

**ENERGY ANALYSIS DESIGN REPORT
APU 3, 4 AND 5 SOLARWALL SOLAR AIR
HEATING RETROFIT
WHITEHORSE GENERAL HOSPITAL
WHITEHORSE, YT**

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1.0 Introduction

Reducing energy use for heating in the Canadian north has always been of prime importance due to the very long and severe heating seasons and high-energy costs. While there are many systems that have been used in the past many have failed or performed very poorly. Due to these past problems designers and contractors have often been reticent in installing energy efficiency measures (EEMs), especially on marginal payback applications, due to concerns over their long-term viability. Recently the use of energy efficiency measures has become globally more important due to higher energy costs and concerns over the impact of high-energy consumption on the environment. With this new demand for energy reduction and recovery systems more efficient and reliable equipment has become available making marginal payback systems more attractive.

One system that is now available is the Solarwall passive air solar air heating system. The Solarwall passive solar heating system is used to preheat ventilation air to reduce ventilation heating energy. To preheat the ventilation air the Solarwall utilizes renewable solar energy through an essentially passive system. While there is great potential energy available in solar energy the limitations of utilizing it for ventilation preheat have traditionally made payback on installations in Northern climates difficult. With higher energy costs, however, the potential for this system has vastly improved.

Within the existing Whitehorse General Hospital there are at this time existing mechanical energy reduction and recovery systems. APU 1 and 2, the main treatment area units are fitted with enthalpy wheel energy recovery units capable of operating efficiencies approaching 70%, reducing ventilation preheat requirements for these units. The majority of the AHU and certain hydronic systems are variable flow allowing reduction in standby losses and pumping/fan operating costs.

Other potentially viable systems were not, however, included in the original systems most likely due to poor payback potential based on energy costs at the time of design. With the increase in energy costs certain systems may be now more viable. Most recently a secondary sales electric LPS boiler retrofit has been initiated with construction scheduled for spring 2003. This system results in a reduction in total energy consumption due to an improvement in system efficiency, a reduction in operating costs due to the low rate of secondary sales energy and a reduction in greenhouse gas production due to the use of hydroelectric energy instead of fuel oil heating.

In addition other areas of potential energy reduction were reviewed in a preliminary investigation completed by Northern Climate Engineering in March 2002. Most significantly, for this analysis, was the use of a Solarwall passive solar air heating system to preheat the ventilation air for APU 3, 4 and 5 located in the new building Fan Mezzanine and the retrofit of a RegentEco heat recovery exchanger (HRE) on APU 6.

The preliminary study completed by Northern Climate Engineering showed positive results for both the RegentEco HRE and the Solar wall air heating with paybacks in the 6 year time period based on fuel oil heating. As a result of the positive findings of the Feasibility Investigation, the Energy Solutions Center in conjunction with the Whitehorse General Hospital has advanced the two projects to the design and construction stage. This report is the first deliverable for this project.

While viability was proven in the feasibility investigation, the modeling tools used were relatively crude. Given the high initial capital expenditures for these two projects (\$122k-March 2002-NCE) it was determined that prior to initiating the actual capital works more in-depth energy models and costing be completed to verify the feasibility investigation conclusions. This Energy Analysis design report is the deliverable for the more detailed model and attendant evaluation for the Solarwall passive solar air heating system.

2.0 Existing Facility Background

The Whitehorse General Hospital is a 49-bed acute care facility completed in approximately 1997. This facility is comprised of about 7150m² of new building joined to 3865m² of old renovated hospital. Basements and service spaces are approximately 8063m². Total building area is 19051m².

In addition to the hospital loads the Energy Center for the hospital also provides building and service water heating to the adjacent Thompson Center. This long-term care facility is a single storey building of 3658m² with a full heated crawlspace and basement.

The hospital layout is programmed over two floors with the existing renovated hospital and the new building linked by an enclosed and heated atrium. Administration, outpatients and offices have been located in the old renovated hospital. The new building houses the main patient care functions including the wards, OR and procedures. Housekeeping and Nutrition are also located within the new building with the physical plant located in a separate attached Energy Center to the north of the main buildings.

The Thompson Building is linked to the south end of the hospital with heating services provided through a service utilidor.

The facility HVAC and mechanical systems are similar to those found in acute care hospitals and long term care facilities in other cold climate regions. Three fuel oil fired low-pressure steam (LPS) boilers provide building heating and service heat for humidification, DHW and service hot water heating and LPS for kitchen appliances. For building heating, steam/water and steam/glycol converters located in the boiler room and Thompson Building basement are used to convert the LPS to hydronic heating. The water circuits are used for all building heating. The glycol circuits for the ventilation system air-processing unit (APU) provide heating for ventilation preheat and reheat.

Recently a secondary sales electric LPS boiler retrofit has been initiated with construction scheduled for spring 2003. This system will result in a reduction in total energy consumption due to an improvement in system efficiency, a reduction in operating costs due to the low rate of secondary sales energy and a reduction in greenhouse gas production due to the use of hydroelectric energy instead of fuel oil heating. Detailed discussion of this system is provided in a series of three reports prepared by FSC Architects and Engineers; the Secondary Sales Feasibility Study-Final Submission Jan 15/02, the Energy Analysis Design Report Secondary Sales Electric Boiler-Final Draft Dec 20/02 and the Design Development Report Secondary Sales Electric Boiler-Final Draft Dec 20/02. To summarize two new 1.36MW LPS boilers will be retrofit into the existing generator room. The new boilers will be operating in parallel with the existing FO fired boilers to provide building and service heating. Secondary sales energy is programmed to be provided at approximately 90% availability at a discounted rate of about \$0.033/kWh resulting in a reduction in annual energy costs by about 60% and a payback in capital investment of less than 3 years.

Seven APU and two AHU (smaller fan coil units) provide ventilation for the hospital. APU 1 and 2 are the main units for the treatment areas. The units operate in parallel and are provided with

energy wheel heat recovery. APU 3 provides ventilation to the lower tech treatment areas and general spaces. Heat recovery is not provided on this unit. APU 4 and 5 are 100% redundant units that provide ventilation to the general spaces and areas of refuge. APU 1 thru 5 all operate on 100% outdoor air and are located in the new fan mezzanine. APU 6 and 7 are located in the renovated hospital mezzanine and are re-circulating units with return fans. APU 6 provides ventilation to the offices while APU7 to the atrium.

The two smaller AHU's are located in the hospital Ambulance Bay (AHU1) and the Energy Center (AHU 2). AHU 1 provides ventilation for control of CO/NOx in the Ambulance Bay. AHU 2 provides cooling and combustion air for boiler operation in the Energy Center.

In the Thompson Building a total of 5 main AHU provide ventilation to the Central, North and South wings of the building. In addition three service units provide ventilation to the two basement mechanical rooms and crawlspace.

LPS for humidification is provided direct from the main LPS system. Steam grid humidifiers located on all the APU provide primary humidity control. In addition local control by duct mounted steam grids provides supplementary humidification for high load critical zones.

Four storage tanks in the Hospital and two in the Thompson Center with tankless heaters provide 82degC service hot water and 60degC domestic hot water in the hospital. An independent high-pressure steam system with two oil-fired boilers provides HPS for sterilization in the Hospital

Medical gas systems, specialty medical mechanical systems, fire protection systems and fuel systems have not been reviewed as a component of this project.

3.0 Energy Modeling and Discussions

Energy Modeling

The purpose of this Energy Analysis was to confirm the findings of the Feasibility Investigation prepared in 2002 by NCE using a RETScreen analysis.

The Solarwall as proposed by NCE in the March 2002 Feasibility Study was recommended for preheat of the outdoor air for APU's 3, 4 and 5. These three fans are all located in the main Hospital fan mezzanine and share a common outdoor air intake located on a southwest exposure wall. The outdoor air intake is located approximately mid wall level with a metal wall finish from the louvers up to the eave and an independent finish for the lower portion of the wall below the louvers. Since the lower wall finish does not lend itself to a solar wall type finish without impacting the architectural finish of the building the initial RETScreen analysis prepared by NCE was completed for the upper portion of the wall area.

The reasoning behind limiting the Solarwall to the upper wall area as elected by NCE is, in review of the building appears to be valid. In addition exposure angles to the lower wall area are poor along with additional obstructions to the South and Southwest of the wall that may affect performance of any lower sections of the Solarwall, these reasonably apparent in Figure 3.1.

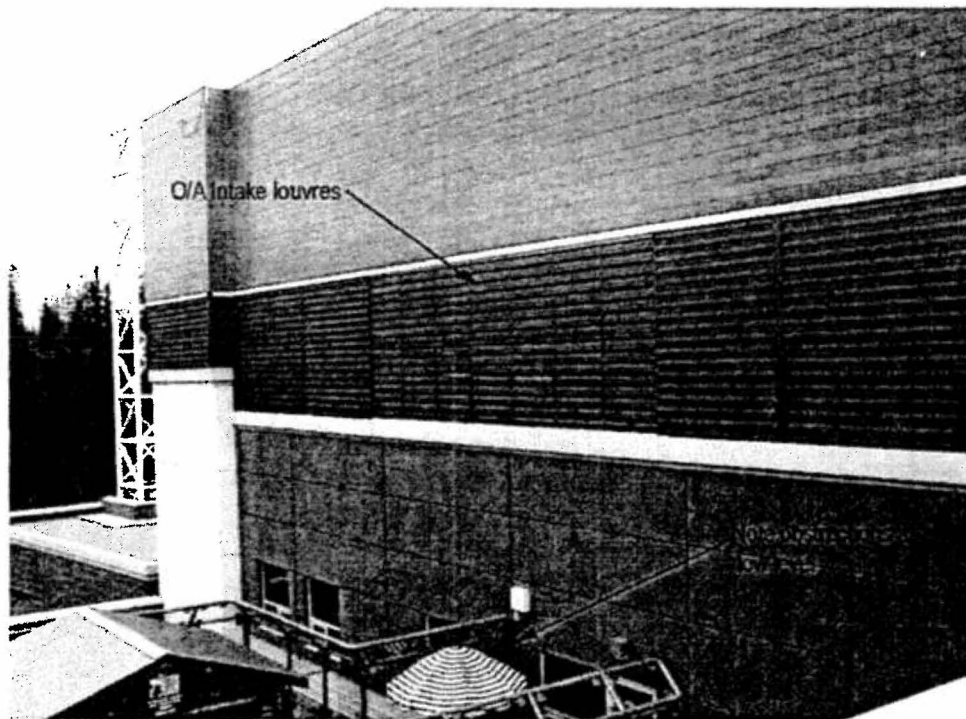


Fig 3.1 SW Facing Wall of Fan Room viewed to west.

NCE completed two models, the first for a smaller wall area covering a lower band of the wall only, and a second model for the Solarwall covering the complete upper section of the SW wall. The conclusion from the NCE models was that the payback was the same for both systems with greater annual savings for the larger wall area due to the higher amount of recovered energy, but with correspondingly higher initial capital investment.

As noted briefly NCE reported that initial payback was the same for the two different wall areas tested. The lower area was defined as the dark banded metal wall area where the intake louvers are located at a total of 84m². The larger area was comprised of the lower area along with the upper lighter wall above the intake louvers for a total area of 232m². For both these estimates the area of wall located along the stairwell on the west end of the wall was not included.

Using these design areas and energy costs of \$0.424/L for heating fuel and a marginal rate of \$0.131/kWh for electrical energy NCE reported the following values:

Design Area	Capital Cost		Energy			Payback	
	w/o REDI grant	w/ REDI grant	Renewable Energy Collected	Bldg Heat Loss Captured	Renewable Energy Delivered	w/o REDI grant	w/ REDI grant
84 m ²	\$28 500	\$20 600	49.3MWh	4.6MWh	53.9MWh	9 yrs	6 yrs
232 m ²	\$62 000	\$43 400	114.7MWh	12.5MWh	127.1MWh	9 yrs	6 yrs

Fig 3.2 NCE March 2002 Data Summary

To verify these results FSC was contracted to complete an updated analysis using a higher accuracy model for energy performance and to update capital cost estimates. To complete this work the DOE2.1e modeling tool was selected as the preferable method. This program is the premier 8760hr-modeling tool currently in use in North America. In essence this program allows designers to accurately model energy consumption in a building on an hourly basis accurately accounting for both internal and external gains and losses and completed detailed analysis of EEM's.

Energys Analytics who specialize in energy modeling building science, load research, and customized energy information systems provided development of the energy performance model. To complete this task Energys utilized the calibrated DOE2 model that was completed for the Secondary Sales Energy Analysis project, details for which are described in the Secondary Sales reports noted in Section 2.0. DOE2, however, did not have the capability to analyze a Solarwall EEM directly so data was extracted from the original DOE2 model on an 8760hr basis by creating a 'solarwall' surface with the same characteristics as an actual Solarwall. This data was then used to calculate the energy reclaimed using an excel spreadsheet and calculation procedures from ASHRAE and the Solarwall manufacturers literature.

More detailed explanations of the procedure are provided in Appendix B, along with summaries provided by Energys Analytics. Included are samples of the data files and analysis files that show the general calculation methods used (note complete output for this report is not possible due to the size of the file to accommodate the 8760hrs of data).

The original intent was that the new model parameters would be selected where possible to coincide with the original NCE values to allow better cross-referencing. This, however, was not deemed to be practical since various differences were immediately noted. First, during discussions with ESC it was determined to evaluate only the larger wall area option since paybacks between the two areas were initially reported as been equal. In addition for the wall area FSC determined that by using the adjacent stairwell area the actual solar wall area could be increased to approximately 248m² to maximize the potential area.

Also of note is the total air volume that the Solarwall is capable of handling. The NCE models allowed the SAH fan flow rate to exceed 980m³/h/m² for the 84m² option and 355m³/h/m² for the 232m² option. Both of these values exceed the Solarwall maximum recommended ventilation rate of 127m³/h/m². Using this value the actual portion of the air that can pass through the Solarwall is greatly reduced from the NCE value of 82300m³/h to about 31740m³/hr. Using these adjusted values the DOE model generated the following energy recovery rates:

Design Area	Energy		
	Renewable Energy Collected	Bldg Heat Loss Captured	Renewable Energy Delivered
248 m ²	70MWh	2.75MWh	72.75MWh

Fig 3.3 DOE Database Annual Energy Saved

Immediately it is apparent that the DOE database calculated energy delivered is only approximately 60% of the value estimated by NCE for a similar wall area. To reconcile this the NCE RETScreen model was updated using the adjusted air volumes and Solarwall area. This comparison showed a reduction in renewable energy delivered to 116.4MWh that still exceeds the DOE database model by approximately the same value.

Design Area	Energy		
	Renewable Energy Collected	Bldg Heat Loss Captured	Renewable Energy Delivered
248 m ²	103.3MWh	13.1MWh	116.4MWh

Fig 3.4 Base RETScreen Annual Energy Saved

This very high difference between models raised concern that either the DOE database model or the RETScreen model was in error. To account for the differences FSC and Enersys evaluated the two model parameters with respect to the input and generated data. First the annual Solarwall energy availability was reviewed. From the DOE database model the annual Solarwall Energy Availability was calculated at 181MWh for a Solarwall absorptive of 0.8 and area of 248m². In comparison the annual availability for RETScreen is calculated at 202MWh or a difference of only about 10%. Further a monthly comparison was completed and is shown in Figure 3.5.

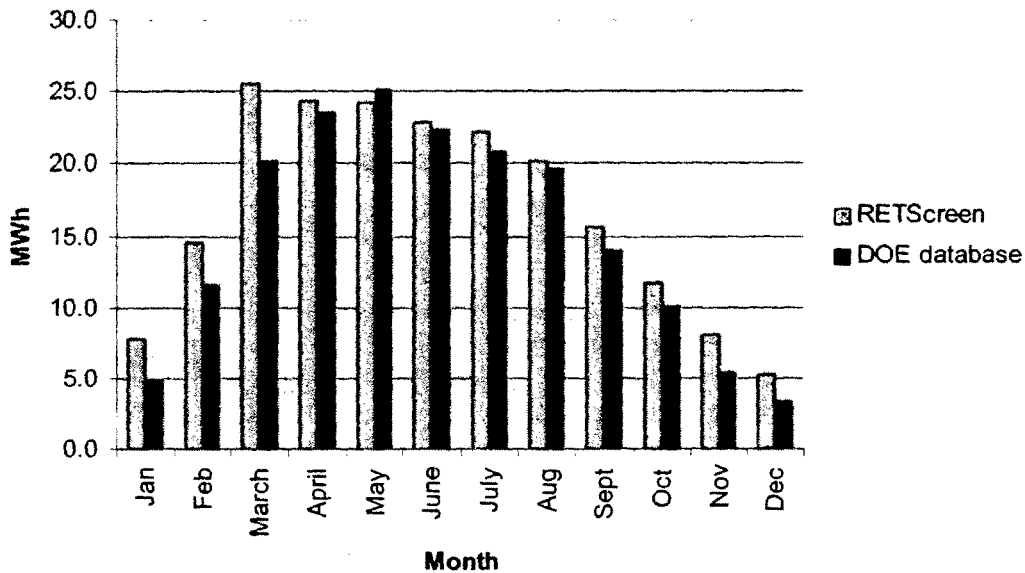


Fig 3.5 DOE Database vs RETScreen Monthly Solarwall Energy Availability

Again general conformance between the two models is very good with the exception of the month of March. This variation can easily be explained due to the method of calculating the availability or due to the level of reflectance that the programs used. The RETScreen model is based on average monthly data that averages the solar radiation, haze and overcast levels to a single monthly value. In comparison the DOE database is an hourly base that uses specific solar radiation, haze and overcast factors for each hour of a typical year. The use of hourly data has been proven as providing a considerably more accurate representation of actual conditions and is the recommended method for modeling energy consumption by ASHRAE and the Canadian National Energy Code for Buildings. What this tended to indicate is that the difference between the two models is neither the solar values used nor the way that they are calculated.

The second area reviewed was the building heat recaptured. In the case of the DOE database model the recaptured heat was estimated at 2.75MWh vs 13.1MWh for the RETScreen model. This is a significant difference, however, when compared to the total energy delivered the variation can only account for error in between 5-10% of the total, which is not significant enough to account for the 40% difference in the total values.

