was obtained from the Kohn-Crippen report, the Rock Group Report, borings undertaken by PWGSC in 1986 and 1987, and sampling programs undertaken by PWGSC in 1995.
 - .4 Topographic survey undertaken by PWGSC in 1995.
 - .5 Location and depth of tailings were compared with reports prepared by United Keno Hill Mines Ltd. in 1980.
 - .6 Selected geotechnical information is appended to these documents as Appendix 'A'.
 - .7 Photographs dating from 1970 until the present were consulted in deriving the extent of tailings.
- This Contract deals with environmental clean up. Information in the various reports regarding the depth and extent of tailings is contradictory. While every effort has been made to accurately depict the nature and extent of the work to be undertaken, some subsurface conditions may vary from those depicted on the drawings. Accordingly, the Owner will arrange for continuous on site testing to ensure that the intent of the specifications will in fact be met.
- .3 The tailings samples are reasonably typical of a polymetallic deposit with sulphur contents ranging from 3 to 20%, iron from 4 to 9%, with associated arsenic (2.5 to 7.9), zinc (0.05 to 1%) and to a lesser degree cadmium, cobalt, copper, lead and nickel values.

5. WORK SCHEDULE

.1 Provide and maintain a work schedule showing anticipated progress stages

and final completion of work within time period required by contract documents.

.2 Interim reviews of work progress based on work schedule will be conducted as decided by the Owner's site representative and schedule updated by contractor in conjunction with and to the approval of the Owner's site representative.

6. COST BREAKDOWN

.1 Before submitting first progress claim, submit breakdown of contract price in detail as directed by the Owner's site representative and aggregating contract price. After approval by Owner's site representative, cost breakdown will be used as basis for progress payments.

7. **MEASUREMENT FOR PAYMENT**

Lump Sum

- .1 Due to the nature of the work it is proposed to use a combination of lump sum payments and unit price items to enumerate the Contractor on this contract.
- .2 Items which the Contractor will submit prices for are as follows:
 - .1 Supply and installation of an impermeable wall (Waterloo barrier) to contain the tailings pile at its current location.

	Pricing to be based on proposal submitted.		
	Lump Sum		
.2	Load, haul, place, grade and compact a silty clay cap. Price to nclude all labour and equipment to construct a silty clay cap.		
	2,650 cu. m. @ =		
.3	Collect and dispose (by burning) wood debris on site, and dispose of brush, and seal decant pipe. Price to include all labour and equipment necessary to clean up work areas at the Venus Mine Tailings site.		

.4 Excavating wind blown tailings and levelling tailings site. Price to include all labour and equipment necessary to excavate wind blown tailings; excavate high areas on the tailings pile and move to low

General Instructions

Section 01005 Page 5 September 7, 1995

areas; final levelling and compaction of tailings site. .1 Excavate and place wind blown tailings, including material in the drainage discharge area. 1,600 cu. metres @ .2 Excavate and relocate tailings on site. 1,700 cu. metres @ _____ Final shaping, grading, and compaction of tailings site. .3 13,300 square metres @ .5 Supply and installation of geotextile. Price to include all labour and equipment necessary to supply a geotextile, and place the geotextile in accordance with manufacturer's recommendations, over the mine tailings. 13,300 square metres @ .6 Constructing a drainage discharge system. Price to include the supply and installation of piping material; supply and installation of end sections and all connections. Lump Sum .7 Loading, hauling, and placing capillary break material. Price to include the loading, hauling, placing, and compaction of a capillary break material to the lines and grades specified. 4,100 cu. m. @ = 8. Supply and place pitrun aggregate in the outfall area. 300 cu. m. @ ____ = ___ .9 Costs to complete project. Price to include supervision, profit, administration, community consultation, supply of temporary facilities, flagpersons, scale persons, dewatering, and any costs for items not covered above.

8. **CONTRACTOR'S USE OF SITE**

- .1 Contractor has use of site with the following restrictions:
 - .1 Use of site shall comply with environmental protection requirements.
 - .2 Tracking of mud onto the Skagway-Carcross Highway is not permitted.
 - .3 Contractor shall undertake any snow clearing at the Venus Mine Tailings Site.
 - .4 The Skagway-Carcross Highway may be subject to snow slides during the winter months. The Owner assumes no responsibility for lost time in the event that access to the site is curtailed for any length of time due to snow slides or other natural phenomenon.

9. **PERMITS**

- The Contractor shall be responsible for paying all costs associated with obtaining licenses, permits and royalties. Costs for these items will be covered under the cash allowance provided in the cost tables.
- .2 The Contractor shall register, obtain and pay for all licenses and permits for individual tradespersons employed for work of their section.

10. **PROJECT MEETINGS**

- .1 The Contractor and the Owner's site representative will develop an appropriate schedule for holding project meetings.
- .2 For contract activities which are ongoing, project meetings shall be held monthly.
- .3 For contract activities which are unique, e.g. Waterloo Barrier, installation of geomembrane and start of winter operations, meetings shall be scheduled at the start of each activity.
- .4 Times and locations of meetings to be approved by Owner's site representative.
- .5 Notify participants of meetings.
- .6 Record minutes of meetings, and distribute to participants within 3 days of meeting.

11. SITE SUPERVISION

.1 Contractor will designate a competent and qualified supervisor to be on site at all times during construction, to have full authority to make decisions for the Contractor, to be knowledgeable of the requirements of the contract, and to act on the Owner's site representative's instructions.

12. **COMMUNITY RELATIONS**

- 1 The Contractor will be responsible for undertaking any community consultations required for this project.
- .2 The Contractor shall be responsible for providing and paying for any required translation services, and for recording and distributing minutes of meetings on approval of the Owner's representative.
- .3 The Owner, and Owner's site representative will attend any community meetings related to this project at the request of the Contractor.

13. **SETTING OUT OF WORK**

- .1 The Owner's representative will arrange and pay for a survey crew to provide initial layout of the work, periodic grade stakes, measurements for final payment, and line and grade for the drain pipe.
- .2 The Contractor shall employ methods to place the drain pipe at the correct elevation from lines and grades provided.
- .3 The Contractor shall take precautions to protect survey stakes. Costs to replace the indiscriminate removal of grade stakes will be back-charged to the Contractor.

14. **EXISTING SERVICES**

Power poles and lines exist at the Venus Mine Tailings Site. These lines are outside the work area and will be left in place.

15. ADDITIONAL DRAWINGS

.1 Owner's site representative may furnish additional drawings for clarification. These additional drawings have same meaning and intent as if they were included with plans referred to in Contract documents.

16. WORK METHODOLOGY PLAN

- .1 The Contractor shall provide, prior to start of work, a Work Methodology Plan that demonstrates how the various activities will be carried out.
- .2 The plan, shall be submitted in three copies, and indicate the equipment to be used, sources of materials, and anticipated durations.

17. **EXAMINATION OF SITE**

- Prior to finalizing pricing negotiations, the Contractor, a representative from DIAND, and a representative from the design team shall visit the site to ensure that all aspects of the work are clearly understood.
- .2 The Contractor shall notify the Owner's site representative, in writing, of any matters which could prejudice proper execution of the work.

18. **DEFINITIONS**

- .1 The **Owner**, as described in these documents is the Manager, Contaminants/Waste Programs, Renewable Resources, Indian and Northern Affairs, Whitehorse.
- .2 The **Owner's Site Representative** is the Divisional Manager, Environmental Services, Public Works and Government Services Canada, Edmonton, Alberta.
- .3 The **Contractor** is the Tagish/Carcross Band.
- .4 It is understood that the contract will be undertaken through a contribution agreement with the Tagish/Carcross Band.

19. LOCAL CONTENT

- .1 Two fundamental principles apply to the manner in which this contract is to be executed. These are as follows:
 - .1 Human resources to execute the work to be recruited from local communities to the maximum extent possible. Any legislation effective in the Yukon Territory relating to use of local human resources must be complied with without exception.
 - .2 Training as required is to be provided to local recruits in undertaking all aspects of the work.

1. PROJECT CONTROL SYSTEM REQUIREMENTS AND APPLICATION

The Owner's site representative will operate a system of overall project control of which this contract forms a part. The Contractor is required to provide the Owner's site representative with information and assistance necessary to manage the project control system.

2. CONTRACTOR PROJECT CONTROL

.1 The Contractor will be required to input into two aspects of the project control system, as follows:

.1 Schedule Control

- .1 The Contractor shall provide a schedule (bar chart) to indicate when various activities in the contract will be carried out.
- .2 Schedules shall be updated monthly to indicate actual performance vs planned performance.
- .3 Deviations from the schedule shall be addressed by the Contractor in such a manner that assurance is provided that the contract will be completed by the specified date.

.2 Cost and Quantity Control

- .1 Maintain accurate up-to-date record of quantities of work carried out.
- .2 Quantities of materials to be paid for by the cubic metre will be measured by the Owner's site representative prior to start of work and after completion of the work.
- .3 Lump sum items shall be submitted by the Contractor as applicable work is carried out.
- .4 On a monthly basis, report status on all items, report statistics on lost time accidents, and cost data for cash allowance items.

3. PURPOSE

.1 The purpose of Project Control Information includes the following:

- .1 Provide the Contracting Authority with the basis for allocating resources to the project.
- .2 Identify cash flow requirements.
- .3 Documents how specific project objectives are being achieved.
- .4 Provide the Contracting Authority with the basis for making contract payments.
- .2 The Contractor is advised that revisions to the plan to maximize project efficiencies will be permitted.

4. UPDATING, MAINTAINING AND REPORTING PROGRESS

.1 As part of each site meeting, the Contractor and the Owner's site representative shall inspect all of the work in progress, and note any variances from the approved contract requirements, or schedules.

5. **EFFECT OF ACCEPTANCE**

.1 Acceptance by the Owner's site representative of the Contractor's schedules does not relieve the Contractor from any duties or responsibilities required by the contract.

.1 This section covers requirements for inspection and testing services for this contract.

2. **APPOINTMENT AND PAYMENT**

- .1 The Contractor will appoint and pay for services of testing laboratory for the following:
 - .1 Inspection and testing required by laws, ordinances, rules, regulations or orders of public authorities.
 - .2 Inspection and testing performed exclusively for Contractor's convenience.
 - .3 Testing, adjustment and balance of weigh scales.
- .2 The Owner's site representative will appoint and pay for services of testing laboratory for the following:
 - .1 Inspection and testing required by the condition of land use permits issued for the work.
 - .2 Testing to confirm the presence or absence of contaminated materials.
 - .3 Testing required under monitoring programs.
 - .4 Compaction testing.
- .3 The Supplier will appoint and pay for testing laboratory for the following:
 - .1 All quality assurance and certificates for compliance related to installation of the Waterloo Barrier.
 - .2 All quality assurance and certificates for compliance related to installation of the geomembrane.

- .1 Temporary facilities consist of essential temporary buildings, structures, utilities and services required at the site during clean up of the site.
- .2 Temporary facilities shall meet the requirements of Federal, Territorial and local authorities having jurisdiction.

2. SANITARY FACILITIES

- .1 Provide sanitary facilities for work force in accordance with governing regulations and ordinances.
- .2 Post notices and take such precautions as required by local health authorities. Keep area and premises in sanitary condition.
- .3 Sanitary facilities to be provided at the mine tailings site.

3. SITE OFFICE

- .1 Provide a site office, at the Venus Mine Tailings Site, for use by the Contractor and the Owner's site representative.
- .2 Inside dimensions for area to be used by Owner's site representative shall be minimum 3.6 m long x 3 m wide, by 2.4 m high, complete with 4-50% opening windows and one lockable door.
- .3 Equip office with 1 x 2 m table, 4 chairs, 6 m of shelving 300 mm wide, one 3-drawer filing cabinet, one plain rack and one coat rack and shelf.
- .4 Site office shall be insulated, and a heating system installed to maintain 22°C inside at -30°C outside temperature.
- .5 Install electrical lighting system to provide min. 750 lx using surface mounted, shielded commercial fixtures with 10% upward light component.
- .6 Arrange and pay for a communication system. Long distance calls placed on this phone by the Owner's site representative will be paid for by the Owner.
- .7 Maintain in clean condition.

Section 01500 Page 2 June 27, 1995

4. PAYMENT

.1 Payment for temporary facilities will be paid for by the Contractor under "costs to complete project".

.1 Personnel safety, and reliable communications are of concern due to the remoteness of the site.

2. CONSTRUCTION SAFETY MEASURES

.1 Observe and enforce construction safety measures required by the latest revisions of Canada Labour Code, Workers' Compensation Board, and applicable Occupational Health and Safety Regulations, Territorial and local statutes and authorities.

3. SIGNAGE AND TRAFFIC CONTROL

- .1 Erect construction signs as indicated on the contract drawings.
- .2 Maintain signs on a daily basis, including covering messages during periods of inactivity.
- .3 Post flag persons at the mine tailings site when hauling is being carried out.
- .4 Two flag persons shall be posted during periods of high tourist traffic. During winter months, with low vehicular traffic, flag persons will not be required.
- .5 Observe any regulations for flag persons required by the Yukon Highway Department.

4. **COMMUNICATIONS**

- .1 Establish a communications network for communications on site, with the nearest community and through long distance networks.
- .2 Flag persons shall be provided with portable radios suitable for communicating with each other, and with a base station located at the construction office.
- .3 Communication facilities in the field office shall be suitable for making long distance calls to Carcross, to Whitehorse and points south.

5. MEASUREMENT FOR PAYMENT

.1 Work under this section will be paid for under "Costs to Complete Project".

The Contractor shall ensure that all applicable legislation, regulations, guidelines and codes of practice are followed.

2. REFERENCES

- .1 Although not necessarily limited to, some key environmental references are:
 - .1 Canadian Environmental Protection Act (1988) CEPA.
 - .2 Occupational Health Regulations.
 - "Guidelines for the Abandonment and Restoration Planning of Mines in the Northwest Territories", Northern Territories Water Board and Northern Territories Region Northern Affairs Program, Department of Indian Affairs and Northern Development, September 1990.
 - "Guidelines for Tailings Impoundment in the Northwest Territories", February 1987.
 - .5 "Acid Rock Drainage Potential in the Northwest Territories: An Evaluation of Active and Abandoned Mines", Minister of Indian Affairs and Northern Development, Ottawa, 1994.
 - .6 MacLaren Plansearch, "Environmental Guidelines: Pits and Quarries", Minister of Indian Affairs and Northern Development, Ottawa, 1989.

3. SUBMITTALS

.1 PWGSC will make necessary submittals for land use permit requirements directly to the responsible agency.

4. **ENVIRONMENTAL ASSESSMENT**

.1 The environmental assessment for this project, prepared by DIAND, forms part of this contract.

5. FIRES

- .1 Fires and burning of rubbish on site permitted only on approval of the Owner's site representative.
- .2 Provide supervision, attendance and fire protection measures as directed.

1.1 WORK INCLUDED

- This section specifies requirements for furnishing all materials and equipment and for performing all operations to install the steel sheet pile barrier walls including joint sealing procedures as shown on the Drawings. Sheet piling shall also be installed where required by the Contractor's method of construction and the existing conditions. This steel sheet pile barrier wall technology is described in a British Patent issued April 7th, 1993 (No. 2228760).
- .2 The Owner has undertaken a geotechnical survey of the site. Information contained in the test logs are generally indicative of the types of materials which will be encountered. Soils information is **not** available on the final selected alignment of the Waterloo Barrier. The supplier, as part of his overall cost, must undertake sufficient additional borings to determine the exact length of sheet piles required.
- .3 The Owner will specify the top elevation and configuration of the sheet piles, and will specify the <u>criteria for acceptance</u> of the bottom elevation of the piles.

1.2 **RELATED WORK**

- .1 Related work, specified in the "Scope of Work" section of the specifications includes:
 - .1 Excavation of wind blown tailings and levelling of the tailings pile.
 - .2 Screening, hauling, and placing capillary break material.
 - .3 Supply and installation of a geomembrane.
 - .4 Construction of a drainage outfall structure.

1.3 **REFERENCE STANDARDS**

- .1 American Society for Testing and Materials (ASTM):
 - .1 A 36 Standard Specification for Structural Steel.
 - .2 A 328 Standard Specification for Steel Sheet Piling.

- .3 A 572 High Strength Low Alloy Columbium-Vanadium Steels of Structural Quality.
- .4 A 668 Standard Specification for Steel Forging, Carbon and Alloy, for General Industrial Use.
- .2 American Welding Society (AWS). D1.1 Structural Welding Code.
- .3 Canadian Standards Association:
 - .1 G40.20 General Requirements for Rolled or Welded Structural Quality Steel.
 - .2 G40.21 Structural Quality Steels.
- .4 Figures showing sections of the Waterloo BarrierTM are provided at the end of this section.

1.4 **SUBMITTAL**

- .1 Submit the following items for review by the Engineer:
 - .1 Certification: Provide documentation of agreement with Waterloo Barrier Inc. licensed installer (C3 Environmental, 519-648-3611, Breslau, Ontario) for provision of quality control services for the sheet pile installation and to complete joint sealing.
 - .2 Pile Installation Plan which outlines detailed pile placement, equipment used, splicing requirements and details, the method to achieve verticality within 1 percent, quality control measures, joint preparation prior to sealing and grout materials, mixing and placement.
 - .3 Mill test documentation for piling to be used on project.
 - .4 Manufacturer's data that indicates the structural properties of piling section(s) to be used, including I, S, Moment Capacity, thickness and width/depth dimensions.
 - .5 Proposed welding procedures and certification of welders.
 - .6 Proposed method of sealing ends between Waterloo Barrier and rock surface.

1.5 **COORDINATION**

.1 Notify the Engineer at least 5 working days prior to beginning pile driving operations at any location. This will not relieve the Contractor of his responsibilities for performing the work in accordance with these specifications and contract drawings.

1.6 **QUALITY CONTROL**

- .1 The Quality Assurance Quality Control (QA/QC) program and joint sealing to be completed by Waterloo Barrier Inc. licensed installer (C3 Environmental, 519-648-3611, Breslau, Ontario).
- .2 Horizontal Alignment and Plumbness Tolerances: The maximum permissible horizontal tolerance in pile driving will be a deviation of not more than 150 mm (6 inches) from the plan location indicated on the Drawings.

2. PART 2 - PRODUCTS

2.1 **RELATED WORK**

- .1 Provide piling as manufactured by Canadian Metal Rolling Mills in Cambridge, Ontario, or other approved manufacturer under licence from Waterloo Barrier Inc.
- .2 A foot plate will be welded to the base of each female joint of the sealable sheet piling to prevent soil from entering the joint as the pile is driven into the ground. The fabrication and attachment of the foot plate will be the responsibility of the Site Contractor. Exact dimensions of the foot plate will be based on the final rolled sheet piles. The Contractor will make the necessary fabrication arrangement to assure manufacture of the foot plates does not delay the sheet pile installation.
- .3 If the Contractor chooses to drive sheet piles in doubles, a cone will be employed to prevent soil from entering the mated (centre) joint. The Contractor will be responsible for the fabrication and installation of the cone for each paired sheet pile set. Foot plates will be welded to the base of the female joint of the paired set as described in the preceding paragraph.
- .4 Minimum Section Properties of Piling:

.1 Thickness:

0.295 inches

7.5 mm

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.2	Nominal Width:	22.25 inches	565 mm
.3	Section Area:	10.47 square inches	6.7 x 10 ⁻¹⁰ m ²
.4	Weight:	19.2 lbs./square foot	93.8 kg/m ²
.5	Radius of Gyration	n: 3.39 inches	86.1 mm

The sealant to be used to seal the Waterloo BarrierTM sheet pile wall will be a silica fume modified, thixotropic cementitious based grout, WBS Type 301 or approved equal.

3. **EXECUTION**

3.1 **SHEET PILE INSTALLATION**

- .1 Handling Sheet Piles:
 - .1 Lift in a manner which will not cause excessive bending stresses.
 - .2 Do not damage sheet piles in either handling or installing operations.
 - .3 The joint of each sheet pile will be visually inspected by the Contractor prior to installation. Any foreign material will be removed and damaged joints and/or sheet piles will be rejected.
 - .4 Replace or repair sheet piles which are damaged during installation.

.2 Location and Tolerances:

- .1 Drive piles vertically and in correct alignment so that the top of the wall lies on a straight line and ensure a proper interlocking throughout the entire length of the piles.
- .2 Sheet pile locations on the Drawings are approximate and will be field located when appropriate and when approved by the Engineer.
- .3 Deviation in horizontal alignment will not exceed 10 degrees at each joint.
- .4 The maximum permissible vertical tolerance (plumbness) in the pile installation will not be greater than a deviation of 1/16 inch per 1 foot vertical. The integrity of the interlock between

adjacent pile will be verified by flushing the joint. Joint inspection and flushing will be performed by the Quality Control Engineer.

.3 The Contractor will use suitable templates to ensure alignment and plumbness during driving.

.4 Pile Installation:

- .1 Install piles with equipment suitable for the conditions encountered. The method and equipment selected will install the piling to the design depths as shown on the Drawings and minimize damage to each end of piling and adjacent interlocks. Suitable procedures must be employed to prevent damage to the pile tops and joints.
- .2 Prevent and correct any tendency of the sheet piles to bend, twist or rotate, and to pull out of interlock. The integrity of each pile and interlocked joint must be maintained during and after driving.
- .3 Top of pile at elevation of cut-off will be within 2 inches (50 mm) of the specified alignment. Manipulation of piles to force them into position will not be permitted. Piles will be checked for heave. Piles found to have heaved will be redriven to the required point elevation.
- .4 Piles damaged or driven outside the above tolerances will be replaced. Any sheet pile ruptured in the interlock or otherwise damaged during installation will be immediately pulled and replaced.
- .5 Piles will be driven not deeper than 1 foot (300 mm) of the specified depths for each location. The Contractor will take the necessary precautions to assure adjacent piles do not penetrate deeper during pile installation.
- .6 Pull any sheet piling that are known to have pulled out of the interlock or are suspected of having tip or interlock damage, as determined by the Quality Control Engineer, and pull for visual inspection before proceeding further.
- .7 Splicing is permitted if shown on the Drawings or as approved by the Engineer.

- .8 Make splices using a full penetration weld or as otherwise directed by the Engineer for structural purposes.
- .9 Space between the end section of Waterloo Barrier, and rock face are to be sealed.

3.2 **JOINT SEALING**

- .1 All sheet pile joints are to be sealed. Joint sealing is to be completed by Waterloo Barrier Inc. licensed installer (C3 Environmental, 519-648-3611, Breslau, Ontario).
- .2 Joint sealing will not be performed adjacent to sheet pile installation within a radius of the length of a sheet plus 10 feet (3 mm) from the sheet piling installation point.
- .3 After sheet piling has been installed in the ground all sealable cavities will be checked by probing and flushing of the joints with pressurized water to remove any remaining loose material.
- .4 During the flushing, a hose or pipe will be inserted into the sealable cavity and advanced downward. The hose will allow soil particles to travel up and out of the cavity.
- .5 The flushing operation will be considered complete when the hose has been passed to the base of the sealable cavity and the water escaping from the top of the joint is reasonably clean. The flushing hose may then be removed from the cavity.
- .6 A tremie hose or tube for pressure injection of the sealant will be inserted into the sealable cavity. When the tube has reached the bottom of the hole, sealant injection will begin. The hose will be withdrawn progressively up the hole as the sealant fills the space below. Keep tremie nozzle at least 6 inches (150 mm) below rising surface of sealant.
- .7 The speed at which the injection tube is withdrawn must be carefully regulated to prevent trapping water bubbles within the sealant and to ensure there is adequate sealant to fill the cavity.

3.3 **RECORDS**

.1 Provide accurate records of each sheet pile driven. Submitted records will include the following information:

- .1 Pile identification number.
- .2 Date and time of driving.
- .3 Model of hammer and energy rating.
- .4 Elevation of top of pile.
- .5 Length of sheet pile in the ground when driving is complete.
- .6 Rate of penetration in feet/minute.
- .7 Detailed remarks concerning alignment, obstructions, etc.
- .8 Plumbness records of each sheet pile installed.
- .9 Joint flushing records for each joint installed.
- .2 Mark waterproof identification number clearly visible on each sheet pile, within 2 feet (600 mm) from the top of pile.
- .3 Spray paint all sheet piles rejected from the work for any reason, at the time of rejection, with the letter "X" within 3 feet (1 m) of both ends.
- .4 Provide accurate sealant installation records. Submitted records will include the following information:
 - .1 Joint identification number.
 - .2 Date and time of sealing operation.
 - .3 A complete list of the equipment used during the installation.
 - .4 Volume of sealant required to seal each joint.

4. **REJECTION**

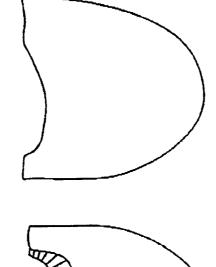
If rejected from the work because of deviation from location, plumbness requirements, excessive bending, twisting, or pulling out of interlock, or other reasons, take suitable corrective action at no additional cost to the Owner. Suitable action includes extracting, and furnishing and driving of replacement sheet piles, so that all sheet piles installed meet the requirements of this Specification.

5. **MEASUREMENT FOR PAYMENT**

- 5.1 Payment for supply and installation of the Waterloo Barrier shall be made on the basis of a proposal to be submitted by the supplier, which shall include as a minimum the following breakdowns:
 - .1 Mobilization and fixed costs.
 - .2 Accommodation, travel and communications expenses.
 - .3 Quality assurance/quality control inspection services.

