B.Y.G.
NATURAL RESOURCES INC.

MT. NANSEN GOLD PROJECT

TAILINGS IMPOUNDMENT

Feasibility Design Update

KLOHN-CRIPPEN

PB 5314 03

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KLOHN-CRIPPEN

April 4, 1995

BYG Natural Resources Inc.
208-3190 St. John Street
Port Moody, British Columbia
V3H 2C7

Mr. Jim Smith

Dear Mr. Smith:

Tailings Dam Feasibility Design

Enclosed are two copies of our final report entitled "Mt. Nansen Gold Project, Tailings Impoundment, Feasibility Design Update". As directed by Tom Higgs, and additional twenty five (25) copies have been sent directly to DIAND in Whitehorse, Yukon. The objective of the study was to consider all possible tailings storage sites on the property, and to prepare a feasibility level design for the best alternative. The report briefly appraises three sites which were considered in the past, and studies a fourth site in detail. It is concluded that Site #4 is the best location available, and a preliminary design is presented for Site #4. This report supersedes a previous report dated September 26, 1994.

We have enjoyed working on this challenging project and look forward to seeing the Mt. Nansen Mine brought into production.

Yours truly,

KLOHN-CRIPPEN CONSULTANTS LTD.

Blair Trenholme

Blair S. Trenholme, P.Eng.
Project Manager

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Klohn-Crippen

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DRAWINGS

1. INTRODUCTION

BYG Natural Resources Inc. (BYG) intends to develop an open pit gold mine on the Mt. Nansen property, near Carmacks, Yukon. Klohn-Crippen has been asked by BYG to prepare a feasibility design for a tailings facility for the proposed mine, considering alternatives to the site upon which a preliminary design (Klohn Leonoff 1990) was based. This report presents the results of field investigations carried out at the site during July 1994, and subsequent design work for a tailings facility. The site work was carried out at a tailings dam site on Dome Creek not previously considered, shown as Site #4 on Drawing D-3003.

A preliminary report was prepared in September 1994. Discussion of that report in a meeting held on March 1, 1995 resulted in recommendations for updates to the study. Changes based on that meeting are included in this report, which supersedes the September 1994 report.

1.1 Project Description

The project site is accessed from Carmacks via gravel road and is about 60 km west of Carmacks. The Mt. Nansen Road was used to develop the underground mine on the property which operated for two brief periods in the 1960s and 1970s. The road is also used by a number of prospectors and placer mining operators in the area. Old underground workings, mill buildings, two small tailings ponds, a small water reclaim pond and many bulldozer trenches are still present on the Mt. Nansen property (see Drawing D-3002).

The proposed project will refurbish and utilize the existing mill. The ore to be mined is oxide rather than sulphide ore, and is not expected to be acid-generating. Tailings generated from the oxide orebody will total about 300 000 tonnes, or about 240 000 m^3, assuming a dry unit weight of settled tailings of 1.25 tonnes/m^3. The tailings facility design must accommodate this volume of tailings. Cyanide will be used in the gold recovery process. Cyanide destruction will be used to remove most of the cyanide from the tailings before delivery to the tailings pond.

It is understood that about 600 000 tonnes of waste rock will be mined from the open pit to liberate the ore, and that this waste rock will not be acid-generating. This waste rock is a potential source of construction material for the tailings dam.

1.2 Previous Work

Mr. T. Harper of Klohn Leonoff, inspected the site in September 1985 and submitted a letter-report to Chevron Canada Resources Ltd. on November 7, 1985. This inspection consisted of a preliminary investigation for tailings disposal and for proposed leach pad sites. The report concluded that a tailing storage facility should be located on Dome Creek at a site just below the mill (Site #2, Drawing D-3002).

In 1990, a report was prepared by Klohn Leonoff presenting a preliminary design of a tailings facility located uphill of the mill area (Site #1).

2. SITE CONDITIONS

The minesite is located within the physiographic region known as the Yukon Plateau. The area has typically rounded mountain tops with broad valleys and gentle topographic features. Side slopes of the valleys in the vicinity of the mine vary from 2H:1V to as flat as 6H:1V. Drainage from the minesite and tailings dam locations flows into Dome Creek, a tributary of Victoria Creek, which is part of the Nisling River system. The Nisling River ultimately flows into the Yukon River. The mine elevation is about 1250 m (about 4,100 ft).

Elevations have been determined from an orthophoto provided by BYG Natural Resources Inc. The orthophoto, which is undated, has a contour interval of 10 m and covers the entire property. For preliminary design purposes, a cross section of the valley topography was created using a tape and clinometer (see Drawing D-3003).

2.1 Surficial Geology

Surficial soils in the Dome Creek valley area consist mainly of colluvial, residual and granular glacial outwash soils overlying bedrock. The soil cover is thin on the steeper valley sides, increasing in the valley bottom to about 20 m deep. Upper slopes are covered in a thin veneer of colluvial soils.

Four glacial advances have been defined across the central Yukon Territory. These are, from oldest to youngest, the Nansen, Klaza, Reid and McConnell advances. However, the area was not glaciated during the most recent (Pleistocene) ice age. The Mt. Nansen minesite is situated within the Nansen drift. At least 2,000 years ago, volcanic ash fell on this area up to 30 cm in depth. Remnants of this ash are visible at many locations on the property. The ash occurs at surface or just below the organic soils, and typically has a depth of less than 10 cm. Some glacial till has been noted at depth in the main valley bottom.

The soils vary from a sandy gravel to a fine sandy silt. The material is generally medium dense with some pockets of loose material.

2.2 Bedrock Geology

The bedrock at the site appears to consist of igneous rocks of the Mt. Nansen Group which have intruded into the Pelly Formation metamorphic rocks. The metamorphic rocks have been mapped as undifferentiated schists, gneisses, quartzites and marbles. The bedrock is highly shattered and broken at the ground surface as observed in exploration trenches and test pits. We understand that the degree of shattering does decrease with depth, but the rock is shattered near surface within the area of the tailings pond. The bedrock is a purplish to brown colour. Bedrock is exposed on the ridge tops where there is very little tree or vegetation cover.

2.3 Permafrost

The site lies within the discontinuous permafrost zone, close to the southern boundary of widespread areas of permafrost islands. Because of the high elevation of the site, permafrost is more widespread than is generally true in this region. The -4°C mean annual air isotherm passes through Carmacks. Taking into account the fact that the elevation of the site is between 600 m and 700 m higher than Carmacks, the mean annual air temperature for the site is expected to be at least 2°C colder than that in Carmacks, or at most -6°C, and possibly -8°C (personal communication with Environment Canada). At the time of the site investigation (mid-July 1994), the soils beneath Site #4 were frozen. Where a thick layer of moss exists, such as over most of the north facing side of the valley, the soils were frozen immediately beneath the moss layer. In the sandy terrace soils where the insulating layer of moss does not exist, the soil was thawed to a depth of about 2 m (active zone), below which the soil was solidly frozen. In the areas of sandy terrace soils, only a thin layer of lichen occurs at ground surface, and in some places, sand is exposed over areas of up to tens of square metres.

2.4 Seismicity

The Mt. Nansen minesite lies within a seismically active area of the Canadian north in Seismic Zone 2, as defined by the National Building Code of Canada, 1990. The site lies within the Northern British Columbia (NBC) source zone between the McKenzie (MKZ) zone and the Denali Shakwak (DSK) zone.

A probabilistic assessment of the seismic risk at the site has been undertaken by the Pacific Geoscience Centre for the Mt. Nansen site (October 1988). The results are enclosed in Appendix I. A peak horizontal ground acceleration of approximately 10% g is expected with probability of exceedance no greater than 0.0021, or one in 475 years, while a peak horizontal acceleration of 12% g is expected with a return period of .001, or one in 1,000 years.

The tailings dam will be founded on medium dense granular soils overlying bedrock. Extensive deposits of loose soils, if they exist, will be removed from the foundation to minimize any potential for liquefaction under earthquake loading.

2.5 Climate

The mean annual precipitation for the project site is about 270 mm. Snow begins falling in October or November and usually remains on the ground until May. The typical snowpack is about 1 m. Approximately 40% of the precipitation falls as snow. Some rainfall occurs as early as April, but the majority of rainfall occurs from June to August. The most intense rainfall occurs in July.

3. TAILINGS DAM SITE SELECTION

3.1 General

Three potential dam sites (Site #1, Site #2 and Site #3 - see Drawing D-3002) have been considered in the past. Those three sites are all located on relatively steep slopes and offer relatively low storage volumes in proportion to the size of the dams required. Because of the lack of permafrost in the foundations, Site #1 was previously chosen as the best of the three. Sites #1 to #3 are described in detail in previous reports (see Klohn Leonoff, 1988 and 1990).

3.2 Site #4

Part of the scope of the current study was to investigate the entire property for additional potential tailings dam sites. A new location, named Site #4 (see Drawing D-3002 and Drawing D-3003) was identified on Dome Creek, downstream of the previously identified sites. Although the site does have frozen foundation soils, it is superior to the other sites (1, 2 and 3) in the following respects:

- Site #4 offers the smallest dam volume for the tailings volume stored. The three other sites examined are all on relatively steep slopes and offer low storage volumes in proportion to the size of the dams.
- A relatively low dam is required to impound the necessary tonnage of tailings. In addition to the improved costs, the dam height improves stability and reduces potential seepage.
- Because of a natural restriction of the valley at Site #4, the volume of the dam is relatively low.
- Good capacity to increase storage with modest future dam construction. This would reduce the number of locations for tailings storage if additional reserves are confirmed in the future.
- Source of granular construction materials close to site.

- Potential to locate a closure spillway in bedrock.
- The location lies downstream of all existing and future mining impacts of the Dome Creek drainage system, thereby offering an excellent monitoring and control point.

3.3 Site 4 Conditions

Site #4 is located in the Dome Creek valley at about elevation 1130 m. Topographically, Site #4 appears to be the best available site on the property. The south side of the valley (right abutment) is quite steep (slopes of about 3:1 on the abutment and 2:1 higher on the slope). On the north side of the stream, there is a sand terrace, with its top elevation about 12 m above the creek level (see Drawing D-3003).

Three boreholes were drilled and 14 test pits were dug in the area of Site #4 during the July, 1994 site investigation. The locations of the test pits and boreholes are shown in plan and section on Drawing D-3003. Test pit locations in Drawing D-3003 are estimated, and borehole locations are surveyed. The boreholes were drilled with a Nodwell mounted CME-750 rig using solid stem augers. Sampling was carried out using a CRREL (Cold Regions Research Engineering Laboratory, US Department of the Army, Hanover, NH) tube sampler which produced cores of 7.6 cm (3 inch) diameter. Because all of the holes drilled were in frozen ground, no SPT tests were carried out. Drawing D-3003 gives a sectional interpretation of the foundation geology along the proposed dam centreline. Test pit logs and borehole logs are included in Appendix II. No test pits were dug south of the creek because it was considered too risky to attempt access across the creek with the backhoe.

In natural outcrops and where exposed in test pits and trenches, bedrock is highly fractured. This is a result of freeze thaw action and is accentuated in this area of the Yukon which was not glaciated in Pleistocene times.

3.3.0.1 Soil Conditions

A layer of apparent glacial till exists over bedrock in the deepest part of the valley. The till is typically a silty fine sand with numerous angular to subrounded pebbles and cobbles. The till is frozen to the maximum depth of 20 m drilled at the site.

Overlying the glacial till is a grey silty fine to medium sandy material up to about 15 m thick and frozen. The fines content of the silty grey sand varies between about 10% and 40%. Within this silty sand, silt layers of varying organic content were observed. More organic-rich soils were noted on the right abutment than on the left abutment or in the valley centre. The more highly organic layers contain higher percentages of fines, a higher ice content, and exhibit a distinctive organic odour when thawed. The grey sand exists immediately below surface in most of the area and, where present at surface, it is generally covered by a thick layer (about 20 cm to 30 cm) of moss. The active layer in this unit is very shallow. In mid-July 1994, the soil immediately below the moss layer was frozen.

Terraces of clean, well rounded fine to medium sand occur along the sides of the valley in some areas. The left (north) abutment of Site #4 is formed on one of these terraces. The local sand terrace deposits are apparently remnants of more extensive deposits which once filled the valley bottom. They consist of fine to medium sand with about 5% to 10% fines. Cross bedding, indicating that the sand was originally deposited in water, is evident in test pits and drill core samples. The terrace sands are well drained and frozen. The active layer in the terrace sands is deeper than in the finer-grained soils because of the thinner cover of moss on the ground surface (typically 10 cm) and lower water content of the sand. In mid-July 1994, this soil horizon was thawed to a depth of about 1.5 m to 2.0 m.

Minor thicknesses of organic soils (usually less than about 15 cm) occur at surface in most areas. Along the creek in the valley centre, peat of up to about 0.9 m was encountered. Moss covers the ground surface throughout the Site #4 area, except on the terrace sand deposits where aspen trees and lichens indicate the better drainage provided by the sandy soil.

3.3.0.2 Permafrost Conditions

The frozen terrace sands below the active layer are well-bonded with no visible ice. Sands with excess ice and ice crystals were encountered in the zone of seasonal thaw penetration which is estimated to extend to a depth of 2.5 m. Occasional layers were also encountered in this zone. The water content of the frozen sands ranged between 15% and 20% at depth, with values as high as 35% within the zone of seasonal thaw. Water contents greater than about 15% indicate that excess ice is present in the sands.

At all depths, ice crystals were observed in the frozen silty sands. Thin ice lenses up to 1 mm thick were found in the silty organic layers present within the sand unit. The water content of the silty sand generally ranged between 20% and 60%. High water contents up to 150% were measured in ice-rich organic layers.

The ice conditions in the basal till unit are expected to be similar to the clean terrace sands.

Ground temperature measurements in the region of the site indicate that the ambient temperature of the permafrost is about -4°C between the depths of 4 m and 15 m. This temperature is consistent with thermal modelling of the site and the frozen condition of soil samples recovered in drill holes. The low ground temperature indicates that the permafrost is well-established and stable under present conditions.

As discussed below, changes in the thermal regime at the tailings impoundment site could cause the foundation soils to thaw. To limit the thaw settlement, below the tailings dam, the upper 2.5 m of seasonally thawing soils will be excavated beneath the dam footprint. The thaw settlements in the deeper soils is estimated to average up to 7% of the total depth of the terrace sands, and up to 20% of the depth of the silty sands. The resulting total ground subsidence below the dam could be as high as 1.3 m to 1.6 m. The tailings dam will be constructed to allow for these possible settlements.

3.4 Comparison of Sites

Approximate dam volumes were calculated for Site #1, Site #2 and Site #4 to provide a rough comparison of the three sites on the basis of construction volumes. Previous work (Klohn Leonoff, 1990) determined that a dam of about 20 m in height would be required at either Site #1 or Site #2 to store approximately 300 000 tonnes of tailings. The approximate dam height required for storage of a similar volume at Site #4 is 12 m. Table 3.1 shows approximate construction volumes for the three options.

Table 3.1 Comparison of Construction Volumes for Site #1, Site #2 and Site #4

SITE	APPROXIMATE CONSTRUCTION VOLUME
Site #1	115 000 m^3 to 140 000 m^3
Site #2	125 000 m^3 to 150 000 m^3
Site #4	50 000 m^3 to 65 000 m^3

Without carrying out detailed cost analysis, it can be seen that Site #4 is the best choice of the three sites under consideration for a tailings facility, because the construction fill volume would be roughly half of that for the other two sites. All further analysis and design work will be directed at Site #4.

4. TAILINGS DAM DESIGN

4.1 General

A tailings facility capable of storing 300 000 tonnes of tailings is required. Based on the best topographic map available (10 m contours), a storage-elevation curve was drawn for Site #4 to determine the probable height of dam required. It appears that a dam approximately 12 m high will be required to store the 300 000 tonnes. In addition, freeboard of about 2 m was assumed for preliminary design purposes, resulting in a total dam height of about 14 m. Additional freeboard to accommodate long-term thaw settlement of the foundations soils may be added in final design. These values are preliminary, subject to a more detailed topographic survey of the impoundment area.

The dam would be constructed primarily of the silty fine to medium sand available on site. Because of its well drained nature, it is a material well suited for excavation and compaction.

The evidence of case histories for water retaining dams constructed on permafrost shows that permanently frozen dams can be constructed under conditions where the dam height is less than 10 m and the annual air temperature is -8°C, or less. For greater dam heights and for warmer mean air temperatures, thawing of the permafrost in the underlying foundation soils will advance from the reservoir side of the dam, unless artificial freezing of the dam is implemented. Because the maximum tailings dam height is 14 m and the mean annual air temperature at the site is between -6°C and -8°C, it is anticipated that thawing of the foundation soils below the tailings dam will, at minimum, occur beneath the middle of the dam. It is possible that the foundation soils below the dam abutments may remain frozen, especially for sections of the dam above the final tailings pond level. However, it is conservatively assumed for design that complete thawing of the foundation soils across the full length of the dam could occur.