The final area of consideration was the usefulness of the solar energy captured. To determine this the energy required for preheat without the solar wall must be compared to the amount of energy available from the Solarwall. Where the energy available from the Solarwall exceeds the required value the energy cannot be used and the recovered energy is 'wasted'. In the case of the ventilation systems the leaving air temperature from the units must not exceed the unit discharge air temperature, which determines the required energy. The Solarwall leaving air temperature can, however, exceed the unit leaving air temperature since the full volume of the ventilation units cannot pass through the Solarwall allowing un-preheated air to blend with the Solarwall preheated

air to meet the heating requirements. Again the RETScreen model uses a monthly average to calculate this based primarily on what appears to be the maximum delivered air temperature. The DOE database model in comparison calculates the hourly values to determine the amount of captured solar energy that can be used. To address the difficulty in using a monthly average the RETScreen designers have provided a user input control "Fraction of Month Used" to allow fine-tuning of the usefulness. To review this the monthly fraction of energy used by the DOE database model was input into the RETScreen model user input control and the acceptable discharge air temperature adjusted to the maximum acceptable Solarwall air temperature to maintain a blended 13.5degC temperature. Using these values the adjusted RETScreen model Renewable Energy Delivered was calculated at 80.4MWh, or only a 10% difference to the DOE database model at 72.75MWh. This seems to indicate that the major difference in the models is in the usefulness of the energy and the method the model uses to estimate this value. The adjusted RETScreen values are summarized in Figure 3.6.

Design Area	Energy		
	Renewable Energy Collected	Bldg Heat Loss Captured	Renewable Energy Delivered
248 m2	70.8MWh	9.5MWh	80.4MWh

Fig 3.6 Adjusted RETScreen Annual Energy Saved

At this stage, models using the SWIFT99 program, which is approved for use on Solarwall analysis by NRCan, were completed in a further attempt to reconcile the RETScreen and DOE database models. Using this program models using parameters similar to those used for the RETScreen and DOE database were completed. The final energy values for a base model with no adjustments generated by this program were as follows in Figure 3.7.

Design Area	Energy		
	Renewable Energy Collected	Bldg Heat Loss Captured	Renewable Energy Delivered
248 m2	120MWh	12.2MWh	132MWh

Fig 3.7 SWIFT99 Annual Energy Saved

As can be noted these values significantly exceeded those estimated by the DOE database but more closely matched the unadjusted RETScreen. In comparison, relative to DOE database the SWIFT values are approximately 40% greater. Relative to the RETScreen models the SWIFT values are 13% to the unadjusted RETScreen model and 40% relative to the adjusted model. To reconcile these differences again an analysis comparing the different models was completed. In this instance the Solarwall Energy Availability is not output from the SWIFT so in-lieu the solar radiation incident on the Solarwall surface was used to compare the potential solar energy. Both on an annual and monthly basis large differences between the solar values are evident. Figure 3.8 provides a graphical representation of the differences.

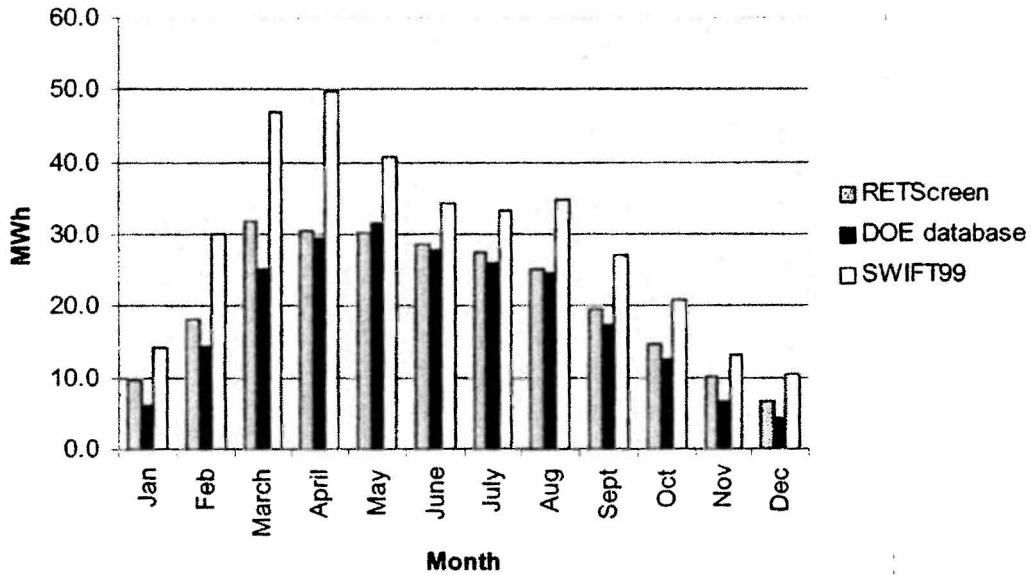


Fig 3.8 DOE Database / RETScreen / SWIFT Monthly Solar Radiation Incident on Solarwall

Figure 3.8 shows the relatively close correlation between the RETScreen and DOE database models, however the SWIFT values are significantly higher throughout the year varying at up to 60% higher.

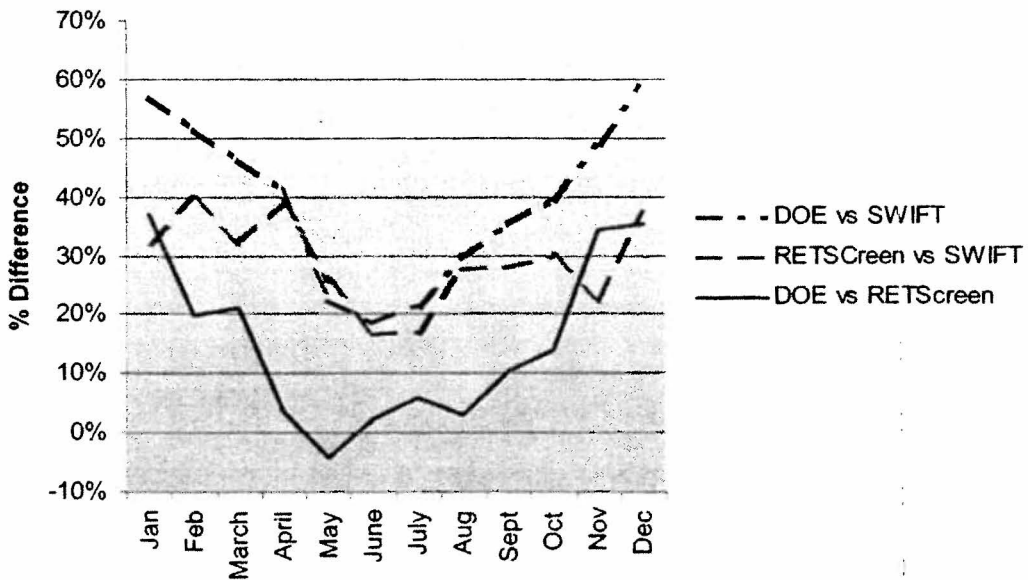


Fig 3.9 DOE Database / RETScreen / SWIFT % Difference in Monthly Solar Radiation Incident on Solarwall

This is especially noticeable during the winter months with the correlations being considerably higher during the summer months. Figure 3.9 displays the difference in a % basis between the models. On an average basis the difference between DOE and SWIFT is 40%, RETScreen and SWIFT 29% and DOE and RETScreen 15%. On a total annual basis SWIFT estimates a total of 355MWh of solar radiation incident on the Solarwall surface in comparison to 253MWh and 226Mwh for RETScreen and DOE respectively. This seems to indicate that the major difference in the output generated between the RETScreen and DOE vs the SWIFT is the actual solar radiation values and the effect of haze, overcast and reflectance. These values unfortunately are fixed within the database of SWIFT and RETScreen and essentially nothing can be done by an end user to modify these values to reconcile them with other modeling programs.

To summarize, initially a DOE database model for the proposed Solarwall installation was completed. This model was completed for comparison to the initial RETScreen energy models developed by NCE in March 2002. Variation between the models was significant prompting FSC to update the NCE RETScreen model to more closely match the new design parameters.

A large difference was still noted between the two models so an analysis of the differences was completed. This analysis indicated that the variation between the models appeared to be due to the solar energy captured and its usefulness. The RETScreen model appeared to be utilizing energy that the DOE model indicated was not usable, due to the operating requirements of the system. Using the DOE model, monthly utilization values were generated and then applied to the "Fraction of month use" available on the RETScreen model. When these values were applied correlation between the two models was excellent.

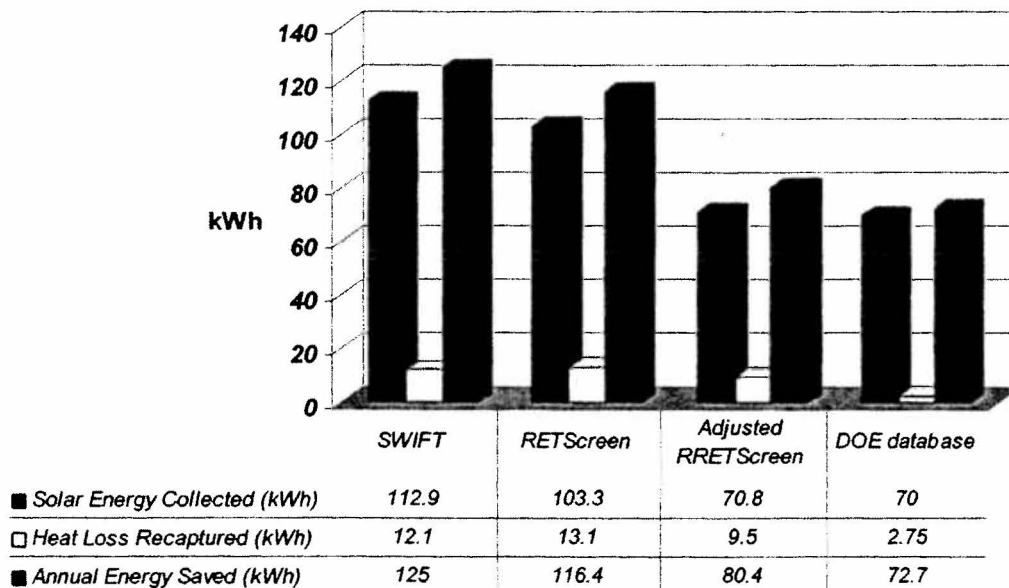


Fig 3.10 Annual Energy Saved by Model Type

Finally a third system, SWIFT99, was used to model the proposed Solarwall. While correlation between the adjusted RETScreen and DOE was completed the SWIFT model indicated considerably higher energy recovery and utilization than any previous model, including the base RETScreen models. A review of the three models indicated that the differences were associated with the calculated solar radiation incident on the Solarwall which is a fixed weather related variable in the program.

The output from the various program models is summarized in Figure 3.10, which shows the energy recovered and the difference between the models. Figure 3.11 shows an annual distribution of the Calculated Collected Solar Energy by the Solarwall. For the two RETScreen models a monthly breakdown of this data was not available.

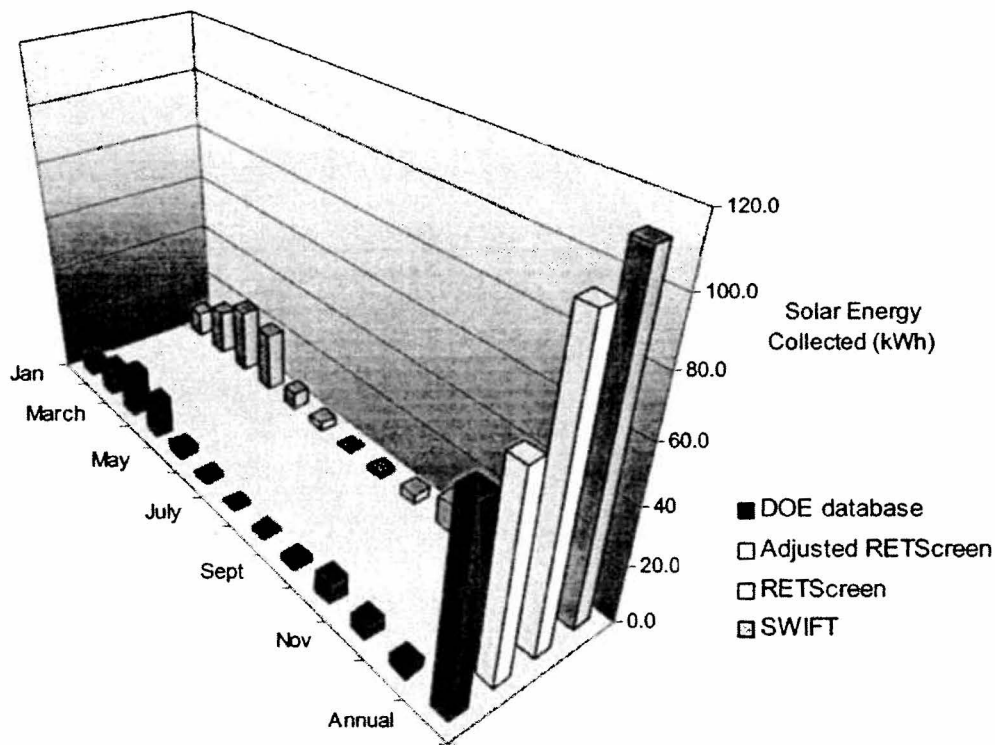


Fig 3.11 Calculated Solar Energy Collected

In conclusion, a significant difference in output of the three models is apparent for essentially the same data inputs. Where possible the differences were reconciled, however, due to the limitations of user input in the RETScreen and SWIFT programs little could be done to reconcile the variation between all the models. The results then predict a difference of up to 40% in annual energy recovered that will result in a corresponding variation in payback and positive cash flows discussed in subsequent sections.

Solarwall Installation

The Solarwall as proposed by NCE in the March 2002 Feasibility Study was for APU 3, 4 and 5 located in the main Hospital fan mezzanine. These APU all share a common outdoor air intake located on the southwest exposure wall of the fan room. The outdoor air intake is located approximately mid wall level with a metal wall finish from the louvers up to the eave and an independent finish for the lower portion of the wall below the louvers. Since the lower wall finish does not lend itself to a solar wall type finish without impacting the architectural finish NCE based their analysis on only the upper portion of the wall area.

The reasoning behind limiting the Solarwall to the upper wall area as elected by NCE, in review of the building, appears to be valid. In addition exposure angles to the lower wall area are poor along with additional obstructions to the South and Southwest of the wall that may affect performance of any lower sections of the Solarwall. As noted previously these are reasonably apparent in Figure 3.1.

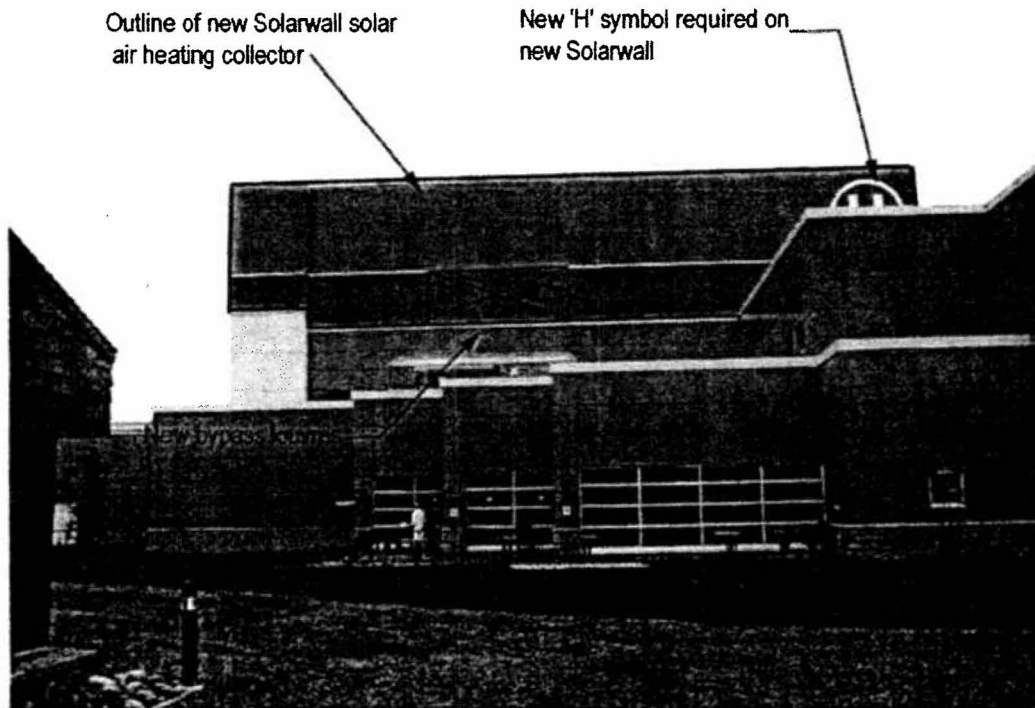


Fig 3.12 Location of new Solarwall and bypass damper

As discussed in the section on Energy Modeling the Solarwall rated air volume is restricted to a maximum of 31740m³/hr. In comparison the total air volume for AHU 3, 4 and 5 under typical operating conditions is 82300m³/hr enabling only 38% of the typical operating outdoor air to pass through the Solarwall. To enable this a volume of air must bypass the Solarwall at all times with the remainder being drawn through the Solarwall. This would be accomplished by providing a

bulkhead approximately 450mm in depth formed by the Solarwall above and around the current location of the existing louvers with a mixing plenum through the bulkhead to the exterior surface of the Solarwall. The mixing plenum will be located in the current location of the existing louvers and will be fitted with a set of new 100% volume bypass louvers and dampers located at the Solarwall surface. Within the void formed by the Solarwall and the building wall, fresh air intake openings from the Solarwall void into mixing plenum will be fitted with control dampers. This system will then enable the nominal 52% fresh air that cannot pass through the Solarwall to go direct to the units while the remaining 48% will be drawn in through the Solarwall and into the mixing plenum through the openings located inside the Solarwall cavity. To optimize the energy recovery the dampers will modulate to maintain a 13.5degC entering air temperature into the existing fresh air intake plenum located inside the fan room. When temperatures exceed the desired set point the dampers will be able to proportionally control to a maximum 100% from the bypass louvers. This arrangement is a relatively simple economizer mixing system that is used throughout the ventilation industry.

During the models the solarwall colour has been selected as a standard Green or Blue. Both colors have a solar absorptivity of 0.80. In comparison black has an absorptivity of 0.95, which helps improve the viability of the Solarwall, but will not match the existing colour scheme as effectively. In addition to the base colour a new hospital symbol will be required to be placed on the new Solarwall surface. This white color will reduce the effectiveness of the system due to its very low absorptivity, however, this effect was not included in any of the models generated.

4.0 Capital Costs and Financial Analysis

Capital investment costs by NCE for the 2002 Feasibility Investigation were estimated at a base value of \$62 000 for a total Solarwall area of 232m². NRCCan Renewable Energy Deployment Initiative grants were applied at the maximum 40%, based on the classification of Whitehorse as a remote community. This resulted in an adjusted cost of \$43 400. Using these construction estimates and based on marginal energy rates of \$0.42/L for fuel and \$0.131/kWh for electrical energy NCE estimated positive cash flow in 5.2 years and simple payback in 5.8 years. For this cost benefit analysis energy escalation was set at 3%, inflation 2% with a discount rate of 7%.