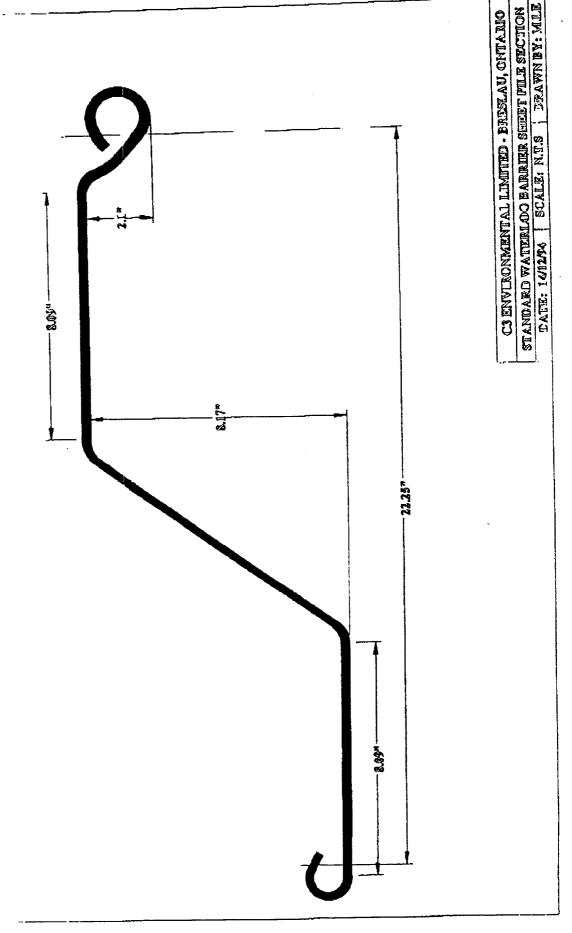
- .4 Waterloo Barrier, Sheet Piling supply and preparation. This cost to be quoted on a square foot basis.
- .5 Waterloo Barrier, Sheet Pile Installation this cost to be quoted on a per linear foot basis, to include any preparation work, and final clean up. Price to also include any support material <u>outside</u> of the containment area to provide stability.
- .6 Waterloo Barrier Sheet Pile Joint Sealing price to include sealing both ends to adjacent rock faces.

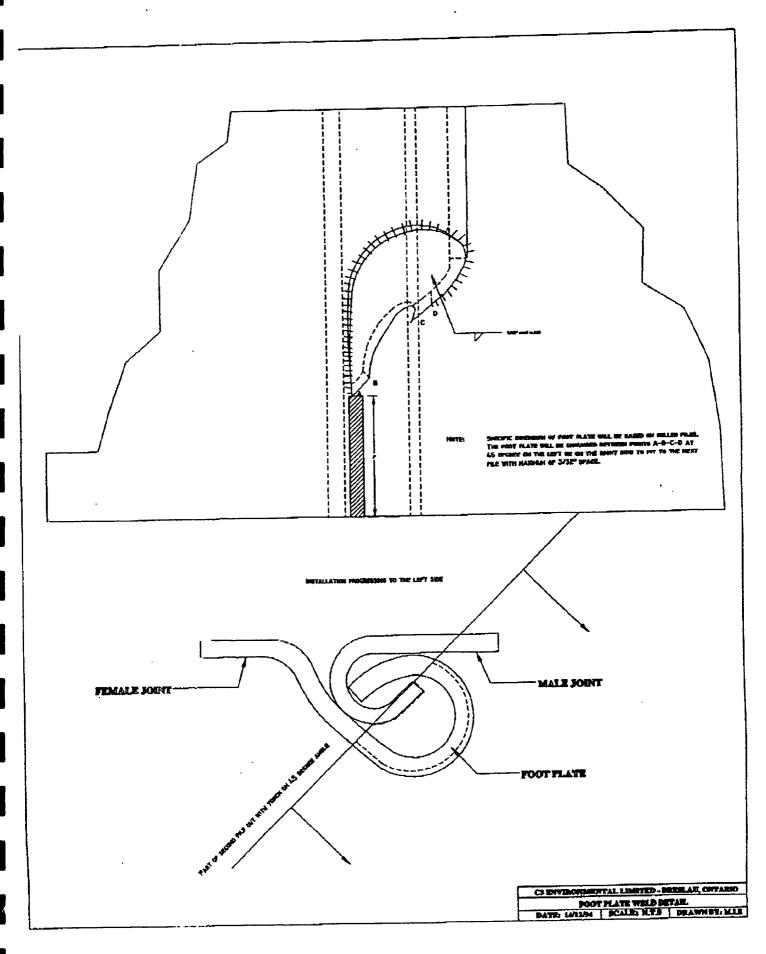
CCCCL



Approximately 45° ground surface

ACTUAL SIZE





1.1 The scope of work under "Collection and Disposal of Debris at the Venus Mine Tailings Site" includes the supply of labour and equipment necessary to collect and dispose of (by burning) wood debris at the Venus Mine Tailings Site, sealing the decant pipe, and cutting and disposing of brush within the work area.

2. **METHODOLOGY**

- 2.1 All loose wood debris located on the mine tailings shall be collected, piled on the mine tailings site and burned.
- 2.2 All scrub brush located in work areas shall be cut to ground level, collected and burned at the mine tailings site.
- 2.3 Ashes from burning are to be collected and spread over the tailings.
- 2.4 The Contractor shall be responsible for obtaining any necessary burning permits, and for compliance with any local or territorial by laws or codes with request to burning.
- 2.5 The decant pipe located in the work area shall be sealed at its inlet, and at the location where the decant pipe crosses the Waterloo Barrier. Sealing may be accomplished by use of lean mixed concrete or any other means proposed by the Contractor and accepted by the Engineer.

3. **MEASUREMENT FOR PAYMENT**

3.1 Work under this section will be paid for at the lump sum price bid for "Collection and Disposal of Debris, Disposal of Brush, and Sealing Decant Pipe".

1.1 The scope of work under "Excavate Wind Blown Tailings, and Level Existing Mine Site" includes excavating wind blown tailings outside the containment area, excavating tailings at the outfall (breech), and levelling the site to the design grade.

2. **METHODOLOGY**

- 2.1 Scrub brush, debris, and the existing pipe is to be removed and disposed of.
- 2.2 Wind blown tailings in the area designated shall be picked up, transported to the tailings area, dumped, and spread out.
- 2.3 Excavation in areas designated as wind blown tailings to be removed to a depth of 0.3 metres.
- 2.4 Tailings in the outfall area to be removed to a depth of one meter, loaded, hauled to low areas in the tailings pile, and spread.
- 2.5 The entire mine tailings area is to be levelled to elevation 82.5.
- 2.6 Compaction in low areas shall be achieved by the judicious routing of contractors equipment, aided with a wobbly wheel packer.
- 2.7 Final compaction shall be achieved by the judicious routing of contractors equipment, plus a minimum of 3 passes with an 8 to 10 tonne wobbly wheel packer. Compaction shall be deemed acceptable only after a minimum of 3 passes, and when the surface is free from ruts caused by the compaction equipment.
- 2.8 Concurrent to levelling and compaction, the entire surface is to be graded to a smooth flat surface, within 25 mm of the established grade, but not uniformly high or low.

3. **MEASUREMENTS FOR PAYMENT**

- 3.1 Payment for cleaning up wind blown tailings, excavation of tailings in the outfall area, and for levelling and compacting the entire mine site area will be made at the unit price bid to supply and labour and equipment under three (3) categories as follows:
 - .1 Clean up wind blown tailings and excavate tailings in the outfall area, will include all costs related to excavating material <u>outside</u> the

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Excavate Wind Blown Tailings, Outfall Area Excavation and Level Existing Mine Site

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Waterloo Barrier.

- .2 Levelling the tailings area will include all costs related to excavation and movement of material <u>inside</u> the Waterloo Barrier.
- .3 Levelling and compaction will include all costs related to achieving specified grade and compaction requirements.

1.1 The scope of work under "Supply and Placement of a Silty Clay Cap" includes loading, hauling, weighing, and placing silty clay materials from a "landfarm" located approximately 2 Km north of Carcross.

2. **METHODOLOGY**

- 2.1 Material to be used to construct a cap over the tailings consists of silty clay material which is currently being landfarmed at a site located approximately 2 Km north of Carcross.
- 2.2 Following excavation of wind blown tailings, site levelling, and placement of geotextile, clay materials to be used as a cap are to be loaded, hauled, weighed, and placed over the geotextile membrane.
- 2.3 Placement of cap material is to be undertaken by spreading silty clay to a depth of 200 mm, levelling and compacting the final surface.
- 2.4 Compaction shall be achieved by the judicious routing of construction equipment, plus a minimum of 3 passes with an 8 to 10 tonne wobbly wheel packer. Compaction shall be deemed acceptable only after a minimum of 3 passes and when the surface is free of ruts caused by the compaction equipment.
- 2.5 The final grade shall be within 25 mm of the design grade, but not uniformly high or low.
- 2.6 Following completion of hauling cap materials, the original "landfarm" site is to be smoothed, to a degree that no ponding occurs on the surface.

3. MEASUREMENT FOR PAYMENT

3.1 Silty clay material to be used as a cap, shall be loaded, hauled, placed, compacted, and graded. Price to include all labour and equipment necessary to construct a silty clay cap, and to smooth the source site, and shall be based on the unit price tendered, per cubic metre, measured "in place", for capping material.

1.1 The scope of work under this section covers the supply and installation of a non woven geotextile.

2. MATERIALS

2.1 Geotextile to be utilized shall be Nilex Geotextile, designation 4551 (C24) or approved equivalent.

3. **METHODOLOGY**

- 3.1 Installation shall be in accordance with manufacturer's guidelines.
- 3.2 Geotextile shall be placed directly over the tailings.

4. MEASUREMENT FOR PAYMENT

4.1 Non woven geotextile shall be paid for at the unit price tendered per square metre for non woven geotextile, and shall include all costs related to supply, freight, and installation of the material in accordance with plans and specifications.



NILEX GEOTEXTILES

Vancouver: (6 20-6443 Edmonton: ⁴○3 (60m, 463-9535 Calgary: ⁴○3 (604) 236-8385 Calgary: 40 3 sea ×e

METRIC ı TYPICAL VALUES

	Test	;			Nonwo	woven Geotextiles	xtiles						Woven Geotextiles	otextiles			
Property	Method	SE	4535 C10	4545	4551	553	15 8	1954	4589 AmoPave	2000 P100	2002 <i>P500</i>	2006	2016	2044	1198	1199	1380 Silt Stop
Grab Tensile Strength	ASTM-D-4632	z	374	690	977	1068	1455	1687	485	•712	•1024	•1513	•1590	€3000	•1429 ▲1268	●1691 ▲1268	• 1046
Grab Tensile Elongation	ASTM-D-4632	%	70	70	02	02	02	0,2	88	•24	•22	27.	25	•22	•32	98	9.76
Mullen Burst	ASTM-D-3786	kPa	1419	1826	2633	3618	4962	6850	1716	2519	2963	4376	2920	10000	3205	3653	2929
Pundure	ASTM-D-4833	Z	215	356	929	700	912	1522	330	356	445	629	623	745	623	899	490
Trapezold Tear	ASTM-D-4533	z	128	727	338	467	009	1055	205	356	490	999	029	1560	400	400	400
UV Resistance	ASTM-D-4355	%	85	85	85	88	88	22	02	02	70	70	08	8	06	96	88
Apparent Opening Size	ASTM-D-4751	Es	115	100	100	75	75	83	n/a	212	212	212	212	150	212	150	300
Permitivity	ASTM-D-4491	- 3ec	2.7	2.5	6.1	1.5	=	7.0	n/a	0.04	90:04	0.02	0.55	0.15	0.5	50:04	0.4
Flow Rate	ASTM-D 4491	Us/m²	200	169	121	92	88	25	n/a	3.4	3.4	1.7	04	12	85	4	36
Unit Weight		g/m²	125	175	230	285	400	455	125	125	180	230	952	425	177	171	234
Thickness		mm	1.2	1.7	3.0	3.2	4.3	5.4	1.5	0.45	0.5	9.0	0.7	0.9	9.0	9:0	7:0

Nilex Product Number Amoco Product Number ● Warp ▲ Fill

The above geotextiles are manufactured for Nilex by Amoco Fabrics and Fibers Company

DEFINITION: Typical Value

Since various companies perform their "typical value" tests differently, it is difficult to define the method used to obtain a Typical Value. Generally, the *Typical Value* is the average (arithmetic mean) value of an indeterminate number of sample tests (I.E. Could be the average of 2 samples or of 2000 samples). *Typical Values* should therefore be used only if *Minimum Average Roll Values* are not available.

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GEOTEXTILES IN SEPARATION APPLICATIONS GUIDE SPECIFICATION

DESCRIPTION

This work shall consist of furnishing and placing a geotextile for use as a permeable separator to prevent inter-mixing of dissimilar materials such as: subgrades and surfaced or unsurfaced pavement materials; and foundations and select fill materials. The geotextile shall be designed to allow passage of water while retaining in-situ soil. This specification does not address geotextiles used for reinforcement.

MATERIAL REQUIREMENTS

Geotextile: The geotextile shall be composed of synthetic fibers formed into a woven or nonwoven fabric. Fibers used in the manufacture of the geotextile shall be composed of at least 85 percent by weight polyolefins, polyesters, or polyamides. The geotextile shall be free of defects or flaws which significantly affect its physical properties. The geotextile shall meet the requirements of Table 5-1. The choice of a geotextile for this application is determined by the ability of the geotextile to survive installation stresses as shown in Table 5-2.

CONSTRUCTION AND INSTALLATION REQUIREMENTS

Geotextile Shipment/Storage: The geotextile rolls shall be furnished with suitable wrapping for protection against moisture and extended ultraviolet exposure prior to placement. Rolls shall be stored in a manner which protects them from the elements. If stored outdoors, they shall be elevated and protected with a waterproof cover. At no time shall the geotextile be exposed to ultraviolet light for a waterproof exceeding fourteen days. The geotextile rolls shall be labeled as per ASTM D 4873, "Guide for Identification, Storage, and Handling of Geotextiles".

Site Preparation: The installation area shall be prepared by clearing all debris or obstructions which may damage the geotextile. Trees and large bushes should be cut at ground level. In most cases, all native vegetation, roots and topsoil must be removed from the roadway subgrade prior to geotextile placement. Where required by the contract documents, soft and otherwise unsuitable subgrade areas shall be identified, excavated and backfilled with select material in accordance with the contract documents. Stabilization of these areas may be enhanced by use of a geotextile at the bottom of the excavation before backfilling. However, when designed for soft or wet subgrade conditions, native vegetation, roots and topsoil may be left in place so as to limit disturbance and resulting shear strength loss of the subgrade soil.

Geotextile Placement: The geotextile shall be unrolled as smoothly as possible on the prepared subgrade in the direction of construction traffic. Geotextile rolls shall be overlapped in the direction of subbase placement. The geotextile shall be overlapped or seamed in accordance with the minimum requirements provided in Table 5-3. Sewing is recommended where subgrade soils exhibit a CBR less than 0.5 and is preferred where subgrade soils exhibit a CBR greater than 0.5 but less than or equal to one.

If required, the geotextile may be held in place prior to subbase placement with pins, sand bags, or piles of fill or rock. On curves, the geotextile may be folded or cut to conform to the curve as illustrated in Figure 5-1. If site conditions require geotextile seaming, the geotextile shall be cut and seamed on the curve. The fold or overlap shall be in the direction of construction and shall be held in place as prescribed above. The geotextile shall not be dragged across the subgrade.

Damaged geotextiles, as identified by the engineer, shall be repaired immediately. The damaged area plus an additional three feet around the damaged area shall be cleared of all fill material. A geotextile patch extending three feet beyond the perimeter of the damage shall be constructed as directed by the engineer. Sewing of a geotextile patch may be required over soft subgrades as directed by the engineer. Damaged geotextile shall be repaired at no cost to the owner.

Aggregate Placement: The aggregate base or subbase (aggregate) shall be placed by end dumping adjacent to the geotextile or over previously placed aggregate. End dumping or tail gate dumping of aggregate on the geotextile will not be permitted. The aggregate shall be spread from the backdumped pile using a bulldozer or motor grader. A sufficient thickness of aggregate should be in place prior to dumping to minimize the potential of subgrade pumping and localized subgrade failure.

The aggregate shall be placed on the geotextile in lifts not less than 6-in. thick. For low volume roads, the minimum lift may be reduced to a 4-in. thickness at the discretion of the engineer. Traffic shall not be permitted directly on the geotextile. Sudden stops or turns by equipment operating on aggregate placed over the geotextile shall be avoided. A smooth drum roller shall be used to achieve specified aggregate density. Any ruts occurring during construction shall be filled with additional aggregate and compacted to the specified density. Vibratory compaction shall not be used on the initial lift over the geotextile.

METHOD OF MEASUREMENT

Geotextile: The geotextile shall be measured by the number of square yards from the payment lines shown on the plans or from the payment lines established in writing by the engineer. This excludes seams and overlaps. Excavation, backfill, bedding, and cover material are separate pay items.

BASIS OF PAYMENT

HC

Geotextile: The accepted quantities of geotextile shall be paid for at the contract unit price per square yard in place.

TABLE 5-1

PHYSICAL REQUIREMENTS^{1, 2, 3}

GEOTEXTILES IN SEPARATION APPLICATIONS

Property Units Required Values Test Method Medium High Survivability⁴ Tensile Ibs 180 270 ASTM D 4632 Strength

	1			
Tensile Strength	lbs	180	270	ASTM D 4632
Elongation	%	50	50	ASTM D 4632
Seam Strength	lbs	160	240	ASTM D 4632
Puncture Strength	lbs	70	100	ASTM D 4833
Trapezoid Tear Strength	lbs	70	100	ASTM D 4533
Permitivity	1/sec	.02(5)	.02(5)	ASTM D 4491
Apparent Opening Size	U.S. Standard Sieve	(6)	(6)	ASTM D 4751
Ultraviolet Stability ⁷	%	70	70	ASTM D 4355

Notes:

- Conformance of geotextiles to specification property requirements shall be determined according to ASTM D 4873, "Guide for Identification, Storage, and Handling of Geotextiles".
- 2. Contracting agency may require a letter from the manufacturer certifying that its geotextile meets specification requirements.
- 3. All numerical values, except those of elongation, represent minimum average roll values (i.e., average test results from any sampled roll in a lot shall exceed the minimum average roll values) in weaker principal direction. Values of elongation represent maximum average roll values. Lot sampled according to ASTM D 4354, "Practice for Sampling Geosynthetics for Testing".

(Table 5-1 continued)

- 4. Recommended survivability ratings are provided in Table 5-2.
- 5. Permitivity shall be greater than the specified minimum value and result in a geotextile permeability which is greater than the permeability of the subgrade soil.
- 6. Minimum #30 U.S. Standard Sieve (maximum 0.6mm) for subgrade soils with 50 percent or greater particles by weight passing the #200 U.S. Standard Sieve. Minimum #50 U.S. Standard Sieve (maximum 0.297mm) for subgrade soils with more than 50 percent particles by weight passing the #200 U.S. Standard Sieve. Design apparent opening size to be selected by the design engineer based on site soil and groundwater conditions.
- Percent of tensile strength retained as evaluated using ASTM D 4632, "Test Method for Breaking Load and Elongation of Geotextiles (Grab Method)" after conditioning for 500 hours.

TABLE 5-2
CONSTRUCTION SURVIVABILITY RATINGS^{1, 2, 3, 4}

Subgrade CBR At	<	1	1-	-2	>	2
Installation Equipment Contact Pressure (psi)	>50	<50	>50	<50	>50	<50
Compacted Aggregate Thickness (in) ⁽⁵⁾				•		
4 ⁽⁶⁾ 6 12 18	NR NR NR H	NR NR H M	Н Н М М	M H M	M M M M	M M M

Notes:

- 1. From "Geotextile Design and Construction Guidelines", Federal Highway Administration, Publication No. FHWA-HI-90-001, October 1989.
- 2. H-HIGH
- 3. M MEDIUM

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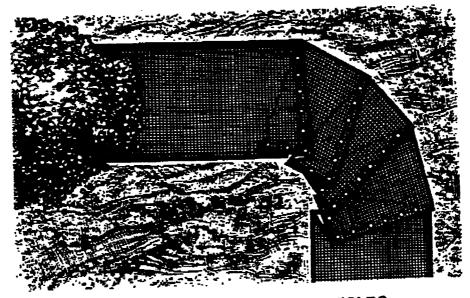
- 4. NR NOT RECOMMENDED
- 5. Maximum aggregate size not to exceed one half the compacted thickness.
- 6. The four inch minimum cover is intended for existing road bases and not intended for use in new construction.

TABLE 5-3
SEAM RECOMMENDATIONS^{1,2}

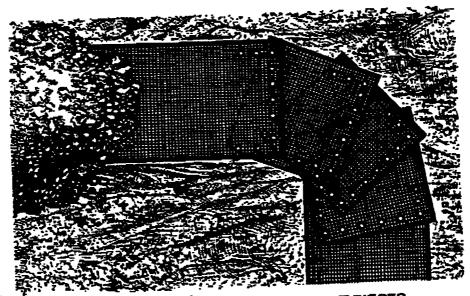
Overlap Location	Soil Strength (CBR)	Minimum Overlap (ft)
	<0.5	(3)
Overlap of adjacent geotextile rolls	<u><</u> 1 > 0.5	3(4)
	<u><</u> 2	2.5 ⁽⁵⁾
	> 2	1.5(5)
Overlap of geotextile roll ends	≤ 0.5	(3)
four ends	> 0.5	3(5)

Notes:

- 1. Adapted from Task Force 25 and "Geotextile Design and Construction Guidelines," Federal Highway Administration Publication No. FHWA-HI-90-001, October 1989.
- 2. Overlap requirements are not applicable to sewn seams.
- 3. Overlaps are not recommended for soil CBR less than 0.5.
- Sewn seams of adjacent geotextile rolls are preferred for soil CBR greater than 0.5 but less than or equal to one.
- 5. Sewn seams are acceptable for all soil CBRs.



A. FORMING A CURVE USING FOLDS



B. FORMING A CURVE USING CUT PIECES

Figure 5-1 PLACEMENT OF SEPARATION GEOTEXTILE ON CURVES [FHWA, 1989]

(Note: o - indicates locations of pins, sandbags, piles of fill or rock, or other means of temporarily anchoring geotextile. Anchors shall be placed on 2 feet centers minimum.)

1.1 The scope of work under "Capillary Break Material" includes the loading, hauling, weighing, placing, grading, and compacting of granular materials.

2. **METHODOLOGY**

2.1 Material for use as a capillary break material shall be screened pit run stone or gravel, meeting the following gradation:

Sieve Designation	% Passing
75 mm	100%
25 mm	60 to 100%
12.5 mm	38 to 70%
0.075 mm	2 to 10%

Material to be tested to ASTM C136 and ASTM C117; sieve sizes up to CAN/CGSB-8.1.

- 2.2 Screened pit run material is to be loaded, hauled, weighed at the mine site, and spread over the clay cap.
- 2.3 Material shall be placed in one 300 mm (compacted) lift.
- 2.4 Compaction shall be achieved by the judicious routing of construction equipment, plus a minimum of 3 passes with an 8 to 10 tonne steel roller.
- 2.5 The final surface shall be graded and compacted to a flat, firm surface, within 25 mm of the established grade, but not uniformly high or low.
- 2.6 Material is to be placed on clean, unfrozen surfaces, free from ice or snow.
- 2.7 Material shall not be frozen when placed.

3. **MEASUREMENT FOR PAYMENT**

Capillary break material shall be paid for at the unit price tendered per cubic metre, measured in place. Price to include all labour and equipment to load, haul, grade, compact, and place the material to the level indicated on the contract drawings.

1.1 The scope of work under this section includes the supply and placement of pitrun aggregate for use as a fill at the outfall, outside of the Waterloo Barrier.

2. **METHODOLOGY**

- 2.1 Material to be used for fill outside the Waterloo Barrier, shall consist of pitrun aggregate, with 100% passing a 200 mm screen.
- 2.2 Screened material shall be loaded, hauled, and placed at the outfall.
- 2.3 Material shall be placed in layers not exceeding 500 mm and compacted with spreading equipment (dozer).
- 2.4 The final surface shall be at the design grade at the Waterloo Barrier, and sloped to blend with existing terrain.

3. MEASUREMENT FOR PAYMENT

3.1 Material used for fill at the outfall shall be paid for at the unit price tendered, per cubic metre, measured in place. Price to include all labour and equipment necessary, to screen, load, haul, weigh, and place material at the outfall.