Non-uniform thaw settlements below the tailings dam are expected because of the varied soil conditions across the site. In addition, the thawing of the soils is expected to progress from the centre of the dam outwards to the dam abutments as the pond level rises. The resulting differential settlements below the dam could lead to tension cracks in the dam fill, particularly in the upper half of the dam. The use of the cohesionless terrace sands for dam construction will mitigate against cracking because of the ability of sands to self-heal tension cracks. Furthermore, the tailings deposited against the upstream face of the dam will provide a source of material to plug and seal cracks. As a precautionary measure against pond seepage through cracks formed during the operating life of the impoundment, a geosynthetic clay liner will be installed in the upstream face of the dam. On closure, a minimum beach width of 50 m will be provided against the upstream side of the dam to minimize seepage.

Appropriate placement and compaction of the dam fill material will ensure adequate strength of the structure itself. Stability of the dam will be affected by the rate of thawing and pore pressures generated in the permafrost beneath the dam. As well, thawed zones of the foundation sands may be susceptible to liquefaction under seismic conditions. To ensure adequate stability of the dam under thawing and seismic conditions, a dam with gentle side-slopes is specified to ensure stability and limit deformations.

A one-dimensional thermal analysis has been carried out to assess the thermal conditions following dam construction. Stability analyses have been carried out for the above cases (frozen and unfrozen). The thermal and stability analyses, and the required dam cross sections are discussed in the following sections.

4.2 Thermal Analysis

A one-dimensional thermal analysis was carried out for the dam using the computer program THERM1 (Nixon, 1990). The program uses the finite difference method to solve one-dimensional heat transfer problems in soils with freezing or thawing. A wide-crested tailings dam can be considered as a one-dimensional problem. The program produces data which has been plotted (see Appendix III) to illustrate the variation of temperature with depth over the course of the year. The primary intent of the modelling is to determine the depth of the active layer in the dam and/or foundations. The active layer is determined as the soil which, at some time of the year, reaches a temperature at or above the freezing point. The active layer freezes each winter and below the active layer, the soil is assumed to remain permanently frozen.

The modelling program requires input data including mean monthly air temperatures throughout the year. Detailed temperature data are available for Carmacks, 700 m lower than the site. Based on discussions with Environment Canada personnel in their Vancouver weather office, adjustments were made to the Carmacks data to account for the higher elevation of the site. Initially, average values of 4°C less than the Carmacks data were used. However, Carmacks data less 3°C produced results more closely matching those observed on site. Consequently, 3°C less than the Carmacks data was adopted for subsequent modelling.

To calibrate the model, input values including soil parameters and temperature data were adjusted until results agreed with observed field conditions. For the clean terrace sand, which is the preferred construction material, an active layer of about 2 m to 3 m is expected to develop, as seen in the in situ deposits. Where the silty grey sand exists at surface, the modelling shows an active layer of less than about 0.5 m, as observed on the right abutment.

Based on the above results, it is concluded that the active layer in the dam may penetrate to about 3 m below the crest elevation. Where the dam height lessens on the abutments, there is potential for the active layer to penetrate into the foundations. On the left abutment, where the foundations are formed in clean terrace sand, or rocky colluvium, this will not be a problem. However, on the right abutment and valley bottom, and part of the left abutment beneath the low section of the dam, some fine-grained, ice-rich soils exist in the foundations. To avoid thawing of fine-grained, potentially ice-rich soils, raising of the crest will be required in these areas. By providing a minimum fill thickness of 4.0 m in all areas of fine grained soils where the foundation surface is at or below the design maximum pond elevation, thawing of these critical zones can be avoided.

4.3 Stability Analysis

Unfrozen Dam Condition

Stability analyses were carried out to determine the cross sectional geometry required to ensure adequate stability of the dam under static and seismic conditions, for the worst case (unlikely) where both the dam and the foundations are thawed.

For the chosen cross sectional geometry, the minimum factor of safety against failure under static conditions is about 2.2.

A stability analysis has been carried out to assess the possibility of failure for a case where foundation soils thaw. This could result in loose sands which may be subject to liquefaction under seismic conditions. Details of the analysis are given in Appendix IV. The results indicate that, to achieve a factor of safety of 1.1, considered reasonable for this case, requires a dam with a base width of at least 80 m. The dam configuration given in Drawing D-3003 meets the necessary criteria, with a base width of about 90 m.

Frozen Dam Condition

A relatively broad-crested dam is required to avoid three-dimensional heating effects and allow freezing of the dam. It is generally accepted in the literature that a dam width to height ratio of about 3:1 is acceptable. The width is taken as the horizontal distance between upstream and downstream faces of the dam at the elevation of the pond water level. In a situation where a tailings beach exists against the dam, the horizontal thickness of the tailings can be included in the calculation. If we assume that the tailings beach is developed to within 1.0 m of the dam crest elevation, and the freeboard above the pond level is 2.0 m, then, the horizontal tailings thickness will be about 100 m. Adding his 100 m to the horizontal dam width at this elevation provides an adequate effective dam width. Consequently, a conventional dam crest width of about 6 m would be acceptable. These calculations are conservative, because the pond level would normally be kept much lower than 2 m below the dam crest.

4.4 Dam Cross Section

The stability analyses were carried out to determine geometric design parameters for the dam under thawing and seismic conditions. The following basic cross sectional geometry has been chosen:

▸ Crest Width	6 m
▸ Upstream Slope Angle	2.5H:1V
▸ Downstream Slope Angle	3.5H:1V
▸ Minimum fill thickness over foundation soils	4.0 m

In addition to the above, upstream and downstream berms are specified at the toe of the dam. These berms will be 4 m thick and up to 10 m wide. The purpose of the berms is to control the rate of thawing in the foundation soils below the dam and to increase the stability of the dam. Drawing D-3004 illustrates the proposed cross sectional geometry of the dam.

The dam will be constructed as a homogeneous earthfill structure using the fine to medium grained terrace sand borrowed from the area downstream of the dam. Grain size tests indicate that this sand contains up to about 10% silt. The siltier grey sand located beneath the terrace deposit is also suitable for construction, but, because of poorer drainage, contains more ice and therefore may be more difficult to excavate and compact. Test pits indicated that in July, the terrace sands were thawed to a depth of about 2 m and that the grey silty sands (insulated with moss) were thawed to a depth of only about 0.5 m or less.

The dam foundations will be excavated to below the active zone, to a depth of up to 2.5 m to limit the thaw settlement below the dam. Below this depth, no significant ice lenses were noted in drill holes, except on the right abutment. Within the active zone, significant ice was noted in drill cuttings and test pits.

Erosion protection will be provided on the downstream face of the dam, on the crest, and on the upstream face above the tailings beach. Waste rock from the open pit will be suitable for this purpose. A layer of rock about 0.5 m thick will be sufficient.

4.5 Spillway and Water Diversions

The tailings facility will require an emergency spillway during mine operation to avoid any potential for overtopping of the dam during extreme storm events. The emergency spillway would be upgraded to a permanent spillway following closure of the mine. At that time, because water discharge from the system would be acceptable (following degradation of any remaining cyanide), Dome Creek would be allowed to flow through the pond and over the spillway.

It appears that the best location for the spillway is on the left (north) abutment. Overburden depths are relatively shallow in that area, probably allowing the spillway crest to be developed in bedrock. Overburden in the area consists of terrace sands and rocky colluvium. Development of the spillway trench in these soil types will avoid problems associated with open excavations in permafrost-rich fine grained soils. Portions of the spillway, such as the outlet channel, to be excavated in sandy soils would require riprap available from the open pit waste. A preliminary alignment and typical cross section for the spillway are shown on Drawing D-3003.

Alternatively, the spillway may be developed in the right abutment. Because of the steep slopes, neither the drill or the backhoe could access this area during the 1994 site investigation. However, if soil conditions permit, a spillway on the right abutment may require a smaller excavation than on the left abutment. Further site investigation will be required to determine overburden depths and the soil types in the area south of the dam (right abutment) to confirm feasibility of this option.

Hydrology aspects of the spillway are discussed in Section 5.

4.6 Seepage Control

It is understood that, during mine operation, cyanide destruction will take place in the mill prior to tailings discharge to the tailings pond. However, some cyanide may remain in the tailings and it will be desirable to maintain a zero discharge system. For this reason seepage should be minimized through the dam. The dam, being built from fine to medium sand with a low percentage of fines, will be a semi-pervious structure. A geosynthetic clay layer is provided on the upstream side of the dam to limit seepage. The tailings to be stored in the impoundment will be quite fine due to the grind in the mill and the high proportion of clay minerals in the ore. By developing a tailings beach on the upstream face of the dam, a very low-permeability blanket will be added to the dam to further reduce seepage.

A seepage analysis was carried out using the two-dimensional finite element computer program SEEP/W. The analysis was run with no clay liner and 5 m of thawed foundation soils below the dam. The results of the seepage analysis (see Appendix V) indicate that the dam will be well drained with all seepage occurring in the lowermost 1 m of the dam. Total seepage through the dam and thawed foundation soils is estimated to be less than 1 ℓ/sec. This is dependant on development of a tailings beach on the upstream face of the dam. Hydraulic conductivities of the various materials used in the analysis are given in Table 4.1.

Table 4.1 Summary of Hydraulic Parameters Used in Seepage Analysis

MATERIAL DESCRIPTION	HYDRAULIC CONDUCTIVITY
Deep foundation soils - will remain frozen and essentially impermeable	1 x 10^{-9} m/s
Shallow foundation soils - assumed to be thawed to a depth of about 5 m - consist of fine to medium sands with varying silt content	1 x 10^{-5} m/s
Dam - compacted clean fine to medium sand with up to about 10% fines	1 x 10^{-4} m/s
Tailings - high fines content - permeability may be as low as 1 x 10^{-7} m/s	1 x 10^{-6} m/s

4.7 Tailings Design Summary

A summary of the major points in the design of the tailings pond are as follows:

- The dam will be designed to contain 300 000 tonnes of tailings, plus provide 2 m of freeboard, designed to meet a 200-year return period wet year, and a 10-year return dry year. Additional freeboard may be provided in final design to accommodate long-term thaw settlement.

- Construction materials will be sourced on site. The bulk of the required material will be composed of the fine to medium grained terrace sand.

- A geosynthetic clay liner will be provided on the upstream side of the dam to minimize seepage through the dam during operation and to guard against increased seepage caused by cracking of the dam. Cracking of the tailings dam is expected because of differential thaw settlement of the foundation soils. The effects of cracking during the operating life are mitigated by using cohesionless fills, the provision of a geosynthetic clay liner, and blanketing the upstream face of the dam with tailings. A minimum beach width of 50 m will be provided at closure as further protection against potential seepage and piping.

- Potential seepage will be intercepted by a pond downstream of the dam proper. Seepage will be reclaimed from this pond and returned to the main impoundment, if necessary, on a continuous basis.
- A diversion channel will be incorporated into the pond design, to divert as much natural drainage as possible around the system.
- Based on average precipitation years, the pond could operate through the projected three year life of the operation with a release to the environment required in Year 3.

5. HYDROLOGY AND WATER MANAGEMENT

5.1 Climate and Extreme Events

Feasibility level hydrological studies were carried out by Klohn Leonoff (Klohn Leonoff 1988 and 1990). The following information was extracted from these studies unless otherwise noted.

Climatological data has been obtained from the nearest Environment Canada meteorological station, No. 2100300, which is located 60 km east of the site at Carmacks. The weather station is at an elevation of 524 m, 776 m below the minesite elevation of 1300 m. Precipitation data from this station were used for the water balance studies. Evaporation data was obtained from Fort Selkirk, Environment Canada Station No. 2100600, located approximately 80 km northwest of the minesite at elevation 454 m.

Precipitation at Mt. Nansen falls in the form of both rain and snow. Snow begins falling in November and remains on the ground until May. We understand that typically, a snowpack of 1 m occurs. Approximately 40% of the annual precipitation falls as snow. Some rainfall occurs as early as April, but the majority of rainfall occurs from June to August. The most intense rainfall occurs in July. Mean annual precipitation values on a monthly basis are summarized in Table 5.1 along with a 200-year return period wet year and a 10-year return period dry year.

The evaporation data for Fort Selkirk is presented in Table 5.1. The highest evaporation rate occurs in June. Water losses due to evaporation drop off significantly in the winter as temperature drops. During the summer months of May through August, evaporation is nearly five times the value of the average precipitation.

Table 5.1 Summary of Monthly Precipitation and Evaporation

MONTH	EVAPORATION	PRECIPITATION		
	Mean Monthly (mm/month)	Mean Year (mm/month)	10-Year Return Period Dry Year (mm/month)	200-Year Return Period Wet Year (mm/month)
January	0.0	19.0	14.0	25.9
February	0.0	13.6	10.0	18.5
March	0.0	10.8	8.0	14.8
April	0.0	8.1	6.0	11.1
May	107.6	16.3	12.0	22.2
June	120.3	40.7	30.0	55.5
July	108.0	46.1	34.0	62.9
August	79.8	35.2	26.0	48.1
September	37.2	27.1	20.0	37.0
October	0.0	19.0	14.0	25.9
November	0.0	19.0	14.0	25.9
December	0.0	16.3	12.0	22.2
TOTAL	452.9	271.0	200.0	370.0

For diversion channel design and preliminary sizing of the operational emergency spillway a 200-year return period one hour rain storm was developed from the data at Carmacks and is presented in Table 5.2. This high intensity storm is expected to occur in July when no snow is on the ground. Thus no allowance was made for snow-melt during this event. Rain on snow events are not expected to be as severe.

Table 5.2 One-Hour 200-Year Return Period Storm

TIME (minutes)	INTENSITY (mm/hr)
5	5.2
10	5.2
15	5.2
20	5.2
25	5.6
30	30.6
35	121.2
40	30.6
45	5.6
50	5.6
55	5.2
60	5.2

For the purposes of preliminary sizing of a closure spillway a statistical Probable Maximum Precipitation (PMP) was estimated using data from Carmacks. This methodology (National Research Council of Canada) uses the mean and standard deviation of the annual extreme precipitation values. The resulting 1 hour, 6 hour and 24 hour PMP rainfall depths were 63 mm, 76 mm, and 108 mm. These estimates are adequate for this feasibility level study. For final design a detailed site specific PMP and Probable Maximum Flood (PMF) study may be required, including an assessment of seasonal variation and maximized snowpack conditions.

5.2 Diversion Channel Design

To divert the flow of Dome Creek around the tailings pond, a diversion channel could be constructed on the left abutment of the dam, as shown on Drawing D-3003. A catchment area of approximately 2.26 km^2 contributes flow to the diversion channel. Based on the 200-year return period 1 hour storm, the peak discharge in the channel was estimated to be 9.1 m^3/s. A trapezoidal channel 3 m wide at the base, 2 m deep with 2H:1V side slopes and a longitudinal slope of 0.1% is adequate to convey the peak discharge. Lining of the channel would not be required since flow velocities are estimated to be 1.1 m/s. The channel will tie into the spillway outlet channel. It would be possible to construct an outlet from the channel into the tailings pond to allow water into the pond if a water deficit were to occur.

In the spring, when snow-melt begins or when infrequent rainstorms may occur, excessive ice, snow and snow drifts must be cleared from the channels to allow for the safe diversion of surface runoff. Every spring and fall, the channel must be checked for vegetation build-up and subsidence due to frost action. Either of these may render the channels useless for runoff control and therefore must be monitored.

5.3 Spillway Design

As discussed in the following section on water balance, it may be possible to manage the water resources to minimize or eliminate discharge during operation. A spillway is required to prevent dam overtopping during an extreme inflow flood event. With the proposed diversion channel, the pond catchment area will be approximately 0.5 km^2. The estimated peak flood inflow resulting from a 200-year return period rainfall event is 2.9 m^3/s. A 3 m wide spillway could carry this discharge with a flow depth of 0.7 m.

If the diversion channel were not constructed, the resulting pond catchment area would be 2.76 km^2 and the estimated 200-year flood inflow would be 11.1 m^3/s. A spillway 5 m wide with a flow depth of 1.2 m could release this discharge. Alternatively, a spillway 10 m wide with a flow depth of 0.8 m would also be adequate.

For mine closure, a closure spillway will be required which is capable of passing the PMF. Using the Rational Method with a runoff coefficient of 0.7, the 1 hour PMP of 63 mm and a catchment area of 2.76 km^2 (including the pond area of 0.04 km^2), resulted in a peak PMF inflow of 34 m^3/s. This is an approximate value for this pre-feasibility level of study. Further studies would be required for detailed design of the closure spillway. To carry this discharge, a closure spillway 10 m wide would have a depth of flow of 1.6 m.

As shown on Drawing D-3003, the spillway has been located on the left abutment. This is subject to the field confirmation of bedrock location on this abutment. The location of the spillway should be reevaluated if, based on additional field investigation, bedrock and soil conditions are more favourable on the right abutment. Based on the studies presented, we recommend that an operational spillway 5 m wide be constructed. The invert of this spillway should be set a minimum of 1.7 m below the crest of the dam, thus providing approximately 0.5 m of freeboard during a 200-year return period flood. Upon mine closure, this spillway could be widened or deepened to provide discharge capacity for the PMF. Alternatively, the dam could be raised approximately 1.5 m to provide sufficient discharge capacity to pass the PMF with the 5 m wide spillway.