The NCE costs were based on the fuel oil fired system costs. As noted in the initial introduction, a secondary sales electric LPS boiler retrofit has been initiated in the interim with construction scheduled for spring 2003. This system will provide energy at a rate of \$0.033/kWh and a thermal efficiency of about 90% or about \$0.0367/ekWh. In comparison the current fuel system, based on a cost of \$0.45/L and the annual calculated thermal efficiency of 80% (calculated during the Secondary Sales Energy Analysis) provides energy at a rate of \$0.052/ekWh.

For the secondary sales system availability is estimated at a maximum of 92%. To allow an accurate cost analysis the blended equivalent energy rate of \$0.0431/ekWh at 100% efficiency was used in the cost analysis spreadsheets.

The updated capital costs for the proposed Solarwall are approximately \$166 000. These costs were provided as a budget quotation through the Vancouver distributor for Solarwall with installation costs provided by a local Whitehorse contractor. In comparison the 2002 Feasibility Investigation estimated capital costs at approximately \$62 000 for a similar area, less than 50% of the current estimated value. Details of the cost estimate can be found in Appendix D. The updated costs include all capital and construction costs plus a 10% construction contingency. The costs do not include design costs, taxes or administration costs.

To allow for an accurate and flexible cost analysis the NRCAN RETScreen analysis tool was used as a financial estimating tool for both the RETScreen and DOE database models. To accomplish the financial analysis for the DOE database the Solarwall model was used with the recovered energy values forced to match the values calculated by the DOE database model. This allowed the use of the financial summary and green house gas tools included in the RETScreen spreadsheets. For the SWIFT model the financial analysis was calculated using the SWIFT financial analysis system. For all estimates similar energy cost escalation rates, inflation and discount rates were used. The discount rate was based on a base ASHRAE Handbook rate of 4.5%, which reflects the USDOE recommended rate. Inflation was set to 3% and fuel escalation to 5%. In addition project life was set to 25 years that reflects a typical life cycle for a long-term energy recovery systems. Cost benefit analysis was completed for all four energy models comparing both a fuel fired system and a blended secondary sales/fuel oil fired system.

The NRCCan Renewable Energy Deployment Initiative grant was applied at the maximum 40%, based on the classification of Whitehorse as a remote community for all financial analysis.

Model Description	Fuel Oil Heating			Secondary Sales Heating		
	Annual Savings*	Positive Cash Flow	Simple Payback	Annual Savings	Positive Cash Flow	Simple Payback
DOE database	\$3806	16.8y	27.0y	\$3125	19.3	33.1
RETScreen (Adjusted)	\$4209	15.6y	24.5y	\$3464	18.0	30.1
RETScreen	\$6099	12.2y	17.1y	\$5007	14.2	21.1
SWIFT	\$6516	n/a**	15.3	\$5375	n/a**	18.5

* Net savings adjusted for increased fan kWh requirements, \$2002

** Output not provided by SWIFT

Fig 4.1 Summary of Financial Analysis by Energy Model

Based on the financial parameters payback on all modeled systems is marginal regardless of the modeling tool used. This is primarily due to the relatively high cost of installation due to retrofit of a new bypass/economizer section, the elevated work necessary for the installation and the lack of any credits on finishes that are typical on new installations. Further the payback and positive cash flows are considerably longer than those estimated in the Feasibility Investigation, again primarily associated with the higher estimated capital costs.

5.0 Green House Gas Reduction

The RETScreen and SWIFT energy models were also utilized as a simple means to estimate the reduction in green house gas emissions by using solar air heating to offset fuel fired energy. This analysis was completed for all four models and for the fuel fired only and blended fuel fired/secondary sales options. Figure 5.1 outlines the values.

Model Description	GHG Emission Reduction	
	Fuel Heating	Blended Fuel / Secondary Sales
DOE database	24.5 tco2	2.0 tco2
RETScreen (Adjusted)	27.0 tco2	2.2 tco2
RETScreen	39.2 tco2	3.1 tco2
SWIFT	41.2 tco2	3.3 tco2

Fig 5.1 Summary of GHG Emission Reduction by Energy Model

6.0 Conclusions

In general it must be stated that there is very poor correlation between energy models. The closest correlation was between the adjusted RETScreen model and the DOE database model. In general the amount of solar energy available for use was fairly consistent between the DOE and RETScreen models but the usefulness of the energy varied considerably. To reconcile the difference, utilization factors from the DOE database were applied to the RETScreen model resulting in similar collected energy. Unfortunately using the DOE utilization factors may actually affect the true validity of the reconciliation since a DOE based value is being input into the RETScreen model.

Differences between the SWIFT and the DOE database and RETScreen models were most marked and appeared to be due to a very large difference in the calculated solar energy incident on the Solarwall. This is most likely due to the haze and reflectance factors used between the various energy models.

Since a very large range in the modeled energy recovered was evident, financial analysis was prepared for each model to show the full range of cost-benefit based on all the models. In addition financial analysis was completed for both the fuel oil fired system and a blended fuel oil fired / secondary sales electric system. Overall each model showed very poor system viability with paybacks extending to a maximum of 33 years and a minimum of 15.3 years.

Based on these extended paybacks the cost benefit of the systems is very marginal. The only means to improve the viability is to either decrease the capital expenditure or increase the solar wall capacity to increase the energy recovery with respect to total capital expenditure. Currently the Solarwall supplier is reviewing their system cost in an attempt to reduce capital expenditure, however, review with the costing contractor tends to indicate that the current cost estimates are reasonable and fair.

APPENDIX A

2002 NCE FEASIBILITY INVESTIAGTION REPORT
AND NCE RETSCREEN OUTPUT



WGH ALTERNATE ENERGY WHITEHORSE, Y.T.

Feasibility Investigation March 2002

1. Introduction

The feasibility of installing several different alternate energy and energy saving technologies at the Whitehorse General Hospital in Whitehorse, Yukon was investigated. The technologies investigated included SOLARWALL® to pre-warm the air to APU-3, APU-4, and APU-5; solar hot water heating to pre-warm the domestic water immediately before the domestic hot water heating system; Regent ECO heat exchanger to capture the heat in the exhaust of the APU-6 ventilation system; and ground water cooling with water-to-water heat pumps to offset the costs for cooling and domestic hot water heating. Throughout this report, it is assumed that the reader is familiar with these technologies. For the feasibility analysis for SOLARWALL® and solar hot water heating, RETScreen™ software was used. Offset fuel costs were based on the provided costs from the maintenance staff at the hospital, namely \$0.4238 per litre for fuel oil, and \$0.1305 per kilowatt-hour plus \$10 per kilowatt demand for electricity. With the exception of the heat pump analysis, electrical demand charges were not considered given that the comparative increase in electrical demand for the other options was nominal.

2. SOLARWALL® for APU-3, APU-4, and APU-5 Ventilation Systems

APU-3, APU-4, and APU-5 share a common fresh air intake on the Southwest wall of the main hospital fan room. APU-3 serves the technical services areas, and APU-4 and APU-5 operate in parallel to serve the critical care areas. All 3 units are 100% fresh air units operating 7 days per week, 24 hours a day. Although the units are variable speed, the maintenance staff confirmed that their flow rates and supply temperatures remain relatively constant year round. The units move approximately 22,860 litres per second (l/s) total, and deliver the air at approximately 13.5°C.

SOLARWALL® is available in a variety of colours. To match the current colouring scheme for the hospital, green was chosen for the feasibility analysis, which has a slightly reduced performance to the default black collector colour. The wall from which the units draw the fresh air is above the second floor of the hospital where two different textured siding schemes exist. The lower scheme forms a 2.7m band around the base in which the fresh air louver is actually installed. The upper scheme forms the top 7.5m of the wall in which the 'H' symbol is located. Runs were completed for installing the SOLARWALL® only on the bottom band, and on the entire face. In both cases, aside from the SOLARWALL® installation, minimal ducting is expected, consisting only of the summer bypass damper in front of the existing louver. As seen in the summary of the results below, the two different SOLARWALL® areas did not make a difference in the estimated payback, only in the estimated annual savings:

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84 m² SOLARWALL® area:

Total estimated capital cost without REDI grant: \$28,500.00
Total estimated annual savings: \$2800.00
Years to positive cash flow: 9

Total estimated capital cost with 40% REDI grant: \$20,600.00
Total estimated annual savings: \$2800.00
Years to positive cash flow: 6

232 m² SOLARWALL® area:

Total estimated capital cost without REDI grant: \$62,000.00
Total estimated annual savings: \$6700.00
Years to positive cash flow: 9

Total estimated capital cost with 40% REDI grant: \$43,400.00
Total estimated annual savings: \$6700.00
Years to positive cash flow: 6

The RETScreen™ printout for the 84 m² SOLARWALL® with REDI grant is included in Appendix A.

3. Solar Hot Water Heating

The domestic hot water needs for the hospital are provided by four 2653 litre tanks heated by the boiler steam plant. Two tanks are set at 82°C for the laundry and kitchen requirements, and the remaining two are set at 60°C. Maintenance and support staff advised that although the hospital has a bed capacity of 56, only 40 beds on average are occupied. Due to the fact that the domestic hot water is not metered, hot water use was based on the RETScreen™ calculation for the above occupancy. Further, the feasibility analysis included the provision for an insulated storage tank given the year round analysis and the service nature of the hot water demand. The existing energy plant does not have room for a storage tank, so the cost of building an attached shelter was included. It was assumed that there would be room for the collectors on the roof of the main fan room.

RETScreen™ feasibility was carried out for each of the solar hot water heating collector technologies: unglazed, glazed, and evacuated. For each analysis, the feasibility was optimized for collector slope, number of collectors, and storage capacity. The results are summarized below:

WGH ALTERNATE ENERGY WHITEHORSE, Y.T.
Feasibility Investigation March 2002

Evacuated Tube Collector:

Total estimated capital cost with 40% REDI grant: \$194,700.00
Total estimated annual savings: \$5300.00
Years to positive cash flow: greater than 25

Glazed Collector:

Total estimated capital cost with 40% REDI grant: \$121,400.00
Total estimated annual savings: \$4500.00
Years to positive cash flow: 24

Unglazed Collector:

Total estimated capital cost with 40% REDI grant: \$111,800.00
Total estimated annual savings: \$7200.00
Years to positive cash flow: 14

The RETScreen™ printouts for the above are included in Appendix B. Further investigation is ongoing to confirm the relative accuracy of the solar hot water heating feasibility analysis.

4. Regent ECO Heat Exchanger

The Regent ECO heat exchanger appears ideal for the Yukon cold weather climate since it is advertised to not suffer from defrost cycles; thus, maintaining heating efficiencies of approximately 90%. This heat exchanger also boasts approximately 80% cooling efficiencies, and minimal loss of building humidity. It's only potential drawbacks are its relatively large mass, and although cross-contamination is negligible, it still exists to some extent. The use of the Regent ECO heat exchanger was considered for the APU-6 ventilation system that serves the Administration Wing. This ventilation system is a mixed air system that does not currently have any heat reclaim provided for it. The APU-6 system includes the air handling unit, APU-6, and three exhaust fans, EF-1, EF-2, and EF-3. The use of EF-3 was not considered for this analysis since this exhaust fan serves chemical exhaust. Although APU-6 is a variable volume unit, the maintenance staff confirmed that airflows and supply temperature for it remain relatively constant year round; namely, 10,616 l/s supply air, 8274 l/s return air, and 2342 l/s fresh air on average, with a supply air temperature setpoint of 12°C. This unit does not have any provision for cooling, so any cooling provided by the heat exchanger would be an asset. EF-1 and EF-2 exhaust 3845 l/s and 1248 l/s respectively. The temperature of the exhaust air is around 24°C. This ventilation system operates 7 days a week from 5:00 AM to 7:00 PM.

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Feasibility Investigation March 2002

There appears to be enough room on the roof above the fan room for the heat exchanger. The most economical means of installing the heat exchanger system is ducting outside from the exhaust fan louvers to the heat exchanger. The fresh air for APU-6 is currently served from the roof. In completing the analysis, it was determined that only a portion of the exhaust air from EF-1 would be required to meet the ventilation heating demands for APU-6. It is expected that the Regent ECO EB5000 will be sufficient to meet the current ventilation demands, though this should be verified against the current upper operating limit of APU-6. It is assumed that the present structure is strong enough to accept the mass of the heat exchanger unit. The results of the feasibility analysis are summarized below:

Total estimated capital cost: \$60,000.00
Total estimated annual savings: \$11,000.00
Estimated simple payback: 5.4 years

5. Ground Water Cooling with Water-to-Water Heat Pumps

The hospital's cooling system is a circulated closed-loop water system cooled by an outdoor water-to-air chiller. The cooling system is activated at an outdoor temperature of 15^oC and provides a cooling capacity of 742 kW. Loop temperatures are maintained at 5.5^oC supply and 11^oC return at 30.2 l/s flow rate. According to maintenance staff, the estimated annual operating cost of the chiller is \$60,000. In the winter, the water to the outdoor chiller is valved off and dumped.

The area around the hospital has a proven aquifer with average reported groundwater temperatures of 7^oC. It is assumed from past experience that it is not feasible to construct a well to match the cooling system flow rate, and further, at an average temperature of 7^oC, the groundwater can only partially meet the heating demands of the school; therefore, the use of water-to-water heat pumps is required. The use of heat pumps has the added benefit of being able to supplement the domestic hot water heating demands of the hospital, stage the cooling in accordance with the demands, and extend the cooling season below 15^oC (the maintenance staff have advised that cooling is required at outdoor temperatures between 0^oC and 15^oC).

With the introduction of heat pumps, the cost of supplying and disposing of groundwater is no longer justified. The heat pumps will for the most part be extracting heat from the cooling system and injecting it into the domestic hot water system. Supplemental heat rejection can be achieved through a fan-coil as required. As such, the expense of burying piping for the heat pump is not required either.

It is estimated that six 30-ton heat pumps will meet 99% of the hospital's cooling demands. These same heat pumps will meet approximately 10% of the facilities domestic hot water heating demands over the cooling season that the chiller traditionally runs. The

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Feasibility Investigation March 2002

heat pumps can be stacked vertically up the wall where the water piping to the chiller exits the building. Because the chiller is required for some of the cooling season, it is assumed that the heat pumps will contribute to the demand charge (approximately \$12,360.00 per year). However, the maintenance staff have also advised that the chiller is not capable of keeping up during the hottest days of the summer; therefore, keeping the chiller will ensure capacity during the hottest days of the year. The results of the feasibility analysis are summarized below:

Total estimated capital cost: \$300,000
Total estimated annual savings: \$33,100
Estimated simple payback: 9 years

6. Conclusions

At this time, preliminary results indicate that the installation of a SOLARWALL® for APU-3, APU-4, and APU-5 ventilation systems may be considered economical with the REDI grant. The installation of the Regent ECO heat exchanger also appears to be a reasonably economical option and worth further exploration. Offsetting cooling costs using heat pumps may be considered if the added comfort levels are factored in. However, the use of solar hot water heating does not appear to be economical.

RETScreen® Energy Model - Solar Air Heating Project **NCE 232 m²**

Site Conditions		Estimate	Notes/Range
Project name		Whitehorse General Hospital	
Project location		Whitehorse	
Nearest location for weather data		Whitehorse A, YT	<u>Complete SR sheet</u>
Annual solar radiation (tilted surface)	MWh/m ²	1.02	
Annual average temperature	°C	-1.0	
Annual average wind speed	m/s	3.8	

System Characteristics		Estimate	Notes/Range
Heating application type	-	Ventilation air	
Base Case Heating System			
Heating fuel type	-	Diesel (#2 oil)	
Heating system seasonal efficiency	%	75%	0% to 350%
Building			
Building type	-	Commercial	
Maximum delivered air temperature	°C	13.5	10.0 to 60.0
RSI-value of building wall	m ² - °C/W	3.5	0.1 to 10.0
Airflow Requirements			
Design airflow rate	m ³ /h	82,300	50 to 1,000,000
Operating days per week	d/w	7.0	1.0 to 7.0
Operating hours per day	h/d	24.0	5.0 to 24.0
Solar Collector			
Design objective	-	Standard operation	
Collector colour	-	Green	<u>See Product Database</u>
Solar absorptivity	-	0.80	0.20 to 0.99
Suggested solar collector area	m ²	762	
Solar collector area	m ²	232	
Percent shading during season of use	%	0%	0% to 50%
SAH fan flow rate	m ³ /h/m ²	355	
Average air temperature rise	°C	1.8	
Incremental fan power	W/m ²	1.0	0.0 to 7.0

Annual Energy Production (12.0 months analysed)		Estimate	Notes/Range
Incremental fan energy	MWh	2.0	
Specific yield	kWh/m ²	548	
Collector efficiency	%	48%	
Solar availability while operating	%	100%	
Renewable energy collected	MWh	114.7	
Building heat loss recaptured	MWh	12.5	
Renewable energy delivered	MWh	127.1	
	GJ	457.7	

Complete Cost Analysis sheet

RETScreen® Solar Resource - Solar Air Heating Project

Site Latitude and Collector Orientation		Estimate	Notes/Range
Nearest location for weather data		Whitehorse A, YT	<u>See Weather Database</u>
Latitude of project location	°N	60.7	-90.0 to 90.0
Slope of solar collector	°	90.0	0.0 to 90.0
Azimuth of solar collector	°	45.0	0.0 to 180.0

Monthly Inputs					
Month	Fraction of month used (0 - 1)	Monthly average daily radiation on horizontal surface (kWh/m ² /d)	Monthly average temperature (°C)	Monthly average wind speed (m/s)	Monthly average daily radiation in plane of solar collector (kWh/m ² /d)
January	1.00	0.33	-18.7	3.6	1.26
February	1.00	1.08	-13.1	4.2	2.61
March	1.00	2.53	-7.2	3.9	4.15
April	1.00	4.25	0.3	3.9	4.09
May	1.00	5.36	6.6	3.9	3.93
June	1.00	5.89	11.6	3.6	3.84
July	1.00	5.28	14.0	3.1	3.60
August	1.00	4.00	12.3	3.3	3.29
September	1.00	2.44	7.3	3.9	2.63
October	1.00	1.17	0.7	4.4	1.91
November	1.00	0.44	-10.0	4.2	1.36
December	1.00	0.19	-15.9	3.9	0.86
			Annual	Season of use	
Solar radiation (horizontal)		MWh/m ²	1.01	1.01	
Solar radiation (tilted surface)		MWh/m ²	1.02	1.02	
Average temperature		°C	-1.0	-1.0	
Average wind speed		m/s	3.8	3.8	

Return to Energy Model sheet

RETScreen® Cost Analysis - Solar Air Heating Project

Type of project:

Currency:

Cost references:

Initial Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
Feasibility Study							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Development							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Engineering							
Other	Cost	1	\$ 3,500	\$ 3,500	-	-	-
Sub-total :				\$ 3,500	5.7%	-	-
Renewable Energy (RE) Equipment							
Solar collector materials	m ²	232	\$ 125	\$ 29,000	-	-	-
Equipment installation	m ²	232	\$ 55	\$ 12,760	-	-	-
Cladding material credit	m ²	-232	\$ -	\$ -	-	-	-
Cladding labour credit	m ²	-232	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ 2,000	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ 41,760	67.6%	-	-
Balance of Equipment							
Fans and ducting materials	L/s	22,861	\$ 0.05	\$ 1,143	-	-	-
Fans and ducting labour	L/s	22,861	\$ 0.15	\$ 3,429	-	-	-
Fan and duct mat'l credit	L/s	-22,861	\$ -	\$ -	-	-	-
Fan and duct labour credit	L/s	-22,861	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ 4,572	7.4%	-	-
Miscellaneous							
Overhead	%	15%	\$ 46,332	\$ 6,950	-	-	-
Training	p-h	0	\$ -	\$ -	-	-	-
Contingencies	%	10%	\$ 49,832	\$ 4,983	-	-	-
Sub-total :				\$ 11,933	19.3%	-	-
Initial Costs - Total				\$ 61,765	100.0%	-	-

Annual Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
O&M							
Property taxes/Insurance	project	1	\$ -	\$ -	-	-	-
O&M labour	project	0	\$ -	\$ -	-	-	-
Travel and accommodation	p-trip	1	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Contingencies	%	0%	\$ 46,332	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Fuel/Electricity	kWh	2,032	\$ 0.1305	\$ 265	100.0%	-	-
Annual Costs - Total				\$ 265	100.0%	-	-

Periodic Costs (Credits)	Period	Unit Cost	Amount	Interval Range	Unit Cost Range
Damper Motor	5 yr	\$ 200	\$ (200)	-	-
		\$ -	\$ -	-	-
		\$ -	\$ -	-	-
End of project life	-	\$ -	\$ -	-	-

Go to GHG Analysis sheet.