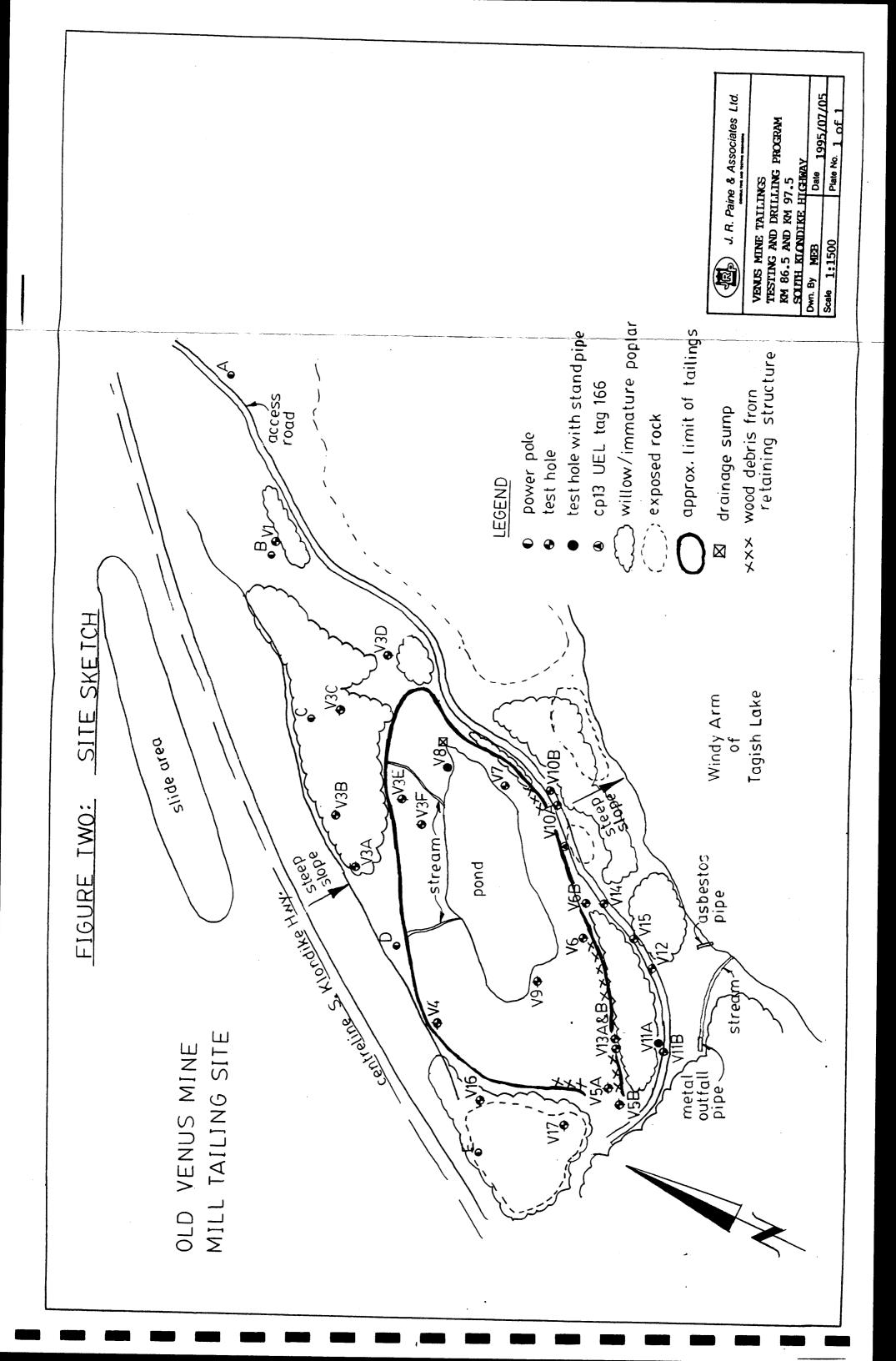
1.1 The scope of work under this section includes supply and installation of piping and end sections at the drainage outfall.

2. **METHODOLOGY**

- 2.1 Water discharging from the tailings shall be collected by means of a galvanized steel end section for round pipe.
- 2.2 Pipe shall be supplied to the configuration shown on the drawings and shall be 600 mm corrugated metal pipe.
- 2.3 Galvanized steel end sections for round pipe shall be installed at both ends.
- 2.4 Pipe and end section leaving the outlet shall be supported by pitrun gravel, maximum size 200 mm.
- 2.5 Pipe at the discharge section shall be covered with a minimum of 300 mm native material and compacted to the density of adjacent undisturbed material.

3. **MEASUREMENT FOR PAYMENT**

3.1 Payment for constructing the outfall structure will be at the lump sum price tendered for constructing the drainage outfall structure. Price to include all labour, equipment and materials, except for 200 mm pitrun aggregate which will be paid for as a separate item.



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J. R. Paine & Associates Ltd. CONSULTING AND TESTING ENGINEERS

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J. R. Paine & Associates Ltd.

CONSULTING AND TESTING ENGINEERS

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J. R. Paine & Associates Ltd.

CONSULTING AND TESTING ENGINEERS

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Public Works Canada Environmental A&ES							&ES		J					DREHOLE NO: V3C					
Drille	d us	sing	CME 7	5 track	mou	nted r	rig						PROJ	OJECT NO: 8054-12					
with s	solic	ste	m ou	gers					(see site sketch)				ELEV	ATION:					
SAMP	LE	TYP		TUBE			LOST		X AUGER	B	ULK	s	PT			CORE			
BACK	FILI	T`	(PE	BENTO	NITE	ĺ	PEA G	RAVEL	III SFONCH	GF GF	ROUT	DRILL CUTTINGS SAND							
	سا		N _O	10	■ UK 20	3010 = 30	40					20	● C	LAY ● 60	80		<u>بر</u>	E	
Œ	IYP	S	IAT		A PL	STIC A		1	SOILS DI	'ION		▲ 5	SILT A	80			ž		
DEPTH(m)	۳	F	MEN	10	20	30 40		-	DOILE DI		1011	20 40 6		AND III	00		SOIL SYMBOL	ELEVATION(m)	
	SAMPLE TYPE SAMPLE NO SAMP						LIQUID					20		60	80		등	E	
	S	0,	NS.	10	20	30	40					20	♦ GR 40	AVEL.♦	80		\ <u>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</u>	1	
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ŧ								0	rganic and tops	oil layer	2.1	/						Ē	
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ŧ									ossibly boulders								Ш	£	
E 2.0					ļ <u>.</u>	ļļ	ļļ		ock in sample, d				-					-2.0	
Ē								lo	ose,			<u> </u>		<u>. </u>		CL-M	4111	Ę	
Ē		T45						CU TO	/ OL 1V		1.8m							ŧ	
3.0		143						'n	l CLAY ome sand, trace	arayol stiff t	tracas	/	·				PERE	- -3.0	
ŧ									f oxidation arour			 						Ē	
Ē.,									ioist; brown and									Ē	
E 4.0											3.0m							E-4.0	
Ę						·		END	OF HOLE @ 3.0M									Ē	
5.0													<u>.</u>					E-5.0	
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1		٠.	49						Julu.	REVIEWED I	BY: WCK		CO	MPLETI	: 95/				
L.				IT I	uren	1012(e. Yuk	OII		Fig. No: 1						10	ige 1	01 1	

Public Works Canada Environmental A&ES							Venus Mine Tailings		BOREHOLE NO: V3D					
					mounted r	rig	V3D located east of		PROJECT NO: 8054-12 ELEVATION:					
with s					·	7	(see site sketch)			SPT CORE				
SAMP				TUBE	NAUTE [LOST PEA GE	AUGER RAYEL SLOUGH	BULK GROUT		L CUITINGS		SAND		
BACK	FILL		(PE	BENTO	# UQUID ■	· PEA GI	CAYEL [[[[] SLOUGH	M - GROOT	K	• CLAY •				
2	TYPE					40	SOILS DES	מרסוסיוראו	20	40 60 ▲ SILT ▲	80		80L	E
불		Ä	ATA T	10	20 30	40	משת פחוספ	OCILIT HON		40 60 SAND III	80	nsc	SYMBOL	E E
DEPTH(m)	SAMPLE	SAMPLE	SE C	PLASTIC	M.C.	LIQUID			20	40 60	80		SOIL	ELEVATION(m)
	S	S	NS.	10	20 30	40			20	GRAVEL ◆ 40 60	80		S	
0.0		T46					SILT							0.0
Ē		140					 -some clay, grey, low organics, firm, damp 					ML		Ē
- 1.0						ļļ	organics, min, damp					-	Ш	-1.0
Ē	\boxtimes	T47						1.2m				CL-ML		Ė
E							SILTY CLAY	light grov maint						-2.0
E 2.0							-trace gravel, beige/l soft, medium plastici							F - 2.0
Ē								1.5m	7					F
= 3.0							END OF HOLE @ 1.5m					1		-3.0
Ē							NOTES: -V3D located in small	channel leading						<u> </u>
Ē							toward tailings area;							Ē.,
E 4.0							appearance on surfa							-4.0 E
Ē							channel							Ē
E 5.0														-5.0
E														Ē
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6.0														-6.0
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14.0	Ш	ī	$\frac{1}{D}$	D -	_ n. #	<u> </u>	-1 - T 1 1	LOGGED BY: MEB	_1_i_i_i_	COMPLETI	ON DEPT	TH: 1.5	nn l	-14.0
		J.	Κ				ates Ltd.	REVIEWED BY: WCK		COMPLETE		5/15		
95/07/11 C				Wh	<u>nitehors</u>	<u>e, Yuk</u>	on	Fig. No: 1		<u> </u>		Pa	ge 1	of 1

Public	Wo	rks	Canac	da Envir	on mr ntal .	A&ES		Venus Mine Tailings Site				BOREHOLE NO: V3E					
	-				mounted	rig		V3E located near northwest perimeter of				PROJECT NO: 8054-12					
with s						<u> </u>	tailings area (see si		<u> </u>	ELEVATION:	CORE		·				
SAMP				TUBE	NITE	LOST	AUGER	BULK GROUT	∭ s	PILL CUTTINGS							
BACK	FILL		(PE	BENTO	NITE LIQUID III	PEA GE	STONCH STONCH	M - I PROUT									
10	(m)			10	20 30 ▲ PLASTIC A	40	SOILS DES	ירסוסיוראו	20	40 60 ▲ SILT ▲	80	SYMBOL	Ē				
불		밀	ENT)	10	20 30		סחורס חדס	CRIPTION	20	40 60 SAND	80 SS	SYM	Ê				
DEPTH(m)	SAMPLE	SAMPLE	INSTRUMENTATION DATA	PLASTIC	M.C.	FIGNID			20	40 60	80	SOIL	ELEVATION(m)				
-	S	S	SNI	10	20 30	40	·		20	◆ GRAVEL ◆ 40 60	80						
0.0	×	T50					ORGANICS and TAILINGS		7		PT-	1 000	0.0				
Ē							SILTY CLAY	0.2m					Ē				
1.0							-firm, medium plastic	sity, grey, moist,			CL		-1.0				
Ę	\boxtimes	T51			•		<u> </u>						£				
Ē.,							END OF HOLE @ 1.5m	1.5m				-	E 2.0				
E- 2.0							END OF HOLE W 1.5m					ł	2.0				
Ē													Ē				
E 3.0					ļļļļ		NOTES:						-3.0				
Ē							-small amount of tail	inas mixed in with					E				
Ē							organics to 0.2m; ap	pears to be area					Ē.,				
F 4.0							of previous high wate	er level					-4.0 -				
Ę							·						Ē				
E 5.0					ļļ ļļ.								-5.0				
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E- 6.0													-6.0				
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- 14.0		Ţ	D '	 D = :	_ a. ±		_ L . T l 1	LOGGED BY: MEB		COMPLETI	ON DEPTH: 1	.5 m	-14.0				
		J.	Κ.				ates Ltd.	REVIEWED BY: WCK			: 95/06/15						
95/07/06 0				Wh	itehors	e, Yuko	on	Fig. No: 1			P	age 1	of 1				

Dried using CME 75 track mounted rig	Public Y	Norks	Canad	da Envir	onmrn	tal A	&ES	Venus Mine Tailings		BOREHOLE NO: V3F					
Value Continue C										PROJECT NO: 8054-12					
SAMPLE TYPE		<u>`</u>						tailings area (see sit	e sketch)						
SOLIC SOLI						[LOST								
SOILS DESCRIPTION 20 40 40 40 40 40 40 40 40 40 40 40 40 40	BACKFI	LL T	YPE	BENTO			PEA GI	RAVEL SLOUGH	GROUT	DRIL		SANE) - 		
TALLINGS		<u> </u>	NO	10		UID m 30	40			20	40 60 8	50	님	E	
TALLINGS			ITAT	40	A PLA	STIC A		1 SOILS DES	CRIPTION	20		ب 🔙 🏡	Y.W.B	NO	
TALLINGS	PTH.	넴급	JAE	DEACTIO				1					(S	VAT	
TALLINGS		SAN	STR	PLASIIC	₩. 	·.					GRAVEL +		S	ELE	
Sity sand, fine grained sand, wet,	1 1		Z	10	20	30	40	THUNOC				80	- XXX	- 0.0	
		752							ed sand, wet.			FI		Ē	
DECAYED ORGANICS D.8m	F	7 '34						1		الم		PI	· 💥	Ę .	
SILTY CLAY	1.0								0.8m				- V//	F-1.(
SILTY CLAY -firm, medium plasticity, grey, moist, notive material 1.5m END OF HOLE © 1.5m NOTES: -approximately 0.8 metres of tailings -well defined arganic layer marks end of tailings material -5.0 -7.0 -8.0 -9.0 11.0 12.0 J.R. Paine & Associates Ltd. Whitehorse, Yukon R. Not 1 Page 1 of 1	E				.ļļ			DECAYED ORGANICS	0.92	-}			Y 22	Ē	
-5.0 -firm, medium plasticity, grey, moist, notive material 1.5m -3.0 -3.0	E 20							SILTY CLAY	U.JIII					-2.0	
notive material 1.5m 1	£ 2"								ity, grey, moist,					Ė	
END OF HOLE ® 1.5m -4.0 NOTES: -approximately 0.8 metres of tailings -well defined organic layer marks end of tailings material -5.0 -6.0 -7.0 -8.0 -7.0 -8.0 -1.0 -														Ę	
NOTES: -approximately 0.8 metres of tailings -well defined organic layer marks end of tailings material -5.0 -6.0 -7.0 -8.0 -9.0 -10.0 -11.0 -12.0 -13.0 J.R. Paine & Associates Ltd. Whitehorse, Yukon Fig. No: 1 -4.0 -4.0 -5.7 -6.0 -6.0 -7.7 -7.7 -7.7 -8.0	= 3.0			ļ		ļļ		END OF HOLE & 15m	1.5m					-3.4 -	
Notes					ļļ	ļļ		END OF HOLE W 1.5m						Ē	
Notes	E													E	
- well defined organic layer marks end of tailings material - 6.0 - 7.0 - 8.0 - 9.0 - 10.0 - 11.0 - 12.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 13.0 - 14.0 - 14.0 - 15.	F 4.0							· ·						Ē	
11.0 12.0 13.0 14.0 15.0 16.0 16.0 16.0 17.0 17.0 18.0	E													Ę	
-6.0 -7.0 -8.0 -9.0 -10.0 -11.0 -12.0 -13.0 J.R. Paine & Associates Ltd. Logged BY: MEB COMPLETION DEPTH: 1.5 m Poge 1 of 1 -14.0 FRVIEWED BY: WCK COMPLETE: 95/06/15 -15.0 Poge 1 of 1 Poge 1 of 1 -14.0 Poge 1 of 1 Poge 1 of 1 -15.0 Poge 1 of 1 Poge 1 of 1 -16.0 Poge 1 of 1 Poge 1 of 1 -17.0 Poge 1 of 1 Poge 1 of 1 -18.0 Poge 1 of 1 Poge 1 of 1 -19.0 Poge 1 of 1 Poge 1 of 1 -19.0 P	5.0				ļļ	ļ <u>.</u>			layer marks end of					E5.	
-7.0 -8.0 -9.0 -10.0 -11.0 -12.0 -13.0 -14.0 J.R. Paine & Associates Ltd. REVIEWED BY: WCK REVIEWED BY: WCK COMPLETE: 95/08/15 Whitehorse, Yukon Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1	[]							runnigs molenui						Ė	
-7.0 -8.0 -9.0 -10.0 -11.0 -12.0 -13.0 -14.0 J.R. Paine & Associates Ltd. REVIEWED BY: WCK REVIEWED BY: WCK COMPLETE: 95/08/15 Whitehorse, Yukon Fig. No: 1 Page 1 of 1														Ė	
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-8.0 -9.0 -10.0 -11.0 -12.0 -13.0 -14.0 J.R. Paine & Associates Ltd. Logged BY: MEB COMPLETION DEPTH: 1.5 m REVIEWED BY: WCK COMPLETE: 95/06/15 -14.0 Fig. No: 1 Poge 1 of 1	E					ļ <u>ļ</u>								Ę	
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9.0 -10.0 -11.0 -12.0 -13.0 J.R. Paine & Associates Ltd. Whitehorse, Yukon LOGGED BY: MEB COMPLETION DEPTH: 1.5 m	E '													Ę	
9.0 -10.0 -11.0 -12.0 -13.0 J.R. Paine & Associates Ltd. Whitehorse, Yukon LOGGED BY: MEB COMPLETION DEPTH: 1.5 m	E					<u> </u>		•						Ē	
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		٠	J.K.						REVIEWED BY: WCK				5		
ROTULT I VICADAM	95/07/11 0 7	7:4344		W	<u>hitel</u>	nors	se, Yuk	con	Fig. No: 1				Page 1	of 1	

Public Works Canada Environmental A&ES								Venus Mine Tailings Site				BOREHOLE NO: V4					
Drilled using CME 75 track mounted rig						ig		V4 located near southwest perimeter of				PROJECT NO: 8054-12					
with s				gers				tailings area (- <u></u>			ATION:				
SAMP				TUBE		Lost		AUGEF		BULK					CORE		
BACK				BENTONITE		PEA GR	RAVEL	SLOUG	 	GROUT			UTTINGS LAY •		SAND		
	0 PE 0	TION	10 20		30 40		COLLO		TDMI O M	20	40	60	80		걸	Œ	
(E)		N N	Y Y	10 20	PLASTIC A	40		SOILS I)ESCh	APTION	20 40		SILT A 60	80	nsc	SYMBOL	Š
DEPTH(m)	SAMPLE TYPE	MP	INSTRUMENTATION DATA	PLASTIC	M.C.	LIQUID					20		AND ma	80	Š	L S	ELEVATION(m)
=	SA	SA	NSTR	 	•							♦ GF	RAVEL •			SOIL	H
- 0.0	++	T36	=_	10 20	330	40	SAND	Y SILT			20	40	<u>50</u>	80		Ш	- 0.0
Ē		130						ine grained so	nd, tailing	s material,	Ţ						Ē
1.0								ose, wet, oxid	ation, grey	, soft					ML		E 1.0
F	\forall	T 3 7					no	on-plastic									Ē
Ē	M	137				1											Ē
2.0						\\		······································		1.8m							-2.0
ŧ							1	r CLAY							CL		ŧ
E	\forall	T38				Ì	-tr	race gravel, fi	rm, moist,	beige/grey							‡
3.0	M	130					<u>m</u>	edium plastici	iy, nalive	3.Dm	$\dashv \dashv$				1	Y22	-3.0
ŧ							END	OF HOLE @ 3.	0m	0.5							Ē
4.0																	-4.0
F *."																	= 4.0
Ē		:															Ē
5.0							NOTE	•							{		E5.0
Ė							NOTE	.5: pilings materio	l avtands	to 18 m							Ē
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6.0																	-6.0
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E 7.0																	<u> </u>
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E																Ē	
14.0			ľ													Ė	
14.0		T	D 1	<u></u>	Π. A			7 1	ling	GED BY: MEB		cc	MPI FTI	ON DEPT	H: 3 f	F	-14.0
		J	π	Paine				s Ltd.		EWED BY: WCK				: 95/08			
95/07/05 O	1.4741			White	horse	. Yuko	n		Fig.	No: 1						ge 1	of 1



J. R. Paine & Associates Ltd. consulting and testing engineers

SCREEN ANALYSIS

													_				CII	ent: _		GSC	•	<u>:</u> -										
am	ple:	T	<u>36</u>					De	epth	: <u> </u>	0.:	2-0	.4	m			_ Pr	oject:	Ve	nus	M	ir	es	R	ecl	.an	ati	Lon				
oca	tion	:	Tai	lir	ngs	Ar	ea	<u>, </u>	Tes	st	<u>H</u> k	ole	: V	4			Ма	ade b	y: <u>I</u>	<u> R.</u>			Job	No	<u>.: _8</u>	105	4-]	2_				
									_								_ Ck	d by	<u>M.</u>	В.		_	Dat	e: _ˈ	95/	06	/23	3				
	٠.	eve		Τ.	Size	of ($\overline{}$						Ī	10/	eight		T	Tot	- I \A	/+		T		orc	ent		Q/	Fine	er Ti	han
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4																	ar-	vel	_	Λ		8										
ш.								-						1			<u>yı.c</u>	10ET														
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															_		sar		=		7	용										
	of S	Sie	ving	-		!	Min.										sar	nd_	=	40.	7	용										
	of S													500			sar fir	nd nes	=	40. 59.	7	96 96		4	100 3	15 2	250		160		80	63
	of S			50 44			Min.							500			sar fir	nd_	=	40. 59.	7	96 96			100 3	15 2	250		160	· · ·	80	63
ne	of S													500	 		sar fir	nd nes	=	40. 59.	7	96 96			100 3	15 2	250		160)]	80	63
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	of													500			sar fir	nd nes	=	40. 59.	7	96 96		4	400 3 400 3	15 2	250		166		80	63
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ne	of													50X			sar fir	nd nes	=	40. 59.	7	96 96			100 3	15 2	250		166		80	63

Public	Wo	orks	Cana	da Enviror	mrntal .	A&ES		Venus Mine Tail	ings Site			BOREHOLE	NO: V5	A		
Drilled	us	ing	CME 7	75 track n	nounted	rig		V5A located wit	hin breach a	rea— south		PROJECT N	3: 8054-	-12		
with s	olic	ste	m au	gers				west corner of	tailings area			ELEVATION:				
SAMP				TUBE		∠ Lost		X AUGER		BULK	s			CORE		
BACK	FILL			BENTONI		PEA G	RAVEL	STONCH	٩	GROUT	D	RILL CUTTING	S 🔯	SAND		Т
	بي		INSTRUMENTATION DATA	10	20 30	40					20	● CLAY ● 40 60	80		7	E
DEPTH(m)	SAMPLE TYPE	ž	NTATA	10	PLASTIC 2			SOILS D	ESCRII	PTION	20	▲ SILT ▲ 40 60	80	ري ا	SYMBOL	ELEVATION(m)
F H	PE	MPL	PATE	PLASTIC	M.C.	LIQUID					20	SAND III	*0	USC	S	VATI
ㅂ	SAM	SA	STR								20	40 60 ◆ GRAVEL ◆	80	1	SOIL	EE
E 0.0	<u> </u>		<u> </u>	10	20 30	40	CUT	CHID			20	40 60	80		1	- 0.0
ŧ ""	×	T34		•				' SAND rown and rust '	in colour, de	amp. loose.				SM		E
Ę	L							ell graded, (tail			<u> </u>					£
1.0	\boxtimes	T35		•						0.8m	_					Έ−1.0 Έ
Ē							1	ELLY SILTY CLA rown, medium		nint noft			ļļ	CL-MI		ŧ
E 2.0								cidation around		oisi, soii,						E 2.0
Ē														l		Ē
Ē								D DEFILON O		2.4m						Ė
3.0							AUGE	R REFUSAL @ 2	.4m				ļļ	1		-3.0
Ē																Ė
£ .,																Ę .,
F 4.0							NOTE									-4.0
Ē							-m	noved drill rig 5	im south of	V5A to				1		Ē
E 5.0							Or re	ill V5B — similo fusal at 2.1 m	ir soli protii	e with						-5.0
Ė							'6	·								Ē
F														}		Ē
F 6.0																-6.0
E													ļļ .			Ē
E 7.0																E 7.0
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9.0						`		•								-9.0
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13.0			-		<u> </u>										Ė	-13.0
			-		ļļ .										Ę	
14.0								·						_	E	-14.0
		J.	R. I	Paine	& A	ssocia	ates	Ltd		BY: MEB		COMPLET			m	
		- • •	•			<u>e. Yuko</u>		, nou.	Fig. No	ED BY: WCK		COMPLETI	E: 95/06		ge 1	of 1
95/07/06 0 5	-1341			1, 111	CITATO	<u>u, iunt</u>	111		ILIA NO	• 1				ra	15 I	VI I