A waste rock lined spillway discharge channel is required to carry the spillway flow down the slope and into Dome Creek. The diversion channel could tie into the spillway discharge channel downstream of the spillway crest.

5.4 Water Balance

A preliminary water balance was carried out to determine if a diversion ditch was required to minimize discharge from the pond. Using annual water volumes it was determined that a small surplus of water would result if a diversion ditch was constructed. Based on this analysis, a monthly water balance analysis, including a diversion ditch, was carried out and is presented in Appendix VI. For final design purposes, refinements to the monthly water balance including detailed mill water requirements should be carried out to determine the variation in pond level to ensure sufficient freeboard during operation and to minimize discharge. The water balance assumes a water reclaim system would be used continuously, to recycle water to the mill, so there is no net addition of water from the mill. Domestic and sewage water, which would be discharged with the tailings, have not been accounted for. However, their volumes would be small compared to the other factors and would not have a significant effect on this level of water balance calculation.

The annual precipitation values of 271 mm, 370 mm and 200 mm, corresponding to mean year, 200-year wet year, and 10-year dry year, were used. A catchment runoff coefficient of 0.6 was used for the mean and dry years while a value of 0.8 was used for the wet year. The natural pond catchment area was estimated to be 0.46 km^2, with the Dome Creek diversion channel in place. Without the diversion channel in place, the natural pond catchment area would increase to 2.72 km^2. The pond area was estimated to be 0.04 km^2 for this preliminary monthly analysis. An annual evaporation of 452.9 mm was used. Seepage losses were assumed to be zero for this level of study. Since information was not available on tailings transport water nor reclaim requirements, these were not accounted for in the water balance. These must be accounted for at the next level of design. The loss of water to voids was estimated to be approximately 40 000 m^3/year based on a daily deposition rate of 274 tonnes/day, in-place dry density of 1.25 tonnes/m^3 and a specific gravity of 2.75. A volume of tailings of 80 000 m^3/yr was assumed to enter the tailings pond raising the pond water level.

The results of the monthly water balance are shown in Appendix VI. Results indicate that, with a stream diversion in place, there may be an annual net gain of water in the pond of about 20 000 m^3 to 37 000 m^3, in an average year. The pond level rises from a starting level of El. 1137 m in August of Year 1 to El. 1148.3 m at the end of July in Year 3. In the winter months the monthly water balance indicates a water deficit. Once tailings transport water and reclaim requirements are known, the pond level water level in the fall must be estimated to ensure that sufficient water is available to supply the reclaim requirements over winter.

During a wet year, a surplus of about 100 000 m^3 may result. This translates into a pond rise, above average levels, of 1 m to 2 m assuming no spillage of water from the pond. In a dry year, close to zero excess water would result along with pond levels less than 1 m below average levels. Based on the water balance analysis, if a diversion channel is not constructed, then under average conditions an excess of approximately 400 000 m^3 could result.

To minimize excess water, we recommend construction of the Dome Creek diversion channel. During a dry year water could be spilled from the diversion channel into the pond to add water, if required. It is recommended that, for final design, refinements to the monthly water balance be carried to include slurry transport water and reclaim water.

Excess water would be discharged to Dome Creek, and may require treatment to meet water quality guidelines. Assessment of water chemistry and treatment is beyond the scope of this report. We understand that these questions are being addressed by others.

5.5 Seepage Collection

There may be some seepage through the dam, particularly in the early part of the operation, prior to freezing of the dam. If the quality of seepage water is unacceptable, a small seepage recovery pond may be required to catch any seepage and allow it to be pumped back into the pond.

A preliminary design for the seepage collection dam has been prepared and is presented in Drawing D-3003. The dam would be built of compacted sand, from the same borrow as the main dam. The dam would be about 2 m high above original topography, and would be founded in an excavation about 1.5 m deep.

Both the impoundment and the dam will be lined with an impermeable geosynthetic membrane to eliminate seepage. The membrane would be anchored in a trench extending below the active zone into permanently frozen ground to provide a positive cutoff.

A sump is provided at the upstream toe of the dam. Water would be pumped from the sump back to the main tailings impoundment.

The seepage recovery impoundment would be required to be able to store the runoff from a design storm. To minimize this requirement, diversion ditches would be provided to divert slope runoff from adjacent valley sides. Only seepage and runoff from the immediate area and main dam would be collected. Calculations indicate that a dam 2 m above original ground would provide adequate storage. This conceptual design will be refined as part of final design.

6. POND OPERATION

To avoid seepage through the thawed portion of the dam (active zone) the pond level should be kept at least 3 m below the dam crest elevation. This value (3 m) may be adjusted based on monitoring of the active zone as the permafrost develops in the dam. However, the tailings beach can be developed above pond level, essentially up to dam crest elevation, to reduce seepage.

Summer Operation

To reduce the permeability of the dam and to increase the effective horizontal width of the dam, a tailings beach will be developed against the upstream face of the dam by spigotting tailings from the crest of the dam. Tailings will be spigotted from the dam during the period from May to September.

Water separated from the tailings slurry will form a pond at the upstream end of the impoundment where it can be reclaimed for use at the mill. A minimum water depth of 4.0 m will be maintained in the pond to allow enough depth to float the pump station, to allow the fines to settle, and to facilitate winter tailings deposition as discussed below.

Winter Operation

During the winter months, ice lens formation or glaciation in the tailings would reduce the storage capacity of the impoundment and reduce the volume of reclaim water. To avoid these problems, subaqueous deposition of the tailings through the ice-covered pond will be carried out during the winter months. Sufficient excess water should be stored in the pond at the end of summer to ensure sufficient reclaim water over winter.

Placement of the tailings sub-aqueously in the tailings pond will reduce the depth of water at the reclaim barge and displace water further up the tailings beach in front of the dam in the beach areas. Controlled spigotting in the summer will be carried out to re-create the beach width in front of the dam and to increase the depth of water in the tailings pond.

7. QUALITY ASSURANCE/QUALITY CONTROL

The tailings impoundment will be designed and constructed under the close scrutiny of BYG's geotechnical consultants to ensure that a safe, reliable facility is in place prior to start-up of operations. Key features of the QA/QC program will include:

- Detailed engineering will be completed prior to start of construction. The detailed engineering will include final water balance calculations, stability analyses, confirming design dam section and dimensions and identifying borrow sources. Detailed technical specifications and a detailed construction schedule will be prepared.
- All site work on the tailings dam will be carried out under the geotechnical consultant's supervision. Stripping of dam foundations will be approved prior to fill placement. All fill materials will be inspected and approved for placement, including regular water content and grain size analyses and Proctor compaction testing. Regular in-situ density testing of the fills will be carried out to ensure compaction meets specification. Excavation and erosion protection of diversion channels will be monitored.
- An as-built report of the tailings dam will be prepared to document and confirm that the facility is constructed according to design.
- Instrumentation will be installed to monitor geotechnical performance of the structure. Instrumentation will include crest settlement survey hubs and piezometers and thermistors in foundation soils. As well, seepage flows will be measured regularly and the pond water and tailings levels will be measured to confirm the water balance.
- Annual inspections will be made during operation to inspect the condition of the structures and to ascertain the facility is being operated according to the design. Annual reports will be prepared.

8. CONCLUSIONS AND RECOMMENDATIONS

The following summary and conclusions have been drawn from the study:

- Of the four sites studied to date, Site #4 is the most attractive site for development of a tailings storage dam.
- It is both technically feasible and practical to build a tailings dam at Site #4 to impound 300 000 tonnes of tailings.
- The valley topography at Site #4 is well suited to a possible later dam raise. This would increase storage capacity to accommodate the discovery of additional ore reserves. In this regard, Site #4 is much more attractive than the other three sites previously considered.
- The foundations at Site #4 consist of sandy soils with varying amounts of fines. Occasional gravelly layers exist within the sandy soils. Some organic rich horizons are present, especially on the right abutment.
- If the foundation materials thaw, only very minor settlement will occur in the sandy soils. The organic-rich soils will consolidate significantly if melted, but because of their limited thickness, total settlement in the dam will not be large.
- Significant ice occurs in about the upper 1.5 m of the overburden at Site #4.
- The estimated annual precipitation values for a mean year, 200-year wet year, and 10-year dry year are 271 mm, 370 mm and 200 mm respectively. The statistically estimated 1 hour, 6 hour and 24 hour Probable Maximum Precipitation(PMP) depths are 63 mm, 76 mm, and 108 mm. The estimated annual evaporation is 452.9 mm.
- A diversion channel should be constructed to divert Dome Creek around the tailings pond. During a dry year, water could be spilled from the diversion channel into the pond to make up possible water deficits.
- An operational emergency spillway 5 m wide should be constructed. Initial siting is on the left abutment but it may be located on the right abutment, based on subsequent investigations. The invert of this spillway should be in rock and set a minimum of 1.7 m below the crest of the dam. A riprap lined discharge channel should be provided.

- A closure spillway approximately 10 m wide with an invert in rock and set 2.0 m below the dam crest should be built.

- The water balance indicates that, with the diversion in place and, under somewhat drier than normal conditions, discharge may be avoided. However, to allow for less than perfect diversion efficiency, higher than average rainfall, or other water balance upsets, provision should be made to allow discharge from the pond.

This study has proven the feasibility of developing a tailings storage facility at Site #4, and that Site #4 is the most attractive location available. For detailed design, some refinements will be required, as listed below:

- A detailed site-specific PMP and Probable Maximum Flood (PMF) study, should be carried out including an assessment of PMF seasonal variation and maximized snowpack conditions.

- Sizing and locating of the closure spillway should be carried out.

- The water balance should be refined by including details of slurry transport water and reclaim water.

- Collection of climatic data for the site should be commenced as soon as staff are on site on a regular basis to maintain equipment.

- Test pits or other methods should be employed to investigate soil depth and condition on both abutments, and particularly the right (south) abutment.

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REFERENCES

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Fulwinder, C.W. (1973). "Thermal Regime in an Arctic Earthfill Dam"; 2nd International Conference on Permafrost, Yakutsk, USSR, pp. 622-628.

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APPENDIX I

Seismic Evaluation

ENERGY, MINES AND
RESOURCES CANADA
GEOLOGICAL SURVEY OF CANADA

ENERGIE, MINES ET
RESSOURCES CANADA
COMMISSION GEOLOGIQUE DU CANADA

SEISMIC RISK CALCULATION * / CALCUL DE RISQUE SEISMIQUE *

REQUESTED BY/ DEMANDE PAR IAN BRUCE / KLOHN LEONOFF CONSULTANTS MJG

SITE MT. NANSEN, YUKON

LOCATED AT/ SITUE AU 62.05 NORTH/NORD 137.17 WEST/OUEST

PROBABILITY OF EXCEEDENCE PER ANNUM/ PROBABILITE DE DEPASSEMENT PAR ANNEE	0.010	0.005	0.0021	0.001
PROBABILITY OF EXCEEDENCE IN 50 YEARS/ PROBABILITE DE DEPASSEMENT EN 50 ANS	40 %	22 %	10 %	5 %
PEAK HORIZONTAL GROUND ACCELERATION (G) ACCELERATION HORIZONTALE MAXIMALE DU SOL (G)	0.057	0.074	0.095	0.117
PEAK HORIZONTAL GROUND VELOCITY (M/SEC) VITESSE HORIZONTALE MAXIMALE DU SOL (M/SEC)	0.126	0.163	0.217	0.262

* REFERENCES

1. NEW PROBABILISTIC STRONG SEISMIC GROUND MOTION MAPS OF CANADA: A COMPILATION OF EARTHQUAKE SOURCE ZONES, METHODS AND RESULTS.
P.W. BASHAM, D.H. WEICHERT, F.M. ANGLIN, AND M.J. BERRY
EARTH PHYSICS BRANCH OPEN FILE NUMBER 82-33, OTTAWA, CANADA 1982.

2. ENGINEERING APPLICATIONS OF NEW PROBABILISTIC SEISMIC GROUND-MOTION MAPS OF CANADA
A.C. HEIDEBRECHT, P.W. BASHAM, J.H. RAINER, AND M.J. BERRY
CANADIAN JOURNAL OF CIVIL ENGINEERING, VOL. 10, NO. 4, P. 670-680, 1983.

3. NEW PROBABILISTIC STRONG GROUND MOTION MAPS OF CANADA.
P.W. BASHAM, D.H. WEICHERT, F.M. ANGLIN, AND M.J. BERRY, BULLETIN OF THE SEISMOLOGICAL SOCIETY OF AMERICA, VOL. 75, NO. 2, P. 563-595, 1985.

4A. SUPPLEMENT TO THE NATIONAL BUILDING CODE OF CANADA 1985, NRCC NO. 23178.
CHAPTER 1: CLIMATIC INFORMATION FOR BUILDING DESIGN IN CANADA.
CHAPTER 4: COMMENTARY J: EFFECTS OF EARTHQUAKES.

4B. SUPPLEMENT DU CODE NATIONAL DU BATIMENT DU CANADA 1985, CNRC NO 23178F.
CHAPITRE 1: DONNEES CLIMATIQUES POUR LE CALCUL DES BATIMENTS AU CANADA.
CHAPITRE 4: COMMENTAIRE J: EFFETS DES SEISMES.