RETScreen® Greenhouse Gas (GHG) Emission Reduction Analysis - Solar Air Heating Project

Use GHG analysis sheet?

[Complete Financial Summary sheet](#)

Version 2000

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RETScreen® Financial Summary - Solar Air Heating Project

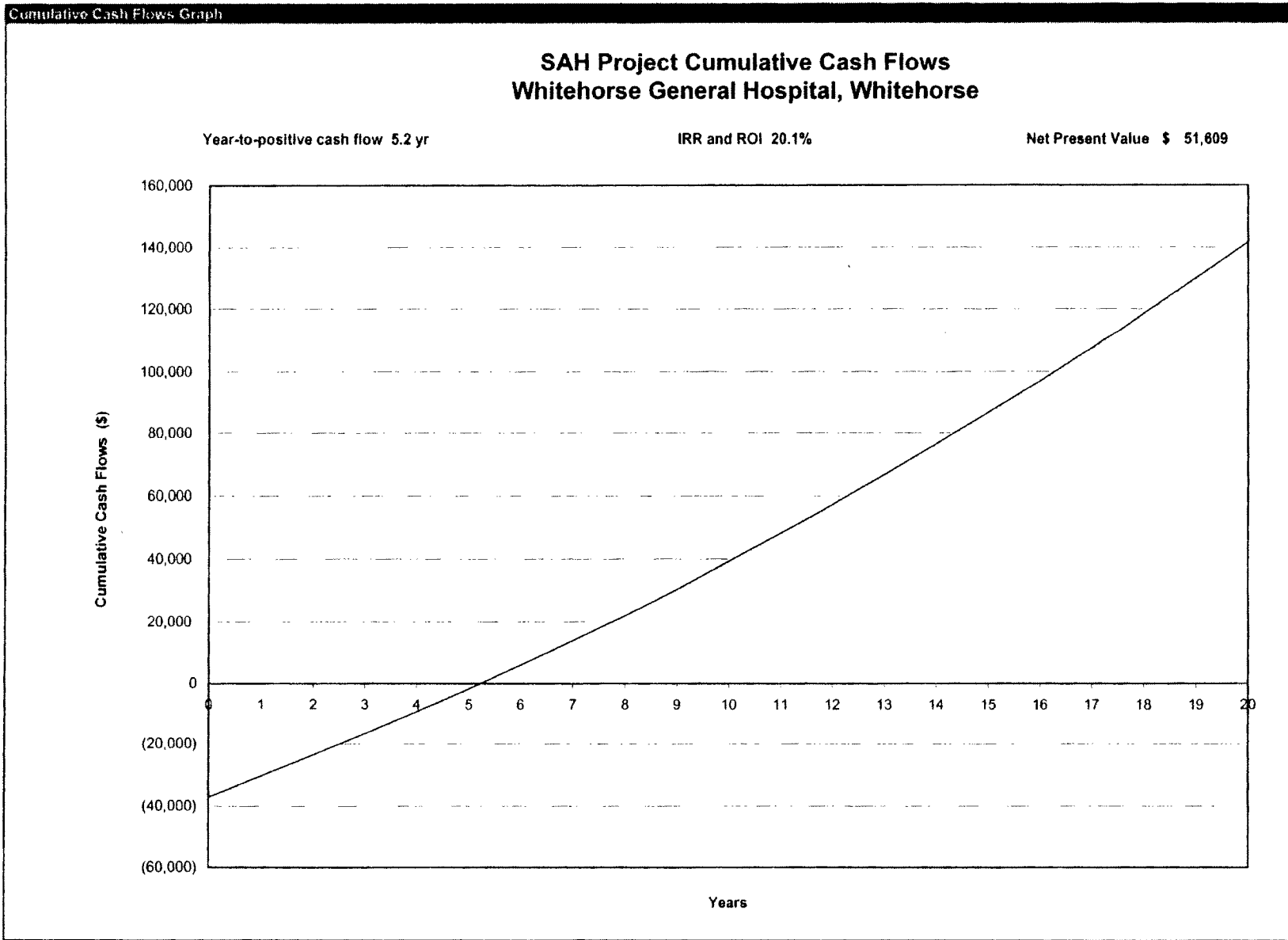
Annual Energy Balance					
Project name	Whitehorse General Hospital	Electricity required	MWh	2.0	
Project location	Whitehorse				
Renewable energy delivered	MWh	127.1	GHG analysis sheet used?	yes/no	No
Heating fuel displaced	-	Diesel (#2 oil)			

Financial Parameters					
Avoided cost of heating energy	\$/L	0.424	Debt ratio	%	0.0%
			Income tax analysis?	yes/no	No
Retail price of electricity	\$/kWh	0.131			
Energy cost escalation rate	%	3.0%			
Inflation	%	2.0%			
Discount rate	%	7.0%			
Project life	yr	20			

Project Costs and Savings					
Initial Costs			Annual Costs and Debt		
Feasibility study	0.0%	\$ -	O&M	\$ -	
Development	0.0%	\$ -	Fuel/Electricity	\$ 265	
Engineering	5.7%	\$ 3,500			
RE equipment	67.6%	\$ 41,760	Annual Costs - Total	\$ 265	
Balance of equipment	7.4%	\$ 4,572			
Miscellaneous	19.3%	\$ 11,933	Annual Savings or Income		
Initial Costs - Total	100.0%	\$ 61,765	Heating energy savings/income	\$ 6,690	
Incentives/Grants		\$ 24,700			
			Annual Savings - Total	\$ 6,690	
Periodic Costs (Credits)			Schedule yr # 5,10,15,20		
Damper Motor		\$ (200)			
		\$ -			
		\$ -			
End of project life -		\$ -			

Financial Feasibility					
Pre-tax IRR and ROI	%	20.1%			
After-tax IRR and ROI	%	20.1%			
Simple Payback	yr	5.8	Project equity	\$ 61,765	
Year-to-positive cash flow	yr	5.2			
Net Present Value - NPV	\$	51,609			
Annual Life Cycle Savings	\$	4,871			
Profitability Index - PI	-	0.84			

Yearly Cash Flows			
Year #	Pre-tax \$	After-tax \$	Cumulative \$
0	(37,065)	(37,065)	(37,065)
1	6,617	6,617	(30,448)
2	6,816	6,816	(23,632)
3	7,020	7,020	(16,612)
4	7,231	7,231	(9,381)
5	7,669	7,669	(1,713)
6	7,671	7,671	5,958
7	7,901	7,901	13,860
8	8,138	8,138	21,998
9	8,382	8,382	30,380
10	8,878	8,878	39,258
11	8,893	8,893	48,151
12	9,160	9,160	57,311
13	9,435	9,435	66,745
14	9,718	9,718	76,463
15	10,278	10,278	86,741
16	10,309	10,309	97,051
17	10,619	10,619	107,669
18	10,937	10,937	118,606
19	11,265	11,265	129,872
20	11,900	11,900	141,772



RETScreen® Energy Model - Solar Air Heating Project

NCE 84m²

Site Conditions		Estimate	Notes/Range
Project name		Whitehorse General Hospital	
Project location		Whitehorse	
Nearest location for weather data		Whitehorse A, YT	<u>Complete SR sheet</u>
Annual solar radiation (tilted surface)	MWh/m ²	1.02	
Annual average temperature	°C	-1.0	
Annual average wind speed	m/s	3.8	

System Characteristics		Estimate	Notes/Range
Heating application type	-	Ventilation air	
Base Case Heating System			
Heating fuel type	-	Diesel (#2 oil)	
Heating system seasonal efficiency	%	75%	0% to 350%
Building			
Building type	-	Commercial	
Maximum delivered air temperature	°C	13.5	10.0 to 60.0
RSI-value of building wall	m ² - °C/W	3.5	0.1 to 10.0
Airflow Requirements			
Design airflow rate	m ³ /h	82,300	50 to 1,000,000
Operating days per week	d/w	7.0	1.0 to 7.0
Operating hours per day	h/d	24.0	5.0 to 24.0
Solar Collector			
Design objective	-	Standard operation	
Collector colour	-	Green	<u>See Product Database</u>
Solar absorptivity	-	0.80	0.20 to 0.99
Suggested solar collector area	m ²	762	
Solar collector area	m ²	84	
Percent shading during season of use	%	0%	0% to 50%
SAH fan flow rate	m ³ /h/m ²	980	
Average air temperature rise	°C	0.8	
Incremental fan power	W/m ²	1.0	0.0 to 7.0

Annual Energy Production (12.0 months analysed)		Estimate	Notes/Range
Incremental fan energy	MWh	0.7	
Specific yield	kWh/m ²	642	
Collector efficiency	%	58%	
Solar availability while operating	%	100%	
Renewable energy collected	MWh	49.3	
Building heat loss recaptured	MWh	4.6	
Renewable energy delivered	MWh	53.9	
	GJ	194	

Complete Cost Analysis sheet

RETScreen® Solar Resource - Solar Air Heating Project

Site Latitude and Collector Orientation		Estimate	Notes/Range
Nearest location for weather data		Whitehorse A, YT	<u>See Weather Database</u>
Latitude of project location	°N	60.7	-90.0 to 90.0
Slope of solar collector	°	90.0	0.0 to 90.0
Azimuth of solar collector	°	45.0	0.0 to 180.0

Monthly Inputs					
Month	Fraction of month used (0 - 1)	Monthly average daily radiation on horizontal surface (kWh/m ² /d)	Monthly average temperature (°C)	Monthly average wind speed (m/s)	Monthly average daily radiation in plane of solar collector (kWh/m ² /d)
January	1.00	0.33	-18.7	3.6	1.26
February	1.00	1.08	-13.1	4.2	2.61
March	1.00	2.53	-7.2	3.9	4.15
April	1.00	4.25	0.3	3.9	4.09
May	1.00	5.36	6.6	3.9	3.93
June	1.00	5.89	11.6	3.6	3.84
July	1.00	5.28	14.0	3.1	3.60
August	1.00	4.00	12.3	3.3	3.29
September	1.00	2.44	7.3	3.9	2.63
October	1.00	1.17	0.7	4.4	1.91
November	1.00	0.44	-10.0	4.2	1.36
December	1.00	0.19	-15.9	3.9	0.86
			Annual	Season of use	
Solar radiation (horizontal)		MWh/m ²	1.01	1.01	
Solar radiation (tilted surface)		MWh/m ²	1.02	1.02	
Average temperature		°C	-1.0	-1.0	
Average wind speed		m/s	3.8	3.8	

Return to Energy Model sheet

RETScreen® Cost Analysis - Solar Air Heating Project

Type of project:

Currency:

Cost references:

Initial Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
Feasibility Study							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Development							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Engineering							
Other	Cost	1	\$ 3,500	\$ 3,500	-	-	-
Sub-total :				\$ 3,500	12.3%	-	-
Renewable Energy (RE) Equipment							
Solar collector materials	m ²	84	\$ 125	\$ 10,500	-	-	-
Equipment installation	m ²	84	\$ 55	\$ 4,620	-	-	-
Cladding material credit	m ²	-84	\$ -	\$ -	-	-	-
Cladding labour credit	m ²	-84	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ 2,000	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ 15,120	53.1%	-	-
Balance of Equipment							
Fans and ducting materials	L/s	22,861	\$ 0.05	\$ 1,143	-	-	-
Fans and ducting labour	L/s	22,861	\$ 0.15	\$ 3,429	-	-	-
Fan and duct mat'l credit	L/s	-22,861	\$ -	\$ -	-	-	-
Fan and duct labour credit	L/s	-22,861	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ 4,572	16.1%	-	-
Miscellaneous							
Overhead	%	15%	\$ 19,692	\$ 2,954	-	-	-
Training	p-h	0	\$ -	\$ -	-	-	-
Contingencies	%	10%	\$ 23,192	\$ 2,319	-	-	-
Sub-total :				\$ 5,273	18.5%	-	-
Initial Costs - Total				\$ 28,465	100.0%	-	-

Annual Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
O&M							
Property taxes/insurance	project	1	\$ -	\$ -	-	-	-
O&M labour	project	0	\$ -	\$ -	-	-	-
Travel and accommodation	p-trip	1	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Contingencies	%	0%	\$ 19,692	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Fuel/Electricity	kWh	736	\$ 0.1305	\$ 96	100.0%	-	-
Annual Costs - Total				\$ 96	100.0%	-	-

Periodic Costs (Credits)	Period	Unit Cost	Amount	Interval Range	Unit Cost Range
Damper Motor	5 yr	\$ 200	\$ (200)	-	-
		\$ -	\$ -	-	-
		\$ -	\$ -	-	-
End of project life	-	\$ -	\$ -	-	-

Go to GHG Analysis sheet

RETScreen® Greenhouse Gas (GHG) Emission Reduction Analysis - Solar Air Heating Project

Use GHG analysis sheet?

[Complete Financial Summary sheet](#)

Version 2000

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UNEP/DTIE and NRCan/CEDRL

RETScreen® Financial Summary - Solar Air Heating Project

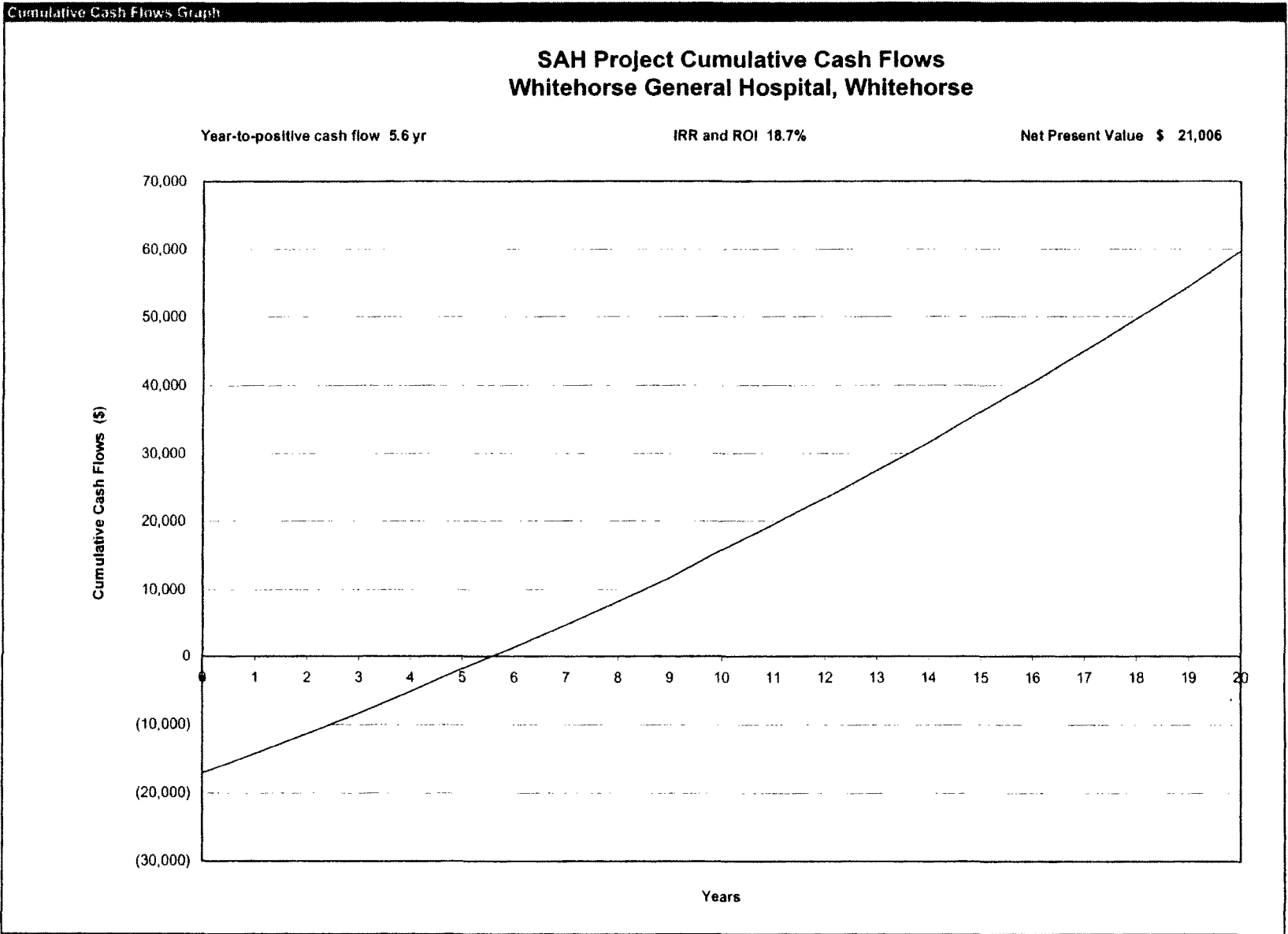
Annual Energy Balance					
Project name	Whitehorse General Hospital	Electricity required	MWh	0.7	
Project location	Whitehorse				
Renewable energy delivered	MWh	53.9	GHG analysis sheet used?	yes/no	No
Heating fuel displaced	-	Diesel (#2 oil)			