Public	: Wo	orks	Cana	da Envira	nmrntal i	A&ES	Venus Mine Tailings	Site		BOREHOLE N	10: V	6	
Drille	d us	sing	CME 7	75 track	mounted	rig		erm at east edge of		PROJECT NO	: 8054	-12	
with s	_						tailings area (see si			ELEVATION:		1	····
SAMP				TUBE		LOST	AUGER	BULK	<u>∭</u> \$			CORE	
BACK	FILI			BENTON	IITE III LIQUID III	PEA GI	RAVEL IIII SLOUGH	GROUT	0	RILL CUTTINGS	<u>::::</u>	SAND	
	TYPE	9	LION	10	20 30	40		CDIDMION	20	40 60 ▲ SILT ▲	80	4	[E
DEPTH(m)	بدا	SAMPLE NO	INSTRUMENTATION DATA	10	A PLASTIC 4 20 30	40	SOILS DES	CRIPTION	20	40 60	80	NSC	SOIL SYMBOL
EPI	SAMPLE	AMP	RUM CV	PLASTIC	M.C.	LIQUID			20	## SAND ## 40 60	80] >	SOIL S
	S	S	ISI	10	20 30	40			20	♦ GRAVEL ♦ 40 60	80		S
0.0	×	T15		10	20 JU	~	SAND		1 20				0.1
E	İ						 -some silt, fine graine throughout, wet, med 						2000
1.0		T16					-becomes silty sand,					-	-1
Ē												SM	
E 2.0													2
Ę													50000 50000
F	∇	T17						2.7m	_				SSSS
F 3.0	X	T18					SANDY SILT	2.7 m				ML-SI	-3
Ē		T19					\ -wet, grey, soft, non-					-	
4.0	\otimes	T20				•	SILTY CLAY	3.4 m					HE-4
E							-some gravel, wet (fre	e water), native					
Ē .							material, loose, soft						
F 5.0							SILTY CLAY —grey, some sand, tra	re provel					-5
Ē							oxidation around grav						
6.0							medium plasticity, tra	ces organics				CL-ML	-6
Ē							within silty clay matrix	(
- 7.0													
E /**													
Ė	\boxtimes	T21			,								
8.0	Ц											-	-8
Ē	\bowtie	T22		ſ			CDANIELLY CUTY OLAY	8.2M		A ♦		0. 00	
9.0							GRAVELLY SILTY CLAY -moist, stiff, gravel to	50 mm diameter				CL-GC	-9.
	X	T23		4			grey, low plasticity		1			GC	
Ē	M	T24	ľ		7		CLAYEY GRAVEL	9.1m					
F 10.0 E			-		1		-auger action indicates	oversize				CL-ML	10
Ē	X	T25	1.		- 4		(cobbles) present, wet	(free water),	<u> </u>				
11.0							GRAVELLY SILTY CLAY	9.4m					<u></u>
							-wet, soft, grey, mediu	m plasticity,					
12.0								10.4m					Ē
							SILTY CLAY trace gravel, dense, fi	irm moist arev					<u> </u>
			-					10.7m	-				<u> </u>
13.0			-				END OF HOLE @ 10.7m						13.
							NOTES: —tailings occur to 3.4m						Ē
14.0							-possible water bearing						E -14.
		J.	R. I	Paine	& A	ssocia	ates Ltd.	LOGGED BY: MEB		COMPLETIO			
					$\frac{1}{\text{tehors}}$			REVIEWED BY: WCK Fig. No: 1		COMPLETE	95/0		ge 1 of 1
5/07/06 Q								[· · · · · · · · · · · · · · · · · · ·		_ 1			



SCREEN ANALYSIS

							CI	ient: _	PW	باحد	A	Ò.	<u> </u>)							
Sample: T22	c	epth: _	8.2	<u>2-8</u> .	. 4m		Pr	oiect:	Ver	nus	Mi	nes	5 F	∞	Lan	at	ion				
Location: Tail	ings Area,	Test	: Hc	<u>ole</u>	<u>V6</u>		М	ade by	y: P.	.R.		Job	No	.: <u>-</u> E	305	4-	<u>12</u>				
							CI	cd by:	M.I	В.		Dat	e: _	95/	'06	/2	3				
	T	7							, 												
Sieve	Size of Openia	ng					Weigh		t	Tota er Th						ent Thai	_		, Fine is Ori		
No.	MM					+-	Retained	gins	FIL	lei II	lang	11115	+-		161	1114		Das	15 011	y. 0	יוקווינ
	00.000								 				+						100	0	
80,000	80.000	_							 				+					 	56		
50,000	50.000					+			 	-			\dagger			•				•	
20,000	20.000					+			 				†	-							
10,000	10.000 5.000												+				-		46	. 2	
5,000 2,500	2.500								1										43		
2,500 2,000	2.000								<u> </u>										43		
1,250	1.250		-					-					1						42		
800	800						,				_					•			42		
630	-630																		41		
400	400																		41		
315	315																		40	_	
250	250																		39	.8_	
160	160																	_	_38	.6	
80	-080																		_35	.0.	
Description of Sa					ı	Me	thod of P	repara	tion			Drv				Wa	shec	X			
silty grave		nd, G	M																		
							narksgra	iver	= ;)3.0) '										
					_		sar	nd	=]	11.2	2										
****					_		fir	nes_	= :	35 <u>.</u> 0)									`	
Time of Sieving _	5.4°-				- 1	N'	DOTE : C		6 1	N	à.	01	٥								
	Min							N DO	1	•											
																		4.04			
63 50			5 10			 		2000	1250			30		400 3 I	15 2	250		160) 	BO (63 II
63 50			5 10	Ш	5									400 3	15 2	250		160	, 	B0 (63
63 50			5 10	Ш	5 									400 3	15 2	250	L	164		80 (63
100			5 10	Ш	5									400 3	15 2	250		160		80 (63
90			5 10		5									400 3	15 2	250		160		80 (63
100			5 10											400 3	15 2	250		160		80 (63
90 80			5 10	Ш	5									400 3	15 2	250		160) ————————————————————————————————————	80 (63
100 63 50			5 10		5 									400 3	15 2	250		160		80 (63
100 63 50 90 80 70			5 10		5 									400 3	15 2	250		164		BO (63
100 63 50 90 80 70			5 10		5 									400 3	15 2	250		164		ВО	63
90 80 70 60			5 10		5									400 3	15 2	250		166		80 (63
100 63 50 90 80 70			5 10		5									400 3	15 2	250		166		80 (63
90 80 70 60 50			5 10		5									400 3	15 2	250		166		80 (63
90 80 70 60			5 10		5									400 3	15 2	250		160		80 (63
90 80 70 60 40 40			5 10		5									400 3	15 2	250		160	, I	80 (63
90 80 70 60 50			5 10		5									400 3	15 2	250		164	, 1	80 (63
100 63 50 90 80 70 60 40 30			5 10		5									400 3	15 2	250		164		80 (63
100 63 50 90 80 70 60 50 40			5 10		5									400 3	15 2	250		161		80 (63
100 63 50 90 80 70 60 40 30 20			5 10		5									400 3	15 2	250		166		80 (63
100 63 50 90 80 70 60 40 30			5 10		5									400 3	15 2	250		166	, II	80 (63
100 63 50 90 80 70 60 40 30 20			5 10		5									400 3	15 2	250		166		80 (63

Public	Works	Cana	da Environmr	ntal A	&ES	Venus Mine Tailings	Site			HOLE N				
Drille	using	CME	75 track mou	inted ri	ig	V10B located on ber	m at east edge of			ECT NO	: 8054	-12		
with s	olid st	em au	gers			tailings area (see si	te sketch)		ــــــــــــــــــــــــــــــــــــــ	ATION:		,		•
SAMP	LE TYP	PE	TUBE		∠ LOST	X AUGER	BULK					CORE		
BACK	FILL	YPE	BENTONITE	[. PEA G	RAVEL SLOUGH	GROUT			UTTINGS		SAND		·
	س _	INSTRUMENTATION DATA	10 20	QUID m 30	40			20	40	● YAK 00	80		7	ELEVATION(m)
Ξ	SAMPLE TYPE SAMPLE NO	Z.	10 20	ASTIC ▲ 30	40	l SOILS DES	CRIPTION	20	≜ :	SILT A 60	80	ں	SYMBOL	No
DEPTH(m)	빌급	A KEN	10 20						S	AND I		nsc	5	/ATI
E	SAN	STRU TRU	PLASTIC N	1.C.	LIQUID			20	40 ♠ 66	60 EAVEL◆	80	+	SOIL	
	S	<u>z</u>	10 20	30	40			20	40	50	80	SM	bibb	1
0.0						SILTY SAND (tailings)	1					3#		£ 0.0
Ę	∀ 75!	5				 fine grained sand size brown, dry, 	es, loose, light							Ē
1.0	M "	1	l I			Diown, dry,	0.15m	┦						[1.0
Ę		Ì	1			CLAYEY SILT						ML-CI		ŧ
F						-trace gravel, brown,								Ē,
F 2.0						traces of organics, st								∤— -2.0 E
Ē						of oxidation around r indicates oversize (co	• •							ŧ
£ ,,	T5	5	•			Indicates oversize (co	2.4m	1				CL		£_3,
3.0			1	(COBBLE and BOULDER ST	RATUM					GP	44	£ 3.
Ē			ļ	\		-very difficult drilling	(destroyed lead							E
E 4.0	X T5	,				auger)	20	ال						ŧ -4.0
£	M "	'				SILTY CLAY	2.8m							Ę
ŧ				/	ļ	-stiff, damp, grey/light	ht brown, traces					CL		ŧ
E 5.0	≥≤ T5	8		<u> </u>		of organics throughou								-5. 0
Ē							5.2m							E
Ē	∑ 75	9	•)		SILTY CLAY							/ //	ŧ
F 6.0					 	-some gravel, wet, so	tt, possibly water							-6. 0
Ē		-			ļ ļ	bearing stratum,	5.8m	٠						E
7.0						AUGER REFUSAL @ 5.8m	0.0					.]		E 7.0
£						NOTES:								Ė '``
Ē						1	irs between 2.4m and							Ę
E 8.0					ļļļ	2.8m -auger refusal due to	hadrook or havider							E8.0
ŧ						stratum	Deditor of Bodioei							Ē
E						-groundwater encount	ered at					¨}		E
9.0						approximately 5.2 m	(believed confined)							-9. 6
ŧ														Ę
£														E F .a.
F 10.0														10.1 -
Ę												-		Ē
E 11.0														<u>-</u> 11.(
E														E
E												1		
F 12.0														12.0
Ē									<u></u>			.]		
Ē														=
F- 13.0				1 1					. <u>.</u>					13.0
E									ļļ			.	ļ	-
14.0													ļ	-14.0
	[R	Paine 8	ν Δο	isanzi	ates Ltd.	LOGGED BY: MEB			MPLETI			m	
	U	.14.					REVIEWED BY: WCK		CC	MPLETE	: 95/0			- F -
95/07/06 C	9:15AM		willfel	10126	. Yuk	OII	Fig. No: 1					Pa	ge 1	of 1

Public	Wor	ks Co	anac	la Enviro	nmrntal /	A&ES		Venus	Mine T	ailings S	ite			BOREHO	LE NO	: V 7	7		
Drille	d usir	ng Ch	4E 7	5 track	mounted	rig				orth east		er of		PROJEC	T NO:	8054	-12		
with s	solid :	stem	aug	ers						(see site				ELEVAT	ION:				
SAMP		YPE		TUBE		LOST			X AUGI			BULK		SPT			CORE		
BACK		TYP		BENTON		PEA GI	RAVEL	.[∭ SLO	JCH	<u>ن</u> غ	GROUT		ORILL CUT			SAND	1	Т
	HI (SAMPLE NO	2	10	20 30	40		G 0 1	~	D TI C	מזמי	mi () i	20	40	60	80	1	ద	Ξ
DEPTH(m)	SAMPLE TYPE		<u>.</u> ⋖	10	A PLASTIC A 20 30	40		SO.	ILS	DES	CKIP	TION	20	▲ SIL1 40	60	80	nsc	SOIL SYMBOL	ELEVATION(m)
E E			A	PLASTIC	M.C.	LIQUID							20	■ SAN		80) 5	2	\
=	SA					 1				÷			20	♦ GRAV		80	1	S	日日
0.0	X T	10 11	_	10	20 30	<u>40</u>	_f		ained s	and, mo		wn, firm,	20				ML-SN		0.0
E- 1.0	MM	12				>•		bove,		st and b									1
3.0	7	T14					-li	r CLAY ight br lasticit	rown/g	rey, firm	n, moist,	1.3m medium					CL-MI		-2. -3.
4.0																			-4
5.0 1 1 6.0							∬ -d		t drillin	g, wet, g		5.0m					GC		-5.
7.0							AUGE	R REF	USAL @	5.5m		5.5m							-7.
8.0										m dept water at									-8
9.0																			-9.
10.0																			10
11.0																			11 11 11 11 11
12.0																			12 13
14.0																			-14
		J.F	2.	Paine	e & A	ssoci	ate	s Lt	d.		LOGGED	BY: MEB D BY: WCK			PLETIO PLETE:			m	
L					itehors						Fig. No:			00#		33/ U		ge 1	of 1
95/07/06	SS-1541																		

Public	: Wo	orks	Cana	da Environmenta	I A&ES	Venus Mine Taili	ngs Site		BOREHOLE N	10: V8	3		
Drilled	d us	ing	CME :	75 track mounte	d rig	V8 located north	east perimeter of		PROJECT NO	: 8054	-12		
with s	olid	ste	m au	gers		tailings area (se	e site sketch)		ELEVATION:				
SAMP	LE	TYP		TUBE	LOST	X AUGER	BULK	<u> </u>			CORE		
BACK	FILL	_ T`	(PE	BENTONITE	PEA G	RAVEL SLOUGH	GROUT		RILL CUTTINGS		SAND		
	u			■ LIQUID 10 20	30 40			20	● CLAY ● 40 50	80		ایرا	E
E	ΙYΡ	2	N N	A PLASTI	C 🛦	SOILS D	ESCRIPTION		▲ SILT ▲	80	1	SYMBOL	ž
DEPTH(m)	SAMPLE TYPE	SAMPLE NO	WELL INSTALLATION	10 20	30 40	DOIDS B.	300111111011	20	40 60 SAND #	- 00	nsc	λ	ELEVATION(m)
님	A P	YAM.	STA	PLASTIC M.C.	LIQUID			20	40 60	80	-	SOIL	ΕĒ
	S	0,	=		30 40			20	◆ GRAVEL ◆ 40 60	80	<u> </u>	0,	-
0.0	×	11				SILTY SAND		Ť			SM		0.0
Ę	M	T2		\rightarrow		-fine grained sand	l, loose, tailings						Ę
E 1.0				\	\	dry, brown	0.1m	_			CL-MI		E1.0
Ē	M	13				SILTY CLAY	0.1111			•	CL-MI		Ē
ŧ	H						isticity, grey, moist,				1		Ę
E 2.0	\boxtimes	T4 T5					ring (decayed organics)	_			-		-2.0
ŧ	\bowtie	15		1			2.1 m						Ē
E				\		GRAVELLY SILTY CLAY							Ē
3.0				\\		-moist to wet, sof	i, grey, difficult possibly cobbles,				CL-CO		3.0 E
Ē _				\		free water noted							Ē
Ţ		16		l l		1100 4000 110100					7		Ē.,
4.0	\boxtimes			\ \ \				_					E-4.0
Ē	M	17		•		CUTY CLAY	4. 2m				-		Ē
Ė.,						SILTY CLAY	decrease in moisture)						E -50
F- 5.0						soft,	decrease in indistare,						Ę
F											-		Ē
E 6.0	X	18	Œ	A		SILTY CLAY	"-L1 -I1"-"L.				CL-MI		-6.0
ŧ "						-soft, wet, grey, s -LL=25.1, PL=18.5							Ē
E						LL-20.1, 1 E-10.0	, 11-0.0, 11-1.2				1		Ę
E 7.0			-		ļļļ								E-7.0
ŧ	A	19	لللبحالا										Ē
E	M	17					7.6m	\dashv				nuu	F
8.0						END OF HOLE @ 7.6							8. 0
E													Ē
Ē													Ē
9.0						NOTES:					"		9.0
Ē					1		m below ground surface	•					F
10.0						—tailings to 0.1 m	•						E 10.1
F						-standpipe installe	d						Ē ·
Ē													Ē
E 11.0													11.
Ē													Ē.
Ē.													F
12.0											-		-12.0
Ē													Ē
Ė													: :
13.0											1		13.0
Ę											-		-
14.0													<u> –14.0</u>
		Ţ	R	Paine &	Aggnei	ates Itd	LOGGED BY: MEB		COMPLET			m	
		ປ .	16.				REVIEWED BY: WCK		COMPLET	E: 95/0			- L 4
95/07/11 (12.610			mnitenoi	<u>rse. Yuk</u>	OH .	Fig. No: 1				PC	ge 1	or i



	CONSULTING AND I	£211v
SODEEN ANALYSIS		

Sample: T1	De	pth: <u>0</u>	0.	<u>2m </u>		Proie	ct: Ve	nus	Mi	nes	Rec.	Lam	atı	on_				
	ilings Area, '			le V		Made	by: F	.R.		Job N	ا_ :.ov	<u>805</u>	4-1	2				
						Ck'd	by: M.	В.		Date:	_95	/06	/23					
Sieve	Size of Opening					Weight		Tota	ıl Wt	.		Perce	ent		% F	iner	Th	an
No.	MM					tained gm:	s Fi	ner Ti					Than	Ε	asis (
80,000	80.000																	
50,000	50.000																	
20,000	20.000																	
10,000	10.000													<u>.</u>				
5,000_	5.000	<u> </u>									~					0.0		
2,500	2.500															9.6		
2,000	2,000						_									9.4		
1,250	1.250						_									9.1		
800	-800	 														8.5		
630_	-630															7.9		
400	400	-			+											6.3		
315	-315	 					_									5.5		
250	.250	+												-		5.2		
160	•160	+												$-\!\!\!\!+$		7.7		
80	080									l					77	7.6	<u> </u>	
	ample				Metho	od of Prepa	aration			Dry _			Wast	red_	X			
ilty sand,	, SM				Rema	rks grave	3 -	Λ-	Q.									
	~			- 1														
						cand		62°	19-									
		_				sand		62.4									-	
						sand fines		62.4 37.6										
me of Sieving	Min																	
63 5							= .		કિ ——	330	400 3	15 2	50		160	80) 6	3
						fines	= .	37.6	કિ ——	530	400 3	15 25	50		160	80	6	3
00 63 5						fines	= .	37.6	કિ ——	630	400 3	15 25	50 T		160	80	- 6 	3
00 63 5						fines	= .	37.6	કિ ——	530	400 3	15 25	50 T		160	80) 6 T	3
90 63 5						fines	= .	37.6	કિ ——	630	400 3	15 25	50 T		160	80) 6 T	3
90 63 5						fines	= .	37.6	કિ ——	530	400 3	15 29	50 T		160	80) 6 T	3
90 63 5					xxx	fines	= .	37.6	કિ ——	530	400 3	115 29	50 T		160	80) 6	3
00 63 5 90 90 90					XXX	fines	= .	37.6	કિ ——	530	400 3	15 25	50° T		160	80	6	3
63 50					xxx	fines	= .	37.6	કિ ——	330	400 3	115 23	50 T		160	80) 6	3
63 5					000	fines	= .	37.6	કિ ——	530	400 3	115 29	50		160	80	6	3
63 5))	fines	= .	37.6	કિ ——	530	400 3	115 29	50		160	800	6	3
63 50					000	fines	= .	37.6	કિ ——	530	400 3	115 29	50		160	80) 6	3
63 5					XXX	fines	= .	37.6	કિ ——	530	400 3	115 29	550		160	80) 6	3
63 5					000	fines	= .	37.6	કિ ——	530	400 3	115 25	50		160	80	6	3
63 50					XXX	fines	= .	37.6	કિ ——	530	400 3	115 29	50		160	80	1	3
63 50					XXX	fines	= .	37.6	કિ ——	530	400 3	115 23	50		160	80) 6 I	3
63 50))	fines	= .	37.6	કિ ——	530	400 3	115 20	500		160	80) 6	3
63 5					XXX	fines	= .	37.6	કિ ——	530	400 3	115 2:	50		160	80	6	3
63 5					xxx	fines	= .	37.6	કિ ——	530	400 3	115 23	50		160	80	6	3
63 50					xxx	fines	= .	37.6	કિ ——	530	400 3	115 29	50		160	80	6	3
90 63 5						fines	= .	37.6	કિ ——	530	400 3	115 29	50		160	80) 6	3
63 5						fines	= .	37.6	કિ ——	530	400 3	115 23	50		160	80	6	3



CONSULTING AND TESTING ENGINEERS

	ECT	EN11 / C	AA 14	ICC	DEC	TAMA.		- GAXIN	CLIENT Rb	k Works	Connda		CROED
		ENO 2					ION		Ew	rament	A & ES	6-26	-95
TA.	•		S		E TYPE		ЭЕРТН ———	1.3 ~	HOLE NO VE	FIEL	D NO.	LAS NO	73
		GF	RAIN S	317F	ΔΝΙΔΙ	VCIC				· Troco			
	S'SF'NER	1	1				Τ		<u> </u>	ETROGRA	APHIC AN	IALYSIS	
SIEVE SIZE	BY WEISHT	SIEVE	% FINER BY WEIGHT	İ	DIA.	% FINER BY WEIGHT	DIA.	FINER BY WEIGHT	MATER	RIAL TYPE		% OF TOTAL	. SAMPL
63	93.6]	.0103	93.06	1	T	SAND			6.0	
	 	!	ļ	1		89.09		1	SILT			20.0	
	 	ļ	!	-		88.50	!	!	CLAY			74.0	
	 	:	<u> </u>	┨ ・		\$5.14	! 	1					
	 	:] 		79.25	1	!					
	1	İ	 	i		64.35				-			
	j	ı]		1		\vdash					
₩ ₽. E	- 1	UNIFIED ASSIFICA		L	. P.L	P.1.	LITTE	¥ 5.5.	PAI	פדורו ב פ	HADE A	NALYSIS	
-3	SILT	/ CL	ΔΥ	i		- 	133		POUND		DIAFE A	IVACI 3IS	
					1		1	+	SUB-ROUND				-
						 	1	1	ANGULAR				
									SUB-ANGLAR				
		С	RUSH C	CUNT		%			FLATS		i		
		J		····			•		MEEDLES				
	100	CLAY	 		SILT			FINE	SAND			RAVEL	
									ME DIUM	COARSE	FINE	COARSE	ml
	90												
		1	1			1 1 1]
	76								 				#
	¥ 60								1 [[1 1 1 1	1 1 1 1	1 1 1 1 1 1 1		N 1 1 1
	\$	i					++i!		+	!		-	
	CCNT PASSOU												
	= 30												
	PERCENT												
	70 27 40												
	20 20												
	20 20	001			.010			JOO SERVICE	1.000		10.000		1000
	20 20 20 20	Y'S RE			VE A		15 \	TON 2	E-MILLIMETRES		10.000		1000
	20 20 20 20	Y'S RE			VE A	NALYS D-SUN	15 \	TON 2	E-MILLIMETRES	CATE SAM	PLED		10000
	20 20 20 20	Y'S RE			VE A		15 \	TON 2	E-MILLIMETRES	CATE SAM	PLED		10000

Public	Wo	rks	Canac	da Enviro	onmrntal A	A&ES	Venus Mine Tailings	Site		DREHOLE NO				
Drilled	us	ing (CME 7	5 track	mounted	rig	V9 located just sout			ROJECT NO:	8054-	12		
with s	olid	ste	n aug	gers			within tailings area			EVATION:				
SAMP	LE.	TYPE		TUBE		LOST		BULK	∭ SPī			CORE		
BACK			PE	BENTO		PEA GR	AVEL SLOUGH	GROUT	DRIL	L CUTTINGS ● CLAY ●		SANU	\neg	
	بر	0	INSTRUMENTATION DATA	10	20 30	40		COLOMICAL	20	40 60 ▲ SILT ▲	80		ద	ELEVATION(m)
$ \mathbf{E} $	Σ	ž	N A	10	A PLASTIC 4 20 30	40	SOILS DES	CRIPTION	20	40 60	80	nsc	SYMBOL	S
DEPTH(m)	SAMPLE TYPE	4	UME Dat	PLASTIC	M.C.	LIQUID			20	■ SAND ■ 40 60	80	>	SOILS	.VA
=	SAM	SA	ISTR	-						♦ GRAVEL ♦	•^	•	S	급
- 0.0	++		=	10	20 30	40	SANDY SILT		20	40 60	80		***	- 0.0
Ē	\times	T26					-wet, fine grained sa	nd, brown and rust					##	Ē
Ė	\blacksquare	T27				\	(oxidation) in colour,		♦■		Δ		***	E 1.0
F 1.0							0.1 m, non-plastic SANDY SILT						****	Ē
Ē						1	-higher sand content	at 1.2 m						Ē
E 2.0							3							-2.0
Ė						{						ML-SN		Ė
E		T28												-3.0
F 3.0		120			1								***	E-3.0
Ē					ļļļļ.	\								E
4.0					ļļļļļ.	1							***	-4.0
Ē	\boxtimes	T31				•							****	Ē
Ē	X	T29						4.5						ŧ
5.0							DECAYED ORGANICS	availad austana				PT		-5.0 E
Ē							-black, maist, previou	5.4m					77	Ę
6.0						ľ	SILTY CLAY	V.						£-6.0
F							-stiff to hard, moist,							£ }
Ē	\triangleright	T32				•	_plasticity, traces_of <	oxidation, grey 6.6M	-	A •		CL		Ę
7.0				ļ			SILTY CLAY	0.0M						[7.0
E	X	T33			4		-some gravel, moist,]					ŧ
Ē.,							mm diameter, traces							-8.0
E 8.0							L=23.1, PL=19.0, F	7=4.1, L1=-0.32 7.6m						E
Ē							END OF HOLE @ 7.6m	7,4,11						Ē
9.0				ļii			NOTEC.							-9.0
Ē	-	l					NOTES: —tailings to 4.5 m							E
Ē							ionings to he in							10.0
F 10.0												Ì		F 10.5
Ė														Ē
E 11.0										_ _ _ _				11.0
E														E
E														Ē
12.0														-12.0 E
E														Ē
13.0														E-13.0
£														E
Ē.														Ē
14.0	1	<u> </u>	<u> </u>	D .			TI1	LOGGED BY: MEB		COMPLETI	ON DEP	TH: 7.	6 m	F -14.0
		J	.K.				ates Ltd.	REVIEWED BY: WCK		COMPLETE		6/14		
95/07/05	00.47	417		W	<u>hitehor</u>	<u>se. Yuk</u>	on	Fig. No: 1				Po	ige 1	of 1