19-OCT-88 18:57:40

```
SITE                                          MT.  ANSEN,   YUKON

     ZONING FOR ABOVE SITE/ ZONAGE DU SITE CI-DESSUS

     1985 NBCC/CNBC:   ZA = 2,   ZV = 4,   V = 0.20 M/S

   ACCELERATION ZONE/ ZONE D'ACCELERATION     ZA=2
   ZONAL ACCELERATION/ ACCELERATION ZONALE  0.10 G

   VELOCITY ZONE/ ZONE DE VITESSE             ZV=4
   ZONAL VELOCITY/ VITESSE ZONALE           0.20 M/S


                1985 NBCC/CNBC **
    SEISMIC ZONING MAPS/ CARTES DU ZONAGE SEISMIQUE

          PROBABILITY LEVEL:  10% IN 50 YEARS
       NIVEAU DE PROBABILITE:  10% EN 50 ANNEES

        ----------------------------------------
         G OR M/S    ZONE       ZONAL VALUE/
                               VALEUR ZONALE
        ----------------------------------------
          0.00
                      0            0.00
          0.04
                      1            0.05
          0.08
                      2            0.10
          0.11
                      3            0.15
          0.16
                      4            0.20
          0.23
                      5            0.30
          0.32
                      6*           0.40
        ----------------------------------------

   * ZONE 6:  NOMINAL VALUE/ VALEUR NOMINALE  0.40;
      SITE-SPECIFIC STUDIES SUGGESTED FOR IMPORTANT PROJECTS/
      ETUDES COMPLEMENTAIRES SUGGEREES POUR DES PROJETS D'IMPORTANCE.


  ** FOR NBCC APPLICATIONS, CALCULATED ZONE VALUES AT A SITE SHOULD BE
      REPLACED BY EFFECTIVE ZONE VALUES [ZA(EFF) OR ZV(EFF)] AS SHOWN BELOW/
     POUR APPLICATIONS SELON LE CNBC, ON DOIT REMPLACER LES VALEURS ZONALES
      CALCULEES POUR UN SITE PAR LES VALEURS EFFECTIVES [ZA(EFF) OU ZV(EFF)]
      COMME MONTRE CI-DESSOUS:

       1.   IF/SI (ZA - ZV) > 1,          ===>  ZA(EFF) = ZV + 1.
  OR/OU
       2.   IF/SI (ZA - ZV) < 1,          ===>  ZA(EFF) = ZV - 1.
  OR/OU
       3.   IF/SI  ZV=0 AND/ET ZA > 0,    ===>  ZV(EFF) = 1.

        (SEE REFERENCE 2 CITED ABOVE, PAGE 677)
        (VOIR PAGE 677 DE LA REFERENCE 2 CI-DESSUS)
                                                        19-OCT-88  18.57:40
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APPENDIX II

Test Pit Logs and Borehole Logs

TEST HOLE LOG

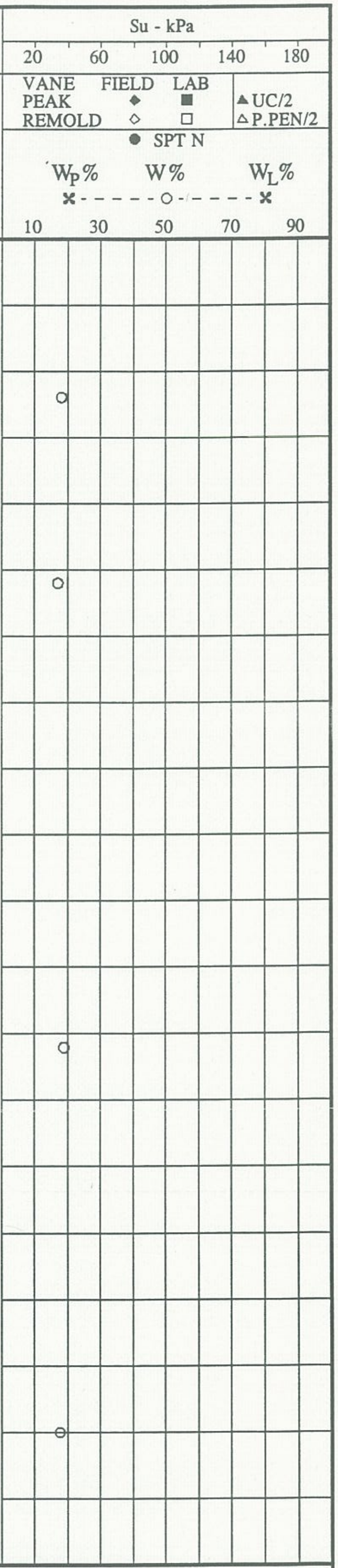
STARTED: 16/07/94 **FINISHED:** 16/07/94

DRILLING METHOD: SOLID STEM AUGER

GROUND ELEV(m):

COORDINATES(m):

DEPTH(m)	SPT BLOWS PER 0.15m	OTHER TESTS	SAMPLE TYPE AND NUMBER	SYMBOL	DESCRIPTION OF MATERIALS	PIEZOMETER DETAILS
0.8					Silty SAND (SM); silty fine to medium sand, top 0.25 m is moss.	
1.2					Silty SAND (SM); sand medium to coarse, trace to little silt, frozen hard, salt and pepper, ice crystals, no visible ice lenses.	
1.8					Gravelly beginning at 1.2 m. Changed to Carrel Tube and solid stem.	
2.1					SAND (SW); fine to medium sand with layers of coarse sand and pebbles, frozen, no visible ice.	
2.6					SAND (SW); medium sand, medium brown, trace silt, some coarse sand, little rounded pebbles.	
3.1					SAND (SW); fine to medium sand, light brown (blond), little coarse sand.	
					SAND (SW); clean fine to medium sand, trace silt, frozen, no visible ice, cross bedded, light brown.	
4.1					SAND (SW); fine to medium clean sand, well rounded gravelly layer 5 to 7.5 cm thick at 3.7 m.	
			CT 1		SAND (SW); fine to medium clean sand with trace coarse sand and silt, frozen, no visible ice, cross bedding visible in sand, well rounded.	
			CT 2		Sand becoming coarser at 6.1 m.	
8.5					Gravelly layer at about 8.4 m.	
			CT 3		SAND (SW); clean medium sand, well rounded, light brown, no visible ice, at 9.1 m gravel angular to sub-rounded, cross bedded, teperature reading = 0.0 degrees celsius, Photo 1 at 9.0 m.	
10					Continued	



FORM: SI01 93/04/12

PROJECT NO.: PM 5314 03 02

PROJECT: BYG MT. NANSEN

LOCATION: SITE #4

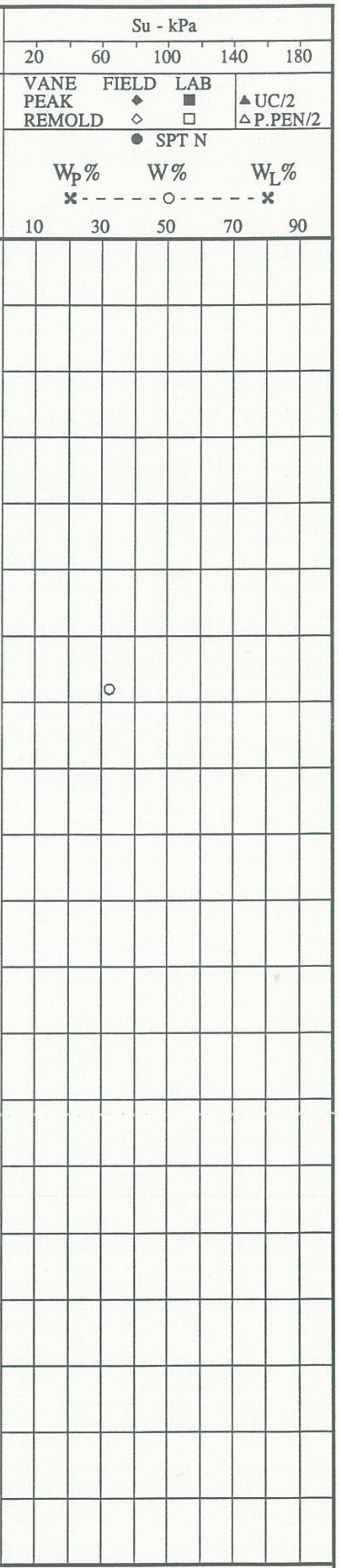
LOGGED BY: BST **CHECKED BY:**

SHEET 1 **OF** 2 **HOLE NO.:** DH94-01

TEST HOLE LOG

STARTED: 16/07/94 **FINISHED:** 16/07/94
DRILLING METHOD: SOLID STEM AUGER
GROUND ELEV(m):
COORDINATES(m):

DEPTH (m)	SPT BLOWS PER 0.15m	OTHER TESTS	SAMPLE TYPE AND NUMBER	DESCRIPTION OF MATERIALS	PIEZOMETER DETAILS
				SAND (SW); (continued) Gravelly layer at 10.7 m. Gravelly layer at 10.8 m. Gravelly layer at 11.3 m.	
11.3				SAND (SW); medium grey fine sand, trace silt, no visible ice.	
11.6				SAND (SW); medium grey fine to medium sand, trace to little silt, no undisturbed sample recovered in tube (fell out).	
12.2				SAND (SW); grey fine to medium sand with trace silt and little coarse sand and gravel, organics, no visible ice.	
13.1			CT 4	SAND (SW); very fine sand with little to some silt, frozen hard, no visible ice, some organic layers and organic smell. Sample taken at 13.4 m.	
13.7			CT 5 CT 6	SAND (SW); medium grey fine to medium sand with trace to little silt, organics, organic smell, no visible ice.	
19.1				GRAVEL (GRAVEL) Very rocky at 19.8 m. Refusal and end of hole at 20.1 m	
20.0					



FORM: SI01 93/04/12

PROJECT NO.: PM 5314 03 02
PROJECT: BYG MT. NANSEN
LOCATION: SITE #4
LOGGED BY: BST **CHECKED BY:**
SHEET 2 **OF** 2 **HOLE NO.:** DH94-01

TEST HOLE LOG

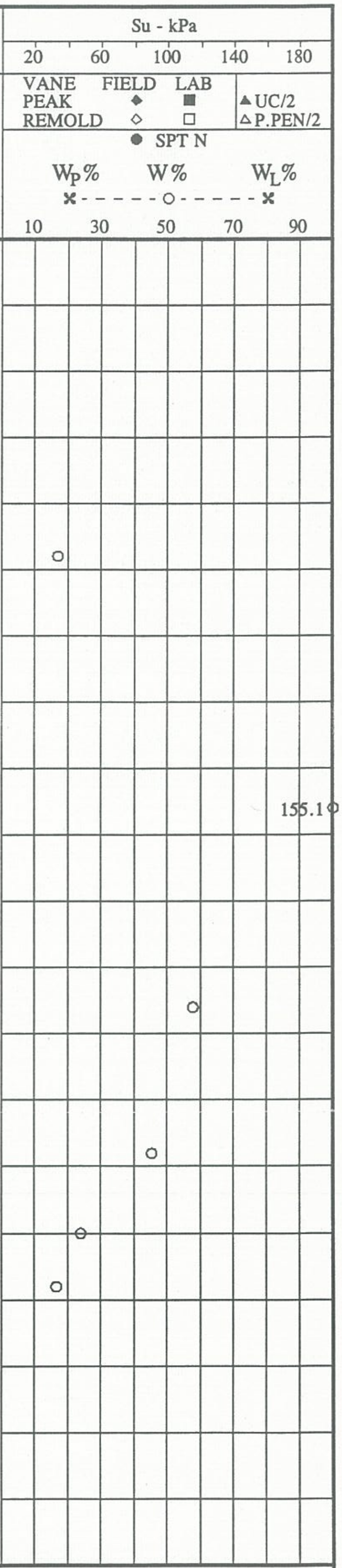
STARTED: 17/07/94 **FINISHED:** 17/07/94

DRILLING METHOD: SOLID STEM AUGER

GROUND ELEV(m):

COORDINATES(m):

DEPTH (m)	SPT BLOWS PER 0.15m	OTHER TESTS	SAMPLE TYPE AND NUMBER	DESCRIPTION OF MATERIALS	PIEZOMETER DETAILS
0.0 – 0.3				MOSS (ORGANICS); 0.3 m cover over frozen soil.	
0.3 – 0.9				SAND (SW); organic rich fine to medium sand with some small pebbles.	
0.9 – 2.3			CT 1	SAND (SW); organic rich at top, grading to little organics by 1.2 m, fine to medium sand with trace to little silt, 5 ice lenses each 1 mm thick in silty or organic-rich layer at 1.2 m depth, otherwise sand shows no visible ice, sand is medium brown, well rounded. Ice cuttings at 1.8 to 2.1 m.	
2.3 – 2.4			CT 2	SAND (SW); dark brown, fine to med., trace silt & organics, no vis. ice.	
2.4 – 3.7				SAND (SW); light brown fine to medium sand becoming coarser with depth, trace silt, some pebbles, no visible ice, 40% angular rock below 2.9 m. Sample taken at 2.4 m.	
3.7 – 4.3				SAND (SW); fine to medium sand, trace silt, trace to little pebbles, no visible ice.	
4.3 – 5.3				Silty SAND (SM); organic, rich brown, silty to sandy, ice rich with many 0.5-1.0 mm ice lenses in organics. Sample taken at 4.4 m. High ice content in cuttings (4.6 to 5.3 m).	
5.3 – 6.1			CT 3	Silty SAND (SM); silty fine to medium sand with organics and roots, numerous ice crystals to 3 mm in size, ice rich layers of frozen peat. Sample taken at 5.8 m.	
6.1 – 6.7				Silty SAND (SM); silty fine sand with organics, strong organic odour, numerous roots, some visible ice crystals.	
6.7 – 7.0			CT 4	Silty SAND (SM); highly organic silty sand, brown.	
7.0 – 7.6				SAND (SW); light grey fine to medium sand, trace to little silt, bedding visible in sand, no visible ice, angular pebbles at 7.6 m, organics melt to very soft consistency.	
7.6 – 8.2				Silty SAND (SM); silty fine to medium sand, frozen, sand well rounded, trace to some silt.	
8.2 – 9.2				Attempted Carrel sample but sample fell from tube - no recovery.	
9.2 – 10.0				Silty SAND (SM); (same as from 7.6 to 8.2 m) Refusal (on bedrock?) and end of hole at 10.0 m.	



FORM: SI01 93/04/12

PROJECT NO.: PM 5314 03 02

PROJECT: BYG MT. NANSEN

LOCATION: SITE #4

LOGGED BY: BST **CHECKED BY:**

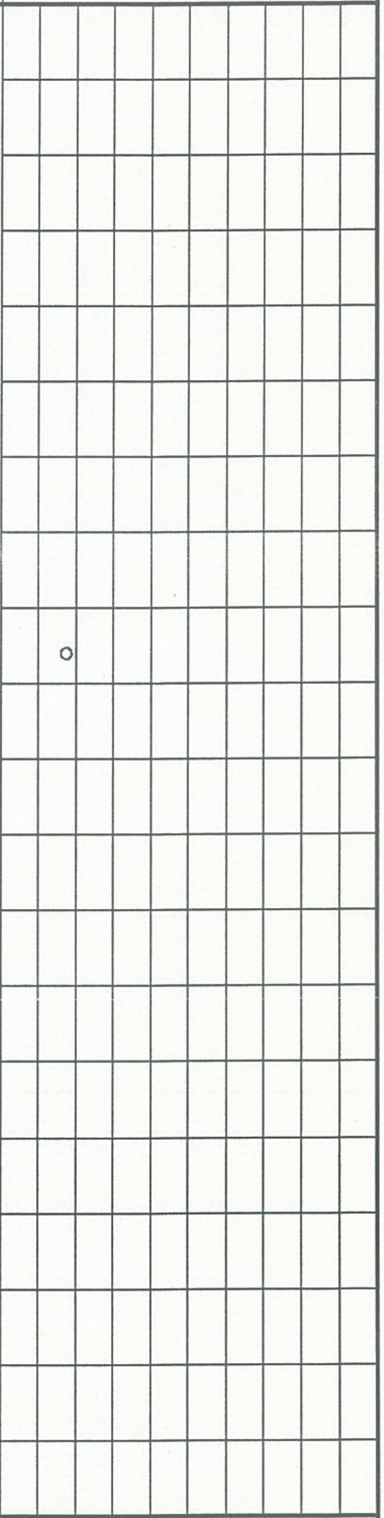
SHEET 1 **OF** 1 **HOLE NO.:** DH94-02

TEST HOLE LOG

STARTED: 18/07/94 **FINISHED:** 18/07/94
DRILLING METHOD: SOLID STEM AUGER
GROUND ELEV(m):
COORDINATES(m):

Su - kPa: 20 60 100 140 180
VANE PEAK: FIELD ◆ LAB ■
REMOLD: FIELD ◇ LAB □
▲ UC/2
△ P.PEN/2
● SPT N
W_P% ✖ - - - - - W% ○ - - - - - W_L% ✖
10 30 50 70 90

DEPTH(m)	SAMPLE TYPE AND NUMBER	DESCRIPTION OF MATERIALS
		Frozen PEAT (PEAT); significant ice in cuttings.
0.8	CT 1	Frozen PEAT (PEAT); with silt, sand and pebbles - ice rich.
0.9		SAND (SW); fine to medium grey sand with little silt, some organic rich layers to 10 mm thick, no visible ice, solidly frozen.
1.5		SAND (SW); medium light brown sand, very clean, very well rounded, some fine gravel, zero to trace silt.
2.3	CT 2	SAND (SW); organic rich, fine to medium sand, trace to some pebbles, trace silt, ice rich but no discrete ice layers.
2.6		SAND (SW); fine to medium sand, light brown to grey cross bedded, very well rounded.
3.0		SAND (SW); grey-brown fine to medium sand, trace silt, well rounded.
3.8	CT 3	SAND (SW); fine to medium sand with trace silt, trace pebbles, sand well rounded, cross bedded, some layers slighty organic.
4.6		SAND (SW); fine to medium sand with pebble layers.
5.3	CT 4	SAND (SW); fine to medium sand with trace to some silt, gravel layer at 5.8 m, sampler refused, no visible ice.
5.8		SAND (SW); fine to medium grey-brown sand, pebbly.
8.5		Sandy SILT (SM); trace pebbles, low plastic.
8.8		SAND AND GRAVEL (SG); trace silt.
9.5	CT 5	SAND (SW); fine to medium sand, some pebbles to pebbley, trace silt, no visible ice, trace gravel, dark grey-brown.



Continued

FORM: SI01 93/04/12

PROJECT NO.: PM 5314 03 02
PROJECT: BYG MT. NANSEN
LOCATION: SITE #4
LOGGED BY: BST **CHECKED BY:**
SHEET 1 **OF** 2 **HOLE NO.:** DH94-03

TEST HOLE LOG

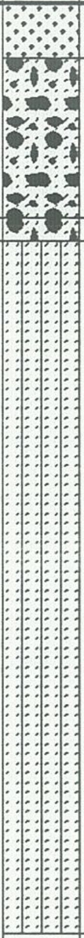
STARTED: 18/07/94 **FINISHED:** 18/07/94

DRILLING METHOD: SOLID STEM AUGER