Financial Parameters					
Avoided cost of heating energy	\$/L	0.424	Debt ratio	%	0.0%
			Income tax analysis?	yes/no	No
Retail price of electricity	\$/kWh	0.131			
Energy cost escalation rate	%	3.0%			
Inflation	%	2.0%			
Discount rate	%	7.0%			
Project life	yr	20			

Project Costs and Savings					
Initial Costs			Annual Costs and Debt		
Feasibility study	0.0%	\$ -	O&M	\$ -	
Development	0.0%	\$ -	Fuel/Electricity	\$ 96	
Engineering	12.3%	\$ 3,500			
RE equipment	53.1%	\$ 15,120	Annual Costs - Total	\$ 96	
Balance of equipment	16.1%	\$ 4,572			
Miscellaneous	18.5%	\$ 5,273	Annual Savings or Income		
Initial Costs - Total	100.0%	\$ 28,465	Heating energy savings/income	\$ 2,835	
Incentives/Grants		\$ 11,400			
			Annual Savings - Total	\$ 2,835	
Periodic Costs (Credits)					
Damper Motor		\$ (200)	Schedule yr #	5,10,15,20	
		\$ -			
		\$ -			
End of project life -		\$ -			

Financial Feasibility					
Pre-tax IRR and ROI	%	18.7%			
After-tax IRR and ROI	%	18.7%			
Simple Payback	yr	6.2	Project equity	\$	28,465
Year-to-positive cash flow	yr	5.6			
Net Present Value - NPV	\$	21,006			
Annual Life Cycle Savings	\$	1,983			
Profitability Index - PI	-	0.74			

Yearly Cash Flows			
Year #	Pre-tax \$	After-tax \$	Cumulative \$
0	(17,065)	(17,065)	(17,065)
1	2,822	2,822	(14,244)
2	2,906	2,906	(11,338)
3	2,993	2,993	(8,344)
4	3,083	3,083	(5,261)
5	3,396	3,396	(1,865)
6	3,271	3,271	1,406
7	3,369	3,369	4,775
8	3,470	3,470	8,245
9	3,574	3,574	11,820
10	3,925	3,925	15,745
11	3,792	3,792	19,537
12	3,906	3,906	23,442
13	4,023	4,023	27,465
14	4,143	4,143	31,609
15	4,537	4,537	36,146
16	4,396	4,396	40,542
17	4,528	4,528	45,069
18	4,664	4,664	49,733
19	4,803	4,803	54,536
20	5,245	5,245	59,781



APPENDIX B

**DOE DATABASE MODEL SUMMARY
AND OUTPUT**



**WHITEHORSE GENERAL HOSPITAL
ENERGY EFFICIENCY STRATEGY ANALYSIS
Curt Hepting, EnerSys Analytics Inc.**

Under contract to Ferguson Simek Clark (FSC), we were retained to evaluate the energy cost savings impacts for implementing the following energy efficiency measures (EEMs):

- 1) RegentEco exhaust heat recovery on APU-6.
- 2) Solarwall to preheat the outside air provided to APU-3, APU-4 and APU-5 and

APPROACH BACKGROUND

The analysis of these EEMs was based on using an hourly DOE2.1e energy performance model of the facility I developed for a previous study on behalf of FSC. This involved representing the building geometry and general systems in an hourly DOE2 model *for the purposes of estimating the building's hourly heating requirements for a typical year*. Hence, the level of detail in the model was appropriate for this original task and is not intended as an exact representation of each specific building component and/or system. However, the model is more than appropriate given not only the purpose of this effort, but also given the level of accuracy of the provided information (for instance, schedules alone embody a set of assumptions which likely exceed the error margins of most other building characteristics).

The development the energy performance simulation first required translating the information provided by FSC into a baseline DOE2 model. This includes describing the building geometry and shell components, the interior space conditions for lighting, equipment, people, process loads, etc., and the mechanical HVAC and DHW systems which serve the building. Since not all inputs can be perfectly known, several assumptions have to be made. The most significant of these assumptions typically resides in the schedules. But other characteristics such as the true amount of outdoor air, the DHW load, the boiler part-load operation, minimum fan configuration settings, and cooking and process loads can all have a significant impact on the heating load and overall fuel oil consumption.

To help provide a relatively high level of confidence to the model's accuracy, we calibrate the model to correspond with the electrical and fuel oil billing history. In this case, I calibrated to the average calendar-normalized fuel oil consumption for summer-1998 through summer-2000, and the average calendar-normalized electrical energy use (demand was not provided) for summer-1997 through summer-2001. These time periods were chosen based on the data provided to me by FSC. The results from this exercise confirmed that the model description and inputs provided by FSC were quite reasonable since I did not need to

significantly change the building inputs, outside of a reasonable expected margin of error, to produce a very good calibration.

Using this baseline energy model, I reflected the necessary changes to estimate the energy savings for the EEMs.

ENERGY EFFICIENCY MEASURE ANALYSIS

I modified to the baseline energy model to appropriately represent each of the EEMs. Because of the differences between the baseline model and specifics with each measure, along with limitations in DOE2, certain assumptions and adjustments are often required. These are described below.

RegentEco Exhaust Heat Recovery

Annual Energy Impacts: 44,960 liters of oil saved (3.6%), 12,490 kWh added in electrical energy (-0.3%) for a total net energy savings of 1,710 GJ (2.7%)
Annual Utility Bill Impacts: \$16,800 at marginal rates of \$0.40/liter, \$0.121/kWh and \$11.53/kW

Note: If fans are actually on only 14 hours/day instead of 17 hours/day (see below), savings would decrease accordingly by approximately 18% to \$13,800/year).

The RegentEco system has an impressive heat recovery effectiveness of 90%. In applying this option in the model using the RECOV-EFF keyword, however, *DOE2 did not produce any savings using its heat recovery capability for an unknown reason.* In checking the hourly mixed air and supply air temperatures, there exists many hours where the mixed air temperature is below the minimum supply air temperature of 59°F (less the fan heat dT of up to 2.5°F). In fact, at 25% outside air estimated for the baseline model, heat recovery should become effective at outside air temperatures below about 11°F.

As a secondary approach to estimating the effectiveness of the heat recovery, I performed simulations with the minimum outside air level decreased by 90%. This is a representative approach for an enthalpy wheel in which the latent heat is also recovered, but will significantly overstate the savings for latent heat recovery. Hence, to estimate only the sensible component, I performed two runs that effectively removed the latent component:

- 1) the baseline without humidification (WGH_B2-NoHumid.std) and
- 2) the baseline without humidification, OA for APU-6 reduced by 90% and the effective static pressure on supply and return increased by 0.5" each (WGH_B2-NoHumid+HRV.std).

The results from this analysis are archived in EEM Analysis, and contained in the DOE2 output files indicated above.

On a final note, I observed the following discrepancies between NCE's assumptions and those embodied in the above modelling analysis:

- Minimum outside air is represented in the models at 4605 l/s (25%), while NCE's is indicated at "2342 l/s fresh air on average" (22%) but exhaust is indicated to be at 5,093 l/s.
- Hours of operation for the fans are 17 hours/day for the models and only 14 hours for NCE. In the model, the fans are allowed to cycle on to meet heating load during setback periods; it is unknown how NCE's analysis accounts for this.
- In the models, the setback by 5°F from about 7pm – 6am; it is unknown how NCE accounts for setback.

Solarwall Preheat on APU-3, 4 and 5

Annual Energy Impacts:

- Lower estimate for 84 m² Solarwall:
 - Annual Energy: 2211 liters of oil saved, 737 kWh *added* in electrical energy.
 - Annual Utility Bill Impacts: **\$814** at marginal rates of \$0.40/liter and \$0.0955/kWh (blended)
- Upper estimate for 262.5 m² Solarwall:
 - Annual Energy: 6909 liters of oil saved, 2302 kWh *added* in electrical energy.
 - Annual Utility Bill Impacts: **\$2544** at marginal rates of \$0.40/liter and \$0.0955/kWh (blended)

Note: SolarWall.xls spreadsheet contains formulas and inputs for figuring calculated impacts.

The Solarwall system acts as a preheat on the outside air when conditions are favourable (i.e., the sun heats up a cavity behind an exterior perforated screen through which the outside air is drawn through *and* the need for preheating exists). DOE2 does not have the capability to analyze this option. However, data extracted from appropriate DOE2 runs can be used to estimate the impact by creating a "solarwall" surface with the same characteristics as exists with the actual solarwall. In summary, I performed the following steps:

- 1) Created a cavity with a 100 m² southwest exposure. The actual wall area for the Solarwall is not required since hourly results from the DOE2 analysis will be imported into a spreadsheet, in which the desired Solarwall area can be input and the impacts recalculated. Note that I estimate the maximum potential coverage at 35 m x 7.5 m → 262.5 m².

- 2) Attach an exterior metal wall with an 80% absorptance, although the absorptance is inherent in the air temperature rise curves provided by Solarwall.
- 3) Provide for an exhaust fan power of 0.093 W/ft² per NCE's Retscreen analysis. Note that added fan power is accounted for in the Solarwall analysis spreadsheet.
- 4) Pull the following hourly data for importing into the Solarwall.xls spreadsheet:
 - a. Energy required for preheating OA, determined from pulling the heating energy for all *apparent* 53,976 cfm¹ of outside air serving the "SYSTEM-NEW" (QH-5 + QHP-10 for System-New), adjusted by the estimated affected amount of OA for APU-3 and APU-4/5 of 22,860 l/s²; this will be used to figure the maximum hourly OA heating requirement
 - b. Incident solar on an hourly basis (SOLI-1 of SolarWall wall). Using published Solarwall information on the air temperature rise vs. W/m² of incident solar radiation by air-flow rate.
 - c. Calculate the maximum air flow that passes through the Solarwall cavity and will be preheated. At the maximum OA air flow, up to 17.1 (22,860 cfm/sf / 262.5 m²) cfm/sf of air would be required to pass through the Solarwall cavity. However, Solarwall indicates that 7.0 cfm/sf is the maximum allowed flow and hence, this limits the direct maximum effect on 7.0/17.1 = 41% of the outside air flow. At less than 100% Solarwall coverage, this percentage would decrease proportionally; for instance, at the minimum 84 m² of coverage, only (7.0/53.6 = 7.7% of the outside air requirements can be directed through the Solarwall.
 - d. Energy available from solarwall determined by applying the linear formulas from the Solarwall product literature for how much the outside air temperature rises on an hourly basis (dT): 1.08 x CFM x dT x 1.070 altitude factor.
- 5) Calculate the hourly OA energy requirements and contributions from the Solarwall . Add in the electrical energy from the additional fan power, assuming no by-pass for when no preheating is applicable (otherwise, Solarwall shouldn't claim wall loss recapture during all heating hours).
- 6) Increase the southwest R-value by R-50 (per Solarwall literature) for the mechanical room area clad with Solarwall. Note that the present assumption is that this space is only marginally conditioned to stay about 50°F. The annual savings obtained from increasing the 2886 ft² SW wall

¹ OA appears lower than actual since it was reduced in model to reflect enthalpy wheel heat recovery on APU1/2, which is combined with APU-3 and APU-4/5. Hence, indicated level effectively represents the net volume flow of outside air that requires full preheating. Actual minimum OA pulled from hourly data.

² From NCE report, although preliminary analysis by FSC in "Secondary Sales Feasibility Study" (Jan 15, 2001) indicated higher estimated amounts. Note that calibration to billed energy use dictated that outdoor air levels had to be on the low side in order to account for the billing data.

by R-50 amounts to about 0.00104 mmBtu/ft², assuming application during all heating hours.

- 7) Apply marginal costs (blended electricity rates since demand coincidence is problematic) to yield annual cost savings.

Note that Retscreen is an accepted and tested (I assume) application that is provided by Natural Resources Canada (NRCan) for performing solar thermal analyses. While I believe my approach with making use of the calibrated hourly baseline model and associated weather data is valid (instead of monthly data, as with Retscreen), it has not been validated against an actual operating system. Furthermore, there appears to be a significant difference between the Retscreen analysis results from NCE, with their lower estimate 3.4 times higher than my calculations. Consequently, FSC should carefully review both approaches to evaluate the merits and validity for the analysis.

Solarwall Hourly Analysis
Whitehorse General Hospital

3-Jan-03
 C. Hepting, EnerSys Analytics
 Modified RDA, FSCC Jan 22/03

Handwritten:
 248 m²

Inputs			
Air Flow Across Solarwall:	7 cfm/ft ²	Seasonal Heating Plant Efficiency:	80.6% (from DOE2)
Corresponding dT vs. solar radiation:	0.01667 °C/(W/m ²)	Fan Power Increase for Solarwall:	0.0930 W/ft ²
Surface Area of Solarwall:	2,669 ft ²	Heating Content for Heating Fuel:	37,003 Btu/liter
Maximum solarwall air flow:	18,683	Marginal Rate for Heating Fuel:	\$0.450 per liter
			\$12.161 per mmBtu
Applicable OA for Preheating:	48,440 cfm	Marginal Rate for Electricity:	\$0.1300 per kWh
Proportion of OA preheated by Solarwall:	38.6%		
Amount of OA preheated by Solarwall:	18,883 cfm		
			For WGH Application: Minimum application = 84 m ² Maximum application = 262.5 m ²
Annual Results			
Preheat Provided by Solarwall:	238.73 mmBtu (in)	251.9 GJ	
Fuel Avoided from Solarwall Preheat:	6,452 liters		
Reclaimed Wall Losses by System:	255 liters	9.9 GJ	
Total Fuel Savings for Solarwall:	6,706 liters	Added Fan Energy (3611 hrs/yr):	<input checked="" type="checkbox"/> By-Pass 896 kWh
Fuel Cost Savings for Solarwall:	\$3,018 /year	Added Electrical Costs from Solarwall:	\$117 /year
Net Utility Cost Savings for Solarwall:	\$2,901 /year		

Day of Year	Month	Day	Hour	Solarwall OA for Solarwall (cfm)	Solarwall OA Htg Req'ts (Btuh)	Solarwall Air Temp. Rise (°F)	Solarwall Preheat Available (Btuh)	Solarwall Energy Used (Btuh)
1	1	1	1	18,683	971,144	0.0	0	0
2	1	1	2	18,683	773,908	0.0	0	0
3	1	1	3	18,683	635,644	0.0	0	0
4	1	1	4	18,683	558,647	0.0	0	0
5	1	1	5	18,683	539,010	0.0	0	0
6	1	1	6	18,683	518,600	0.0	0	0
7	1	1	7	18,683	576,364	0.0	0	0
8	1	1	8	18,683	556,347	0.0	0	0
9	1	1	9	18,683	520,268	0.0	0	0
10	1	1	10	18,683	518,459	0.0	0	0
11	1	1	11	18,683	478,511	0.1	2,008	2,008
12	1	1	12	18,683	477,119	0.4	9,329	9,329
13	1	1	13	18,683	481,496	8.9	192,665	192,665
14	1	1	14	18,683	496,194	6.5	140,061	140,061

Solarwall OA Heating Requirements



Monthly Energy (mmBtu)

Month	Htg. Reqts for OA thru Solarwall	Solarwall Energy Available	Usable Solarwall Energy	"Wasted" Solarwall Energy	
1 Jan	760.90	16.66	16.66	0.00	0.999782
2 Feb	462.87	39.59	36.48	3.11	0.921521
3 Mar	381.77	68.83	54.50	14.33	0.791795
4 Apr	208.37	80.13	45.72	34.41	0.570569
5 May	79.72	85.99	12.89	73.11	0.149857
6 Jun	31.80	76.08	6.21	69.87	0.081615
7 Jul	8.30	71.15	2.03	69.12	0.028521
8 Aug	26.79	67.10	3.51	63.59	0.052294
9 Sep	68.15	47.78	7.19	40.59	0.15053
10 Oct	215.87	34.49	24.62	9.87	0.713782
11 Nov	470.92	18.16	17.23	0.92	0.949069
12 Dec	634.48	11.69	11.69	0.00	1
Annual	3,349.94	617.65	238.73	378.92	
		651.62 GJ			

Solarwall Hourly Analysis
Whitehorse General Hospital

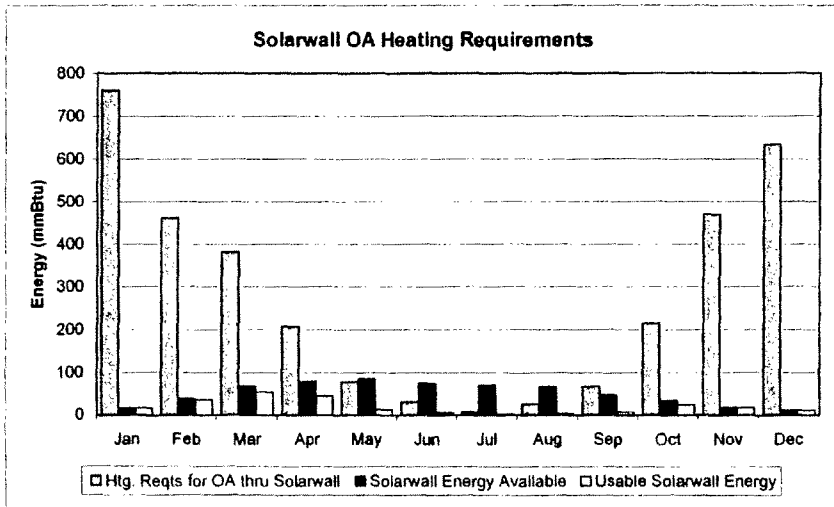
3-Jan-03
C. Hepting, EnerSys Analytics
Modified RDA, FSCC Jan 22/03