	% Finer Than sis Orig. Samp 100.0 99.8 99.7 99.6 99.4 99.0 98.1
Sieve Size of Opening Weight Total Wt. Percent Finer Than gms Finer Than Ba	100.0 99.8 99.7 99.6 99.0 98.1 94.1
Sieve No. MM Retained gms Finer Than gms Finer Than Ba	100.0 99.8 99.7 99.6 99.0 98.1 94.1
No. MM	100.0 99.8 99.7 99.6 99.0 98.1 94.1
80,000 80,000 50	100.0 99.8 99.7 99.6 99.4 99.0 98.1
50,000 50,000 20,000 10,000 10,000 5,000 2,500 2,500 2,500 2,000 2,000	99.8 99.7 99.6 99.4 99.0 98.1 94.1
50,000 50,000 20,000 10,000 10,000 5,000 2,500 2,500 2,500 2,000 2,000	99.8 99.7 99.6 99.4 99.0 98.1 94.1
20,000	99.8 99.7 99.6 99.4 99.0 98.1 94.1
10,000	99.8 99.7 99.6 99.4 99.0 98.1 94.1
5,000 5,000 2,500 2,500 2,000 2,000 1,250 1,250 800 800 630 630 400 400 315 315 259 259 160 160 80 080 Description of Sample silt , trace sand, ML Time of Sieving Min. Method of Preparation Dry Washed Remarks gravel = 0 % sand = 5,9% fines =94.1%	99.8 99.7 99.6 99.4 99.0 98.1 94.1
2,500	99.8 99.7 99.6 99.4 99.0 98.1 94.1
2,000 2.000 1,250 1.250 800 800 630 630 400 400 315 315 250 250 160 160 80 080 Description of Sample silt	99.8 99.7 99.6 99.4 99.0 98.1 94.1
1,250	99.8 99.7 99.6 99.4 99.0 98.1 94.1
800 800 630 630	99.8 99.7 99.6 99.4 99.0 98.1 94.1
A	99.7 99.6 99.4 99.0 98.1 94.1
400	99.6 99.4 99.0 98.1 94.1
315 315 250 250 160 160 80	99.4 99.0 98.1 94.1
250	99.0 98.1 94.1
160	98.1 94.1
Nethod of Preparation Dry Washed Nethod of Preparation Dry Nethod of Preparation Dry Nethod of Preparation Dry Nethod of Preparation Dry Nethod of Preparation Dry Nethod of Preparation Dry Nethod of Preparation Dry N	94.1
Remarks	
Remarks	ζ
Sand = 5.98	
Time of Sieving Min	
Time of Sieving Min	
100 63 50 40 25 20 16 14 12.5 10 5000 2000 1250 800 630 400 315 250 16 90 80	
90 80	
90 80	
80	0 80 63
80	
70	
70	-++
_	
60	
50	
50	
30	1 1
20	
10	
100 10 Grain Size - mm 1.0	



CONSULTING AND TESTING ENGINEERS

FOJE		VENU	S M	INES	REC		ATION		CLIENT		. Works				6-20	etoroe! 6 - 95
TA.	•		5	AMPI.	E TYPE		DEPTH	5.9 m	HOLE NO		FIEL				LAB NO	T 32
	·	GF	RAIN S	SIZE	ANAI	YSIS		.		ΡĖ	TROGR	API	4IC	ANALYS		
SIZE	SETHER BY WEIGHT	SIEVE	% FINER BY WEIGHT		DIA.	% FINEA 8Y WEIGHT	DIA.	FINER 8Y WEIGHT	V	ATERIA	AL TYPE			% 0	OF TOTAL	SAMPL
	1				,0192 .0137	39.99	1,0012	52,47	SANT						0.0 35,0	
	i	<u> </u>				98.01	<u> </u>		CIV.	<u></u>					65.0	
		i I]	.0037	91.08 84.15 75.24	1	<u> </u> 							 	
₩ ~ _£ NO.		· UNIFIES ASSIFICA		<u> </u>	T	65.34	- Junion	¥ 55.								
32 32	·	Y CL					132		POUND	PAR	TICLE	SHA	APE	ANALY	rsis	
									SUB-ROUND ANGULAR							
	1			!		!	_l		SUB-ANGLA	R						
		C	RUSH C	OUNT		°	%		FLATS MEEDLES							
	100	CLAY			SILT			FINE	SAND	/W	COARSE	-	FINE	GRAVEL	COARSE	
	•0															
	•0									•						
	70										!		$\frac{1}{1}$			
	PASSIU	/														
	40	 								ļ						
		- ;		$\Pi \Pi$	1			11-		 	! 	#	\coprod			511 1
٠	30	ļ								1	i			ij		
٠	30 20															
	, ic.															
	20 . IC	001			.010			JOO TRANS	ZF - MILLIMETAES	1.000			**	0.000		
LA3-	20 , ic o	Y'S RE			VE A			77 NO	77 - MILLIMETARS	(CAYE SAN		Ð .			100.0
L A 3: —	20 , ic o	Y'S RE			VE A		51S W/D SANC	77 NO	ZF - MILLIMETARS	(DATE REC	EIV	ED _		T.D.	1000

Public	: Wc	orks	Cana	da Environmental	A&ES	Venus Mine Tailings	Site		BOREHOLE NO				
Drille	l us	ing	CME 7	5 track mounted	rig	V10A located on acc	cess road east of		PROJECT NO:	8054	-12		
with s	olid	ste	m ou	gers		tailings area			ELEVATION:				
SAMP	LE	TYP		TUBE	LOST	X AUGER	BULK	∭ SI			CORE		
BACK	FILL	_ T	PE	BENTONITE	PEA G	RAVEL III SLOUGH	GROUT	DI	RILL CUTTINGS		SAND		
	ш		NO	■ LIQUID ■ 10 20 30				20	● CLAY ● 40 50	80		7	(F)
DEPTH(m)	SAMPLE TYPE	2	INSTRUMENTATION DATA	A PLASTIC	A	SOILS DES	CRIPTION		▲ SILT ▲	80	1,	SOIL SYMBOL	ELEVATION(m)
Ĕ	ш	PLE	MEN	10 20 30		DOIDS DIE	OIVII IIOI	20	40 60 SAND	00	USC	Σ	A E
님	A M	NA.	E C	PLASTIC M.C.	LIQUID			20	40 60	80	4	등	
	S	0,	≅	10 20 30	40			20	♦ GRAVEL ♦ 40 50	80		0,	1
0.0	X	T53		•		GRAVELLY SILTY SAND						***	0.0
ŧ				- -		-dense, dry, brown, d							E
1.0						auger action indicates					SM		E-1.
£ ""			·			possibly boulders thro	oughout, possibly						E
E	X	T54				-rock chips found wit	hin auger cuttings					****	ŧ
E 2.0		157				(from bedrock or box							E2.6
E			·				1.8m						E
ŧ						AUGER REFUSAL @ 1.8 n	n						Ė
= 3.0						NOTES					-		-3.0
ŧ						NOTES: -no groundwater enco	untarad						Ē
Ę						-test hole V10A locate							Ė
4.0						outcrop and thus ref					1		-4.0
E						be due to bedrock	•						E
ŧ						-move drill rig 5 m n							F
F 5.0						V10B to determine re	fusal depth				1		-5. (
F													Ē
Ē.,													Ē.,
F 6.0													-6.0
E													E
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95/07/06 0	0.4944	,		Whitehors	se, ruk	OII	Fig. No: 1				Pa	ge 1	01 1

Drilled using CME 75 track mounted rig V10B located on access road east of PROJECT NO: 80 with solid stem augers tailings area ELEVATION: SAMPLE TYPE TUBE LOST AUGER BULK SPT	54-12 CORE	
SAMPLE TYPE TUBE LOST AUGER BULK SPT	CORE	
DAMILL III	COKE	
	SAND	
BACKFILL TIPE BEHINNIE TEX SHAVE	SANU	Т Т
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C C C C C C C C C C	- OSC	SOIL SYMBOL ELEVATION(m)
E SAND ■ 20 40 60 80	Š	S
→ GRAVEL →		8 표
0.0 SILTY SAND		- 0.0
-some gravel, dense, dry, brown,		
E auger action indicates cobbles and		-1.0
possibly boulders throughout, possibly		
road fill material	SM	
		-2.0
2.8m		-3.0
AUGER REFUSAL © 2.8 m		
NOTES: -no groundwater encountered		E
-auger refusal at similar elevation as		-4.0
In V10A, assumed bedrock presence		<u> </u>
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J.R. Paine & Associates Ltd. LOGGED BY: MEB COMPLETION REVIEWED BY: WCK COMPLETE: 9:		.8 m
Whitehorse, Yukon Fig. No: 1		age 1 of 1

With bodd using CME 75 track mounted rig	Public	Worl	ks C	anad	la Envira	onmrntal A	&ES	Venus Mine Tailings	Site		BOREHOLE NO				
CLAYE SIT -1.06 CLAY												8054-1	12		
SAMPLE TYPE USE								adjacent to road (s	ite sketch)			- (4)			
							LOST	AUGER							
10 20 30 40 40 40 40 40 40 4					BENTO	NITE	PEA GR	RAVEL IIII SLOUGH	GROUT			<u> </u>	AND		
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CLAYEY SILT -trace gravel, non-plastic, biege with light grey pockets, traces of oxidation around gravel, damp, firm CLAYEY SILT -trace gravel, grey, layering, moist, firm, black decayed organic seems, medium plasticity, cloy pockets within silt, LL=36.7 Pl=261. Pl=10.6, LL=0.1 -5.0 T65 BOULDER LAYER -very difficult drilling 3.9m CLAYEY SILT -trace gravel, vayering, oxidation around gravel, wet, soft, medium plasticity, cloy pockets within silt -becomes very wet and soft at 4.9m CL-ML -5.0 GRAVELLY SILT -some sond, moist to wet, brown/grey, auger action indicates oversize material starts of 8.8m 9.1m END OF HOLE @ 9.1m NOTES: -standplope installed to 7.0 m below gravel gravel and soft at 4.9m J.R. Paine & Associates Ltd. Whitehorse, Yukon Fig. No. 1 Fig. No. 1 Foge 1 of 1 -1.0 CL-ML -2.0 -1.0 CL-ML -2.0 -2.0 -3.0 -3.0 CLAYEY SILT -1.2m	E 0.0	⊠ ī	62	11		7		GRASS COVER, ORGANIC	RICH SUIL	الـ					£
-1.0 -1	E		F	1 B		1		CLAYEY SILT	0,03111				ML-CL		<u> </u>
around gravel, damp, firm 1.2m CLAYEY SILT -3.0 Total planting plasticity, clay pockets within silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -4.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -5.0 CLAYEY SILT -4.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -5.0 CLAYEY SILT -4.0 CLAYEY SILT -4.0 CLAYEY SILT -5.0 CLAYEY SILT -6.0 Total plasticity, clay pockets within silt -becomes very wet and soft of 4.9m -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6, L=0.1 -6.0 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.7, PL=26.1, PL=10.6 End with a silt, LL=6.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with a silt, LL=6.7, PL=26.1 End with	1.0		ţ	18		\		-trace gravel, non-p							1—-1.0 E
CLAYEY SILT -trace gravel, grey, layering, moist, firm, black decayed organic seems, medium plasticity, clay pockets within sill, LL=36.7, PL=26.1, Pl=10.6, Ll=0.1 2.7m BOULDER LAYER -very difficult drilling 3.9m CLAYEY SILT -trace gravel, layering, oxidation cround gravel, wet, soft, medium plasticity, clop pockets within sill -becomes very wet and soft at 4.9m 60 GRAVELLY SILT -some sand, moist to wet, brown/grey, ouger action indicates oversize material starts at 8.8m 9.1m END OF HOLE © 9.1m NOTES: -standpipe installed to 7.0 m below ground surface -boulder stratum cocurs between 2.7m and 3.9m -water stratum may occur at depths below 4.0 m J.R. Paine & Associates Ltd. LOGGED BY: MEB COMPLETION DEPTH: 9.0 m	E		-	<i>a 1</i> 0											Ē
CLAYEY SILT -1.0 Tess Tess CLAYEY SILT -1.0 Stock decayed organic seems, medium plasticity, clay pockets within silt, IL-35.7, PI=26.1, PI=10.6, IL=0.1 BOULDER LAYER -2.7m BOULDER LAYER -2.7m BOULDER LAYER -2.7m BOULDER LAYER -2.7m BOULDER LAYER -2.7m -3.9m CLAYEY SILT -3.9m CLAYEY SILT -4.0 -5.0 -5.0 -6.0 Tess GRAVELLY SILT -3.0 -6.0 Tess GRAVELLY SILT -3.0 -3.0 GRAVELLY SILT -3.0 -	Ē		ţ	18		1		around gravel, dam					CL-ML		E -2.0
- 17.0 -	E 2.0		F	<i>a</i> 19				CLAYFY SILT	1.203						ŧ
firm, black decayed organic seems, medium plasticity, clay pockets within sith, LI=35.7, PI=26.1, PI=10.6, LI=0.1 5.0 164 BOULDER LAYER	Ē	Ų,	63	10			•	i e	layering, moist,					W	ŧ
medium plasticity, clay pockets within sith. LI=36.7, Pt=28.1, Pt=10.6, Lt=0.1 2.7m BOULDER LAYER very difficult drilling 5.0 CLAYEY SILT -trace gravel, layering, oxtdation cround gravel, wet, soft, medium plasticity, clay pockets within sith -becomes very wet and soft at 4.9m 7.0 GRAYELLY SILT -some sand, moist to wet, brown/grey, auger action indicates oversize material starts at 8.8m 9.1m END OF HOLE @ 9.1m NOTES: -standpips installed to 7.0 m below grounds surface -boulder stratum may occur at depths below 4.0 m J.R. Paine & Associates Ltd. Whitehorse, Yukon Fig. No: 1 Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1 Page 1 of 1	E	\Box		10				firm, black decayed	organic seems,	1				444	-3.0
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BOULDER LAYER -s.0 Total To	Ė			11				sill, LL=56./, PL=26		7				44	Ė
-very difficult drilling CLAYEY SILT -trace gravel, layering, oxidation around grovel, wet, soft, medium plasticity, clop pockets within silt -becomes very wet and soft at 4.9m 7.0 8.2m GRAVELLY SILT -some sand, moist to wet, brown/grey, augre action indicates oversize material starts at 8.8m 9.1m END OF HOLE @ 9.1m NOIES: -standpipe installed to 7.0 m below ground surface -boulder stratum occurs between 2.7m and 3.9m -water stratum may occur at depths below 4.0 m J.R. Paine & Associates Ltd. LOGGED BY: MEB COMPLETION DEPTH: 9.0 m COMPLETE: 955/05/21	4.0	IJ.	, <u>,</u>	16				BOULDER LAYER	2.711					W	∓-4.0 ₹
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8.2m Second Seco	Ę				/	/								1	£
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J.R. Paine & Associates Ltd. Whitehorse, Yukon J.R. Page 1 of 1	E 12.0							1	occur at depths below						£ '2'
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5/07/11 \$2.55PM	S / 2 / 2 / 2	AS EXIS			W)	<u>nitehors</u>	<u>e, Yuk</u>	ron	Fig. No: 1				Po	2ge 1	1 of 1



CONSULTING AND TESTING ENGINEERS

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Public	Worl	rs Can	nada Envi	ronmrı	ntal A	&ES	Venus Mine Tailings S	ite		BOREHOLE				
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with se		<u> </u>					adjacent to road (site		L	ELEVATION:		000-		
SAMPL			TUBE			∠ LOST		BULK	∭ \$			CORE		
BACK	FILL	TYPE	BENT	ONITE		PEA GR	RAVEL SLOUGH	GROUT		ORILL CUTTING	s 🔯	SAND	 1	r
	سا	No	10		QUID =	40			20	● CLAY ● 40 50	80	1	ಕ	E
Έ		SAMPLE NO INSTRUMENTATION		▲ PU	ASTIC A		SOILS DESC	CRIPTION	20	▲ SILT ▲ 40 60	80	ا ن	SYMBOL	ELEVATION(m)
DEPTH(m)			Y 10		<u>30</u> _			-		E SAND		USC	S	/ATI
H	SAMPLE	SAMPLE	PLASTIC	, \\	1.C.	LIQUID			20	40 50 ◆ GRAVEL ◆	80	-	SOIL	E.E.
i l	S	INS	10	20	30	40		1011 2011	20		80	PT	777	- 0.0
0.0	-						GRASS COVER, ORGANIC R	RICH SOIL 0.05m	1				瞇	£
Ę							CLAYEY SILT	mcu.u				ML-CL	瞇	Ę
E 1.0							-trace gravel, non-plas					1	HH	₹-1.0 ₹
E					<u>.</u>		light grey pockets, trac	ces of axidation	.			-	1//	ŧ
E							around gravel, damp,							£ -2.0
2.0							CLAYEY SILT	1.2m				CL	1//	£ -/.
E							CLAYEY SILI —trace gravel, grey, lay	rering, moist.						Ŧ
3.0							firm, black decayed or						14	-3.0
E 3.0							low plasticity					GP	144	¥.
Ė							BOULDER LAYER	3.0m	4				44.	ŧ
4.0							BOULDER LAYER -very difficult drilling							-4.
Ē			ļi.					3.7m	-				1//	£
Ę							CLAYET SILT							ŧ.
- 5.0 E							-trace gravel, layering,						1//	75. (
Ę							around gravel, wet, so plasticity	лі, meaium				1		ŧ
<u>E</u>							plasticity -becomes very wet and	1 soft at 4.9m				. CL	1//	£-6.
E 6.0							wei uit							Ŧ "
Ę							1						1//	‡
7.0				_		,								£-7.
Ē														£
Ė														Ŧ
8.0									4				14	[-8. 6
Ē							COAUTILY CUT	8.2m				GC	2	\$
Ē ,.							GRAVELLY SILT -some sand, moist to	wet_brown/grey				الا		¥ -9.0
F- 9.0 F							auger action indicates						لمعت	ŧ "
Ę							material starts at 8.8n	m				1		Ē
10.0								9.1m				-		E-10.
E							AUGER REFUSAL @ 9.1m NOTES:							Ę
Ē							NOTES: -boulder stratum occur	rs between 3.0m and						Ē
11.0							3.7m					1		E-11.
Ė							-water stratum may oc	ccur at depths below						Ę
ŧ							4.0 m	1 Am asult OF						E-12.
F 12.0							—test hole V11B located east of THV11A	u 4m south, U.5m						E
Ę							-two test holes were di	rilled 4m E, 5m S				-		Ē
13.0							of V11, however auger	r refusal occurred						13.
E							at boulder layer (3.7m							E
E													1	E -14.
F 14.0		1 -	<u>ъ.</u>		0		- T 1 1	LOGGED BY: MEB		COMPLE	ETION DEP	γTH: 9.	8 m	<u>14.1</u>
		J.R					iates Ltd.	REVIEWED BY: WCK			ETE: 95/0	06/21		
AF /A=	W		W	hite	<u>hors</u>	<u>se. Yuk</u>	on	Fig. No: 1				Po	age 1	1 of 1
\$5/07/11	JZ:49Ph.	•												

Public	Wo	rks	Canad	da Enviro	onmrntal	A&ES		Venus Mine Tailings S	ite				0: V			
Drilled	us	ing	CME 7	5 track	mounted	rig		V12 located east of t	ailings-				: 8054	-12		
with s	olid	ste	ท อนรุ	gers				adjacent to road (site	sketch)			ATION:				
SAMP	LE	TYPE		TUBE		<u> </u>	OST	AUGER	BULK	<u></u>		-		CORE		
BACK	FILL	_ <u>T</u>	PE	BENTO			EA GF	AVEL SLOUGH	GROUT			UTTINGS		SAND		1
	ш		NOI	10	## LIQUID ## 20 30	40)			20	40	LAY • 50	80		9	E
DEPTH(m)	SAMPLE TYPI	SAMPLE NO	NSTRUMENTATION DATA	10	▲ PLASTIC 2			SOILS DES	CRIPTION	20	▲ 5	SILT A 60	80	ں	SOIL SYMBOL	ELEVATION(m)
E	밁	<u>a</u>	JME) DAT,	DI ACTIC							m S	AND =		nsc	S	ATI
	AM	SAN	STRL	PLASTIC	M.C.	Li	QUID			20	40 €8	60 AVEL.♦	80	-	SS	15
1	S		N.	10	20 30	40	'			20	40	60	80	<u> </u>	1	- 0.0
0.0	×	T 6 7			•			SILT	, ,,	,				ML	Ш	£ 0.0
Ę								-some gravel, road sur traces of oxidation are								ŧ
E 1.0								Indices of oxidation un	0.3m	-						F-1.0
ŧ								SILTY CLAY								ŧ.
Ē					1	****		-trace gravel, medium	plasticity, maist,							Œ
2.0			•					firm, oxidation around	rocks							‡−2.0
Ē														CL-M	4111	ŧ
E																<u> </u>
F 3.0	X	T68														[-3.0
E	M															#
Ē					\											ŧ
E 4.0					1				4.1m					"[}−4.0
Ę	X	T69			} → ■			-becomes wet, soft at -sample T69, LL=22.7,								ŧ
Ē								L=0.4	1 1 - 1 3 (4) 1 1 - 7 . 3							£.,
5.0																-5.0
E	X	T70			?			-becomes very soft at	5.2m					CL		ŧ
£																₽ -6.0
E 6.0					1											F-8.0
ŧ					ļ											‡
7.0									6.7m					GC		<u>₹</u> _7.0
£ /**	M	171		•				CLAYEY GRAVEL						CL		‡
E	×	T72			•			-auger action indicates		I				GC		ŧ
8.0	V	T73						possibly oversize mate	<u>rial</u> 7.0m	4				المال		ኍ Έ8.0
E	M	173						GRAVELLY CLAY	/.um						SKY	Ē
ŧ								-grey, soft, wet (free v	rater), medium		1	1 1		1		E
E 9.0								plasticity								E-9.0
ŧ									7.3m							È
E								CLAYEY GRAVEL								E
10.0	$\mid \cdot \mid$:						-difficult drilling indica			ļ <u></u>					10.0
Ę		İ						material, wet, soft cla	8.2m	_	ļ	ļļ				E
E								AUGER REFUSAL @ 8.2m	0.211							Ē
F 11.0								NOTES:						1		-11.0
Ē								-free water may occur	at depths of 4.5					.		Ē
£								metres and greater								ŧ
12.0								-at completion, water 1								-12.0 E
ŧ l		ĺ	İ					3.6 m in hole (appear aquifer)	s to be contined		<u> </u>	-	_	1		E
13.0								uquiter)						1		E A
ŧ '`.'			ĺ								1]		13.0 -
											ļļ			}		Ē
14.0																-140
		J	R	Paine	e & A	SSC)cia	ates Ltd.	LOGGED BY: MEB	_			ON DEP		2 m	
			_ ••		itehors				REVIEWED BY: WCK		CO	MPLETI	: 95/0		- ·	a.f. 1
					LUCITUI	oc. i	unt	711	Fig. No: 1		- 1			FQ	ige 1	0 ∤

Public	: Wc	orks	Cana	da Environmenta	I A&ES	Venus Mine Tailings S	Site		HOLE NO: V13			
				75 track mounte	d rig	V13A located on sout	heast area of berm		ECT NO: 8054-1	2		
with s				<u> </u>		(see site sketch)			ATION:	ORE		
SAMP				TUBE	LOST	AUGER	BULK	SPT DRILL C		AND		
BACK	FILL			BENTONITE	PEA GI	AVEL SLOUGH	GROUT		AAY ●	ANU		
	TYPE	0	NOIL	10 20	30 40		aninmiali	20 40	50 80 SILT ▲		忌	(m)
Ē	<u>T</u>	N.	Y Y	▲ PLASTI 10 20	C ▲ 30 40	SOILS DES	CRIPTION	20 40	60 80	nsc	X	NO!
DEPTH(m)	SAMPLE	SAMPLE NO	INSTRUMENTATION DATA	PLASTIC M.C.	LIQUID			20 40	AND 188 60 80	D	SOIL SYMBOL	ELEVATION(m)
0	SA	3	NST	40 00				♦ 69	RAVEL ♦ 80 80		8	ᆵ
0.0		T60	<u>-</u>	10 20	30 40	SAND		1 20 40	W 03	SM	Ш	0.0
Ē		100				-fine grained, loose, d	ry, light brown,					=
1.0						tailings	0.1]		ML		-1.0
E	\forall	T61				CLAYEY SILT	0.1 m					=
E						-trace gravel, damp, f	irm, traces of				Ш	=
2.0						oxidation around grav	el					-2.0
Ę					ļļ ļļ	 -auger action indicates bedrock - difficult dri 						
Ē.,						Dedrock - difficult of	1.6m	4				
3.0						AUGER REFUSAL @ 1.6m						= "
Ē												
E 4.0												-4.0
Ē												-
Ē												
F 5.0						NOTES:						 -5.0
E						-attempted to drill and						=
6.0						(V13B) 5 m north of v -similar soil profile in	VI 3A VI 3R as VI 3A					-6.0
Ē						with refusal at 1.6 m	1100 43 110A				ŀ	=
E												
F 7.0												-7.0
Ē											į	
8.0												
E												
E												=
E 9.0												-9 .0
Ē											Į	
10.0					ļ. ļ. ļ. ļ					İ		10.0
E											F	
Ē											F	
11.0											F	11.0
Ē											Ē	
12.0											Ē	<u> </u>
£											Ē	
Ę		ļ									Ē	
13.0											Ė	13.0
Ė											Ē	
14.0											E	-14.0
		J	R.	Paine &	Associ	ates Itd	LOGGED BY: MEB		OMPLETION DEPTH		m	\Box
		J .			rse. Yuk		REVIEWED BY: WCK Fig. No: 1	C	OMPLETE: 95/06,		ge 1	of 1
95/07/06	20.044			minicilo	LOC, LUM	J11	priga HO. I				, ·	ž: i