GROUND ELEV(m):

COORDINATES(m):

DEPTH(m)	SPT BLOWS PER 0.15m	OTHER TESTS	SAMPLE TYPE AND NUMBER	SYMBOL	DESCRIPTION OF MATERIALS	PIEZOMETER DETAILS
					SAND (SW); (continued)	
10.4					SAND AND Coarse GRAVEL (SG); very dense, dark grey-brown, trace silt, possibly glacial till.	
11.4			CT 6			
11.6					11.4 to 11.6 m: Silty SAND AND GRAVEL (SG); some silt, gravel angular to sub-rounded (possibly glacial till), no visible ice, dense. Sample bagged at 11.6 m.	
					Silty SAND (SM); grey brown silty to sandy (possibly glacial till) with numerous rocky layers, rocks angular to sub-rounded, very hard drilling, dense, rocky.	
16.2					Refusal at 16.2 m. Assumed bedrock.	
					END OF TEST HOLE AT 16.2 m.	

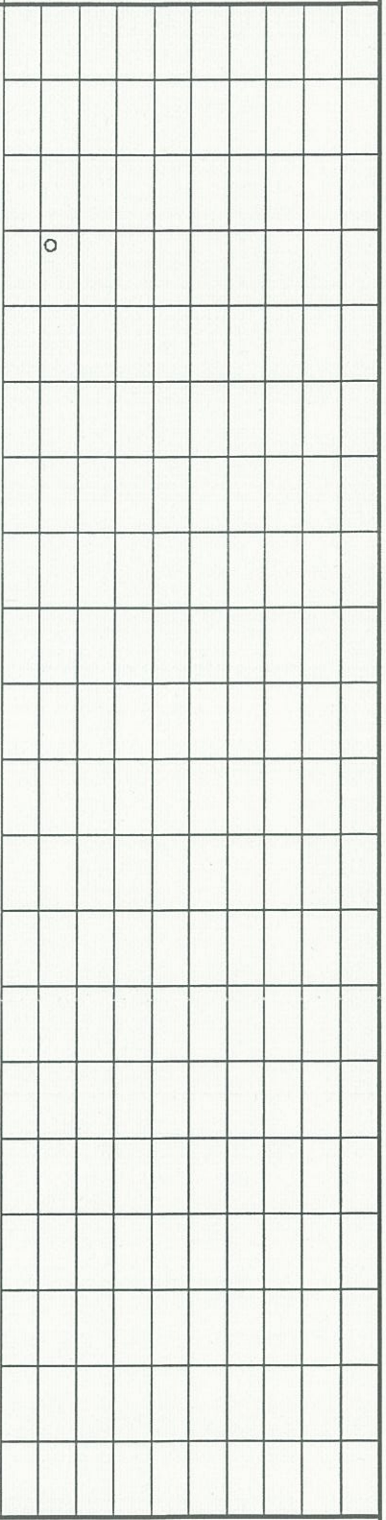


Su - kPa: 20 60 100 140 180

VANE	FIELD	LAB
PEAK	◆	■
REMOLD	◇	□

▲ UC/2
△ P.PEN/2
● SPT N

W_P% W% W_L%
× - - - - - ○ - - - - - ×



FORM: SI01 93/04/12

PROJECT NO.: PM 5314 03 02

PROJECT: BYG MT. NANSEN

LOCATION: SITE #4

LOGGED BY: BST **CHECKED BY:**

SHEET 2 **OF** 2 **HOLE NO.:** DH94-03

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES
JOB No. PB5314 03 PIT No. 9401 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE
WEATHER CLEAR
INSPECTOR B. TRENHOLME
SITE SITE #4, MT NANSEN
TEMP. 25 °C
STARTED ____ .M. ______ 19__
LOCATION: LATITUDE ______
DEPTH 1.0 m
FINISHED ____ .M. ______ 19__
DEPARTURE ______
WIDTH ______
ELEVATIONS: DATUM ______
CONTRACTOR I CAN DIG IT CONTRACTING
LENGTH ______
GROUND SURFACE ______
METHOD OF EXCAVATION BACK HOE
WATER LEVELS ______

LOG LEGEND
- ▥ SILT
- ▨ CLAY
- ░ SAND
- ● GRAVEL

*** SAMPLE CONDITION**
- ▩ GOOD
- ☰ FAIR
- ☒ DISTURBED
- ■ LOST

**** SAMPLING METHOD**
- B - THIN WALL TUBE
- C - PISTON SAMPLER
- E - AUGER
- G - SHOVEL
- H - CARVED, BLOCK

**** SHIPPING CONTAINER**
- O - TUBE
- P - WATER CONTENT TIN
- Q - GLASS JAR
- R - CLOTH BAG
- S - PLIOFILM BAG
- T - METAL CAN
- U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR; CONSISTENCY; DENSITY; TEXTURE; STRUCTURE; SHAPE AND SURFACE CONDITION OF GRAINS; TESTING AND SAMPLING PROCEDURES AND EQUIPMENT; WATER AND GAIN; ODOUR, ETC.
PEAT									0-15 cm Peat
			0.2						15cm - 1m fine to medium
									clean grey SAND, trace
SAND			0.4						silt. 10cm thick ice
									lens at 80 cm.
			0.6						Water inflow at 40 cm.
ICE			0.8						Refusal on solidly frozen
SAND									ground at 1.0 m
FROZEN SAND ↓			1.0						

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT. NANSEN MINE
HOLE No. 9401 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9402 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4 , MT NANSEN TEMP. 25 °C STARTED ____ .M. ________ 19__
LOCATION: LATITUDE ________ DEPTH 1.5 m FINISHED ____ .M. ________ 19__
DEPARTURE ________ WIDTH ________ ELEVATIONS: DATUM ________
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ________ GROUND SURFACE ________
METHOD OF EXCAVATION BACK HOE WATER LEVELS ________

LOG LEGEND
▥ SILT ░ SAND
▨ CLAY ⁘ GRAVEL

*** SAMPLE CONDITION**
▩ GOOD ☒ DISTURBED
☰ FAIR ▓ LOST

**** SAMPLING METHOD**
B - THIN WALL TUBE
C - PISTON SAMPLER
E - AUGER
G - SHOVEL
H - CARVED BLOCK

**** SHIPPING CONTAINER**
O - TUBE
P - WATER CONTENT TIN
Q - GLASS JAR
R - CLOTH BAG
S - PLIOFILM BAG
T - METAL CAN
U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH (m)	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
BROWN PEAT									0-50 cm brown peat
			0.2						50cm - 1.0m medium grey fine to medium SAND, some organics, containing ice crystals
			0.4						
			0.6						1.0m - 1.5m dark grey fine SAND, trace silt ice crystals
fine dark grey SAND			0.8						
			1.0						1.5m - refusal on solidly frozen ground
			1.2						
			1.4						
solidly frozen ↓			1.6						

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BST
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9402 INSPECTOR BST
APPROVED BST DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9403 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4 , MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__
LOCATION: LATITUDE ______ DEPTH 0.6 m FINISHED ____ .M. ______ 19__
DEPARTURE ______ WIDTH ______ ELEVATIONS: DATUM ______
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______
METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND
▥ SILT ░ SAND
▨ CLAY ⁘ GRAVEL

*** SAMPLE CONDITION**
▩ GOOD ☒ DISTURBED
▤ FAIR ■ LOST

**** SAMPLING METHOD**
B - THIN WALL TUBE G - SHOVEL
C - PISTON SAMPLER H - CARVED, BLOCK
E - AUGER

**** SHIPPING CONTAINER**
O - TUBE S - PLIOFILM BAG
P - WATER CONTENT TIN T - METAL CAN
Q - GLASS JAR U - WOODEN BOX
R - CLOTH BAG

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
ORGANIC SOIL									0-5cm organic soil
SAND trace silt			0.2						5cm - 60 cm fine to medium SAND, Trace silt, little pebbles. Pebbles angular
			0.4						
solidly frozen ↓			0.6						Refused on solidly frozen soil at 60 cm no visible ice
			0.8						
			1.0						

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9403 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9404 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4 , MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__
LOCATION: LATITUDE ______ DEPTH 2.1 m FINISHED ____ .M. ______ 19__
DEPARTURE ______ WIDTH ______ ELEVATIONS: DATUM ______
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______
METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND
- ▥ SILT
- ░ SAND
- ▨ CLAY
- ⁘ GRAVEL

*** SAMPLE CONDITION**
- ▒ GOOD
- ☒ DISTURBED
- ▤ FAIR
- ■ LOST

**** SAMPLING METHOD**
- B - THIN WALL TUBE
- C - PISTON SAMPLER
- E - AUGER
- G - SHOVEL
- H - CARVED , BLOCK

**** SHIPPING CONTAINER**
- O - TUBE
- P - WATER CONTENT TIN
- Q - GLASS JAR
- R - CLOTH BAG
- S - PLIOFILM BAG
- T - METAL CAN
- U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
Moss & Roots									0-10 cm moss & roots
			0.2						10 cm - 2.1 m uniform fine to med
			0.4						SAND little pebbles trace silt
			0.6						no visible ice, cross- bedded, med brown
SAND			0.8						
			1.0						
			1.2						
			1.4						
			1.6						
			1.8						
			2.0						
frozen hard ↓			2.2						

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9404 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9405 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B. TRENHOLME
SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__
LOCATION: LATITUDE ______ DEPTH 2.0 m FINISHED ____ .M. ______ 19__
DEPARTURE ______ WIDTH ______ ELEVATIONS: DATUM ______
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______
METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND
▥ SILT ░ SAND
▨ CLAY ⁘ GRAVEL

*** SAMPLE CONDITION**
▦ GOOD ☒ DISTURBED
☰ FAIR ■ LOST

**** SAMPLING METHOD**
B - THIN WALL TUBE
C - PISTON SAMPLER
E - AUGER
G - SHOVEL
H - CARVED BLOCK

**** SHIPPING CONTAINER**
O - TUBE
P - WATER CONTENT TIN
Q - GLASS JAR
R - CLOTH BAG
S - PLIOFILM BAG
T - METAL CAN
U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	*	** TYPE	NO.	SIZE	RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
ORGANIC SOIL									10 cm organic soil
med. brown SAND			0.2						10 cm - 20 cm med brown fine to medium SAND
light brown SAND			0.4						
			0.6						20 cm - 2.0 M light brown fine to medium clean SAND, little pebbles, cross bedded, pebbles angular to sub-rounded no visible ice
			0.8						
			1.0						
			1.2						
			1.4						
			1.6						
			1.8						
			2.0						
frozen solidly ↓			2.2						

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9405 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314/03 PIT No. 9406 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__
LOCATION: LATITUDE ______ DEPTH 2.5m FINISHED ____ .M. ______ 19__
DEPARTURE ______ WIDTH ______ ELEVATIONS: DATUM ______
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______
METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND
- ▥ SILT
- ▨ CLAY
- ░ SAND
- ⠿ GRAVEL

*** SAMPLE CONDITION**
- ▓ GOOD
- ☒ DISTURBED
- ▤ FAIR
- ■ LOST

**** SAMPLING METHOD**
- B - THIN WALL TUBE
- C - PISTON SAMPLER
- E - AUGER
- G - SHOVEL
- H - CARVED, BLOCK

**** SHIPPING CONTAINER**
- O - TUBE
- P - WATER CONTENT TIN
- Q - GLASS JAR
- R - CLOTH BAG
- S - PLIOFILM BAG
- T - METAL CAN
- U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
organic soil									0-5cm organic soil
med. brown SAND									5cm-20cm medium brown
			0.2						fine SAND, some roots,
light brown SAND			0.4						Volcanic ash mixed in top
									5cm
			0.6						
									20 cm - 2.5m fine to
			0.8						medium clean SAND, cross
									bedded, medium dense
			1.0						no visible ice, light brown
			1.2						Refusal on solidly frozen
									ground at 2.5m
			1.4						
			1.6						
			1.8						
			2.0						
			2.2						
			2.4						
solidly frozen									

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9406 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES
JOB No. PB5314 03 PIT No. 9407 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE
WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4, MT NANSEN
TEMP. 25 °C STARTED ____ .M. ________ 19__
LOCATION: LATITUDE ________
DEPTH 0.5m FINISHED ____ .M. ________ 19__
DEPARTURE ________
WIDTH ________ ELEVATIONS: DATUM ________
CONTRACTOR I CAN DIG IT CONTRACTING
LENGTH ________ GROUND SURFACE ________
METHOD OF EXCAVATION BACK HOE
WATER LEVELS ________

LOG LEGEND
▥ SILT
▨ CLAY
░ SAND
● GRAVEL

*** SAMPLE CONDITION**
▩ GOOD