Inputs				
Air Flow Across Solarwall:	7 cfm/ft²	Seasonal Heating Plant Efficiency:	80.6%	(from DOE2)
Corresponding dT vs. solar radiation:	0.01667 °C/(W/m²)	Fan Power Increase for Solarwall:	0.0930	W/R²
Surface Area of Solarwall:	2,869 ft²	Heating Content for Heating Fuel:	37,003	Btu/liter
Maximum solarwall air flow:	18,683	Marginal Rate for Heating Fuel:	\$0.450	per liter
			\$12.161	per mmBtu
Applicable OA for Preheating:	48,440 cfm	Marginal Rate for Electricity:	\$0.1300	per kWh
Proportion of OA preheated by Solarwall:	38.6%			
Amount of OA preheated by Solarwall:	18,683 cfm			

For WGH Application:
Minimum application = 84 m²
Maximum application = 262.5 m²

Annual Results				
Preheat Provided by Solarwall:	238.73 mmBtu (in)	251.9 GJ		
Fuel Avoided from Solarwall Preheat:	6,452 liters			
Reclaimed Wall Losses by System:	255 liters	9.9 GJ		
Total Fuel Savings for Solarwall:	6,706 liters		Added Fan Energy (3611 hrs/yr): <input checked="" type="checkbox"/> By-Pass	896 kWh
Fuel Cost Savings for Solarwall:	\$3,018 /year		Added Electrical Costs from Solarwall:	\$117 /year
Net Utility Cost Savings for Solarwall:	\$2,901 /year			

Day of Year	Month	Day	Hour	OA for Solarwall (cfm)	Solarwall OA Htg Req'ts (Btuh)	Solarwall Air Temp. Rise (°F)	Solarwall Preheat Available (Btuh)	Solarwall Energy Used (Btuh)	Solarwall Air Temp. Rise (°F)	Solarwall Leaving Air Temp (degF)	
1	1	1	1	18,683	971,144	0.0	0	0	N/A	N/A	<<Avg air temp rise
2	1	1	2	18,683	773,908	0.0	0	0	N/A	N/A	<<Avg Solarwall LAT
3	1	1	3	18,683	635,644	0.0	0	0	N/A	N/A	
4	1	1	4	18,683	558,647	0.0	0	0	N/A	N/A	
5	1	1	5	18,683	539,010	0.0	0	0	N/A	N/A	
6	1	1	6	18,683	518,600	0.0	0	0	N/A	N/A	
7	1	1	7	18,683	576,364	0.0	0	0	N/A	N/A	
8	1	1	8	18,683	556,347	0.0	0	0	N/A	N/A	
9	1	1	9	18,683	520,268	0.0	0	0	N/A	N/A	
10	1	1	10	18,683	518,459	0.0	0	0	N/A	N/A	
11	1	1	11	18,683	478,511	0.1	2,008	2,008	0.0930186	22.0930186	
12	1	1	12	18,683	477,119	0.4	9,329	9,329	0.4320864	22.4320864	
13	1	1	13	18,683	481,496	8.9	192,665	192,665	8.9237844	30.9237844	
14	1	1	14	18,683	498,194	6.5	140,061	140,061	6.4872972	27.4872972	



Monthly Energy (mmBtu)

Month	Htg. Reqs for OA thru Solarwall	Solarwall Energy Available	Usable Solarwall Energy	"Wasted" Solarwall Energy	
1 Jan	760.90	16.66	16.66	0.00	0.999782
2 Feb	462.87	39.59	38.48	3.11	0.921521
3 Mar	381.77	68.83	54.50	14.33	0.791795
4 Apr	208.37	80.13	45.72	34.41	0.570569
5 May	79.72	85.99	12.89	73.11	0.149857
6 Jun	31.80	76.08	6.21	69.87	0.081615
7 Jul	8.30	71.15	2.03	69.12	0.028521
8 Aug	26.79	67.10	3.51	63.59	0.052294
9 Sep	68.15	47.78	7.19	40.96	0.15053
10 Oct	215.87	34.49	24.62	9.87	0.713782
11 Nov	470.92	18.16	17.23	0.92	0.949069
12 Dec	634.48	11.69	11.69	0.00	1
Annual	3,349.94	617.65	238.73	378.92	

651.62 GJ

RETScreen® Greenhouse Gas (GHG) Emission Reduction Analysis - Solar Air Heating Project

Use GHG analysis sheet? Yes

Type of analysis Standard

Background Information

Project Information

Project name Whitehorse General Hospital
 Project location Whitehorse

Global Warming Potential of GHG

1 ton CH₄ = 21 tons CO₂ (IPCC 1996)
 1 ton N₂O = 310 tons CO₂ (IPCC 1996)

Base Case Electricity System (Reference)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	T & D losses (%)	GHG emission factor (t _{CO2} /MWh)
Small hydro	100.0%	0.0	0.0000	0.0000	100.0%	8.0%	0.000
Electricity mix	100%	0.0	0.0000	0.0000		8.0%	0.000

Base Case Heating System (Reference)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	GHG emission factor (t _{CO2} /MWh)
Heating system Diesel (#2 oil)	100.0%	74.1	0.0020	0.0020	80.0%	0.336

Proposed Case Heating System (Mitigation)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	GHG emission factor (t _{CO2} /MWh)
Heating system Electricity	2.9%	0.0	0.0000	0.0000	100.0%	0.000
Solar	97.1%	0.0	0.0000	0.0000	100.0%	0.000
Heating energy mix	100.0%	0.0	0.0000	0.0000		0.000

GHG Emission Reduction Summary

	Base case GHG emission factor (t _{CO2} /MWh)	Proposed case GHG emission factor (t _{CO2} /MWh)	End-use annual energy delivered (MWh)	Annual GHG emission reduction (t _{CO2} /yr)
Heating system	0.336	0.000	72.7	24.45
			Net GHG emission reduction	24.45

Complete Financial Summary sheet

APPENDIX C

**RETScreen AND SWIFT ANALYSIS OUTPUT
AND MISC CALCULATIONS**



RETScreen® Energy Model - Solar Air Heating Project

Site Conditions		Estimate	Notes/Range
Project name		Whitehorse General Hospital	
Project location		Whitehorse	
Nearest location for weather data		Whitehorse A, YT	<u>Complete SR sheet</u>
Annual solar radiation (tilted surface)	MWh/m ²	1.02	
Annual average temperature	°C	-1.0	
Annual average wind speed	m/s	3.8	

System Characteristics		Estimate	Notes/Range
Heating application type	-	Ventilation air	
Base Case Heating System			
Heating fuel type	-	Diesel (#2 oil)	
Heating system seasonal efficiency	%	75%	0% to 350%
Building			
Building type	-	Commercial	
Maximum delivered air temperature	°C	13.5	10.0 to 60.0
RSI-value of building wall	m ² - °C/W	3.5	0.1 to 10.0
Airflow Requirements			
Design airflow rate	m ³ /h	31,740	50 to 1,000,000
Operating days per week	d/w	7.0	1.0 to 7.0
Operating hours per day	h/d	24.0	5.0 to 24.0
Solar Collector			
Design objective	-	Standard operation	
Collector colour	-	Green	<u>See Product Database</u>
Solar absorptivity	-	0.80	0.20 to 0.99
Suggested solar collector area	m ²	294	
Solar collector area	m ²	248	
Percent shading during season of use	%	0%	0% to 50%
SAH fan flow rate	m ³ /h/m ²	128	
Average air temperature rise	°C	4.3	
Incremental fan power	W/m ²	1.0	0.0 to 7.0

Annual Energy Production (12.0 months analysed)		Estimate	Notes/Range
Incremental fan energy	MWh	2.2	
Specific yield	kWh/m ²	470	
Collector efficiency	%	41%	
Solar availability while operating	%	100%	
Renewable energy collected	MWh	103.3	
Building heat loss recaptured	MWh	13.1	
Renewable energy delivered	MWh	116.4	
	GJ	419.1	

Complete Cost Analysis sheet

RETScreen® Solar Resource - Solar Air

Site Latitude and Collector Orientation

Nearest location for weather data
Latitude of project location
Slope of solar collector
Azimuth of solar collector

Monthly Inputs

Month	Fraction of month used (0 - 1)	
January	1.00	
February	1.00	
March	1.00	
April	1.00	
May	1.00	
June	1.00	
July	1.00	
August	1.00	
September	1.00	
October	1.00	
November	1.00	
December	1.00	

Solar radiation (horizontal)
Solar radiation (tilted surface)
Average temperature
Average wind speed

RETScreen® Greenhouse Gas (GHG) Emission Reduction Analysis - Solar Air Heating Project (FO Heating)

Use GHG analysis sheet? Yes

Type of analysis Standard

Background Information

Project Information

Project name Whitehorse General Hospital
Project location Whitehorse

Global Warming Potential of GHG

1 ton CH₄ = 21 tons CO₂ (IPCC 1996)
1 ton N₂O = 310 tons CO₂ (IPCC 1996)

Base Case Electricity System (Reference)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	T & D losses (%)	GHG emission factor (t _{CO2} /MWh)
Small hydro	100.0%	0.0	0.0000	0.0000	100.0%	8.0%	0.000
Electricity mix	100%	0.0	0.0000	0.0000		8.0%	0.000

Base Case Heating System (Reference)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	GHG emission factor (t _{CO2} /MWh)
Heating system Diesel (#2 oil)	100.0%	74.1	0.0020	0.0020	80.0%	0.336

Proposed Case Heating System (Mitigation)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	GHG emission factor (t _{CO2} /MWh)
Heating system Electricity	1.8%	0.0	0.0000	0.0000	100.0%	0.000
Solar	98.2%	0.0	0.0000	0.0000	100.0%	0.000
Heating energy mix	100.0%	0.0	0.0000	0.0000		0.000

GHG Emission Reduction Summary

Heating system	Base case GHG emission factor (t _{CO2} /MWh)	Proposed case GHG emission factor (t _{CO2} /MWh)	End-use annual energy delivered (MWh)	Annual GHG emission reduction (t _{CO2})
	0.336	0.000	116.4	39.17
			Net GHG emission reduction	Δt _{CO2} /yr 39.17

Complete Financial Summary sheet

RETScreen® Energy Model - Solar Air Heating Project

Adjusted

Site Conditions		Estimate	Notes/Range
Project name		Whitehorse General Hospital	
Project location		Whitehorse	
Nearest location for weather data		Whitehorse A, YT	<u>Complete SR sheet</u>
Annual solar radiation (tilted surface)	MWh/m ²	1.02	
Annual average temperature	°C	-1.0	
Annual average wind speed	m/s	3.8	

System Characteristics		Estimate	Notes/Range
Heating application type	-	Ventilation air	
Base Case Heating System			
Heating fuel type	-	Diesel (#2 oil)	
Heating system seasonal efficiency	%	75%	0% to 350%
Building			
Building type	-	Commercial	
Maximum delivered air temperature	°C	60.0	10.0 to 60.0
RSI-value of building wall	m ² - °C/W	3.5	0.1 to 10.0
Airflow Requirements			
Design airflow rate	m ³ /h	31,740	50 to 1,000,000
Operating days per week	d/w	7.0	1.0 to 7.0
Operating hours per day	h/d	24.0	5.0 to 24.0
Solar Collector			
Design objective	-	Standard operation	
Collector colour	-	Green	<u>See Product Database</u>
Solar absorptivity	-	0.80	0.20 to 0.99
Suggested solar collector area	m ²	294	
Solar collector area	m ²	248	
Percent shading during season of use	%	0%	0% to 50%
SAH fan flow rate	m ³ /h/m ²	128	
Average air temperature rise	°C	4.7	
Incremental fan power	W/m ²	1.0	0.0 to 7.0

Annual Energy Production (6.4 months analysed)		Estimate	Notes/Range
Incremental fan energy	MWh	1.2	
Specific yield	kWh/m ²	324	
Collector efficiency	%	66%	
Solar availability while operating	%	43%	
Renewable energy collected	MWh	70.8	
Building heat loss recaptured	MWh	9.5	
Renewable energy delivered	MWh	80.4	
	GJ	289.3	

Complete Cost Analysis sheet

RETScreen® Solar Resource - Solar Air Heating Project

Site Latitude and Collector Orientation		Estimate	Notes/Range
Nearest location for weather data		Whitehorse A, YT	<i>See Weather Database</i>
Latitude of project location	°N	60.7	-90.0 to 90.0
Slope of solar collector	°	90.0	0.0 to 90.0
Azimuth of solar collector	°	45.0	0.0 to 180.0

Monthly Inputs					
Month	Fraction of month used (0 - 1)	Monthly average daily radiation on horizontal surface (kWh/m ² /d)	Monthly average temperature (°C)	Monthly average wind speed (m/s)	Monthly average daily radiation in plane of solar collector (kWh/m ² /d)
January	1.00	0.33	-18.7	3.6	1.26
February	0.92	1.08	-13.1	4.2	2.61
March	0.80	2.53	-7.2	3.9	4.15
April	0.57	4.25	0.3	3.9	4.09
May	0.15	5.36	6.6	3.9	3.93
June	0.08	5.89	11.6	3.6	3.84
July	0.03	5.28	14.0	3.1	3.60
August	0.05	4.00	12.3	3.3	3.29
September	0.15	2.44	7.3	3.9	2.63
October	0.71	1.17	0.7	4.4	1.91
November	0.95	0.44	-10.0	4.2	1.36
December	1.00	0.19	-15.9	3.9	0.86
			Annual	Season of use	
Solar radiation (horizontal)		MWh/m ²	1.01	0.28	
Solar radiation (tilted surface)		MWh/m ²	1.02	0.43	
Average temperature		°C	-1.0	-8.9	
Average wind speed		m/s	3.8	4.0	

Return to Energy Model sheet

RETScreen® Greenhouse Gas (GHG) Emission Reduction Analysis - Solar Air Heating Project *(Adjusted) FO Heating*

Use GHG analysis sheet? Yes

Type of analysis Standard

Background Information

Project Information		Global Warming Potential of GHG	
Project name	Whitehorse General Hospital	1 ton CH ₄ =	21 tons CO ₂ (IPCC 1996)
Project location	Whitehorse	1 ton N ₂ O =	310 tons CO ₂ (IPCC 1996)

Base Case Electricity System (Reference)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	T & D losses (%)	GHG emission factor (tCO ₂ /MWh)
Small hydro	100.0%	0.0	0.0000	0.0000	100.0%	8.0%	0.000
Electricity mix	100%	0.0	0.0000	0.0000		8.0%	0.000

Base Case Heating System (Reference)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	GHG emission factor (tCO ₂ /MWh)
Heating system Diesel (#2 oil)	100.0%	74.1	0.0020	0.0020	80.0%	0.336

Proposed Case Heating System (Mitigation)

Fuel type	Fuel mix (%)	CO ₂ emission factor (kg/GJ)	CH ₄ emission factor (kg/GJ)	N ₂ O emission factor (kg/GJ)	Fuel conversion efficiency (%)	GHG emission factor (tCO ₂ /MWh)
Heating system Electricity	1.4%	0.0	0.0000	0.0000	100.0%	0.000
Solar	98.6%	0.0	0.0000	0.0000	100.0%	0.000
Heating energy mix	100.0%	0.0	0.0000	0.0000		0.000

GHG Emission Reduction Summary

Heating system	Base case GHG emission factor (tCO ₂ /MWh)	Proposed case GHG emission factor (tCO ₂ /MWh)	End-use annual energy delivered (MWh)	Annual GHG emission reduction (tCO ₂)
	0.336	0.000	80.4	27.04
Net GHG emission reduction				27.04

Complete Financial Summary sheet

SOLAR HEATING SYSTEM SPECIFICATIONS

ENERGY INPUTS

System	Flow (l/s)	Schedule	Heating Fuel	Heating Efficiency	Cost of Fuel
Wall 1	8816	* 7 days/week 24 hrs/day	Oil (l)	80.0 %	\$ 0.45

BUILDING INPUTS

System	Min. Supply Air Temp. (°C)	Max. Useful Supply Temp. (°C)	Ceiling R-Value (°C-m ² /W)	Wall R-Value (°C-m ² /W)	Building Temperature (°C)	Ceiling Temperature (°C)	Exhaust Fan Location
Wall 1	13.5	12.5	2.11	3.50	20.0	25.0	Ceiling

COLLECTOR

System	Total Area (m ²)	Porosity	Depth (m)	Collector Height (m)	Canopy Height (m)	Collector Width (m)	Canopy Width (m)
Wall 1	248.20	High	0.50	7.30	2.50	34.00	34.00

BYPASS DAMPERS

System	Number of Bypass Dampers	Type of Bypass Damper	Damper Area (m ²)	Bypass Temperature (°C)	Damper Width (m)	Damper Height (m)
Wall 1	1	Wall	3.33	13.5	3.65	0.91

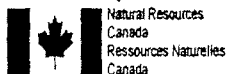
SOLARWALL FAN

System	Number of Fans	Fan Efficiency	Motor Efficiency	Flow (l/s)	Power (kW)	Pressure (Pa)
Wall 1	1	High	High	8816	12.5	873.1

DUCTING

System	Number	Length (m)	Duct Area (m ²)	Accessories
Wall 1	1	100.00	0.50	Tapered Inlet

SWift was produced by:

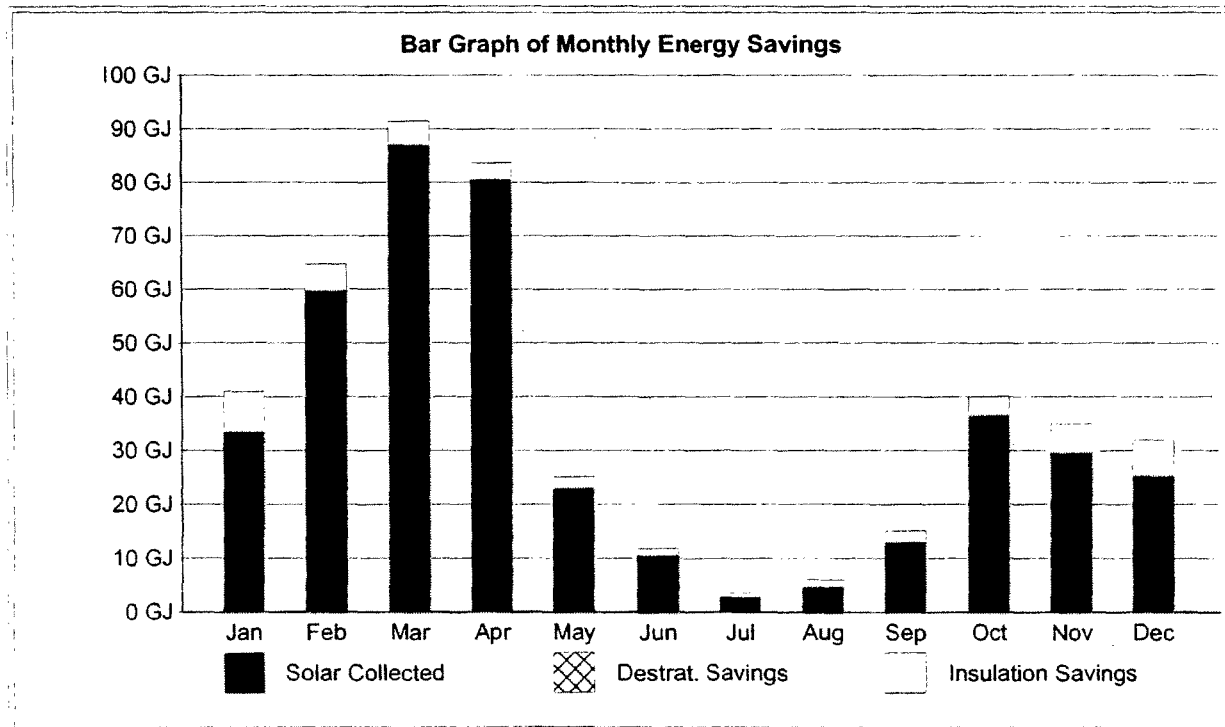


Monthly Results for Wall: 1

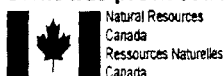
Month	Degree-Days Base (18°C)	Solar Radiation Incident (GJ)	Solar Radiation Incident Operational	Average Daytime Temp. Rise	Solar Energy Collected (GJ)	Insulation Savings (GJ)	Destrat. Savings (GJ)	Total Savings (GJ)
January	1193	51.3	48.7	4.3	33.5	7.5	N/A	41.0
February	821	108.0	90.3	6.2	59.7	5.0	N/A	64.8
March	752	168.9	135.8	6.4	87.1	4.5	N/A	91.6
April	536	179.4	132.1	5.0	80.5	3.1	N/A	83.6
May	350	146.2	44.6	1.2	23.0	2.1	N/A	25.1
June	196	123.0	20.8	0.6	10.5	1.3	N/A	11.9
July	125	119.6	5.3	0.2	2.7	0.9	N/A	3.6
August	198	125.7	8.9	0.3	4.8	1.3	N/A	6.1
September	328	97.6	24.6	1.0	13.1	2.1	N/A	15.2
October	552	75.3	59.1	3.2	36.6	3.5	N/A	40.1
November	848	47.0	44.7	3.6	29.6	5.4	N/A	35.0
December	1047	37.9	37.5	3.6	25.4	6.7	N/A	32.0
TOTAL	6946	1279.8	652.4	2.5	406.5	43.5	N/A	450.0

ANNUAL SYSTEM PERFORMANCE

PERFORMANCE	LOAD	
	Solar	Total
Annual Savings (GJ/m ²)	1.64	1.81
Collector Efficiency (%)	62	—
	Daytime	Total
Annual Ventilation Load (GJ)	1783.70	5181.07
Ventilation Load by Collector (%)	24	9



SWift was produced by:



Friday, January 24, 2003

SOLAR HEATING SYSTEM SPECIFICATIONS

ENERGY INPUTS

System	Flow (l/s)	Schedule	Heating Fuel	Heating Efficiency	Cost of Fuel
Wall 1	8816	* 7 days/week 24 hrs/day	Elec. (kWh)	100.0 %	\$ 0.04

BUILDING INPUTS

System	Min. Supply Air Temp. (°C)	Max. Useful Supply Temp. (°C)	Ceiling R-Value (°C-m²/W)	Wall R-Value (°C-m²/W)	Building Temperature (°C)	Ceiling Temperature (°C)	Exhaust Fan Location
Wall 1	13.5	12.5	2.11	3.50	20.0	25.0	Ceiling

COLLECTOR

System	Total Area (m²)	Porosity	Depth (m)	Collector Height (m)	Canopy Height (m)	Collector Width (m)	Canopy Width (m)
Wall 1	248.20	High	0.50	7.30	2.50	34.00	34.00

BYPASS DAMPERS

System	Number of Bypass Dampers	Type of Bypass Damper	Damper Area (m²)	Bypass Temperature (°C)	Damper Width (m)	Damper Height (m)
Wall 1	1	Wall	3.33	13.5	3.65	0.91

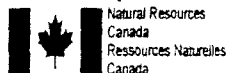
SOLARWALL FAN

System	Number of Fans	Fan Efficiency	Motor Efficiency	Flow (l/s)	Power (kW)	Pressure (Pa)
Wall 1	1	High	High	8816	12.5	873.1

DUCTING

System	Number	Length (m)	Duct Area (m²)	Accessories
Wall 1	1	100.00	0.50	Tapered Inlet

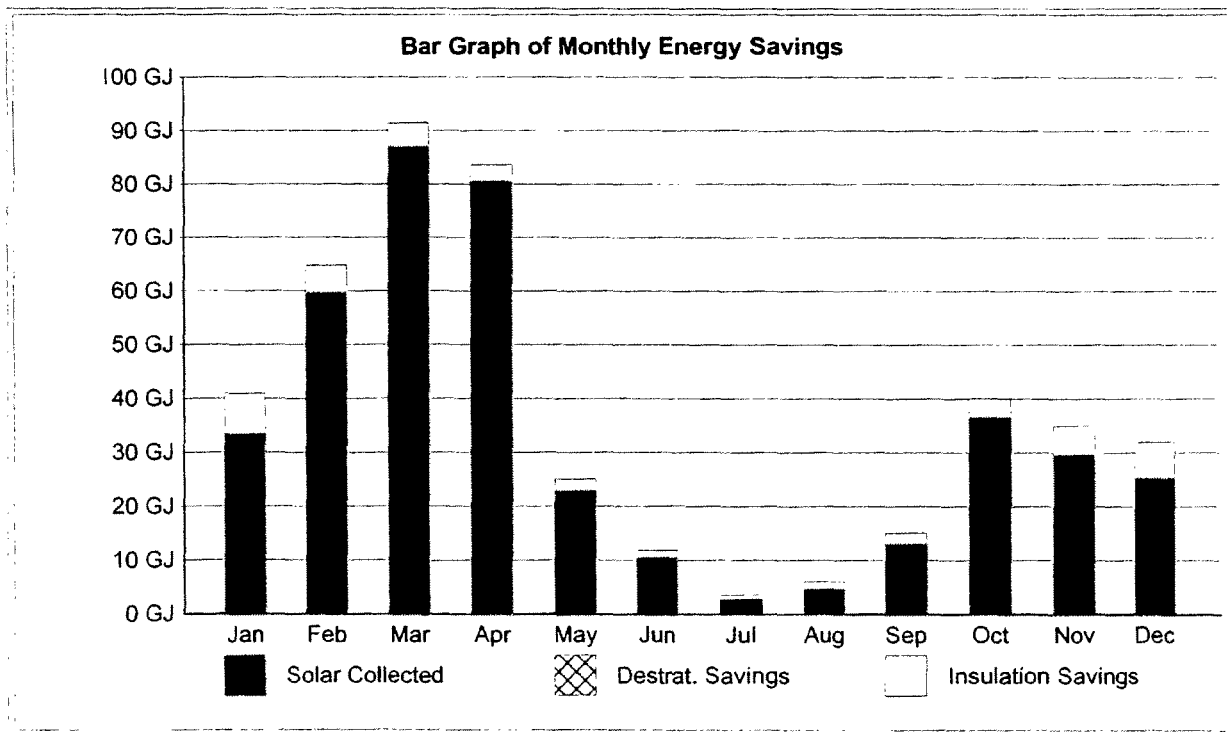
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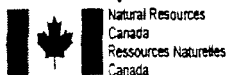
Monthly Results for Wall: 1

Month	Degree-Days Base (18°C)	Solar Radiation Incident (GJ)	Solar Radiation Incident Operational	Average Daytime Temp. Rise	Solar Energy Collected (GJ)	Insulation Savings (GJ)	Destrat. Savings (GJ)	Total Savings (GJ)
January	1193	51.3	48.7	4.3	33.5	7.5	N/A	41.0
February	821	108.0	90.3	6.2	59.7	5.0	N/A	64.8
March	752	168.9	135.8	6.4	87.1	4.5	N/A	91.6
April	536	179.4	132.1	5.0	80.5	3.1	N/A	83.6
May	350	146.2	44.6	1.2	23.0	2.1	N/A	25.1
June	196	123.0	20.8	0.6	10.5	1.3	N/A	11.9
July	125	119.6	5.3	0.2	2.7	0.9	N/A	3.6
August	198	125.7	8.9	0.3	4.8	1.3	N/A	6.1
September	328	97.6	24.6	1.0	13.1	2.1	N/A	15.2
October	552	75.3	59.1	3.2	36.6	3.5	N/A	40.1
November	848	47.0	44.7	3.6	29.6	5.4	N/A	35.0
December	1047	37.9	37.5	3.6	25.4	6.7	N/A	32.0
TOTAL	6946	1279.8	652.4	2.5	406.5	43.5	N/A	450.0

ANNUAL SYSTEM PERFORMANCE				
PERFORMANCE			LOAD	
	Solar	Total	Daytime	Total
Annual Savings (GJ/m ²)	1.64	1.81	1783.70	5181.07
Collector Efficiency (%)	62	—	24	9
			Annual Ventilation Load (GJ)	
			Ventilation Load by Collector (%)	

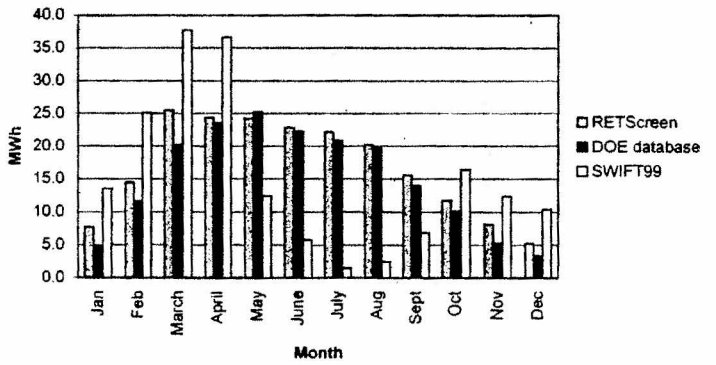
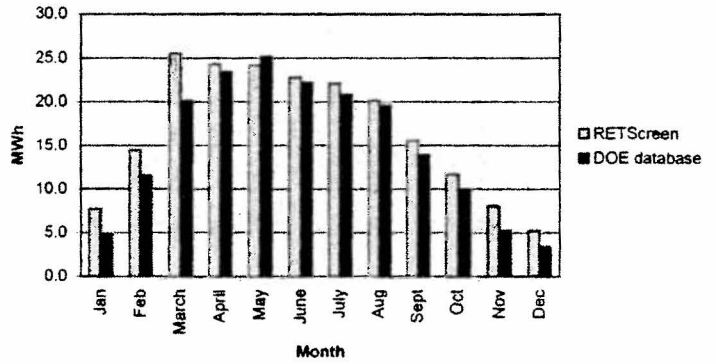


Swift was produced by:



ANALYSIS OF AVAILABLE SOLAR ENERGY THRU SOLARWALL ON MONTHLY BASIS

RETScreen values			
	kWh/m ² /d	MWh	Avail MWh
Jan	1.28	31	9.7
Feb	2.81	28	18.1
March	4.15	31	31.9
April	4.09	30	30.5
May	3.93	31	30.2
June	3.84	30	28.5
July	3.60	31	27.7
Aug	3.29	31	25.3
Sept	2.63	30	18.5
Oct	1.91	31	14.7
Nov	1.36	30	10.1
Dec	0.88	31	6.6
		252.9	202.3
Area	248		
absorptive	0.8		
DOE values			
	mmBtu	Avail MWh	
	16.68	4.9	
	38.59	11.6	
	68.83	20.2	
	80.13	23.5	
	85.99	25.2	
	76.08	22.3	
	71.15	20.9	
	67.1	19.7	
	47.78	14.0	
	34.49	10.1	
	18.18	5.3	
	11.69	3.4	
	617.65	181.0	
SWIFT99 values			
	GJ	MWh	
	48.7	13.5	0.69
	90.3	25.1	0.66
	135.8	37.7	0.64
	132.1	36.7	0.61
	44.6	12.4	0.52
	20.8	5.8	0.50
	5.3	1.5	0.51
	8.9	2.5	0.54
	24.6	6.8	0.53
	59.1	16.4	0.62
	44.7	12.4	0.66
	37.5	10.4	0.68
	652.4	181.2	



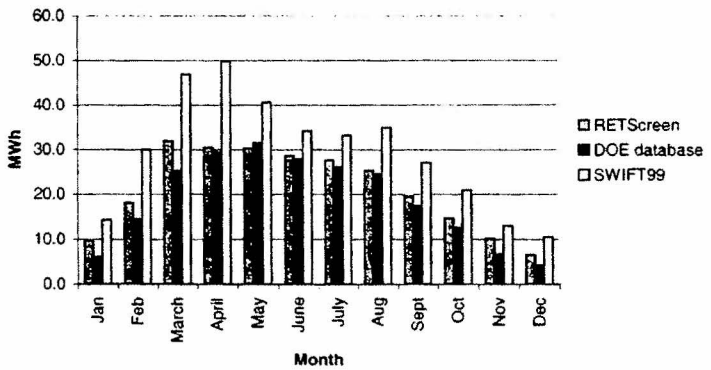
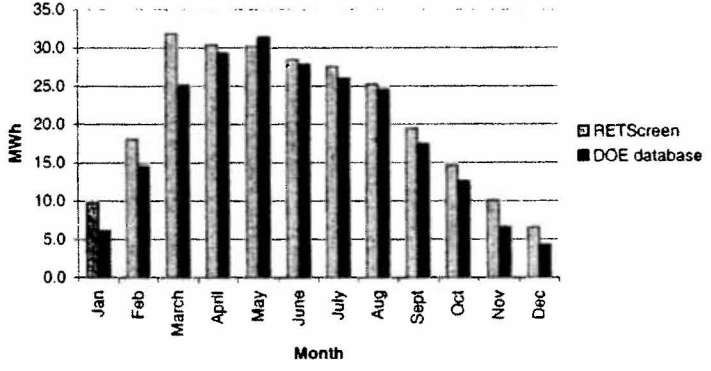
*****TABLE NOT VALID INPUT IS NOT SAME PARAMETERS

ANALYSIS OF TOTAL SOLAR RADIATION INCIDENT ON SURFACE AREA ON MONTHLY BASIS

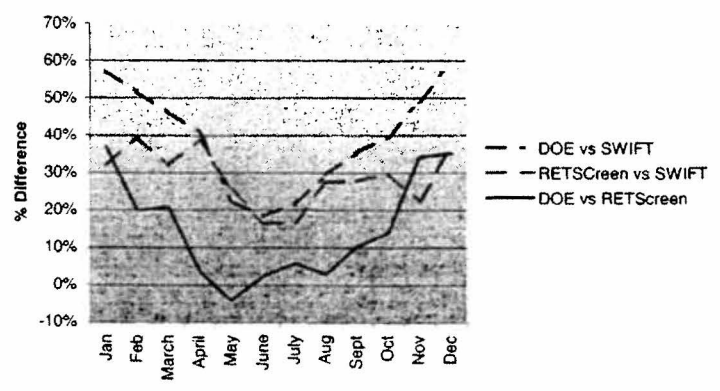


DOE values	mmBtu	Avail MWh
	16.66	6.1
	39.59	14.5
	56.83	25.2
	80.13	29.4
	86.99	31.5
	78.06	27.9
	71.15	26.1
	67.1	24.6
	47.78	17.5
	34.49	12.6
	16.18	6.7
	11.69	4.3
	617.65	226.3

SWIFT99 values	GJ	MWh
	51.3	14.3
	108	30.0
	168.9	46.9
	179.4	49.8
	146.2	40.6
	123	34.2
	119.6	33.2
	125.7	34.9
	97.8	27.1
	75.3	20.9
	47	13.1
	37.9	10.5
	1279.9	355.5



% diff	DOE/S	RET/S	DOE/RET
Jan	57.17%	31.99%	37.03%
	51.66%	39.64%	19.91%
	46.26%	32.02%	20.94%
	41.10%	38.89%	3.61%
	22.44%	25.52%	-4.13%
	18.43%	16.47%	2.35%
	21.55%	16.73%	5.79%
	29.60%	27.53%	2.86%
	35.44%	27.95%	10.40%
	39.60%	29.80%	13.95%
	49.05%	22.48%	34.27%
Dec	59.32%	37.15%	35.28%
Avg	39.30%	28.85%	15.19%

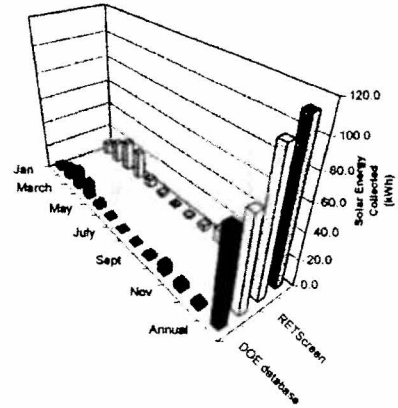


	Solar Energy Collected SWIFT	Insulation Savings			Total Energy	
Jan	33.5	9.3	7.5	2.1	41	11.4
Feb	59.7	16.6	5	1.4	64.7	18.0
March	87.1	24.2	4.5	1.3	91.6	25.4
April	80.5	22.4	3.1	0.9	83.6	23.2
May	23	6.4	2.1	0.6	25.1	7.0
June	10.5	2.9	1.3	0.4	11.8	3.3
July	2.7	0.8	0.9	0.3	3.6	1.0
Aug	4.8	1.3	1.3	0.4	6.1	1.7
Sept	13.1	3.6	2.1	0.6	15.2	4.2
Oct	36.6	10.2	3.5	1.0	40.1	11.1
Nov	29.6	8.2	5.4	1.5	35	9.7
Dec	25.4	7.1	6.7	1.9	32.1	8.9
Annual	406.5 GJ	112.9 kWh	43.4 GJ	12.1 kWh	448.9 GJ	125.8 kWh

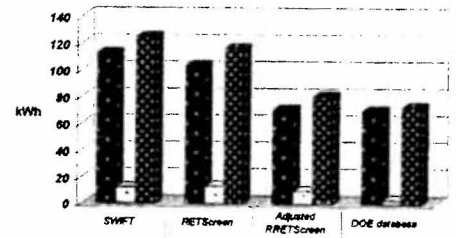
RETScreen						
Jan						
Feb						
March						
April						
May						
June						
July						
Aug						
Sept						
Oct						
Nov						
Dec						
Annual		103.3 kWh		13.1 kWh		116.4 kWh

Adjusted RETScreen						
Jan						
Feb						
March						
April						
May						
June						
July						
Aug						
Sept						
Oct						
Nov						
Dec						
Annual		70.8 kWh		9.5 kWh		80.4 kWh

DOE Database						
Jan	16.66	4.9				
Feb	36.48	10.7				
March	54.5	16.0				
April	45.72	13.4				
May	12.89	3.8				
June	6.21	1.8				
July	2.03	0.6				
Aug	3.51	1.0				
Sept	7.19	2.1				
Oct	24.62	7.2				
Nov	17.23	5.0				
Dec	11.69	3.4				
Annual	mmBtu	70.0 kWh		2.75 kWh		72.7 kWh



SWIFT	RETScreen	Adjusted R	DOE database	70
112.9	103.3	70.8	70	Solar Energy Collected (kWh)
12.1	13.1	9.5	2.75	Building Heat Loss Recaptured
125	116.4	80.4	72.7	Annual Energy Saved



	SWIFT	RETScreen	Adjusted RRETScreen	DOE database
■ Solar Energy Collected (kWh)	112.9	103.3	70.8	70
□ Heat Loss Recaptured (kWh)	12.1	13.1	9.5	2.75
■ Annual Energy Saved (kWh)	125	116.4	80.4	72.7

APPENDIX D

FINANCIAL ANALYSIS

The logo for FSC (Forest Stewardship Council) consists of the letters 'FSC' in a stylized, serif font, with the word 'GROUP' written in a smaller, sans-serif font directly below it.