Public	Wor	ks C	anac	la Envir	onmr	ital A	&ES		Venus Mine Tailings	Site		1	EHOLE				
Drilled	usir	ng C	ME 7	5 track	mour	nted	rig		V14 located on acce	ss road east of		PRO.	JECT N	D: 8054	-12		
with s	olid	sterr	ouç	ers					tailings area			<u> </u>	VATION:				
SAMP	LE T	YPE		TUBE			Z LOST		AUGER	BULK					CORE		
BACK	FILL	TY	PE	BENTO	NITE		·. PEA G	RAVEL	∭ SLOUGH	GROUT			CUTTING	S ::	SAND		
	u		5	10	■ LIQ 20	UID a	40				20		CLAY ● 50	80		=	E
(E)	TYPE	2	₹ .		A PLA	STIC A		1	SOILS DES	CRIPTION	20		SILT A	80	٦.,	¥₩	Ž
DEPTH(m)			A E	10	20	30	40	1	SOIDS BIS		70		SAND =		USC	\	AŢ
3	SAMPLE	SAMPLE	INSTRUMENTATION DATA	PLASTIC	M.	.C.	LIQUID				20) 60 GRAVEL ♦	80	-	SOIL SYMBOL	ELEVATION(m)
1	S		ž	10	20	30	40				20			80		1	- 0.0
0.0									VELLY CLAYEY SILT	. 1 1* .					ML		E 0.5
Ē									trace sand, brown, doossibly cobbles, fine		,						Ē
- 1.0					ļļ	ļ <u>.</u>			izes, firm	gramed sand	1				ML-C	. 1111	-1.0
Ē					įį					0.9m					mr. C		‡
Ē									YEY SILT						GP	4.4	<u> </u>
F 2.0		1							trace sand, easier di	rilling, grey/light						44.4	ı
E					<u> </u>	ļ <u>ļ</u>		.}	orown, firm, damp	1.5m							Ė
3.0								COB	BLES and BOULDERS								E -3.0
£									difficult drilling								Ē
ŧ								1110	ED DEFLICAL & 2.1 -	2.1 m							Ē
E- 4.0					ļļ	ļ <u>.</u>		NOT	ER REFUSAL @ 2.1 n	1							-4.0
Ē					ļļ				exposed bedrock app	proximately 25 m	,			ļļļ.			Ē
Ē.									orth of Test Hole V1								Ē.,
E 5.0					1												-5.0
Ē					<u> </u>	ļ <u>‡</u>											Ē
E 6.0					<u></u>	ļ								ļļ			-6.0
E																	E
Ē																	E
7.0		ĺ						-									-7.0
Ę					įį									ļļļ.			Ē
Ē.,																	
F 8.0								1									E -0.0
Ē																	Ē
E 9.0		İ												ļļļ.			E-9.0
Ē																	Ē
Ē																	Ē
10.0																	-10.0
Ē					ļļ												Ē
11.0			Ì														E11.0
F																	E '''
E																	Ē
12.0							ļļ										12.0
Ė																	Ē
E																	Ē
13.0						·											13.0
E							<u> </u>										Ė
14.0						_		L									-14.0
]]	?	Pain	م ک	, Δ	ggnei	ate	s Ltd.	LOGGED BY: MEB			COMPLET			1 m	
		J . J	•						ы ши.	REVIEWED BY: WC	K	C	COMPLET	E: 95/		700 1	of 1
95/07/06 C	9:05AM			11	Hre!!	ULS	<u>e, Yuk</u>	OII		Fig. No: 1					P(ige 1	or I

Public	Wor	ks Ca	nada i	nviro	mrni	al A	&ES		Venus Mine To	ailings S	ite			REHOLE				
Drilled	usir	ng CMI	75 t	rack r	nount	ed r	rig		V15 located o	n acces	s road east of			JECT N		4-12		
with s	olid	stem	augers						tailings area					VATION:				
SAMP	ET	YPE	T	UBE		[LOST		X AUGE	R	BULK		SPT		-	CORE		
BACK	ILL	TYPE	B	ENTON	TE		PEA G	RAVEL	∭ SLOU	CH	GROUT			CUTTING	S E	SAND)	
	w	_ 8			ELIQU 20	1D = 30	40					2	0 4	CLAY ● 0 60	80		占	Ê
E	TYPE	SAMPLE NO INSTRUMENTATION	_		PLAS	TIC 🔺		1	SOILS :	DES(CRIPTION	,	0 4	SILT A	80	ں ا	SOIL SYMBOL	ELEVATION(m)
DEPTH(m)			Y DA	10	20	30	40	1						SAND I		SS	L S	/ATI
19	SAMPLE		_ PU	ISTIC	M.C). 		1				2	0 4	0 60 GRAVEL◆	80	\dashv	SO	13
	S	¥ ≅		10	20	360	40							0 60	80		rer	- 0.0
0.0									'EY SILT		1							F 0.0
Ē									ome sand, tir rown, firm, lo		ed sand sizes,							E
1.0							ļļ	Di	rown, mim, io	w piusii	City,							-1.0
ŧ						:												Ē
Ę																10		£
E 2.0								1								ML		1—-2.0 E
ŧ								ļ					ļļ					ŧ
£																		E_30
E 3.0								1										‡ "
Ē		-																<u> </u>
E 4.0											3.9n						XXX	E4.0
Ē								GRAV	/ELLY SILT and	d CLAY	3 ,31	''				ML-		ŧ
ŧ	Ø١	73			•				noist, firm, a		lion indicates	1						Ę
E 5.0								p	resence of ov	ersize n	naterial							-5.0
E						<u></u>		CUT	. OL 1V		4. 5n	n			<u> </u>			ŧ
ŧ								1	CLAY	ol wol	soft, axidation							Ē.,
F-60									round gravel,		Sori, Uxidalion							E-6.0
Ē									,					ļ <u>.</u>	-			Ė
7.0															<u></u>			E 7.0
F'"																		Ē
E		1																E
8.0						<u>ļ</u>	ļļļ	-				ļ <u>i</u>				CL		-8.0
Ē																		Ę
ŧ																		Ē.,
F 9.0																		9. 0
Ē					4	<u>.</u>												Ė
E 10.0																		E10.0
F 10.0						:												È ' '-'
E					<u> </u>													Ė
E 11.0					 													11.0
Ę	\boxtimes	74			•													Ē
E								C: 43	ירע פטגעירו		11.4n	n				CL		Ė
120									'EY GRAVEL lifficult drilling	n indico	tes nossible	d					Y24	12.0
Ē.							ļļļ		versize materi		ios hossinie				ļļļ			<u> </u>
Ē ,											12.0n	n						
F 13.0								AUGE	R REFUSAL @	12.0m								13.0
E]						Ē
14.0		Ш.,															لـلـ	-14.0
		J.R	. Pa	aine	&	A	ssoci	ate	s Ltd.		LOGGED BY: MEB REVIEWED BY: WI	~v		COMPLE COMPLE			2.0 m	
			- `				<u>e, Yuk</u>		·		Flg. No: 1	<u>- N</u>		COMPLE	IC. 93,		Page 1	of 1
95/07/06 0	- Ke			1111	LLI	دیں	<u>, , , u n</u>	TIL								<u> </u>	- 3 -	

Public	Wo	rks	Cana	da E nvi r	ronmrntal	A&ES	Venus Mine Tailin	gs Site		OREHOLE NO			
					mounted	rig	_,	nwest of tailings (see		ROJECT NO:	8054-12		
with s							site sketch)	FT		LEVATION:	CORE		
SAMP				TUBE		LOST	AUGER	BULK	SPI		SAND		
BACK	FILL			BENTO		PEA GI	RAVEL SLOUGH	GROUT		• CLAY •	SAME		
	旧	9	INSTRUMENTATION DATA	10	20 30	40	GOILG DI		20		80	点	ELEVATION(m)
DEPTH(m)	TYPE	Ž W	V V	10	▲ PLASTIC A		SOILS DE	ESCRIPTION	20		SC OSC	SYMBOL	8
🖹	SAMPLE	SAMPLE	N E	PLASTIC		LIQUID			20	■ SAND ■ 40 60	80	S	X X
=	SAN	SA	ISTR							♦ GRAVEL ♦		SOIL	
0.0			=	10	20 30	40	GRAVELLY SANDY SILT		20	40 60	80	1	0.0
Ē								-cobbles and possibly			SM		E
Ē							boulders present,				38		E -1.0
F 1.0	\boxtimes	75		•						4		533	-1.0
E							AUGER REFUSAL @ 1.	1.2m					Ē
2.0							AUGER REFUSAL W 1.	2111					-2.0
Ē										•			E
Ė													E
= 3.0													E-3.0
Ē													Ē
Ē .													-4.0
F 4.0							NOTES:						F 4.0
Ē			-					(or bedrock) along					E
E 5.0						_ _		ea of test hole V16 m north of V16; auger					E5.0
E							refusal occured at						Ę
Ē							, , , , , , , , , , , , , , , , , , , ,						E
6.0													-6.0
Ē													Ė
Ē.,													E7.0
7.0													F -/.
Ē													E
8.0													-8.0
Ē													E
E													Ē.
9.0													-9.0
E													Ē
10.0								•					E10_0
Ē													Ē
Ė				 									Ē
11.0													-11.0
Ę													Ė
Ē													
F 12.0													-120
Ē					 								Ė
13.0					ļļ <u>.</u>					4 4			13.0
E													Ē
E													Ę ,,,
14.0		T	D	D		<u></u>	-1713	LOGGED BY: MEB		COMPLETIC	N DEPTH: 1	.2 m	<u> -14.0</u>
		J.	K.				ates Ltd.	REVIEWED BY: WCK			95/06/21		
95/07/06 0	10 50			W	<u>hitehor:</u>	<u>se. Yuk</u>	on	Fig. No: 1				age 1	of 1



10

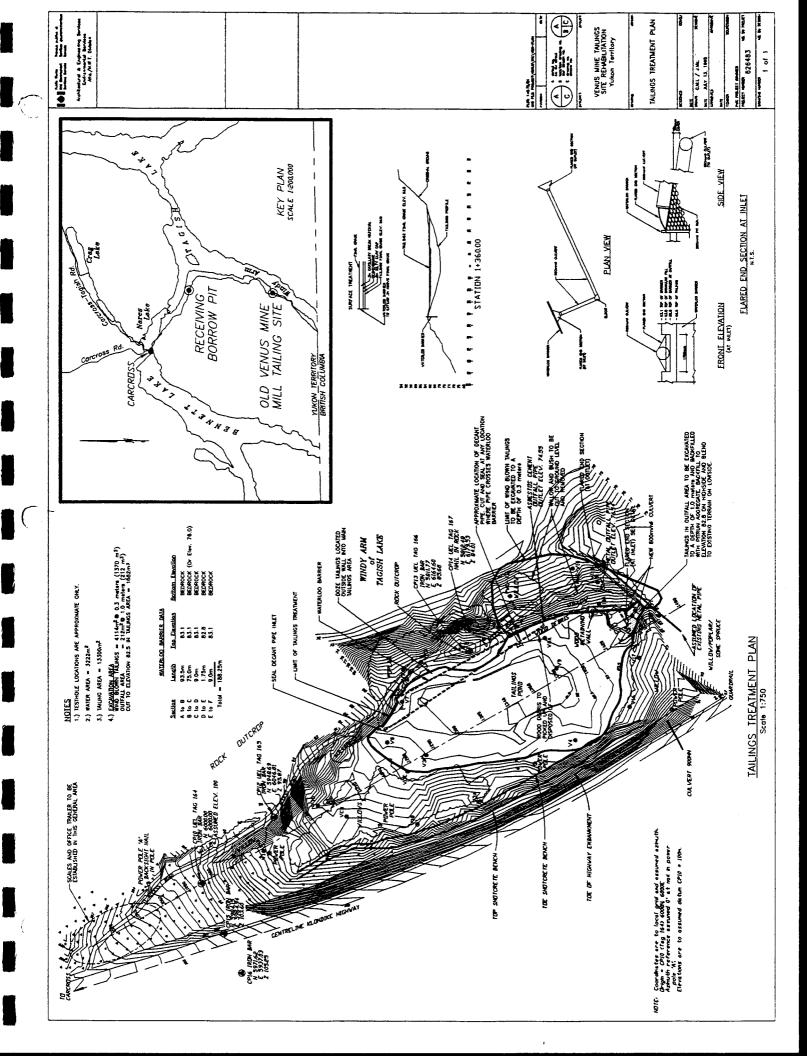
J. R. Paine & Associates Ltd.

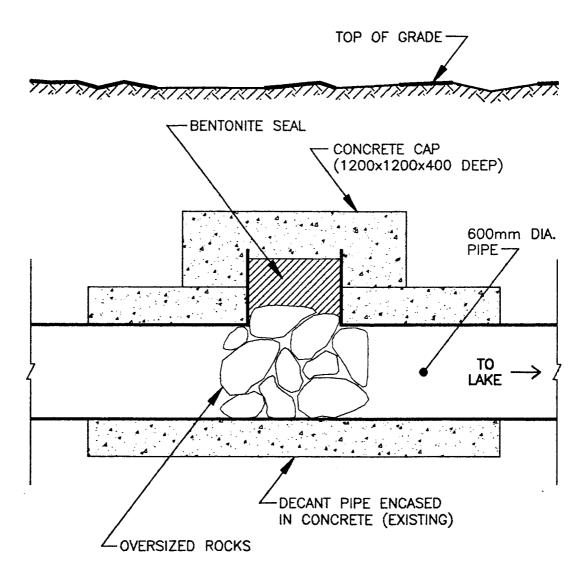
Sam	ple: _	ידי	5				_ [])ent	h:	_ ().9	m-	-1.	2m			Cli	ent: piect: _	PW Ver	SC nus	, A Mi	. &	ES S F	; ≀ec.	Lan	nat	ion				
Loca	ation:	Т	ail	in	gs. A	re	a,	T	es	it.	Ж)le	<u></u> V	16			_ Ma	de by	: <u>P</u>	. K.		. Jo	b No	o.: _₹	30:	<u> </u>	12	·			
																	_ Ck	d by:	M. I	3.		_ Da	ite: _	95/	00	72	<u> </u>				
	Siev	-		Si	ze of	Оре ИМ	enir	ng							R		eight ned g	ms	Fin	Tota er Ti			5			ent Tha		, , ,	Fine s Orio		
	80.0	വ	-	-	80.	വ	<u> </u>							1									+					-			
	50.0				50.																								100.	0	
	20,0				20.																								96.	4	
	10,0				10.																								84.	1	
	5,0				_5.		_																						73.	8	
	2,5				2.		_																						66.	0_	
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Grain Size - mm

Public Works Canada Environmental A&ES Venus Nin					us Mine Tai	ilings Site			OREHOLE								
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with solid stem augers site sketch) ELEVATION:																	
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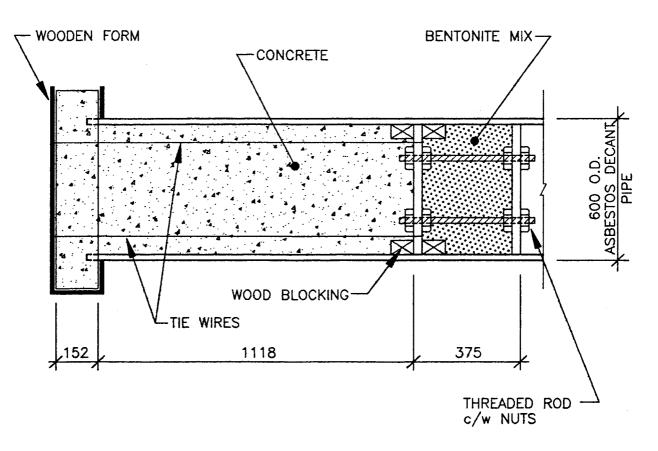


SECTION

DECANT PIPE PLUG AT INLET N.T.S.

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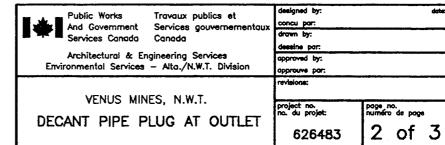


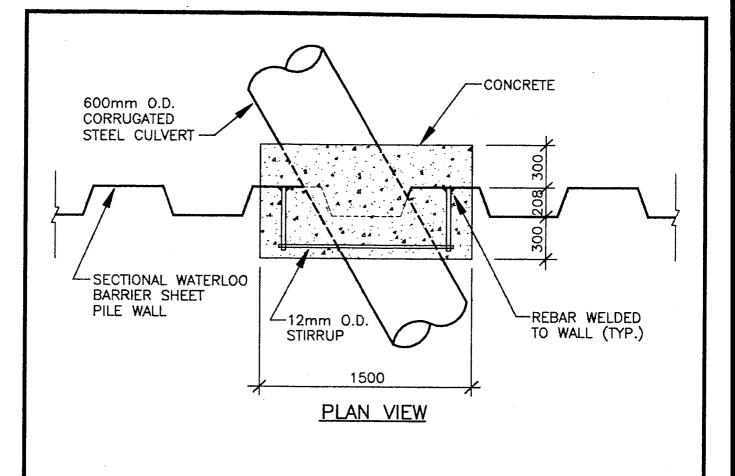
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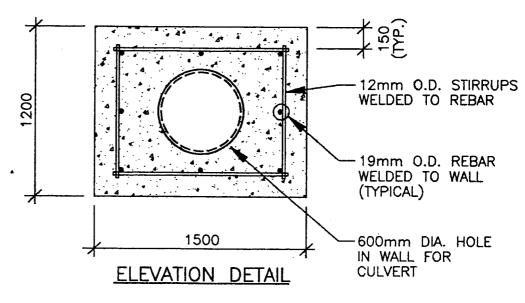
DECANT PIPE PLUG AT OUTLET

N.T.S.

PLOT 0 1=1 CAD FILE: VENUS\V-02







HIGHWAY CULVERT REPAIR

N.T.S.

PLOT @ 1=1 CAD FILE: VENUS\V-03





BTY (Alberta) Ltd.

Chartered Quantity Surveyors and Cost Consultants

July 4th, 1995

Suite 308

Strathcona Centre

10328 - 81 Avenue

Edmonton, Alterta

T6E 1X2

Public Works and Government Services Canada Architectural and Engineering Services 9th Floor Canada Place 9700 Jasper Avenue Edmonton, Alberta T5J 4E2

Fax: (403) 435-2458

Tel: (403) 43-1056

John R. Yates FRICS, PQS

G.Graeme Aston FRICS, PQS

Attention: Mr. Lawrence Borowski, P. Eng.

Dear Sir:

Re:

Venus Mine Tailings

Skagway Carcross Highway

Yukon Territory

We have finalized our cost estimate for the removal of the contaminated material from the Venus Mine Tailings Site based on the proposed scope of work.

The cost estimate totals \$ 1 556 000 and includes a 10% contingency. The estimated amounts exclude the Goods and Services Tax. A more detailed breakdown has been summarized on the attached sheets.

Should you require any further information, please do not hesitate to contact us.

Yours very truly

900

GGA:mm Enclosure

COST BREAKDOWN

Item	Quantity	Unit Rate	Estimated Cost
Improve access to the receiving pit by installing a culvert in the highway ditch, and surfacing the access route with pit run gravel. Price to include supply of culvert, installation of culvert, hauling and placing granular material and any other costs related to providing access.	Allow	Sum	13 000
Set up scales at the receiving borrow pit. Price to include all costs related to supply of scales, rentals, site preparation, erection and dismantling scales at the conclusion of the project.	Allow	Sum	25 000
Receiving Burrow Pit - Excavate, load, haul, weigh and stockpile borrow pit material under summer conditions. Price to include all labour, materials and equipment required to move borrow pit material using trucks, loaders and heavy earth moving equipment.	10 000 t	6.00	60 000
Receiving Borrow Pit - Excavate, load, haul, weigh, place and compact borrow pit material under summer conditions. Price to include all labour, materials and equipment required to move borrow pit material using trucks, loaders and heavy earth moving equipment.	7 500 t	8.00	60 000
Venus Mines Tailings Site - Excavate, load, haul, weigh and stockpile mine tailings material under summer conditions. Price to include all labour, materials and equipment required to move mine tailings material using trucks, loaders and heavy earth moving equipment.	2 500 t	6.00	15 000
Venus Mine Tailings Site - Excavate, load, haul, weigh, place and compact mine tailings material under summer conditions. Price to include all labour, materials and equipment necessary to move mine tailings material using trucks, loaders, and heavy earth moving equipment	10 000 t	8.00	80 000

COST BREAKDOWN (continued)

Item	Quantity	Unit Rate	Estimated Cost
Final placement of stockpiled borrow pit and tailings material. Load, haul, place and compact and/or doze, spread and compact stockpiled borrow pit and tailings material. Price to include all costs necessary for final placement of stockpiled borrow pit and tailings material, including clean up of stockpile areas: . mine tailings . borrow pit material	2 500 t 10 000 t	3.00 3.00	7 500 30 000
Venus Mine Tailings Site - Excavate, load, haul, weigh, place and compact mine tailings material under winter conditions. Price to include all labour, materials and equipment necessary to rip, load, haul, weight and place mine tailings material during winter months.	30 000 t	11.00	330 000
Vibratory drum compactor. Use of vibratory drum compactor for additional compaction effort at the toe of the highway embankment: . base lease rate . operating time c/w operator	Allow 75 hrs	Sum 100.00	12 000 7 500
Liner material, Load, haul, weigh, place and compact silty clay liner materials in the receiving borrow pit. Price to include all labour and equipment necessary to load and haul the material, place in the receiving borrow pit, shape to required dimensions and compact.	6 500 t	7.00	45 500
Capping material. Load, haul, weigh and stockpile materials to be used for capping the final mine tailings pile. Price to include all labour and equipment necessary to prepare the stockpile area, load and haul the material and stockpile.	3 500 t	7.00	24 500

COST BREAKDOWN (continued)

Item	Quantity	Unit Rate	Estimated Cost
Level capping material at the site near Carcross. Price to include labour and equipment necessary to restore the current "landfarm" to a smooth, drained surface.	Allow	Sum	5 000
Remove, (or relocate) power lines. Price to include actual costs incurred by a local power company to complete the work.	Allow	Sum	5 000
Collect and dispose (by burning) wood debris on site, and dispose of brush and decant pipe material. Price to include all labour and equipment necessary to clean up work areas at the Venus Mine Tailings site.	Allow	Sum	5 000
Final clean up of mine tailings area, including levelling and shaping the mine tailings site. Price to include all labour and equipment necessary to shape the Venus mine site to the final grades indicated on the contract drawings.	Allow	Sum	10 000 (1. 96.
Licences, permits and royalties. Cash allowance to cover payments made by the contractor for licenses, permits, bonds and royalties.	Allow	Sum	20 000
Cost to complete project. Price to include supervision, profit, administration, community consultation, supply of temporary facilities, flagpersons, scale persons and any costs for items not covered above.	Allow	Sum	757 1998 2 89 1996 200 000
Supply 3/4" granular fill. Price to include loading, hauling, placing and compacting the material in two (2) lifts, each 300 mm in thickness and constructing berm in accordance with design details. Assume 15 km haul. . berm (Land Constructed in 1915) . granular fill	6 500 t 9 000 t	crush/stec Hasa/pec 14.00 12.00	877/2 1995

COST BREAKDOWN (continued)

Item	Quantity	Unit Rate	Estimated Cost	-
Geocomposite clay liner. Supply and install Bentofix GCL or equivalent clay liner	9 000 m2	20.00	180 000	(1796)
Vegetation cover. Hydro seed borrow pit area. Price to include supply of seed mixture, hydroseeding and placement of a degradable erosion blanket	9 000 m2	3.00	27 000	(१९१४)
De-watering of existing pond	Allow	Sum	40 000	
Place capping material/grade/compact	3 500 t	4.00	14 000	(1996)
Contingency allowance (10%)	Allow	Sum	141 500	
TOTAL			\$ 1 556 500	-

Eralden - 1948 909000 1996 - 506,674 Contingen 141,500



${f B} \, {f T} \, {f Y}$ (Alberta) Ltd.

Chartered Quantity Surveyors and Cost Consultants

July 17th, 1995

Suite 308

Strathcona Centre

10328 - 81 Avenue

Edmonton, Alberta

T6E 1X2

Public Works and Government Services Canada Transportation Architectural and Engineering Services 9th Floor Canada Place 9700 Jasper Avenue Edmonton, Alberta

Fax: (403) 433-2458 Tel: (403) 439-0056

John R. Yates

FRICS, PQS

G.Graeme Alston FRICS, PQS

Attention: Mr. Henry Westerman

Dear Sir:

T5J 4E2

Re:

Venus Mine Tailings

Skagway Carcross Highway

Yukon Territory

Following our meeting with Mr. Lawrence Borowski, we have finalized our cost estimate for the containment of the contaminated material at the Venus Mine Tailings Site based on the proposed scope of work.

The cost estimate totals \$ 1 221 000 and includes a 10% contingency. The estimated amounts exclude the Goods and Services Tax. A more detailed breakdown has been summarized on the attached sheets.

Should you require any further information, please do not hesitate to contact us.