▤ FAIR
☒ DISTURBED
■ LOST

**** SAMPLING METHOD**
B - THIN WALL TUBE
C - PISTON SAMPLER
E - AUGER
G - SHOVEL
H - CARVED BLOCK

**** SHIPPING CONTAINER**
O - TUBE
P - WATER CONTENT TIN
Q - GLASS JAR
R - CLOTH BAG
S - PLIOFILM BAG
T - METAL CAN
U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE					DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
				*	** TYPE	NO.	SIZE	RET'D.	
Moss & peat									0-20cm Moss & Peat
			0.2						
SAND									20cm-50cm Medium SAND clean, no visible ice salt & pepper texture
			0.4						
REFUSAL FROZEN SOLID			0.6						Refusal at 50cm in solidly frozen SAND, as above

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9407 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9408 SHEET No. 1 of 1

PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME

SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__

LOCATION: LATITUDE ______ DEPTH 0.5m FINISHED ____ .M. ______ 19__

DEPARTURE ______ WIDTH ______ ELEVATIONS: DATUM ______

CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______

METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND

- ▥ SILT
- ▨ CLAY
- ░ SAND
- ● GRAVEL

*** SAMPLE CONDITION**

- ▦ GOOD
- ☰ FAIR
- ☒ DISTURBED
- ■ LOST

**** SAMPLING METHOD**

- B - THIN WALL TUBE
- C - PISTON SAMPLER
- E - AUGER
- G - SHOVEL
- H - CARVED BLOCK

**** SHIPPING CONTAINER**

- O - TUBE
- P - WATER CONTENT TIN
- Q - GLASS JAR
- R - CLOTH BAG
- S - PLIOFILM BAG
- T - METAL CAN
- U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE					DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
				*	** TYPE	NO.	SIZE	RET'D.	
ORGANIC SOIL & ROOTS			0.2						0-30 cm Organic soil and roots
SAND			0.4						30 cm - 50 cm fine to medium SAND, little silt (source of silt may be ash?) salt & pepper no visible ice
FROZEN SAND ↓			0.6						
			0.8						
			1.0						Refusal on solidly frozen sand, as above, at 50 cm

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT

PROJECT MT. NANSEN

LOCATION MT NANSEN MINE

HOLE No. 9408 INSPECTOR BBT

APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9409 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ____ 19__
LOCATION: LATITUDE ____ DEPTH 1.0 M FINISHED ____ .M. ____ 19__
DEPARTURE ____ WIDTH ____ ELEVATIONS: DATUM ____
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ____ GROUND SURFACE ____
METHOD OF EXCAVATION BACK HOE WATER LEVELS ____

LOG LEGEND
▥ SILT ▨ SAND
▧ CLAY ⁘ GRAVEL

*** SAMPLE CONDITION**
▩ GOOD ☒ DISTURBED
▤ FAIR ■ LOST

**** SAMPLING METHOD**
B - THIN WALL TUBE
C - PISTON SAMPLER
E - AUGER
G - SHOVEL
H - CARVED, BLOCK

**** SHIPPING CONTAINER**
O - TUBE
P - WATER CONTENT TIN
Q - GLASS JAR
R - CLOTH BAG
S - PLIOFILM BAG
T - METAL CAN
U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE					DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
				*	** TYPE	NO.	SIZE	RET'D.	
organic soil & roots ASH									0-10cm organic soil & roots
			0.2						
SAND			0.4						10cm-12cm volcanic ash mixed with underlying sand & overlying organics
			0.6						
			0.8						12 cm - 1.0m medium brown fine to medium clean SAND trace silt, no visible ice
frozen SAND ↓			1.0						
			1.2						Refusal at 1.0m on solidly frozen SAND; as above

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9409 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9410 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ____ 19__
LOCATION: LATITUDE ____ DEPTH 0.5m FINISHED ____ .M. ____ 19__
DEPARTURE ____ WIDTH ____ ELEVATIONS: DATUM ____
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ____ GROUND SURFACE ____
METHOD OF EXCAVATION BACK HOE WATER LEVELS ____

LOG LEGEND
- ▥ SILT
- ▧ CLAY
- ⁘ SAND
- ● GRAVEL

*** SAMPLE CONDITION**
- ▩ GOOD
- ☰ FAIR
- ☒ DISTURBED
- ■ LOST

**** SAMPLING METHOD**
- B - THIN WALL TUBE
- C - PISTON SAMPLER
- E - AUGER
- G - SHOVEL
- H - CARVED BLOCK

**** SHIPPING CONTAINER**
- O - TUBE
- P - WATER CONTENT TIN
- Q - GLASS JAR
- R - CLOTH BAG
- S - PLIOFILM BAG
- T - METAL CAN
- U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH (m)	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR; CONSISTENCY; DENSITY; TEXTURE; STRUCTURE; SHAPE AND SURFACE CONDITION OF GRAINS; TESTING AND SAMPLING PROCEDURES AND EQUIPMENT; WATER AND GAIN; ODOUR, ETC.
organic soil & roots									0-10 cm organic soil & roots
SAND			0.2						
			0.4						10cm-50cm grey-brown fine to coarse SAND, Trace silt, some pebbles sand rounded, pebbles angular to sub-rounded, larger fragments more angular. No visible ice
frozen SAND ↓			0.6						
			0.8						
									Refusal on frozen SAND as above at 50 cm

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9410 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314/03 PIT No. 9411 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B. TRENHOLME
SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__
LOCATION: LATITUDE ______ DEPTH 1.2 m FINISHED ____ .M. ______ 19__
DEPARTURE ______ WIDTH ______ ELEVATIONS: DATUM ______
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______
METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND
- ▥ SILT
- ░ SAND
- ▨ CLAY
- ⁘ GRAVEL

*** SAMPLE CONDITION**
- ▩ GOOD
- ☒ DISTURBED
- ▤ FAIR
- ■ LOST

**** SAMPLING METHOD**
- B - THIN WALL TUBE
- C - PISTON SAMPLER
- E - AUGER
- G - SHOVEL
- H - CARVED, BLOCK

**** SHIPPING CONTAINER**
- O - TUBE
- P - WATER CONTENT TIN
- Q - GLASS JAR
- R - CLOTH BAG
- S - PLIOFILM BAG
- T - METAL CAN
- U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
ORGANIC SOIL, ROOTS									0-10cm organic soil & roots
SAND, ASH			0.2						
			0.4						10cm-12cm mixed sand and volcanic ash
SAND			0.6						
			0.8						12cm-1.2m medium brown SAND trace silt sand well rounded, no visible ice. Loose
			1.0						
ROCKY AT BOTTOM			1.2						Refusal on frozen SAND, as above at 1.2m
frozen hard ↓			1.4						Some angular rock frags at base of pit - may be close to bedrock?

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9411 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9412 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B. TRENHOLME
SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__
LOCATION: LATITUDE ______ DEPTH ______ FINISHED ____ .M. ______ 19__
DEPARTURE ______ WIDTH ______ ELEVATIONS, DATUM ______
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______
METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND		* SAMPLE CONDITION		** SAMPLING METHOD		** SHIPPING CONTAINER	
▥ SILT	▒ SAND	▩ GOOD	☒ DISTURBED	B - THIN WALL TUBE	G - SHOVEL	O - TUBE	S - PLIOFILM BAG
▨ CLAY	● GRAVEL	☰ FAIR	■ LOST	C - PISTON SAMPLER	H - CARVED, BLOCK	P - WATER CONTENT TIN	T - METAL CAN
				E - AUGER		Q - GLASS JAR	U - WOODEN BOX
						R - CLOTH BAG	

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
ORGANICS									0-20cm organics
SAND			0.2						20cm - 30cm oxide stained salt & pepper SAND fine to medium
FROZEN ↓			0.4						
									Refusal on frozen SAND, as above at 30cm

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9412 INSPECTOR BBT
APPROVED BBT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9413 SHEET No. 1 of 1
PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME
SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ___ .M. ___ 19__
LOCATION: LATITUDE ___ DEPTH 1.2 m FINISHED ___ .M. ___ 19__
DEPARTURE ___ WIDTH ___ ELEVATIONS: DATUM ___
CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ___ GROUND SURFACE ___
METHOD OF EXCAVATION BACK HOE WATER LEVELS ___

LOG LEGEND
▥ SILT ▒ SAND
▨ CLAY ⁘ GRAVEL

*** SAMPLE CONDITION**
▩ GOOD ☒ DISTURBED
☰ FAIR ■ LOST

**** SAMPLING METHOD**
B - THIN WALL TUBE
C - PISTON SAMPLER
E - AUGER
G - SHOVEL
H - CARVED BLOCK

**** SHIPPING CONTAINER**
O - TUBE
P - WATER CONTENT TIN
Q - GLASS JAR
R - CLOTH BAG
S - PLIOFILM BAG
T - METAL CAN
U - WOODEN BOX

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	** TYPE	NO.	SIZE	RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
ORGANIC SOIL & ROOTS									0-15cm organic soil & roots
			0.2						15cm - 1.2m
									Clean, fine to medium
			0.4						SAND, med. brown,
SAND									no visible ice med
			0.6						dense, some angular
									pebbles - Angular
			0.8						broken rock at base
									of pit - close to
angular rock at base			1.0						bedrock?
△ ◇ △									
			1.2						Refusal on frozen SAND
frozen ↓									as above at 1.2 m
			1.4						

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BGT
PROJECT MT. NANSEN
LOCATION MT NANSEN MINE
HOLE No. 9413 INSPECTOR BGT
APPROVED BGT DATE 16 JULY 94

FIELD TEST PIT LOG

CLIENT B.Y.G NATURAL RESOURCES JOB No. PB5314 03 PIT No. 9414 SHEET No. 1 of 1

PROJECT MT. NANSEN GOLD MINE WEATHER CLEAR INSPECTOR B.TRENHOLME

SITE SITE #4, MT NANSEN TEMP. 25 °C STARTED ____ .M. ______ 19__

LOCATION: LATITUDE ______ DEPTH 1.5M FINISHED ____ .M. ______ 19__

DEPARTURE ______ WIDTH ______ ELEVATIONS: DATUM ______

CONTRACTOR I CAN DIG IT CONTRACTING LENGTH ______ GROUND SURFACE ______

METHOD OF EXCAVATION BACK HOE WATER LEVELS ______

LOG LEGEND

▥ SILT ░ SAND

▨ CLAY ⁘ GRAVEL

*** SAMPLE CONDITION**

▩ GOOD ☒ DISTURBED

☰ FAIR ■ LOST

**** SAMPLING METHOD**

B - THIN WALL TUBE G - SHOVEL

C - PISTON SAMPLER H - CARVED BLOCK

E - AUGER

**** SHIPPING CONTAINER**

O - TUBE S - PLIOFILM BAG

P - WATER CONTENT TIN T - METAL CAN

Q - GLASS JAR U - WOODEN BOX

R - CLOTH BAG

SKETCH	LOG	ELEVATION	DEPTH	SAMPLE *	SAMPLE ** TYPE	SAMPLE NO.	SAMPLE SIZE	SAMPLE RET'D.	DESCRIPTION AND FIELD NOTES: COLOUR, CONSISTENCY, DENSITY, TEXTURE, STRUCTURE, SHAPE AND SURFACE CONDITION OF GRAINS, TESTING AND SAMPLING PROCEDURES AND EQUIPMENT, WATER AND GAIN, ODOUR, ETC.
ORGANIC SOIL, roots									0-10cm organic soil & roots
			0.2						10cm-1.5m
									colluvial soil, SAND,
			0.4						trace to little silt,
									some angular pebbles
			0.6						no visible ice
SANDY COLLUVIUM			0.8						Refusal on fractured
									rock at 1.5m
			1.0						
			1.2						
			1.4						
X1 fractured rock ↓			1.6						

KLOHN-CRIPPEN

JOB No. PB5314 03 LOGGED BY BBT

PROJECT MT. NANSEN

LOCATION MT NANSEN MINE

HOLE No. INSPECTOR BBT

APPROVED DATE 16 JULY 94

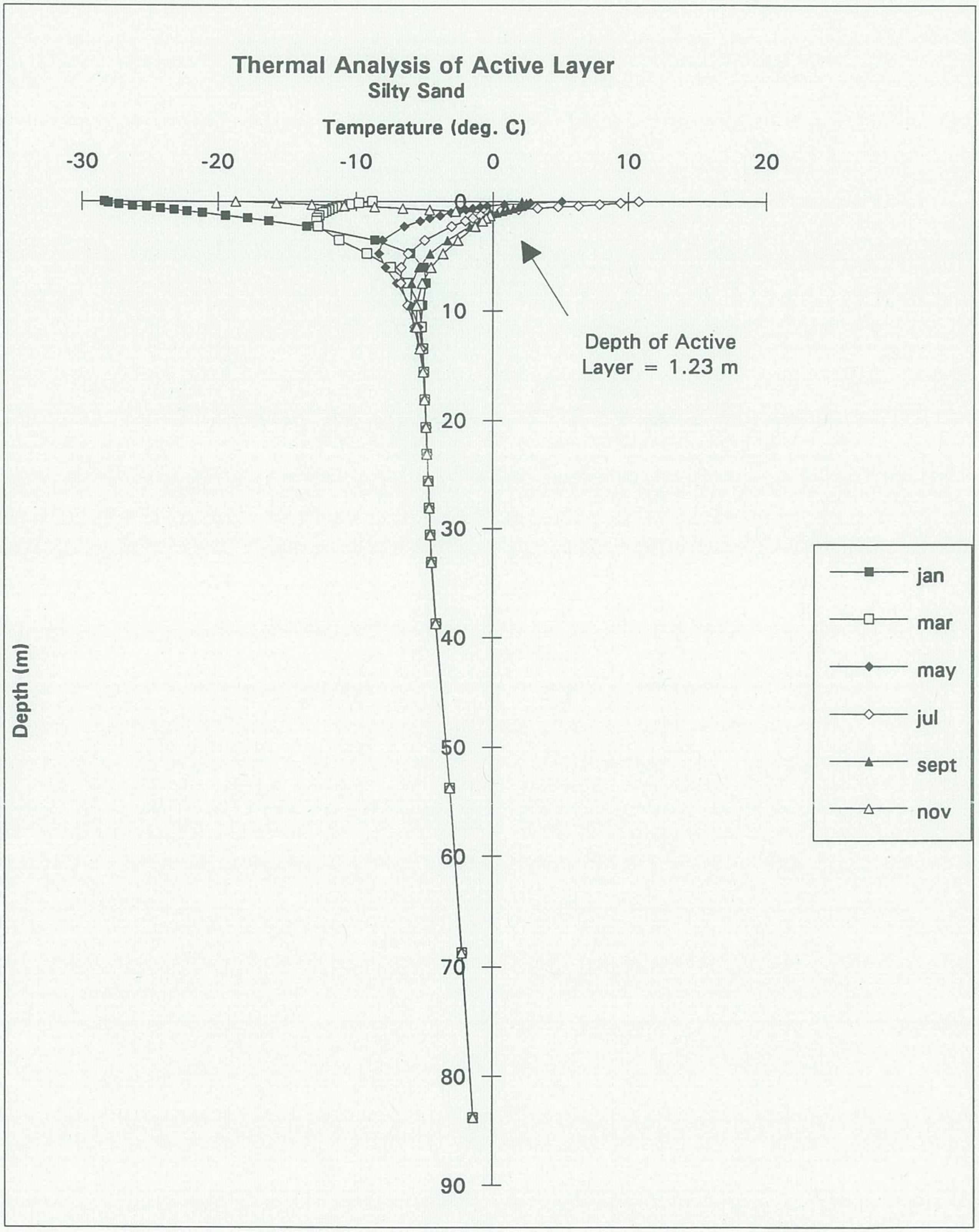
APPENDIX III

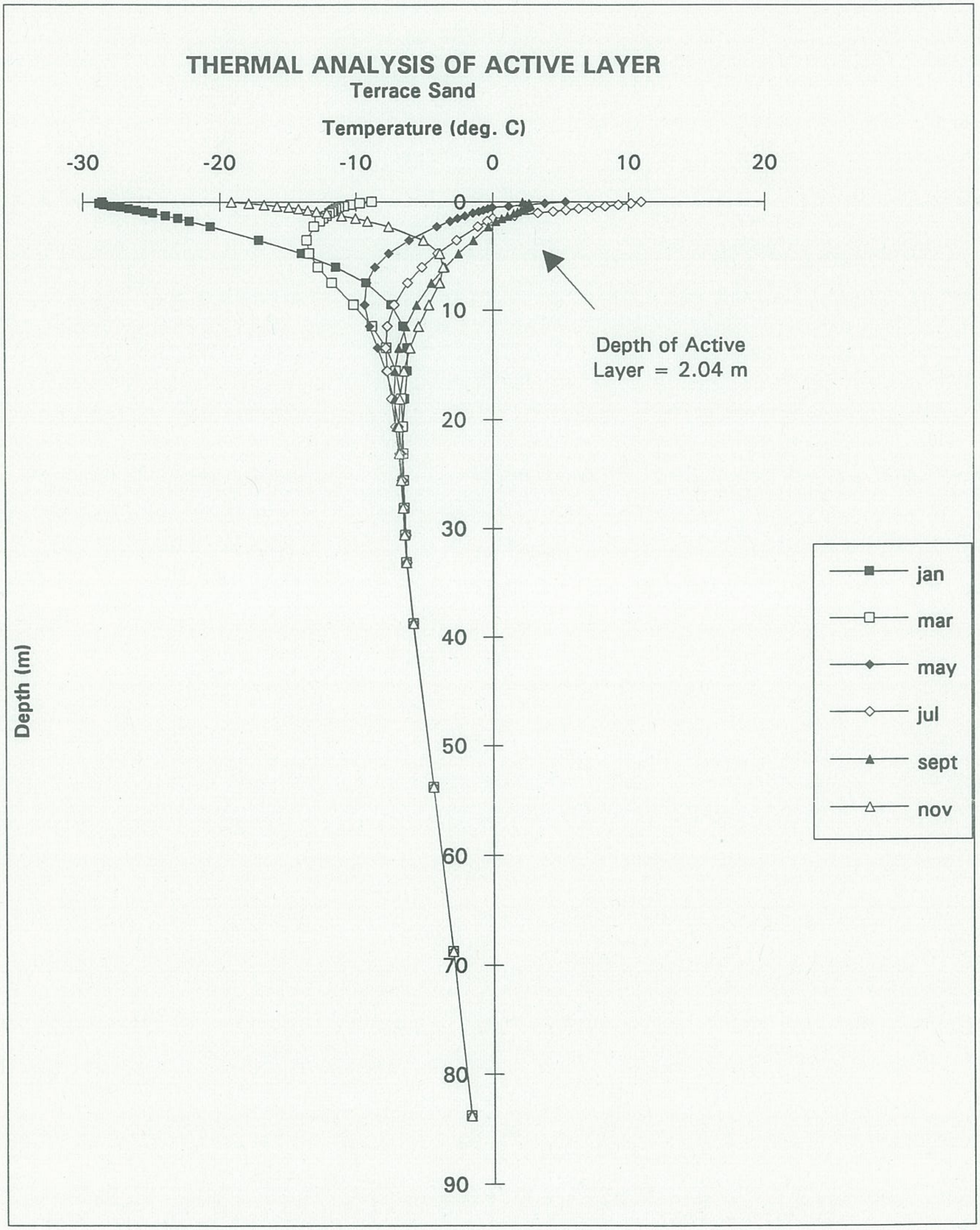
Thermal Analysis

APPENDIX III

THERMAL ANALYSIS

Thermal analyses were carried out to determine the depth of the active layer. Two plots are shown (terrace sand and silty sand) representing the two main soil types on site. The terrace sand will probably be used for low construction.


Thermal Analysis of Active Layer
Silty Sand
Temperature (deg. C)
-30
-20
-10
0
10
20
Depth (m)
0
10
20
30
40
50
60
70
80
90
Depth of Active Layer = 1.23 m
jan
mar
may
jul
sept
nov


THERMAL ANALYSIS OF ACTIVE LAYER
Terrace Sand
Temperature (deg. C)
-30
-20
-10
0
10
20
0
10
20
30
40
50
60
70
80
90
Depth (m)
Depth of Active Layer = 2.04 m
jan
mar
may
jul
sept
nov

APPENDIX IV

Stability Analysis for Foundation Liquefaction

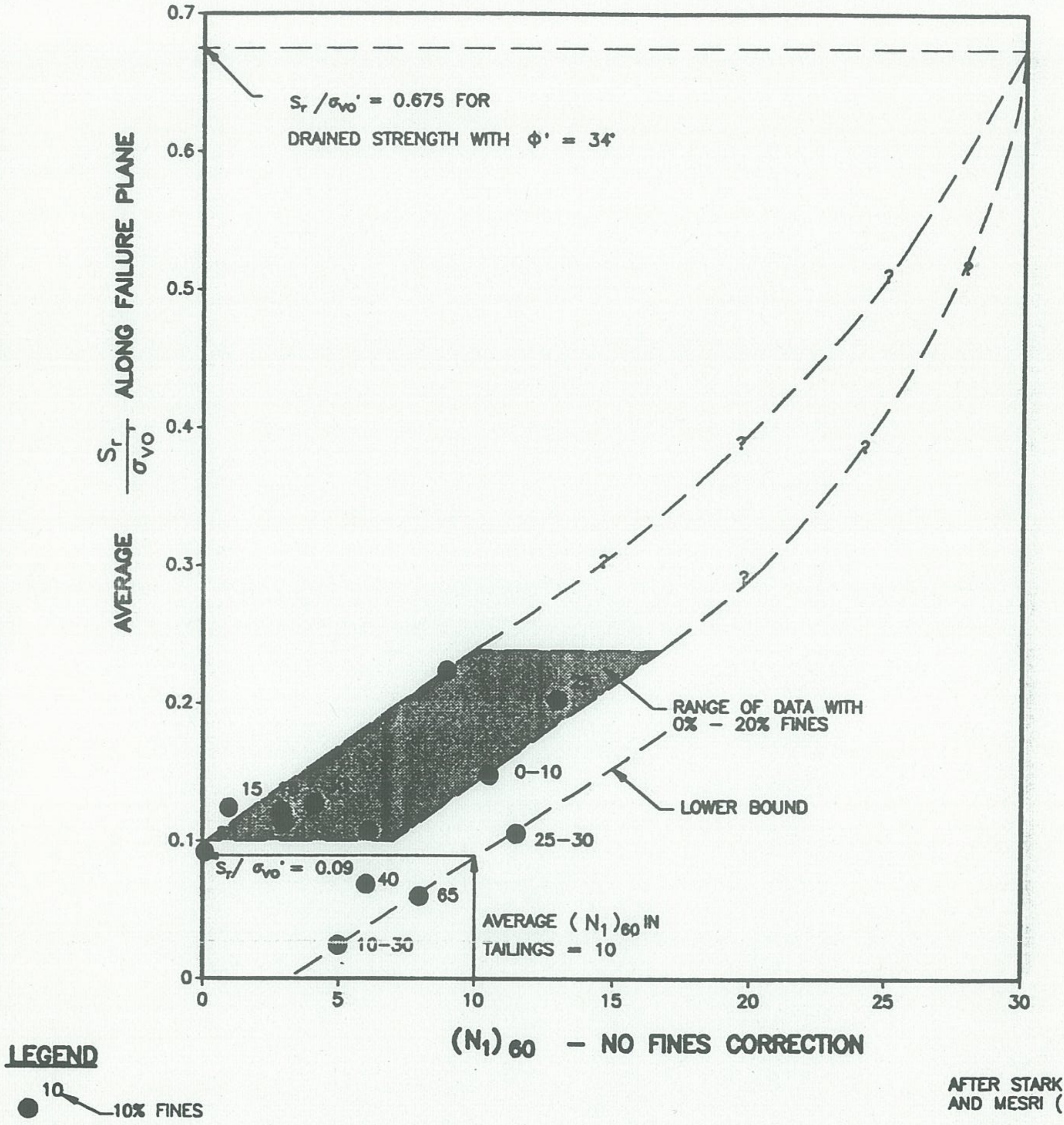
APPENDIX IV

STABILITY ANALYSIS FOR FOUNDATION LIQUEFACTION

There is a small potential for thawing of the foundations, particularly at the beginning of operations. This could result in loose sands which may be subject to liquefaction under seismic conditions. The residual strength of the tailings following liquefaction (S_{r1}) has been assessed using relationships developed from case histories (see Figure IV.1). Using these relationships, the residual strength can be estimated as a fraction of the initial vertical stress (σ_{v0}') related to the $(N_1)_{60}$ value. The $(N_1)_{60}$ value is normally derived from cone penetration tests. However, this is impossible in frozen ground. Based on previous experience, $(N_1)_{60}$ values in the range of 8 to 10 are conservatively assumed for the thawed foundation sands and for the tailings. From the lower bound of the plot of $(N_1)_{60}$ vs. S_r/σ_{v0}' (see Figure IV.1 after Stark and Mesri, 1992), a value of 0.09 is implied for S_r/σ_{v0}'. Consequently, a residual strength for liquefied tailings and foundation sands of 0.09 times the vertical stress is assumed for design.

For the overall stability of the embankment, a simple two-dimensional model is used to calculate a factor of safety (see Figure IV.2). It is assumed that the entire saturated mass of tailings behind the embankment will liquefy. It is also assumed that a layer of saturated sand in the foundations will also liquefy, producing a potential horizontal failure path underneath the dam. The dry density of the tailings is assumed to be about 1.25 tonnes/m^3 (12.26 kN/m^3). The dry density of the compacted sand embankment is assumed to be about 1.75 tonnes/m^3 (17 kN/m^3). The residual strength following liquefaction (S_{r1}) of the tailings is calculated according to the average depth of tailings, or about 6 m:

$$S_{r1} = (0.09)(12.26 \text{ kN/m}^3)(6 \text{ m}) = 6.6 \text{ kPa}$$



AFTER STARK
AND MESRI (1992)

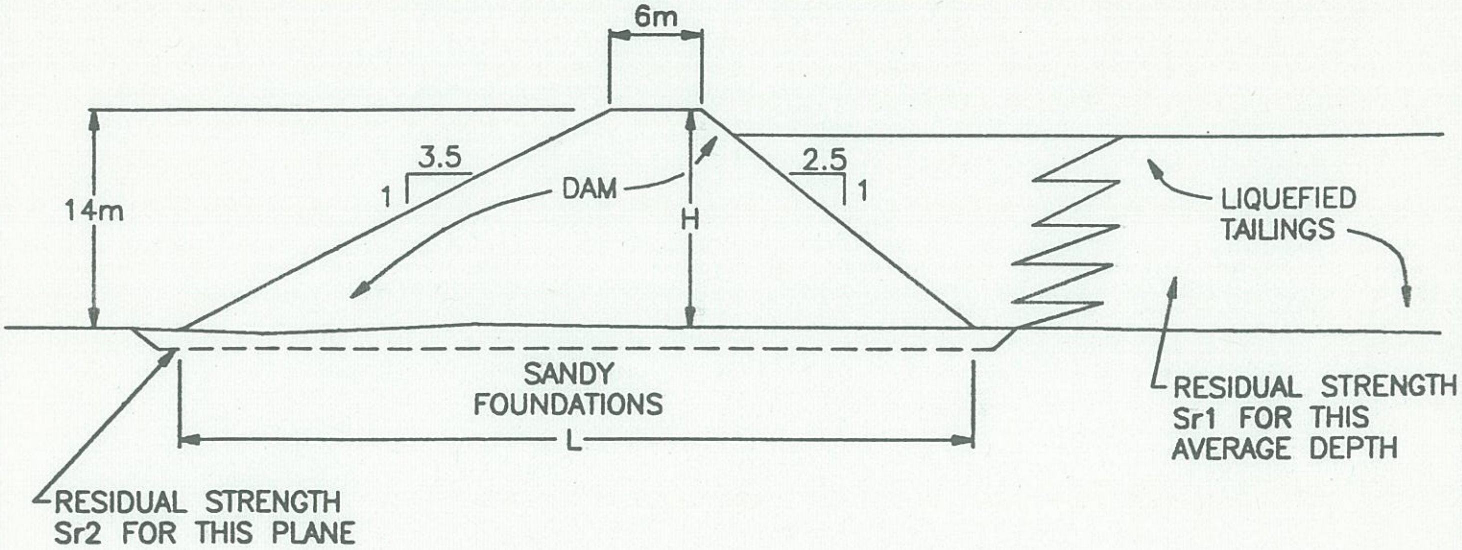
NOTES:

S_r = AVERAGE RESIDUAL SHEAR STRENGTH BACKCALCULATED ALONG FAILURE PLANE IN LIQUEFIED SOIL MASS USING POST–FAILURE GEOMETRY

σ_{vo}' = AVERAGE INITAIL VERTICAL STRESS IN LIQUEFIED SOIL MASS PRIOR TO FAILURE.

KLOHN-CRIPPEN	SCALE PROJECT MT. NANSEN GOLD PROJECT
	TITLE **STRESS – NORMALIZED S_r VERSUS $(N_1)_{60}$ FROM CASE HISTORIES**

CLIENT:	DATE OF ISSUE	PROJECT No.	DWG. No.	REV.
B.Y.G. NATURAL RESOURCES INC.		PB531403	FIG. IV–1	



Sr1 = RESIDUAL STRENGTH OF LIQUEFIED TAILINGS

Sr2 = RESIDUAL STRENGTH OF LIQUEFIED SANDS ALONG THE HORIZONTAL FAILURE SURFACE.

L = HORIZONTAL WIDTH OF DAM BASE

H = AVERAGE DEPTH OF THE FAILURE SURFACE.

SCALE NOT TO SCALE

KLOHN-CRIPPEN

PROJECT
MT. NANSEN GOLD PROJECT

TITLE
LIQUEFACTION FAILURE MODEL

CLIENT:
B.Y.G. NATURAL RESOURCES INC.

DATE OF ISSUE

APPROVED

PROJECT No.
PB531403

DWG. No.
FIG IV–2

REV.

The driving force (P_d) is generated by the hydrostatic head of the liquefied tailings (behaving as a dense slurry) behind the embankment, less a small strength component calculated from the residual strength (S_{r1}). The driving force is calculated according to the following equation:

$$P_d = 0.5\ \gamma\ h^2 - 2\ S_{r1}$$

$$P_d = (0.5)(12.26)12^2 - (2)(6.6) = 869\ \text{kN/m}$$

If we assume that the average depth of embankment dam above the foundation failure surface is about 8 m, then the residual strength (S_{r2}) along the basal failure plane is:

$$S_{r2} = (0.09)(17\ \text{kN/m}^3)(8\ \text{m}) = 13.8\ \text{kPa}$$

The length (L) of the failure surface times the residual strength (S_{r2}) gives the force resisting failure (P_r). Assuming a foundation length of 100 m, the resisting force is calculated according to the following equation:

$$P_r = L\ S_{r2}$$

$$P_r = (100)(13.8) = 1377\ \text{kN/m}$$

So the factor of safety against failure is equal to the ratio of the resisting force over the driving force:

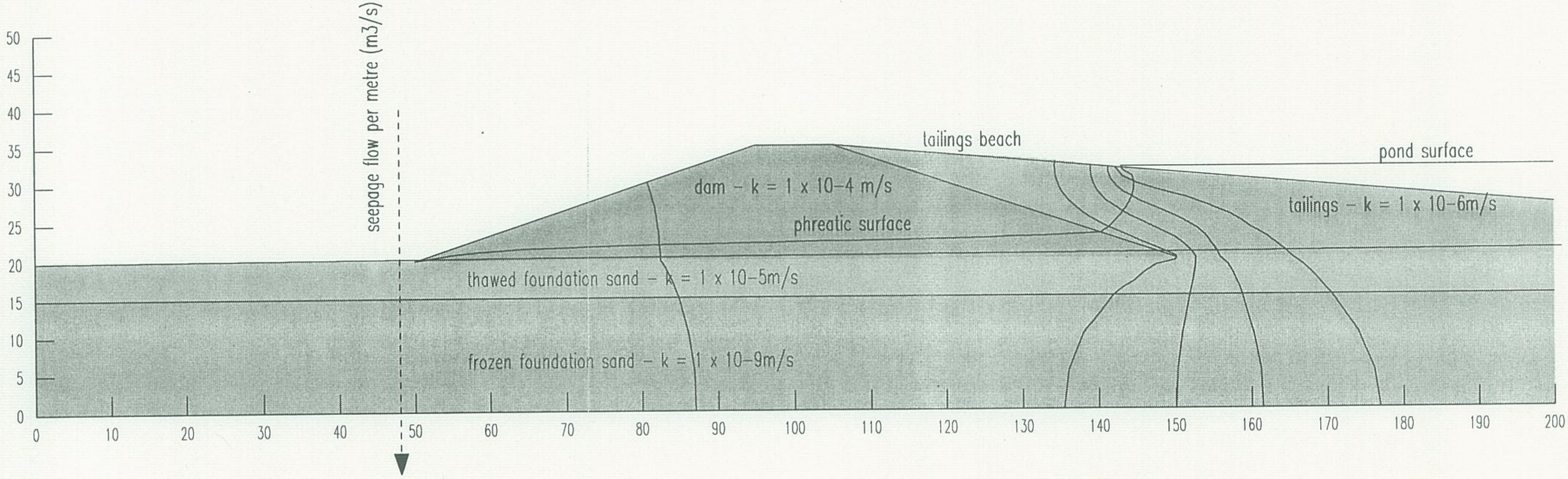
$$F = P_r\ /\ P_d = 1377/869 = 1.6$$

From this it can be seen that the factor of safety is proportional to the length of the failure surface, or the width of the dam. For this situation, a factor of safety of 1.1 is considered appropriate for design. A factor of safety of 1.1 is achieved when the dam base width is about 80 m.

APPENDIX V

Seepage Analysis

SEEPAGE ANALYSIS RESULTS



APPENDIX VI

Water Balance Analysis

Water Balance for Mt. Nansen

Average Year

Description	Units	Year 1											
		Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
Beginning of the Month WL		1137.0	1138.6	1139.6	1139.9	1140.1	1140.3	1140.5	1140.7	1140.8	1141.0	1142.9	1143.4
INFLOWS													
Average Year	mm	271											
Monthly Precipitation	mm	35.2	27.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	* 122.0	40.7	46.1
Natural Catchment	sq.km.	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46
Runoff Coefficient		0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Runoff Volume	cu.m.	9,723	7,480	0	0	0	0	0	0	0	33,658	11,219	12,715
Direct Inflow	cu.m.	1,409	1,084	0	0	0	0	0	0	0	4,878	1,626	1,843
Solids Inflow	cu.m.	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667
Total Inflow	cu.m.	17,799	15,230	6,667	6,667	6,667	6,667	6,667	6,667	6,667	45,203	19,512	21,225
OUTFLOWS													
Annual Evaporation	mm	453											
Monthly Evaporation	mm	79.7	37.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	107.8	120.5	107.8
Evaporation Loss	cu.m.	576	390	0	0	0	0	0	0	0	1,924	3,088	3,031
Loss to Voids	cu.m.	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333
Total Losses	cu.m.	3,910	3,724	3,333	3,333	3,333	3,333	3,333	3,333	3,333	5,257	6,421	6,364
Net Inflow	cu.m.	13,890	11,506	3,333	3,333	3,333	3,333	3,333	3,333	3,333	39,945	13,091	14,861
Existing Volume	cu.m.	19,655	33,544	45,051	48,384	51,717	55,051	58,384	61,717	65,051	68,384	108,329	121,420
Total Volume in Pond	cu.m.	33,544	45,051	48,384	51,717	55,051	58,384	61,717	65,051	68,384	108,329	121,420	136,281
End of the Month WL	m	1138.6	1139.6	1139.9	1140.1	1140.3	1140.5	1140.7	1140.8	1141.0	1142.9	1143.4	1143.9

* Cumulative precipitation from
October through May

Water Balance for Mt. Nansen

Average Year

Description	Units	Year 2											
		Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
Beginning of the Month WL		1143.9	1144.3	1144.5	1144.6	1144.7	1144.8	1144.9	1145.0	1145.1	1145.2	1146.1	1146.3
INFLOWS													
Average Year	mm	271											
Monthly Precipitation	mm	35.2	27.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	* 122.0	40.7	46.1
Natural Catchment	sq.km.	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46
Runoff Coefficient		0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Runoff Volume	cu.m.	9,723	7,480	0	0	0	0	0	0	0	33,658	11,219	12,715
Direct Inflow	cu.m.	1,409	1,084	0	0	0	0	0	0	0	4,878	1,626	1,843
Solids Inflow	cu.m.	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667
Total Inflow	cu.m.	17,799	15,230	6,667	6,667	6,667	6,667	6,667	6,667	6,667	45,203	19,512	21,225
OUTFLOWS													
Annual Evaporation	mm												
Monthly Evaporation	mm	79.7	37.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	107.8	120.5	107.8
Evaporation Loss	cu.m.	2,466	1,229	0	0	0	0	0	0	0	4,216	5,497	5,092
Loss to Voids	cu.m.	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333
Total Losses	cu.m.	5,799	4,562	3,333	3,333	3,333	3,333	3,333	3,333	3,333	7,549	8,831	8,426
Net Inflow	cu.m.	12,000	10,668	3,333	3,333	3,333	3,333	3,333	3,333	3,333	37,654	10,682	12,799
Existing Volume	cu.m.	136,281	148,281	158,949	162,283	165,616	168,949	172,283	175,616	178,949	182,283	219,936	230,618
Total Volume in Pond	cu.m.	148,281	158,949	162,283	165,616	168,949	172,283	175,616	178,949	182,283	219,936	230,618	243,417
End of the Month WL	m	1144.3	1144.5	1144.6	1144.7	1144.8	1144.9	1145.0	1145.1	1145.2	1146.1	1146.3	1146.6

* Cumulative precipitation from