Youks very truly,

Greene Alsto

GGA:mm Enclosure

COST BREAKDOWN

ltem	Quantity	Unit Rate	Estimated Cost
Set up scales at the Venus Mine Tailings Site. Price to include all costs related to supply of scales, rentals, site preparation, erection and dismantling scales at the conclusion of the project Supply and installation of an impermeable wall (Waterloo Barrier) to contain the tailings pile at its current location:	Allow	Sum	12 000
. Mobilization and fixed costs	Allow	Sum	35 000
. Accommodation, travel and communication expenses	Allow	Sum	40 000
. Quality Assurance/Quality Control inspection services	Allow	Sum	30 000
. Waterloo Barrier sheet piling supply and installation	Allow	Sum	210 000
. Waterloo Barrier sheet pile installation	Allow	Sum	145 000
. Waterloo Barrier sheet pile joint sealing	Allow	Sum	90 000
Load, haul, weigh, place, grade and compact a silty clay cap. Price to include all labour and equipment to construct a silty clay cap. Collect and dispose (by burning) wood debris on site and dispose of brush and seal decant pipe.	4 500 t	8.00	36 000
Price to include all labour and equipment necessary to clean up work areas at the Venus Tailings site.	Allow	Sum	5 000

COST BREAKDOWN (continued)

la	Quantity	Unit Rate	Estimated Cost
Item	Country		
Excavating wind blown tailings and levelling tailings site. Price to include all labour and equipment necessary to excavate wind blown tailings; excavate high areas on the tailings pile and move to low areas; final leveling and compaction of tailings site:	·	·	
. Excavate and place wind blown tailings, including material in the drainage discharge area	1 600 m3	3.00	4 800
. Excavate and relocate tailings on site	1 700 m3	3.00	5 100
. Final shaping, grading and compaction of tailings site	13 300 m2	2.00	26 600
Supply and installation of geomembrane. Price to include all labour and equipment necessary to supply a geomembrane and place (including field welding, if specified) a geomembrane over the silty clap cap.	13 300 m2	18.00	239 400
Constructing a drainage discharge system. Price to include the supply and installation of piping material; supply and installation of end sections and all connections	Allow	Sum	7 000
Screening, hauling and placing capillary break material. Price to include the screening, hauling, placing and compaction of a capillary break material to the lines and grades specified.	7 300 t	13.00	94 900
Supply and place pitrun aggregate in the outfall area	500 t	12.00	6 000
Licenses, permits and royalties. Cash allowance to cover payments made by the contractor for licenses, permits, bonds and royalties.	Allow	Sum	10 000

Venus Mine Tailings Skagway Carcross Highway Yukon Territory

COST BREAKDOWN (continued)

Item	Quantity	Unit Rate	Estimated Cost
Costs to complete project. Price to include supervision profit, administration, community consulting, supply of temporary facilities, flagpersons, scale persons, dewatering and any costs for items not covered above	a, Allow	Sum	113 200
Contingency allowance (10%)	Allow	Sum	111 000
TOTAL			\$ 1 221 000

VENUS MINE TAILINGS REMEDIATION: CONSTRUCTION COST SUMMARY

ITEM		CONSTR	CONSTRUCTION COST ESTIMATE	ESTIMATE		START UP		PROGRESS CLAIM #2	#2	PR	PROGRESS CLAIM #3	AIM #3	PRC	PROGRESS CLAIM #4	AIM #4
S	DESCRIPTION	Unit of measure	Expected Quantity	Unit price	Total Item Cost(\$)	PC #1	Percent Quantity		Claimed	Percent complete	Quantity	Claimed	Percent	Quantity	Claimed
+	Setup weigh scales												Complete		
7	Waterloo Barrier	L.S.			548,000.00	,	%56		520,600.00	100%	-	548,000.00	100%		548.000.00
က	Haul & place clay cap	cu.m.	2650	18.90	50,085.00	•		2650	50,085.00		3850			3850	72 765 00
4	Collect & dispose of debris	نـ زی			4,032.00	•	100%		4,032.00	100%			100%		4 032 00
Sa	Excavate wind blown tallings	G.m.	1600	0 6.10	9,760.00	1		1600	9,760.00		3656	~		3656	22.301.60
Sb	Excavate tallings pond	cu.m.	1700	0 8.82	14,994.00	•		1700	15,000.00		2226			2226	19 633 32
ည	Level tailings pond	eq.m.	13300	0.35	4,655.00	•		13300	4,655.00		13300			13300	4.655.00
ဖ	Supply & Install geolexille	SQ.T.	13300	3.38	44,954.00	1		6650	22,477.00		12426	4		13300	44.954.00
7	Construct drainage system	L.S.	80	188.16	15,052.81	٠	%0		0.00	%0		00.0	%	25	4 704 06
80	Screening & hauling gravel	cu.m.	4100) 16.16	66,256.00	,	%0		0.00		0	00 0		4725	76 356 00
O	Hauf and place pitrun(outfall)														(0,000,00
9	Cesh allowance														
=	Cost to complete	Ľ.S.			344,779.00	•	20%		172,389.50	%06		310,779.00	100%		344 779.00
										Extra		43,000.00			51,700.00
	TOTAL				1,102,567.81	434,000.00			798,998.50			1,067,165.80			1,193,879,98
	(less) 10% Holdback								79,899.85			106,716.58			67,588.02
	Net Amount					434,000.00			719,098.65			960,449.22			1,126,291.96
	(less) Previous Payment					00:00			434,000.00			719,098.65			1,012,249,20
	NET AMOUNT PAYABLE					434,000.00			285,098.65			241 350 57			414 042 7E

Traverse	hline		REQUEST NO. DEPT.	
Public Works Travaux pu Canada Canada	REQUEST FUR PR	OGRESS PAYMENT	5 / 28	
REGION/DISTRICT	PAYMENT PERIOD	Aug 1-15- INIT	PL Contribution	
	FROM:	TO	:	
CONTRACTOR (NAME AND ADD	RESS)		R.O. FILE NO.	
P.C. Box 130			D.O. FILE NO.	
DESCRIPTION AND LOCATION C		THE RESERVE OF THE PARTY OF THE	CONTRACT NO.	
tieras mine TA	LINGS Rehabligi	a Tiori	PROJECT NO.	
PART 1 – PROGRESS CLAIM		THIS PERIOD	TOTAL TO DATE	· -
A) Portion of work completed		\$ 434,000	\$ 434 000 00	
B) Material delivered to site but not incorporated in work		\$ 6	\$ &	
	AMOUNT CLAIMED	\$ 434,000.00	\$ 430,000.	æ
but not incorporated in the work, th	ne whole as described in the attached	ment of the above contract for work COST BREAKDOWN.		to site
CONTRACTOR: V - (C./	i lan	Managec.	(ict 10/95	. <u>-</u>
	ED SIGNING OFFICER	ŢIJŻĹĔ	DATE	
PART 2 – PROGRESS REPORT	TOTAL AMOUNT	(LESS) HOLDBACK	NET AMOUNT	
A) Work completed to date	s a	\$ £	· 434, 050 -	
B) Material delivered to site but not incorporated in the work	\$	\$	\$ &	
TOTALS TO DATE	\$	\$	\$ 434,000-	-
	(Less) Previo	ous Payment(s)	\$	
		NET AMOUNT PAYABLE	The state of	(V).
DPW:	ED SIGNING OFFICER	to site, described in the above Pro	n Oct 95	195
PRE-AUDIT BY:	CERTIFIED PURSUANT TO SEC THE FINANCIAL ADMINISTRAT	TION ACT TO SECTION TRATION ANCE WITH COUNT VE	IONED FOR PAYMENT PURSU IN 26 OF THE FINANCIAL ADI ACT AND CERTIFIED IN ACCO H SUBSECTION 7(1) OF THE A RIFICATION AND PAYMENT GULATIONS.	MINIS- DRD- NC-
	SIGNATURE		SIGNATURE	
ORIGINAL CONTRACT AMOUNT		APPROVED DEDUCTIONS	AUTHORIZED CONTRACT	
REF, NO. 2 Section 12 Section 12 Section 1	\$ ACCOUN	T CODING	AMOUNT	CR.
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Carcross/Tagish Development Corporation

Head Office: P.O. Box 130

Carcross, Yukon

YOB 1BO

Tel: (403) 821-4109

Fox: (403) 821-4811

D.I.A.N.D. Action on Waste Management 300 Main Street Whitehorse, Yukon

October 20, 1995

Attn: Mrs. Dorothy McLeod, Administrator.

Dear Mrs. McLeod;

Re: Expenditures Paid Under the Venue Mine Site Rehabilitation.

Further to our meeting of Thursday, October 19, 1995 regarding expenditures from the first advance of \$434,000.00 the following is a list of these for your records.

		\$ 28,000.00
Coine & Sons Equipment Rental		22,000.00
L & J Construction		16,400.00
Riverside Contracting		15,000.00
H.R. Vance		
United Keno Hill	•	10,000.00
Camp Rental & Food		26,000.00
L.W. Dickson Contracting		56,000.00
		143,000.00
Labour		2,500.00
Insurance		6,000.00
Job Site Offices		27,000.00
Hilker		3,000.00
Legal Fees		22,000.00
Y.T.G. Highways		
Bray-Shay Enterprises		8,000.00
Nilex		17,000.00
		3,000.00
Caddock Trucking		1,500.00
Hawkshaw Transport		5,000.00
Helm Trucking		4,000.00
Butch Beattie Trucking		2,740.00
Beaver Lumber		5,786.00
Kilrich Industries	_	
A1440	Total:	423,926.00

The above numbers have been rounded to the nearest \$10.00. As of this date the project is completed and attached please find our final progress claim for work done.

We hope the foregoing to be to your satisfaction and look forward to payment.

Regards, Larry Whelan

Larry Whelan, Manager

LW/mp

Public Works Travaux pu	blics REQUEST FOR PR	OGRESS PAYMENT	REQUEST NO.	DEPT.	
Canada Canada	7120207 . 0777 .		12	28	
REGION/DISTRICT	PAYMENT PERIOD				
	FROM: Aug		:5EPT 13	5, 199	5
CONTRACTOR (NAME AND ADD	HESS)	ne de booken al	R.O. FILE NO.		
	TAGISH FIRST N		D.O. FILE NO.		
DESCRIPTION AND LOCATION O	OF WORK	0	CONTRACT NO.		
VENUS MINE TI	AILINGS REHABI	LITATION Project	PROJECT NO.		
PART 1 – PROGRESS CLAIM		THIS PERIOD	TOTAL TO DATE		
A) Portion of work completed		s 798, 998. 5 0	\$ 798,9	198.50	
B) Material delivered to site but not incorporated in work		\$ -0-	\$ E) -	
	AMOUNT CLAIMED	s 798, 998 <u>00</u>		998.5	
	nce with TP 4.2 of the Terms of Pay ne whole as described in the attached	ment of the above contract for work COST BREAKDOWN.	completed and mate	rial delivered	to sit
CONTRACTOR: LAWY	ence Whilan	. Monager	Sept:	30/95	_
AUTHORIZ	ED SIGNING OFFICER	TITLE //	Ε	DATÉ	
PART 2 – PROGRESS REPORT	TOTAL AMOUNT	(LESS) HOLDBACK	NET AMOUNT		
A) Work completed to date	* 798, 998.50	: 79, 899.85	\$ 719,0	98. E	,s
B) Material delivered to site but not incorporated in the work	\$ D	\$ ->	•		
TOTALS TO DATE	\$ 798,998.50	s 79, 899.85	\$ 719,	098.6	<u>15</u>
	(Less) Previo	ous Payment(s)	\$ 434,	000.0	10
		NET AMOUNT PAYABLE	285,	598=	65
The value of the portion of the w	ork completed and material delivere	d to site, described in the above Pro	ogress Claim is as sho	own in this P	rogres
DPW: Jalen	Valle	Project Maran	_ Oct	3/98	3
PRE-AUDIT BY:	ED SIGNING OFFICER CERTIFIED PURSUANT TO SEC	TION 27 OF REQUISITI	ONED FOR PAYME	NT PURSUA	ANT
	THE FINANCIAL ADMINISTRA	TRATION A ANCE WITH COUNT VE	N 26 OF THE FINA ACT AND CERTIFII I SUBSECTION 7(1 RIFICATION AND GULATIONS.	ED IN ACCO	RD- C-
	SIGNATURE		SIGNATURE		
ORIGINAL CONTRACT AMOUNT	APPROVED ADDITIONS	APPROVED DEDUCTIONS	AUTHORIZED CO		
• · · · · · · · · · · · · · · · · · · ·	\$	\$	\$	-	
REF. NO.	ACCOUN	T CODING	AMOUN	Т	CR.
CHEQUE NO. & DATE					20
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					133
SERVICE OFFICER					
	·	TOTAL ▶			

			REQUEST NO.	DEPT.	
Public Works Travaux pub Canada Canada	REQUEST FOR PR	OGRESS PAYMENT		28	
REGION/DISTRICT	PAYMENT PERIOD				
	FROM: SEP	<i>t 15</i> to:	Oct 10	1995	
CONTRACTOR (NAME AND ADDI		The state of the s	R.O. FILE NO.		
	w Development		D.O. FILE NO.		
P.D. BOX 130 CA	eceses (false)		CONTRACT NO.		
DESCRIPTION AND LOCATION O	ailings REHABILI	TATION Project	CONTINUE		
VENUS MINE IT	TENNOS NERMOL	<i>/////////////////////////////////////</i>	PROJECT NO.		
PART 1 - PROGRESS CLAIM		THIS PERIOD	TOTAL TO DATE		
A) Portion of work completed		\$ 268, 167.50	\$ 1067	165.80	J
B) Material delivered to site but not incorporated in work		\$	\$ ~	-	
	AMOUNT CLAIMED	\$ 268 167.50	\$ 1067	165.	80
This claim is submitted in accordangular not incorporated in the work, the	ce with TP 4.2 of the Terms of Payr e whole as described in the attached	ment of the above contract for work COST BREAKDOWN.	completed and mate	erial delivered	to site
CONTRACTOR! Whe	lan	manager	Cct	10/95	-
	ED SIGNING OFFICER	manager		DATÉ	
PART 2 – PROGRESS REPORT	TOTAL AMOUNT	(LESS) HOLDBACK	NET AMOUNT	449 2	ي
A) Work completed to date	\$ 1067,165.80	\$ 106 716.58	\$.960 ,	79 /	
B) Material delivered to site but not incorporated in the work	\$	\$ 0	\$	<u>e</u>	
TOTALS TO DATE	\$ 1067,165.80	\$ 106, 71658	\$ 960	449.	رزد.
	(Less) Previo	ous Payment(s)	\$ 719	098.	65
		NET AMOUNT PAYABLE	Selection is	50:.5	₹Z:
DPW:	ork completed and material delivered	d to site, described in the above Pro	n. <u>Oc</u>	FID /	95
PRE-AUDIT BY:	CERTIFIED PURSUANT TO SEC THE FINANCIAL ADMINISTRAT	TION ACT TO SECTION TRATION: ANCE WITH COUNT VE	ONED FOR PAYM IN 26 OF THE FINA ACT AND CERTIFI H SUBSECTION 7(1 RIFICATION AND GULATIONS.	ANCIAL ADM ED IN ACCO I) OF THE AC	MINIS- RD- C-
	SIGNATURE		SIGNATUR		
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Public Works Canada Travaux publics Canada

COST BREAKDOWN FOR UNIT PRICE CONTRACT

REQUEST NO.

PAGE

OF

DESCRIPTION AND LOCATION OF WORK

CONTRACT NO.

					•	PROJECT NO.	
	CLASS OF LABOUR	UNIT OF	Τ	QUANTITIES			VALUE TO DATE
NO.	PLANT OR MATERIAL	MEASURE	AUTHORIZED	THIS PERIOD	TO DATE	UNIT PRICE	VALUE TO DATE
7/	SUT-ep WEIGHT SUPLES	<i>مإ</i> ر	NIP	NA			N/A
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?	Silry Clay	11.3	2650	1200	3850	18 90	72, 765.0
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5,4	EXCAUATE TALLINGS	M3	1600.00	2056	3656	610	22,301.6
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C-	•	54 M	1320	0	13,300	0 35	4655.
, .	Expoly Geomembrane	Sq. M	13300	5776	12,426	3.75	41999
)	Centificat Dainage	1.M	80	A	0	158	↔
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7	Supply place + compact lit how	113	300	æ	D	33. M	<u> </u>
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	C.O NO1		43,600	43,550	43000		43, 650
`	,						
-							
							1,067,165
			 				

I hereby certify that the work done and material delivered to site up to the date of this request for payment are as listed above. Work and material are according to plans, specifications and contract, that the prices are according to contract or, if not specified by contract, are reasonable.

CONSULTANT	DATE	AUTHORIZED DPW OFFICER	DATE
DA.(1) (1)	n 4/x/9-		
auch vallend	Oct 10/13.		<u> </u>
FINAL CERTIFICATE OF MEASUREMENT	<i>'</i>		

The quantities shown are those obtained in the final measurement of this contract. I hereby issue this Final Certificate of Measurement in accordance with GC 44.7 and 44.8 of the General Conditions.

CONSULTANT	DATE	ENGINEER	DATE
	1	Ì	

PROJECT: Venus Mine Tailings Rehabilitation Project.

CLIENT: D.I.A.N.D. Action On Waste/Federal D.P.W.

DATE: October 10, 1995

APPROVED BY: Project Engineer,

Project Manager,

ITEM #01- Excavate/Repair Highways

Culvert (not known previously)

Agreed Price

\$12,000.00

ITEM #02- Additional Eqpt. Time

Required When Tailings

Could Not Be Relocated And Compacted Due To Unstable

Soil Conditions.

\$20,000.00

ITEM #03- Additional Labour,

Supervision And Surveying Time

To Cover Increases In Unit

Pay Items.

\$11,000.00

\$43,000.00

AMOUNT DUE

\$43,000.00

Canada Canada				28
REGION/DISTRICT	PAYMENT PERIOD	/ <i>C</i> 10	. Cct 20	195
		70	n.o. FILE NO.	
CONTRACTOR INAME AND ADI		William College	1,0,7722.00.	
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DESCRIPTION AND LOCATION	OF WORK (/	() ,	CONTRACT NO.	
	Site Tailings	Kebabikijnswy	PROJECT NO.	<u></u>
Caucros (jo		THIS PERIOD	TOTAL TO DATE	
PART 1 - PROGRESS CLAIM				:21
A) Portion of work completed		* 126, 714 J8	\$ 1.93 6	3077 70
ti) Material delivered to site tier not incorporated in work		\$ <u>-</u>	\$ &	
		: 126,714.8		
This claim is submitted in accorda but not incorporated in the work, t	nce with TP 4.2 of the Terms of Pay the whole as described in the attached	ment of the above contract for work COST BREAKDOWN.	completed and mater	ial deli∳ered to si
	Colina	Minsi	Och 2	0/05
CONTRACTORY / /	CED SIGNING OFFICER	Mindiga.	17	ATF
		(LESS) HOLDBACK	NET AMOUNT	
PART 2 - PROGRESS REPORT	TOTAL AMOUNT			2.11.00
A) Work completed to date	\$ 1. 193 379 78	+ 67, 588.02	\$1,126 2	14. 96
B) Material delivered to eite but not incorporated in the work	\$.0-	\$ 6		· · · · · · · · · · · · · · · · · · ·
TOTALS TO DATE	s 1, 193 879 98	\$ 67,588 00	\$ 1, 126,	291.96
	(Less) Previo	ous Payment(s)	\$ 1,012,	249, 20
		NET AMOUNT PAYABLE	114,0	4.2.76
The value of the portion of the v Report.	vork completed and material delivers	nd to site, described in the above Pri	ogress Claim is as sho	wn in this Progre
Drive faturil 1	1)allow k	rose (marage	- Oct	-20/25
AUTHORIZ	ED SIGNING OFFICER	TITLE		A T E
FRE AUDIT BY:	THE FINANCIAL ADMINISTRAT	TION ACT TO SECTION TRATION: ANGE WITH COUNT VE	IONED FOR PAYMEN AS OF THE FINAL ACT AND CERTIFIE HIS SECTION 7(1) HIFICATION AND PROJECTIONS.	ICIAL ADMINIS O IN ACCORD- OF THE AC-
	SIGNATURE		SIGNATURE	· · · · · · · · · · · · · · · · · · ·
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Public Works Canada

Travaux publics Canada

COST BREAKDOWN FOR UNIT PRICE CONTRACT

REQUEST NO.

PAGE /

DESCRIPTION AND LOCATION OF WORK

CONTRACT NO.

			• .			PROJECT NO.	
ITEM NO.	CLASS OF LABOUR	UNIT OF	AUTHORIZED	QUANTITIES		UNIT PRICE	VALUE TO DATE
<u></u>	SET-UP WEIGHT SCALS	 	NA	NA	M/A	;	N/H
C2	LUATERIES BARRIER	1.5	548 000		548 000	1.5	545 ac ac
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	Collect DEBUS	1.5	0		100%	403200	
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20	<i>91 1</i> •						113 000-0
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CERTIFICATION (Sign Last Page Only)

I hereby certify that the work done and material delivered to site up to the date of this request for payment are as listed above. Work and material are according to plans, specifications and contract, that the prices are according to contract or, if not specified by contract, are reasonable.

CONSULTANT	2 Tentr		AUTHORIZED DPW OFFICER	DATE
Varin la	Weny Jan 20	195		
FINAL CERTIFICATE OF A		(,)		

FINAL CERTIFICATE OF MEASUREMENT

The quantities shown are those obtained in the final measurement of this contract. I hereby issue this Final Certificate of Measurement in accordance with GC 44.7 and 44.8 of the General Conditions.

CONSULTANT	DATE	ENGINEER	DATE
DDW 4303 www.			

Correspond Tropicals Decreptor consequent and consequent

Head Office: P.O. Box 130

Carcross, Yukon YOB 1BO

Tel: (403) 821-4109 Fax: (403) 821-4811

Change Order No. 2

Venus Mill site Tailings Rehabilitation

Client - DIAND-Action on Waste Management

Approved: Government of Canada Engineer

Carcross/Tagish DEV. Corp. Manager

Date: October 20, 1995

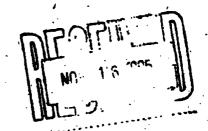
To increase the contract amount to compensate for cost to complete due to increases in unit quantities:

Amount of this change order \$8700.00



ENVIRONMENTAL

Environmental Contractors & Engineers



November 14, 1995

Indian and Northern Affairs Canada Arctic Environmental Strategy Action on Waste/Contaminants #345, 300 Main Street Whitehorse, Yukon Y1A 2B5

Attention: Mr. Mark Palmer/Mr. Brett Hartshorne

Dear Sirs:

Re: Waterloo Barrier™ Installation -Old Venus Mine Site, Yukon Territory

Please find attached, the following documentation regarding this project:

- i) Statutory Declaration, re: payment of accounts;
- ii) Workers' Compensation Board Clearance Certificate;
- iii) Warranty Letter.

Should you have any questions or require additional information, please do not hesitate to contact the undersigned at your convenience.

Yours truly,

C³ Environmental

Murray C. Gamble, P.Eng. President

Enclosure

MCG:kp

Containment • Control • Corrective Action

P.O. Box 188, Breslau, Ont. N0B 1M0 Phone (519) 648-3611 Fax (519) 648-3505

CCDC Document 9A

Statutory Declaration

TO BE MADE BY THE CONTRACTOR WHEN APPLYING FOR RELEASE OF HOLDBACK, SECURITY DEPOSIT OR BOTH UPON SUBSTANTIAL/TOTAL PERFORMANCE

	IN THE MATTER OF THE CONTRACT
	between . Indian and Northern Affairs Canada
	between
•	3 Environmental, a division of Canadian
	Construction Controls Administration - Old
	for Waterloo Barrier History
	Venus Mine Site, Yukon Territory (insert title of the Work and the Project)
	(insert title of the Work and the Project)
Marray Camble	the . townofBreslau
I, Murray Gamble of Ontario	DO SOLEMNLY DECLARE:
in the Province of	
Procident	(See Note 1) of .C ³ Environmental the Contractor named in the Contract abovementioned,
THATIAM Plesident	the Contractor named in the Contract abovementioned,
	that all accounts for labour, subcontracts, pro-
and as such have personal knowledge of the facts her	eunder declared, and that all accounts for independent which may have been incurred by the Contractor in the crime might in any way be held responsible have been paid in full
dusts construction machinery and equipment and other	er indebtedness which may have been head responsible have been paid in full the Owner might in any way be held responsible have been paid in full
Bucks, constitutions of the Work (See Note 2) and for which	the Owner might in any way be need responsible may be
Performance of the Work (see Attained	
except holdback monies properly retained.	
·	conscientiously believing it to be true and knowing it is of the same force
AND I MAKE THIS SOLEMN DECLARATION	conscientiously occiteding to the state of t
and effect as if made under oath.	
appendiction as a second	
DECLARED before me at the	
DECLARED before me at the Breslau of Breslau	
in the province this	14th Signed
ofOntario thi	95.
day of November	9
1/1-1000	
A Commissioner for Oaths, Notary Public, Judice of the Pe	nce.
A COMMENT OF THE PROPERTY OF T	
Print Ado Stock a Commissioner, etc.,	
County of Wollington, for Conadian	- Director of an incorporated
Construction Controls United by the President	t, a Vice President, the Secretary, the Treasurer, or a Director of an incorporated claration provided that two copies of the by-law issued under the Corporation seal nies the first Declaration on each Contract. For a partnership the Declaration must nies the first Declaration on each Court make the Declaration. The position of the
NOTE I. The Declaration intist the made may make the Dec	claration provided that two copies of the by-law issued thick in the Declaration must nies the first Declaration on each Contract. For a partnership the Declaration of the ship the sole proprietor himself must make the Declaration. The position of the
company such individual to execute documents accompa	nies the first Declaration on each count make the Declaration. The position of the
be made by one of the partners and for a sole proprieto	nies the first Declaration on each Contract. For a partnership the Declaration of the ship the sole proprietor himself must make the Declaration. The position of the oted.
declarant and the name of the Community	
	the the Contractor to persons in privity of contract with him, debts arising
NOTE 2 Other indebtedness shall mean only such debts	incurred by the Contractor to persons in privity of contract with him, debts arising actor's workers any debt arising out of collective bargaining agreements, legislation ace, and minimum wage standards where applicable.
ohtheisticutory requirements, and in the case of the Contrappying to worker a compensation, unemployment insura	nce, and minimum wage standards where applicable.
applying to worker seempensation, unemprovinces management	
II was at you in	•
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700 04 - 1987 File 10825	
CCDC 9A — 1982 File 00825	



Workers* Compensation Board Commission des accidents du travail 151 FREDERICK STREET KITCHENER, ONTARIO N2H 2M2 (519) 576-4130 Clearance Certificate Certificat de décharge

The Workers' Compensation Board (WCB) hereby waives its rights under Section 11 (3) (R.S.O. 1990) of the Workers' Compensation Act to hold the Principal that is in a contractual agreement with the Contractor named, liable for any Section 11(3) (R.S.O. 1990) liability of the Contractor for assessments and levies of the WCB owing now or within 60 days from the date of this Certificate.