October through May

Water Balance for Mt. Nansen

Average Year

Description	Units	Year 3											
		Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
Beginning of the Month WL		1146.6	1146.8	1146.9	1147.0	1147.1	1147.1	1147.2	1147.3	1147.3	1147.4	1148.0	1148.2
INFLOWS													
Average Year	mm	271											
Monthly Precipitation	mm	35.2	27.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	* 122.0	40.7	46.1
Natural Catchment	sq.km.	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46
Runoff Coefficient		0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Runoff Volume	cu.m.	9,723	7,480	0	0	0	0	0	0	0	33,658	11,219	12,715
Direct Inflow	cu.m.	1,409	1,084	0	0	0	0	0	0	0	4,878	1,626	1,843
Solids Inflow	cu.m.	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667
Total Inflow	cu.m.	17,799	15,230	6,667	6,667	6,667	6,667	6,667	6,667	6,667	45,203	19,512	21,225
OUTFLOWS													
Annual Evaporation	mm												
Monthly Evaporation	mm	79.7	37.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	107.8	120.5	107.8
Evaporation Loss	cu.m.	3,920	1,885	0	0	0	0	0	0	0	6,015	7,368	6,719
Loss to Voids	cu.m.	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333
Total Losses	cu.m.	7,253	5,219	3,333	3,333	3,333	3,333	3,333	3,333	3,333	9,348	10,701	10,052
Net Inflow	cu.m.	10,546	10,012	3,333	3,333	3,333	3,333	3,333	3,333	3,333	35,855	8,811	11,173
Existing Volume	cu.m.	243,417	253,963	263,975	267,308	270,641	273,975	277,308	280,641	283,975	287,308	323,163	331,974
Total Volume in Pond	cu.m.	253,963	263,975	267,308	270,641	273,975	277,308	280,641	283,975	287,308	323,163	331,974	343,146
End of the Month WL	m	1146.8	1146.9	1147.0	1147.1	1147.1	1147.2	1147.3	1147.3	1147.4	1148.0	1148.2	1148.3

* Cumulative precipitation from
October through May

Water Balance for Mt. Nansen

200-Year Wet

Description	Units	Year 1											
		Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
Beginning of the Month WL		1137.0	1139.3	1140.6	1140.7	1140.9	1141.1	1141.3	1141.5	1141.7	1141.9	1144.4	1144.9
INFLOWS													
200-Year Wet	mm	370											
Monthly Precipitation	mm	48.1	37.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	* 166.5	55.5	62.9
Natural Catchment	sq.km.	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46
Runoff Coefficient		0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8
Runoff Volume	cu.m.	17,701	13,616	0	0	0	0	0	0	0	61,272	20,424	23,147
Direct Inflow	cu.m.	1,924	1,480	0	0	0	0	0	0	0	6,660	2,220	2,516
Solids Inflow	cu.m.	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667
Total Inflow	cu.m.	26,291	21,763	6,667	6,667	6,667	6,667	6,667	6,667	6,667	74,599	29,311	32,330
OUTFLOWS													
Annual Evaporation	mm	453											
Monthly Evaporation	mm	79.7	37.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	107.8	120.5	107.8
Evaporation Loss	cu.m.	576	460	0	0	0	0	0	0	0	2,249	4,073	4,063
Loss to Voids	cu.m.	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333
Total Losses	cu.m.	3,910	3,793	3,333	3,333	3,333	3,333	3,333	3,333	3,333	5,582	7,406	7,396
Net Inflow	cu.m.	22,382	17,969	3,333	3,333	3,333	3,333	3,333	3,333	3,333	69,017	21,904	24,934
Existing Volume	cu.m.	19,655	42,036	60,006	63,339	66,672	70,006	73,339	76,672	80,006	83,339	152,356	174,260
Total Volume in Pond	cu.m.	42,036	60,006	63,339	66,672	70,006	73,339	76,672	80,006	83,339	152,356	174,260	199,194
End of the Month WL	m	1139.3	1140.6	1140.7	1140.9	1141.1	1141.3	1141.5	1141.7	1141.9	1144.4	1144.9	1145.6

* Cumulative precipitation from
October through May

Water Balance for Mt. Nansen

200-Year Wet

Description	Units	Year 3											
		Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
Beginning of the Month WL		1146.6	1147.0	1147.3	1147.3	1147.4	1147.5	1147.5	1147.6	1147.7	1147.7	1148.7	1149.0
INFLOWS													
200-Year Wet	mm	370											
Monthly Precipitation	mm	48.1	37.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	* 166.5	55.5	62.9
Natural Catchment	sq.km.	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46
Runoff Coefficient		0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8
Runoff Volume	cu.m.	17,701	13,616	0	0	0	0	0	0	0	61,272	20,424	23,147
Direct Inflow	cu.m.	1,924	1,480	0	0	0	0	0	0	0	6,660	2,220	2,516
Solids Inflow	cu.m.	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667
Total Inflow	cu.m.	26,291	21,763	6,667	6,667	6,667	6,667	6,667	6,667	6,667	74,599	29,311	32,330
OUTFLOWS													
Annual Evaporation	mm												
Monthly Evaporation	mm	79.7	37.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	107.8	120.5	107.8
Evaporation Loss	cu.m.	3,950	1,947	0	0	0	0	0	0	0	6,299	8,116	7,519
Loss to Voids	cu.m.	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333
Total Losses	cu.m.	7,283	5,280	3,333	3,333	3,333	3,333	3,333	3,333	3,333	9,632	11,450	10,852
Net Inflow	cu.m.	19,008	16,482	3,333	3,333	3,333	3,333	3,333	3,333	3,333	64,967	17,861	21,477
Existing Volume	cu.m.	245,910	264,918	281,401	284,734	288,067	291,401	294,734	298,067	301,401	304,734	369,701	387,562
Total Volume in Pond	cu.m.	264,918	281,401	284,734	288,067	291,401	294,734	298,067	301,401	304,734	369,701	387,562	409,039
End of the Month WL	m	1147.0	1147.3	1147.3	1147.4	1147.5	1147.5	1147.6	1147.7	1147.7	1148.7	1149.0	1149.3

* Cumulative precipitation from
October through May

Water Balance for Mt. Nansen

10-Year Dry

Description	Units	Year 1											
		Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
Beginning of the Month WL		1137.0	1138.3	1139.1	1139.4	1139.7	1140.0	1140.2	1140.4	1140.6	1140.7	1142.3	1142.7
INFLOWS													
10-Year Dry	mm	200											
Monthly Precipitation	mm	26.0	20.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	* 90.0	30.0	34.0
Natural Catchment	sq.km.	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46
Runoff Coefficient		0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Runoff Volume	cu.m.	7,176	5,520	0	0	0	0	0	0	0	24,840	8,280	9,384
Direct Inflow	cu.m.	1,040	800	0	0	0	0	0	0	0	3,600	1,200	1,360
Solids Inflow	cu.m.	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667
Total Inflow	cu.m.	14,883	12,987	6,667	6,667	6,667	6,667	6,667	6,667	6,667	35,107	16,147	17,411
OUTFLOWS													
Annual Evaporation	mm	453											
Monthly Evaporation	mm	79.7	37.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	107.8	120.5	107.8
Evaporation Loss	cu.m.	576	367	0	0	0	0	0	0	0	1,813	2,742	2,659
Loss to Voids	cu.m.	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333
Total Losses	cu.m.	3,910	3,700	3,333	3,333	3,333	3,333	3,333	3,333	3,333	5,146	6,075	5,993
Net Inflow	cu.m.	10,973	9,287	3,333	3,333	3,333	3,333	3,333	3,333	3,333	29,961	10,071	11,418
Existing Volume	cu.m.	19,655	30,628	39,914	43,248	46,581	49,914	53,248	56,581	59,914	63,248	93,208	103,280
Total Volume in Pond	cu.m.	30,628	39,914	43,248	46,581	49,914	53,248	56,581	59,914	63,248	93,208	103,280	114,698
End of the Month WL	m	1138.3	1139.1	1139.4	1139.7	1140.0	1140.2	1140.4	1140.6	1140.7	1142.3	1142.7	1143.1

* Cumulative precipitation from
October through May

Water Balance for Mt. Nansen

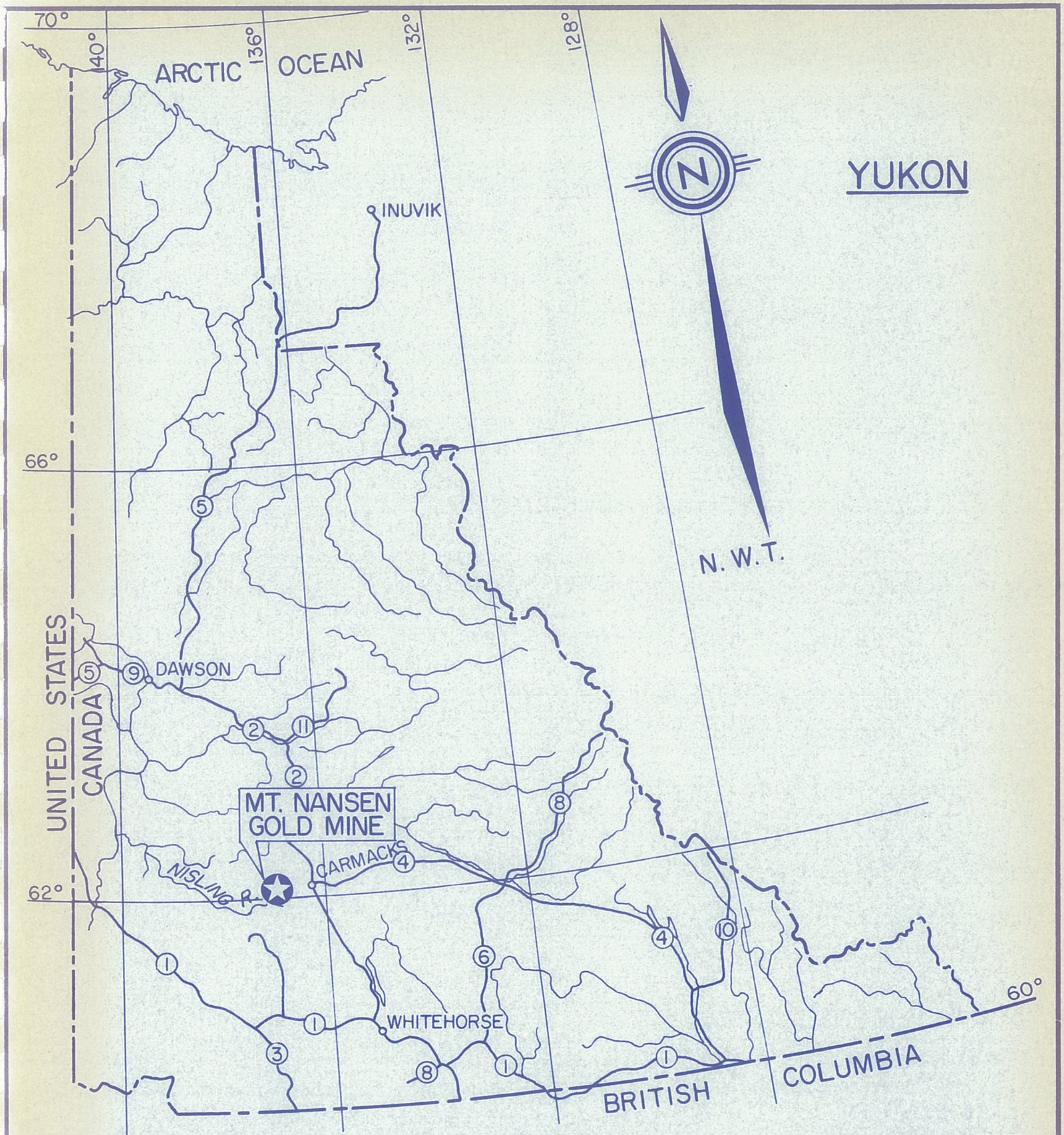
10-Year Dry

Description	Units	Year 3											
		Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul
Beginning of the Month WL		1146.6	1146.7	1146.9	1147.0	1147.0	1147.1	1147.1	1147.2	1147.3	1147.3	1147.8	1147.9
INFLOWS													
10-Year Dry	mm	200											
Monthly Precipitation	mm	26.0	20.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	* 90.0	30.0	34.0
Natural Catchment	sq.km.	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46
Runoff Coefficient		0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
Runoff Volume	cu.m.	7,176	5,520	0	0	0	0	0	0	0	24,840	8,280	9,384
Direct Inflow	cu.m.	1,040	800	0	0	0	0	0	0	0	3,600	1,200	1,360
Solids Inflow	cu.m.	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667	6,667
Total Inflow	cu.m.	14,883	12,987	6,667	6,667	6,667	6,667	6,667	6,667	6,667	35,107	16,147	17,411
OUTFLOWS													
Annual Evaporation	mm												
Monthly Evaporation	mm	79.7	37.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	107.8	120.5	107.8
Evaporation Loss	cu.m.	3,950	1,883	0	0	0	0	0	0	0	5,971	7,143	6,483
Loss to Voids	cu.m.	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333	3,333
Total Losses	cu.m.	7,283	5,216	3,333	3,333	3,333	3,333	3,333	3,333	3,333	9,304	10,476	9,817
Net Inflow	cu.m.	7,599	7,770	3,333	3,333	3,333	3,333	3,333	3,333	3,333	25,802	5,670	7,594
Existing Volume	cu.m.	245,910	253,509	261,280	264,613	267,947	271,280	274,613	277,947	281,280	284,613	310,415	316,086
Total Volume in Pond	cu.m.	253,509	261,280	264,613	267,947	271,280	274,613	277,947	281,280	284,613	310,415	316,086	323,680
End of the Month WL	m	1146.7	1146.9	1147.0	1147.0	1147.1	1147.1	1147.2	1147.3	1147.3	1147.8	1147.9	1148.1

* Cumulative precipitation from
October through May

DRAWINGS

A-3001	Location Plan
D-3002	General Arrangement Plan
D-3003	Plan, Section and Profile, Site #4



SCALE 0 50 100 miles

KLOHN-CRIPPEN

PROJECT
MOUNT NANSEN GOLD PROJECT

TITLE
SITE LOCATION

CLIENT:
B.Y.G. NATURAL RESOURCES INC.

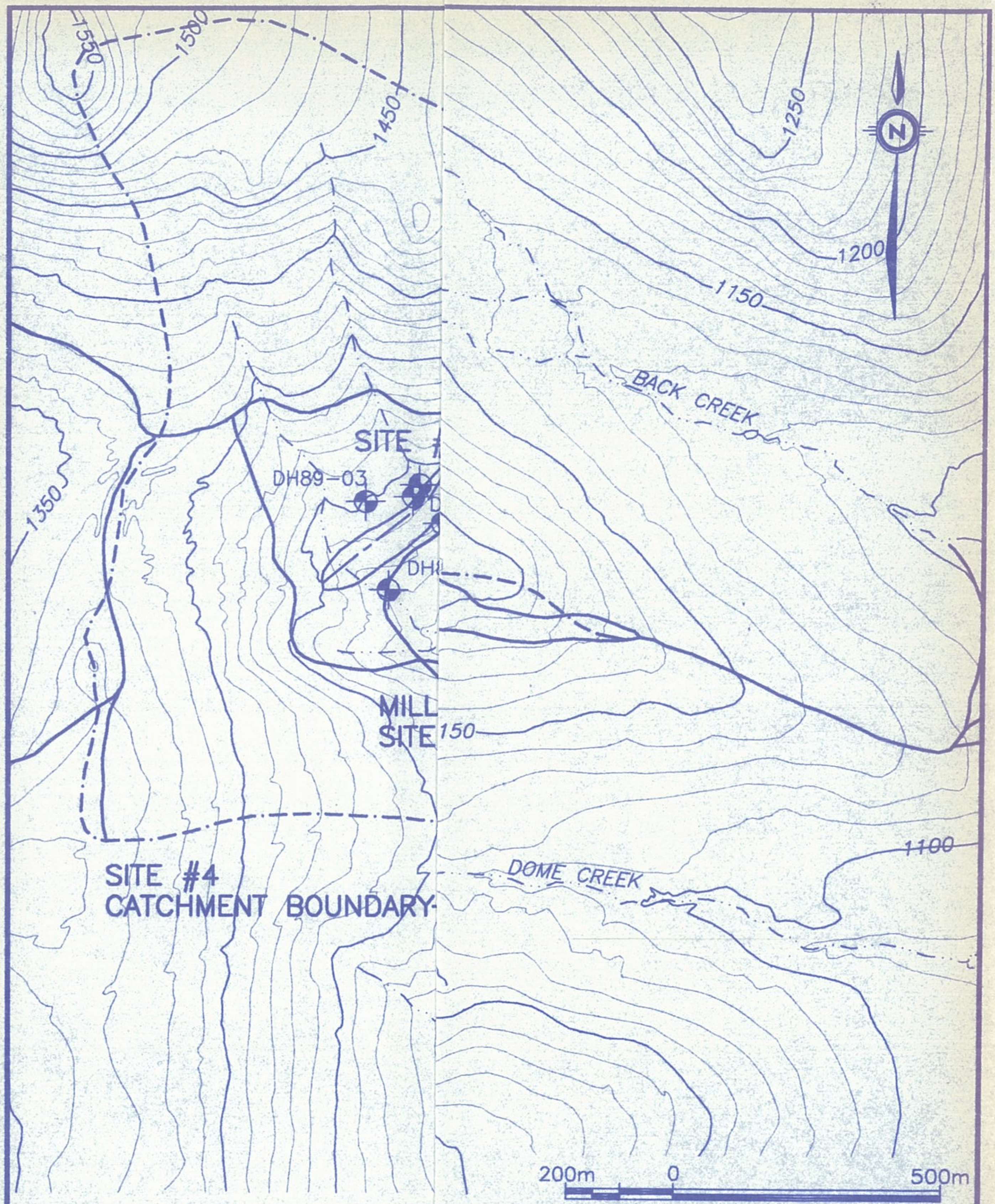
DATE OF ISSUE
APR 5, 1995

APPROVED

PROJECT No.
PB5314 03

DWG. No.
A-3001

REV.



PROJECT
MT. NANSEN GOLD PROJECT

TITLE
GENERAL ARRANGEMENT
PLAN

DATE OF ISSUE	PROJECT No.	DWG. No.	REV
APR 5, 1995	PB531403	D-3002	

August 23, 1994 9:09:21 a.m.
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