CONTRACTOR L'ENTREPRENEUR

CANADIAN CONSTRUCTION CONTROLS LIMITED BOX 188 BRESLAU NOB 1M0 Par la présente, la Commission des accidents du travail (CAT) renonce aux droits qui lui sont conférés en vertu du paragraphe 11 (3) de la <u>Loi sur les accidents du travail</u> (L.R.O. 1990) et qui l'autorisent à tenir l'entrepreneur principal, qui a signé une entente contractuelle avec l'entrepreneur dont le nom figure sur le présent certificat, responsable du palement de toute cotisation ou de toute somme que l'entrepreneur est tenu de verser à la CAT immédiatement ou dans les 60 jours suivant la date indiquée sur ce certificat.

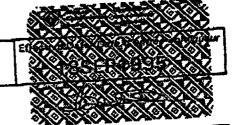
THIS CERTIFICATE IS VALID FOR ALL CONTRACTS OF THE NAMED CONTRACTOR DURING THE EFFECTIVE PERIOD

ON

LE PRESENT CERTIFICAT EST VALIDE POUR TOUS LES CONTRATS PASSES PAR
LEDIT ENTREPRENEUR PENDANT LA PERIODE D'APPLICATION DU CERTIFICAT
Valid only when signed by an authorized Officer of the WCB.

Man valide cans le sinneture d'un agent autorisé de la CAT.

Account No./ N° de compte Firm No./ N° d'entreprise 240643FD



	Retei Toux Description		Description
Rete/Teux 723	Description GENERAL CONTRACTOR	745	CONCRETE/FORMING

Comract Description Description du contret

Gertificate No./ Nº de certificat
200583900

F5196483505

Coptact the WCB-it you question the validity of this document.

Verillez Communiquer evec is CAT si yous doutez de la validité du présent document.



Environmental Contractors & Engineers

November 14, 1995

Indian and Northern Affairs Canada Arctic Environmental Strategy Action on Waste/Contaminants #345, 300 Main Street Whitehorse, Yukon Y1A 2B5

Attention: Mr. Mark Palmer/Mr. Brett Hartshorne

Dear Sirs:

Waterloo Baπier™ Installation -Re: Old Venus Mine Site, Yukon Territory

This letter is to confirm that as per our contract with the Carcross/Tagish Development Corporation, C³ Environmental warrants against defects in workmanship and materials related to the supply and installation of the Waterloo Barrier™ system for a period of one year (effective as of final completion September 25, 1995).

This warranty is limited only to the provision of materials and services necessary to repair/reinstate the barrier in order to achieve the specified performance criteria and does not cover contingent liabilities.

C³ Environmental does not assume liability with respect to the performance of the overall site remediation program and cannot be responsible for subsequent damage to the barrier caused by other parties or activities beyond our control.

Should you have any questions or require additional information, please do not hesitate to contact the undersigned at your convenience.

Yours truly,

C3 Environmental

Murray Gamble, P.Eng.

President

ace:Ko

Containment • Control • Corrective Action.

P.O. Box 188, Breslau, Ont. N0B 1M0 Phone (519) 648-3611 Fax (519) 648-3505 \(\text{1} \)



CONSULTING AND TESTING ENGINEERS

EDMONTON - GRANDE PRAIRIE - WHITEHORSE - PEACE RIVER

ADDRESS ALL CORRESPONDENCE TO

14 Burns Road

Whitehorse, Yukon

Y1A 4Y9

File No: 8054-12

September 07, 1995

PUBLIC WORKS CANADA Architectural and Engineering Services 1000 Canada Place 9700 Jasper Avenue Edmonton, Alberta T5J 4E2

Attention: Mr. George Strynadka, Senior Project Engineer

Dear Sir:

Re: Venus Mine Tailings Project Construction Management Services

The following letter summarizes the results of the construction management services which our firm has performed for the subject project.

J.R. Paine & Associates Ltd. role during construction was to provide interim construction management services between the dates of August 14, 1995 and September 06, 1995. This essentially consisted of facilitating the construction activities by providing recommendations to the contractor as required. Michael Billowits, P. Eng. was the J.R. Paine & Associates Ltd. site representative.

This letter will summarize the activities which occurred during our management period and provide details of testing services which we performed to facilitate the site rehabilitation program.

ACTIVITY REVIEW

The construction activities progressed in accordance with the tentative schedule drawn up by yourself at the meeting with the Carcross First Nations Corporation on August 11, 1995. The following includes a summary of the activities, expected and actual completion dates.

Item	Activity	Expected Completion Date	Actual Completion Dates
1	Mobilization - prepare work area, field office, site access	95/08/21	95/08/18
2	Clean-up debris, brush and dispose	95/08/21	95/08/11
3	Provide temporary drainage and filter	95/08/21	95/08/25
4	Cut off and plug existing decant line	95/08/21	95/08/30
5	Excavate and place peripheral tailings	95/08/28	95/08/23
6	Level tailings area, grade and compact	95/09/05	Anticipated 95/09/08
7	Install sheet barrier wall	95/10/02	In progress on schedule

The remainder of the activities have yet to be initialised. Exception to this includes Item 10 which involves the provision to screen and process granular/rock fill (capillary break material). The contractor has secured an 80 millimetre minus subbase aggregate from the Government of Yukon, Transportation Maintenance Branch. As such, the screening activity no longer will be required.

As mentioned, our role on site was to facilitate the construction activities. Specific details of the events on site are provided below. Also, several photographs which were taken during our management period are depicted in Appendix B.

Although each activity required some input from our site representative, extensive direction was necessary specifically for the design and placement of the temporary drainage trench. Also required was the communication with applicable government authorities to finalize and gain authorization for said design provisions.

Verbal direction was received from George Strynadka to drain the pond and re-route (through the life of the construction) the existing creek near power pole 'D' shown on Figure One in Appendix A. Provision was to be made to avoid excessive sediments entering the lake via suspended solids in the drain water.

In order to satisfy the above objectives, the following steps were taken.

- •determine location of and elevation of lowest point in pond.
- •stake out primary trench location as shown in Figure One in Appendix "A".
- •Move tailings south and west of trench location inside the tailings area (to avoid crossing the trench after it had been excavated).
- •Excavate trench to design grade as shown in Figure Two in Appendix "A".
- •Place rock material along -4.5% grade section for erosion protection.
- •Establish secondary trench using backhoe and then with hand digging.

The trench excavation was delayed when the backhoe unexpectedly hit and damaged the corrugated steel pipe which derives from a highway drainage system (culvert location shown on Figure One). In the specifications, this culvert was assumed to not enter the tailings area. The culvert was damaged at approximately Sta 5+195 on August 17, 1995. A repair crew from Government of Yukon, Transportation Maintenance Branch mobilized to site immediately and had the damaged section repaired by the morning of August 18, 1995. Refer to Photos 10 and 11 for photo documentation. The remaining section of culvert leading toward the highway embankment was identified with a metal detector and the primary trench was rerouted to avoid damaging it again.

The trench was completed on August 25, 1995 and the pond was drained on August 28, 1995. Once the surface water was drained, the contractor was directed to close the secondary trench. This decision was based on the concern that water deriving from the tailings (below the ground surface) may have excessive levels of impurities in solution and of suspended solids which, if drained directly into the lake, would compromise the Land Use Permit and the direction of DIAND, Water Resources (Refer to Appendix C).

The peripheral tailings were excavated and placed within the tailings area and the levelling process was initiated on August 26, 1995.

The levelling of the tailings proved to be difficult due to the presence of saturated fine grained silty sand material. With excessive disturbance induced by machines, the water greatly undermined the structure of the soil and caused water to migrate to the surface through capillary action. This was evident in the letter provided to your organization September 05, 1995 regarding the release of surface water from the tailings area.

The decant pipe was capped on August 30, 1995 with the as-built detail provided as Figure Three in Appendix A.

TESTING DURING CONSTRUCTION

Testing services were performed as required to facilitate the construction activity.

As mentioned, an 80 millimetre minus screened source identified at a government borrow pit was proposed by the contractor to be used as the capillary break material. A grain size analysis was performed with the results displayed in Appendix D. Note that the 80 millimetre source essentially meets the specification provided for the capillary break material. It appears that the sand sizes are coarser than those specified, however, it is recommended that this would be favourable for the intended use of the material.

The proposed material for the clay cap was inspected and sampled for analyses. An Atterberg limit was performed with the following results:

Liquid Limit = 23.1
Plastic Limit = 13.6
Plasticity Index = 9.5
Unified Soil Classification = CL
(Using Casagrandes's Plasticity Chart)

That the material had a strong hydrocarbon odour, a sample was tested for Total Extractable Hydrocarbons and BETX with the results presented in Appendix D. It is understood that your department has retained another consultant for the

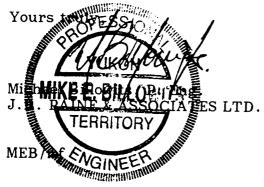
environmental design considerations at this site. As such, it was our intention to provide recent information for your purposes regarding the level of impurities in the proposed material.

CONCLUSIONS

It is envisioned that the information presented herein adequately summarized the construction management services which our firm performed for the Venus Tailings Site Rehabilitation Project.

To supplement this report and to aid in the transfer of management responsibilities, extensive site meeting was held on September 06, 1995. This meeting was successful in ensuring that the contractor and PWC site representative were in understanding of the duties performed to date and of the activities to follow.

Thank you for the opportunity to be of service to your organization. If you should have any questions or comments regarding this summary report, please do not hesitate to contact our office.



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CONSULTING AND TESTING ENGINEERS

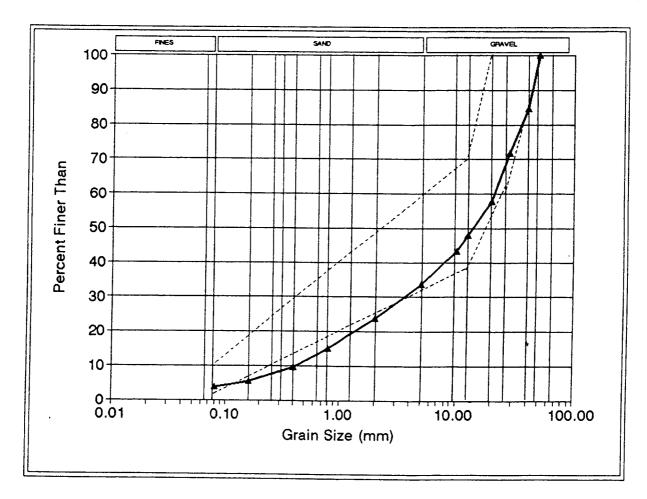
EDMONTON - GRANDE PRAIRIE - WHITEHORSE - PEACE RIVER

GRAIN SIZE ANALYSIS

SAMPLE:	РП-1	CLIENT:	PWGSC, A&ES
DEPTH:	n/a		
LOCATION	80mm stockpile	PROJECT:	VENUS MINE TAILINGS
DATE:	95/8/23		STUDY
MADE BY:	MEB	CHECKED:	

CHARACTERISTICS OF SAMPLE:		
MOIST. CONT.:	1.6	CRUSH COUNT:
% QRAVEL:	66.5	% FRAC. FACES:
% SAND:	29.8	LIQUID LIMIT:
% FINES:	3.7	PLASTIC LIMIT:
DESCRIPTIC	ON OF SAMPLE:	REMARKS:
SANDY GRA	VEL, GW	-sample originated from the 80mm minus sub-
		aggregate stockpile from YTG borrow pit located
		approximately 2 km north of subject site
		-this material proposed for capitlary break

	Size of	% Finer Tha
Sieve No.	Opening	Basis Orig.
	(mm)	Sample
50000	50.0	100.0
40000	40.0	84.4
28000	28.0	71.7
20000	20.0	57.7
14000	14.0	
12500	12.5	47.8
10000	10.0	43.2
5000	5.0	33.5
2000	20	23.7
1250	1.250	
800	0.800	14.8
630	0.630	
315	0.315	
250	0.250	
160	0.160	5.3
80	0.080	37





CONSULTING AND TESTING ENGINEERS

EDMONTON - GRANDE PRAIRIE - WHITEHORSE - PEACE RIVER

ADDRESS ALCOMRESPONDENCE TO.
14 Burns Road
Whitehorse, Yukon
Y1A 4Y9

File No: 8054-12

October 23, 1995

PUBLIC WORKS CANADA Architectural and Engineering Services 1000 Canada Place 9700 Jasper Avenue Edmonton, Alberta T5J 4E2

Attention: Mr. George Strynadka, Senior Project Engineer

Dear Sir:

Re: Venus Mine Tailings Project Construction Management Services

From a grains size analysis (GSA) completed on the proposed capillary break material sample we have estimated the following range of coefficient of permeability.

For a clean well graded sand and gravel mixture, GW, (See attached GSA) a coefficient of permeability would be expected to be between 1.0 to 10⁻² centimetres/second.

This variation in the coefficient may be expected due to variations in fines contents, compactness, hydraulic head, etc..

...\2

We trust the above is suitable for your purpose. If you should have any questions or comments, please feel free to contact the undersigned.

Yours truly,

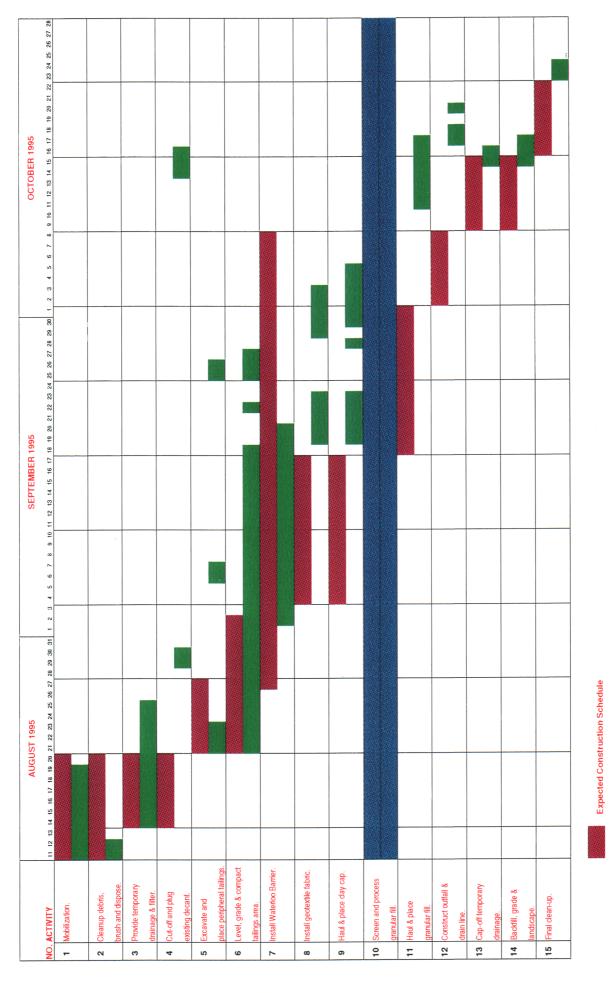
Wilbur C. Koffed, P. Eng.

Office Manager

J.R. PAINE & ASSOCIATES LTD.

WCK/mf

VENUS MINE TAILINGS REMEDIATION: PROJECT WORK SCHEDULE



Activity Omitted from contract

Actual Construction Schedule



Photo 3: Welder Cutting Top of Wall to Design Elevation 8 September 1995



Photo 1: Waterloo Barrier Installation 5 September 1995

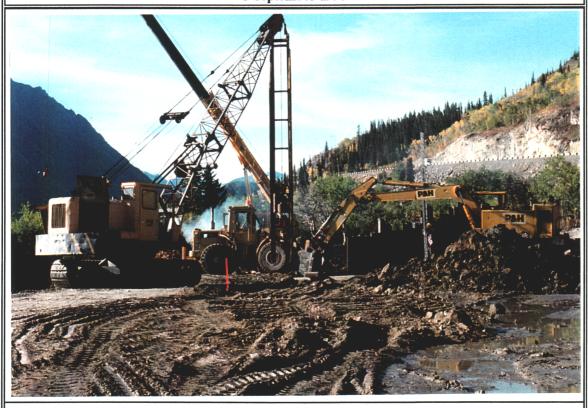


Photo 2: Waterloo Barrier Installation 5 September 1995

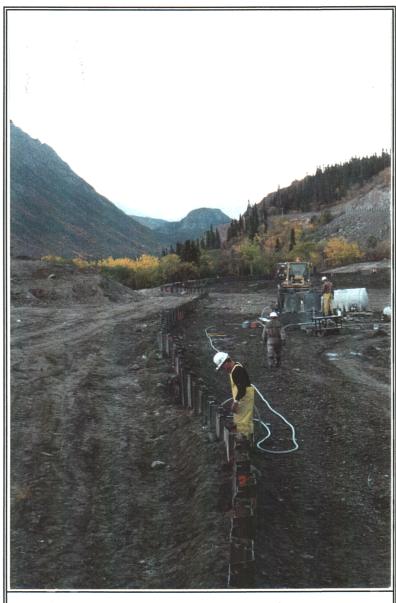


Photo 4: Sealing Wall Joints 18 September, 1995

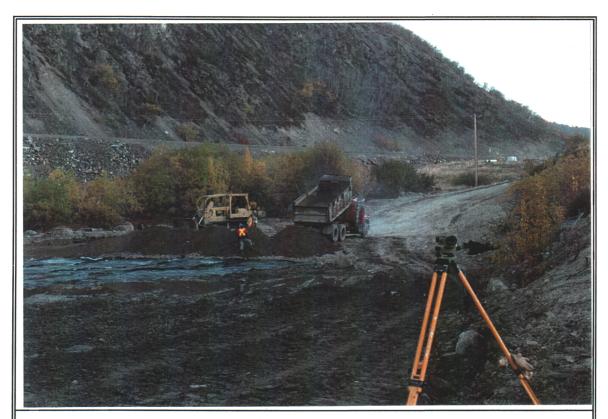


Photo 5: Hauling and Placing of Clay Cap Material
19 September 1995



Photo 6: Placing Clay Layer above Geotextile 2 October 1995

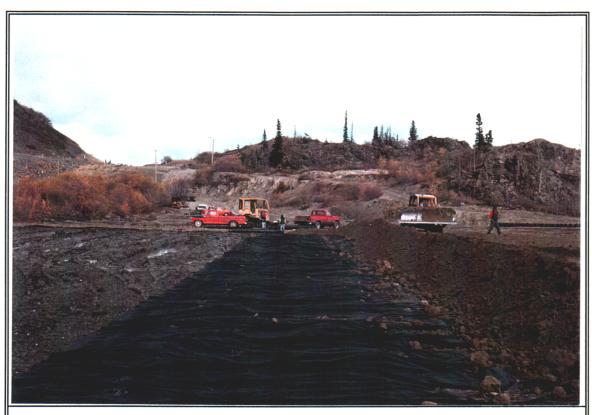


Photo 7: Placing Wind Blown Tailings onto Tailings Area.
7 September 1995



Photo 8: Difficulties during the Levelling of the Tailings 9 September 1995

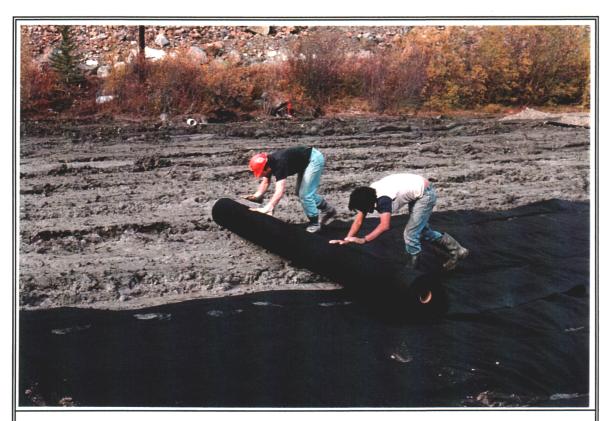


Photo 9: Labourer Placing Geotextile 2 October 1995



Photo 10: Hauling and Placing of Capillary Break Material
11 October 1995

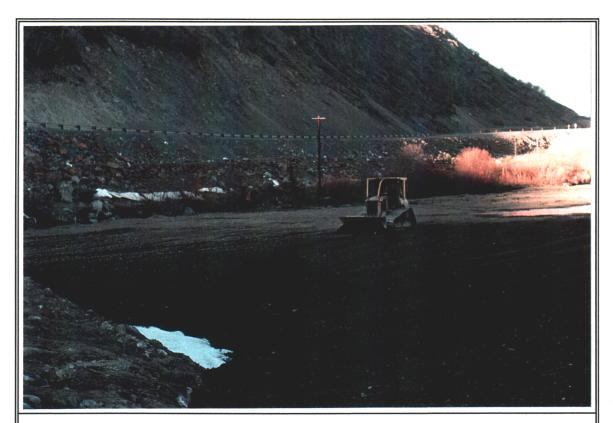


Photo 11: Final Levelling of the Capillary Break Material 17 October 1995



Photo 12: Concrete Plug at Inlet of Decant Pipe 8 September 1995



Photo 13: Filter Dike in Temporary Drainage Ditch 5 September 1995



Photo 14: Highway Culvert Repair 17 September 1995



Photo 15: Excavation for HDPE Pipe



Photo 16: New Pipe Bedding; Old Pipe Alongside



Photo 17: Removal of Section of Old Pipe at Connection Location



Photo 18: Pipe Connections



Photo 19: New Pipe at Outlet through South Wall



Photo 20: Excavation to Locate Old Pipe, Outside Wall

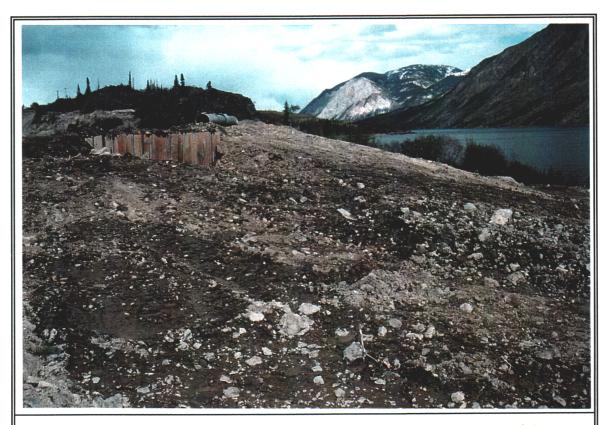


Photo 21: Depressions at South Wall requiring Additional Material



Photo 22: Site in May, 1997

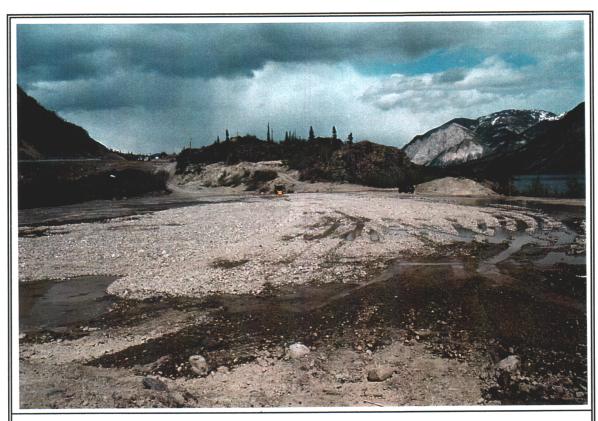


Photo 23: Coarse Material placed in December, 1996

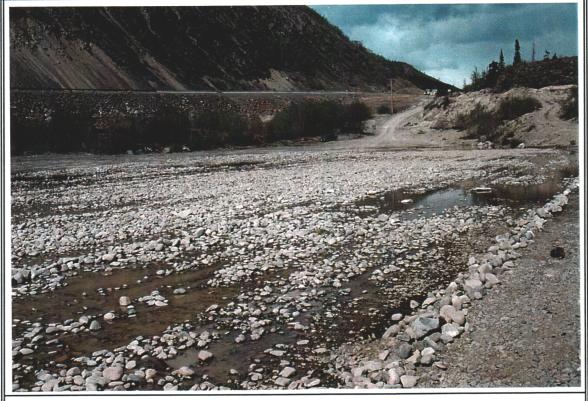


Photo 24: Coarse Material regraded. Final Appearance May, 1997