JOB NAME: WGH Solarwall
 JOB NUMBER: 2002-4110.22
 LOCATION: Whitehorse, YT
 COMMUNITY FACTOR 1.30
 ESTIMATED BY: RDA
 DATE ESTIMATED: Jan 24/03
 MAN HOUR RATE \$70.00

Description	Qty	@	Material	Hrs	Labour	TOTAL	Subtotals	% sub	Adj Subtotals
Item		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -	\$ -		
		\$ -	\$ -		\$ -	\$ -			
Solarwall		\$ -	\$ -		\$ -	\$ -			
Painting "H" symbol	1 uc	\$ 500.00	\$ 650	40.00	\$ 2,800.00	\$ 3,450	\$ 3,450	12.57%	\$4,264
		\$ -	\$ -		\$ -	\$ -			
Item		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -	\$ -		
		\$ -	\$ -		\$ -	\$ -			
Controls		\$ -	\$ -		\$ -	\$ -			
Reprogramming	1 uc	\$ 500.00	\$ 650	20.00	\$ 1,400.00	\$ 2,050			
Total new points	5 uc	\$ 500.00	\$ 3,250		\$ -	\$ 3,250			
Site and startup	1 uc	\$ 500.00	\$ 650	20.00	\$ 1,400.00	\$ 2,050	\$ 7,350	26.77%	\$9,085
		\$ -	\$ -		\$ -	\$ -			
Startup and Commissioning		\$ -	\$ -		\$ -	\$ -			
Mech	1 uc	\$ 2,500.00	\$ 3,250	20.00	\$ 1,400.00	\$ 4,650			
Controls	1 hr	\$ -	\$ -	16.00	\$ 1,120.00	\$ 1,120			
Commissioning	1 uc	\$ 150.00	\$ 195	16.00	\$ 1,120.00	\$ 1,315	\$ 7,085	25.81%	\$8,757
		\$ -	\$ -		\$ -	\$ -			
Misc		\$ -	\$ -		\$ -	\$ -			
Permits	1 uc	\$ 1,000.00	\$ 1,300		\$ -	\$ 1,300			
TAB	1 uc	\$ 500.00	\$ 650	16.00	\$ 1,120.00	\$ 1,770			
Admin		\$ -	\$ -		\$ -	\$ -			
Travel(Controls 1 trips/startup 1 trip)	2 uc	\$ 2,500.00	\$ 6,500		\$ -	\$ 6,500	\$ 9,570	34.86%	\$11,829
		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -			
		\$ -	\$ -		\$ -	\$ -			
SUB-TOTAL 1			\$ 17,095	148	\$ 10,360	\$ 27,455		100%	\$33,934
Plus 3% Inflation			\$ 513		\$ 311	\$ 824			
SUB-TOTAL 1			\$ 17,608	296	\$ 10,671	\$ 28,279			
Plus 10% O/H & 10% Profit			\$ 3,522		\$ 2,134	\$ 5,656			
SUB-TOTAL 2			\$ 21,129		\$ 12,805	\$ 33,934			
Plus Solarwall Quotation			-		-	116,950			
SUB-TOTAL 2			\$ 21,129		\$ 12,805	\$ 150,884			
Plus 10% Contingency			2,113		1,280	15,088			
TOTAL			\$ 23,242		\$ 14,085	\$ 165,973			

Notes: 1. Class D estimate accurate within +/- 20% with more than 3 bids in public tender.

From: "dml" <2dl@telus.net>
To: altodom.altapo(Ross)
Date: Fri, Jan 24, 2003 12:33 PM
Subject: Solarwall

Hi Ross

Thank you for your patience. Have just heard from Steve.
Preliminary cost estimate based on information given to date:

\$116,000 plus GST including freight and also including modulating dampers for both main air intakes to create suction for Solarwall cavity, also dampers connected to Solarwall cavity plus all controls.

Pat has asked Steve to e-mail you a copy of his quote so you will know the details included.
Thanks again for your patience.

Sincerely,

Donna Lewis, MBA

Astravan Distributors

Your Environmental Partner

1-800-663-8405

From: "Steve Duncan" <steve@duncansltd.com>
To: fscykd3.gwiafscy3("info@astravan.com")
Date: Fri, Jan 24, 2003 1:11 PM
Subject: Whitehorse General Hospital

Hi Pat:

I have the following budget only price for the supply and installation of all materials necessary to provide a complete solar wall installation for the Whitehorse General Hospital as per the information provided. Included are the following items.

1. All necessary 18 Ga. Z bars for a 6" cavity behind all of the panels except where the ducts will be installed, based on a 2' grid system.
2. Supply and installation of all solar wall panels as supplied by Astravan, for wall area of about 118' x 25'.
3. Removal of the existing outside air intake louvre and the extension of the 25' x 9' duct by about 30"
4. To supply and install a motorized damper assembly for the 25' x 9' duct, and to install the louvre on the outside of the extended duct.
5. To install one smaller and one larger duct into the 25' x 9' duct extension. Each duct will have its own damper and actuator. These ducts will be extended approximately 12' up to the inlet location near the top of the solar wall.
6. The perimeter of the wall will have insulation installed and flashings provided for watertight finishing of the installation. Flashings will be provided for the jog on the left side of the wall and for the duct shaft enclosure area.
7. All necessary craning, lifts, scaffolds etc. necessary for the installation are included.
8. All necessary control and electrical wiring is included.

The above is for budget purposes only and is based on a wall spaced 6" except for the enclosure around the vertical ducts where the enclosure will be approximately 30" from the existing wall surface.
Our budget only price: \$116,959.00 GST extra

Please call if you have any questions or require additional information.

Steve Duncan
President
Duncan's Limited
867-667-6613

CC: altodom.altapo(Ross)

RETScreen® Cost Analysis - Solar Air Heating Project

FO Heating

Type of project:

Currency:

Cost references:

Initial Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
Feasibility Study							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Development							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Engineering							
Other	Cost	1	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Renewable Energy (RE) Equipment							
Solar collector materials	m²	248	\$ 608	\$ 150,883	-	-	-
Equipment installation	m²	248	\$ -	\$ -	-	-	-
Cladding material credit	m²	-248	\$ -	\$ -	-	-	-
Cladding labour credit	m²	-248	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ 150,883	90.9%	-	-
Balance of Equipment							
Fans and ducting materials	L/s	8,817	\$ -	\$ -	-	-	-
Fans and ducting labour	L/s	8,817	\$ -	\$ -	-	-	-
Fan and duct mat'l credit	L/s	-8,817	\$ -	\$ -	-	-	-
Fan and duct labour credit	L/s	-8,817	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Miscellaneous							
Overhead	%	0%	\$ 150,883	\$ -	-	-	-
Training	p-h	0	\$ -	\$ -	-	-	-
Contingencies	%	10%	\$ 150,883	\$ 15,088	-	-	-
Sub-total :				\$ 15,088	9.1%	-	-
Initial Costs - Total				\$ 165,972	100.0%	-	-

Annual Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
O&M							
Property taxes/Insurance	project	1	\$ -	\$ -	-	-	-
O&M labour	project	0	\$ -	\$ -	-	-	-
Travel and accommodation	p-trip	1	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Contingencies	%	0%	\$ 150,883	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Fuel/Electricity	kWh	2,172	\$ 0.1305	\$ 284	100.0%	-	-
Annual Costs - Total				\$ 284	100.0%	-	-

Periodic Costs (Credits)	Period	Unit Cost	Amount	Interval Range	Unit Cost Range
Damper Motor	5 yr	\$ 200	\$ (200)	-	-
		\$ -	\$ -	-	-
		\$ -	\$ -	-	-
End of project life	-	\$ -	\$ -	-	-

Go to GHG Analysis sheet

RETScreen® Financial Summary - Solar Air Heating Project

FO Heating

Annual Energy Balance					
Project name	Whitehorse General Hospital		Electricity required	MWh	2.2
Project location	Whitehorse		GHG analysis sheet used?	yes/no	Yes
Renewable energy delivered	MWh	116.4	Net GHG emission reduction	t _{CO2} /yr	39
Heating fuel displaced	-	Diesel (#2 oil)	Net GHG emission reduction - 25 yrs	t _{CO2}	979

Financial Parameters					
Avoided cost of heating energy	\$/L	0.450	Debt ratio	%	0.0%
GHG emission reduction credit	\$/t _{CO2}	-	Income tax analysis?	yes/no	No
Retail price of electricity	\$/kWh	0.131			
Energy cost escalation rate	%	5.0%			
Inflation	%	3.0%			
Discount rate	%	4.5%			
Project life	yr	25			

Project Costs and Savings					
Initial Costs			Annual Costs and Debt		
Feasibility study	0.0%	\$ -	O&M	\$	-
Development	0.0%	\$ -	Fuel/Electricity	\$	284
Engineering	0.0%	\$ -			
RE equipment	90.9%	\$ 150,883	Annual Costs - Total	\$	284
Balance of equipment	0.0%	\$ -			
Miscellaneous	9.1%	\$ 15,088	Annual Savings or Income		
Initial Costs - Total	100.0%	\$ 165,972	Heating energy savings/income	\$	6,099
Incentives/Grants		\$ 66,388			
			Annual Savings - Total	\$	6,099
Periodic Costs (Credits)			Schedule yr #		5, 10, 15, 20, 25
Damper Motor		\$ (200)			
		\$ -			
		\$ -			
End of project life -		\$ -			

Financial Feasibility					
Pre-tax IRR and ROI	%	8.4%	Calculate GHG reduction cost?	yes/no	No
After-tax IRR and ROI	%	8.4%			
Simple Payback	yr	17.1	Project equity	\$	165,972
Year-to-positive cash flow	yr	12.2			
Net Present Value - NPV	\$	56,002			
Annual Life Cycle Savings	\$	3,777			
Profitability Index - PI	-	0.34			

Yearly Cash Flows			
Year #	Pre-tax \$	After-tax \$	Cumulative \$
0	(99,584)	(99,584)	(99,584)
1	6,106	6,106	(93,478)
2	6,411	6,411	(87,066)
3	6,732	6,732	(80,335)
4	7,068	7,068	(73,266)
5	7,654	7,654	(65,613)
6	7,793	7,793	(57,820)
7	8,182	8,182	(49,638)
8	8,592	8,592	(41,046)
9	9,021	9,021	(32,025)
10	9,741	9,741	(22,284)
11	9,946	9,946	(12,338)
12	10,443	10,443	(1,895)
13	10,965	10,965	9,070
14	11,514	11,514	20,584
15	12,401	12,401	32,985
16	12,694	12,694	45,679
17	13,328	13,328	59,007
18	13,995	13,995	73,002
19	14,695	14,695	87,696
20	15,790	15,790	103,487
21	16,201	16,201	119,687
22	17,011	17,011	136,698
23	17,861	17,861	154,559
24	18,754	18,754	173,314
25	20,111	20,111	193,425

FO Heating

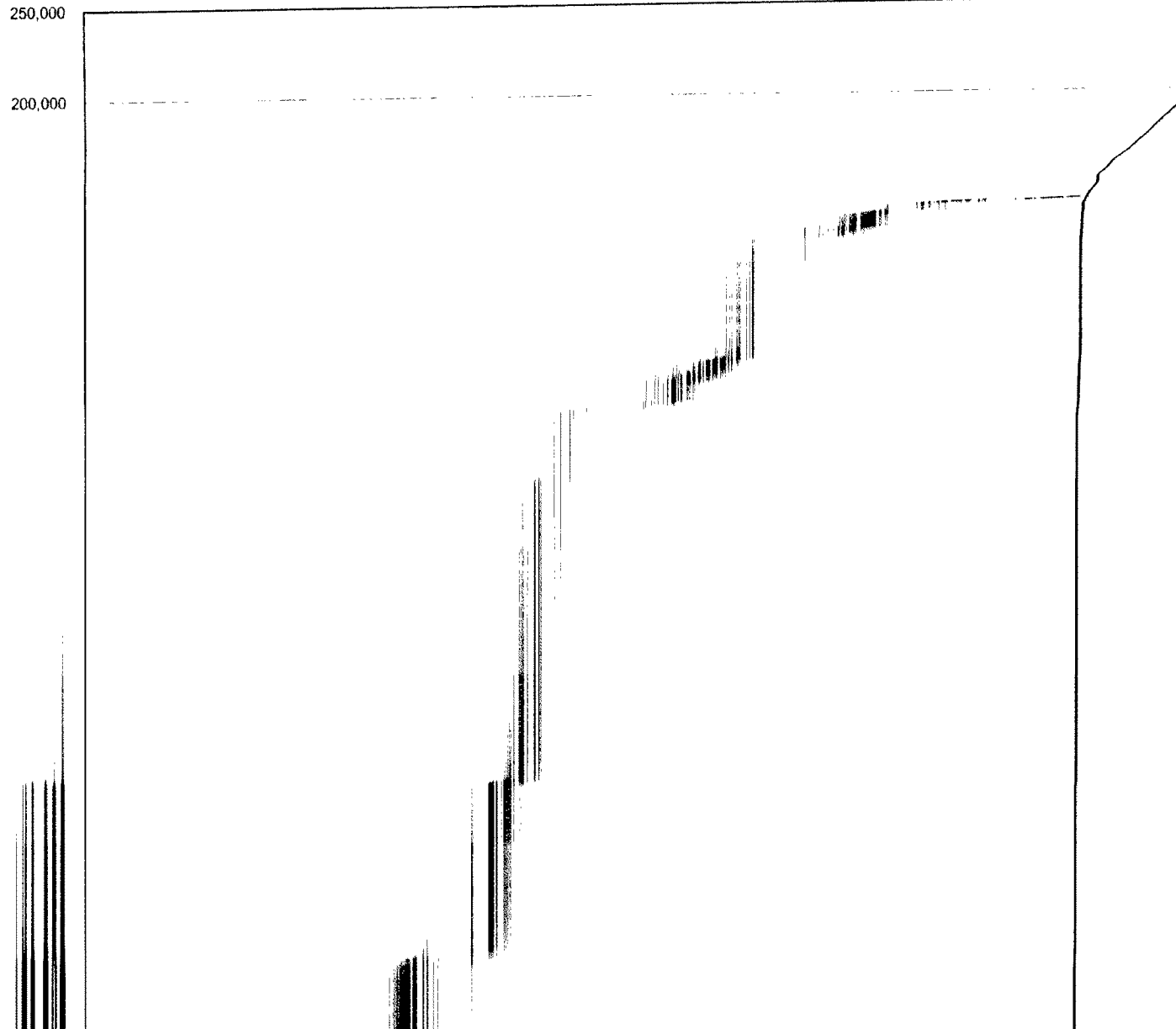
Cumulative Cash Flows Graph

SAH Project Cumulative Cash Flows Whitehorse General Hospital, Whitehorse

Year-to-positive cash flow 12.2 yr

IRR and ROI 8.4%

Net Present Value \$ 56,002



RETScreen® Cost Analysis - Solar Air Heating Project

Secondary Sales

Type of project:

Currency:

Cost references:

Initial Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
Feasibility Study							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Development							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Engineering							
Other	Cost	1	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Renewable Energy (RE) Equipment							
Solar collector materials	m ²	248	\$ 608	\$ 150,883	-	-	-
Equipment installation	m ²	248	\$ -	\$ -	-	-	-
Cladding material credit	m ²	-248	\$ -	\$ -	-	-	-
Cladding labour credit	m ²	-248	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ 150,883	90.9%	-	-
Balance of Equipment							
Fans and ducting materials	L/s	8,817	\$ -	\$ -	-	-	-
Fans and ducting labour	L/s	8,817	\$ -	\$ -	-	-	-
Fan and duct mat'l credit	L/s	-8,817	\$ -	\$ -	-	-	-
Fan and duct labour credit	L/s	-8,817	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Miscellaneous							
Overhead	%	0%	\$ 150,883	\$ -	-	-	-
Training	p-h	0	\$ -	\$ -	-	-	-
Contingencies	%	10%	\$ 150,883	\$ 15,088	-	-	-
Sub-total :				\$ 15,088	9.1%	-	-
Initial Costs - Total				\$ 165,972	100.0%	-	-

Annual Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
O&M							
Property taxes/Insurance	project	1	\$ -	\$ -	-	-	-
O&M labour	project	0	\$ -	\$ -	-	-	-
Travel and accommodation	p-trip	1	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Contingencies	%	0%	\$ 150,883	\$ -	-	-	-
Sub-total :				\$ -	0.0%	-	-
Fuel/Electricity	kWh	2,172	\$ 0.1305	\$ 284	100.0%	-	-
Annual Costs - Total				\$ 284	100.0%	-	-

Periodic Costs (Credits)	Period	Unit Cost	Amount	Interval Range	Unit Cost Range
Damper Motor	5 yr	\$ 200	\$ (200)	-	-
		\$ -	\$ -	-	-
		\$ -	\$ -	-	-
End of project life	-	\$ -	\$ -	-	-

Go to GHG Analysis sheet

Secondary Sites

Annual Energy Balance				
Project name	Whitehorse General Hospital	Electricity required	MWh	2.2
Project location	Whitehorse			
Renewable energy delivered	MWh	116.4	GHG analysis sheet used?	Yes
			Net GHG emission reduction	t _{co2} /yr 0
			Net GHG emission reduction - 25 yrs	t _{co2} 0
Heating fuel displaced	-	Electricity		

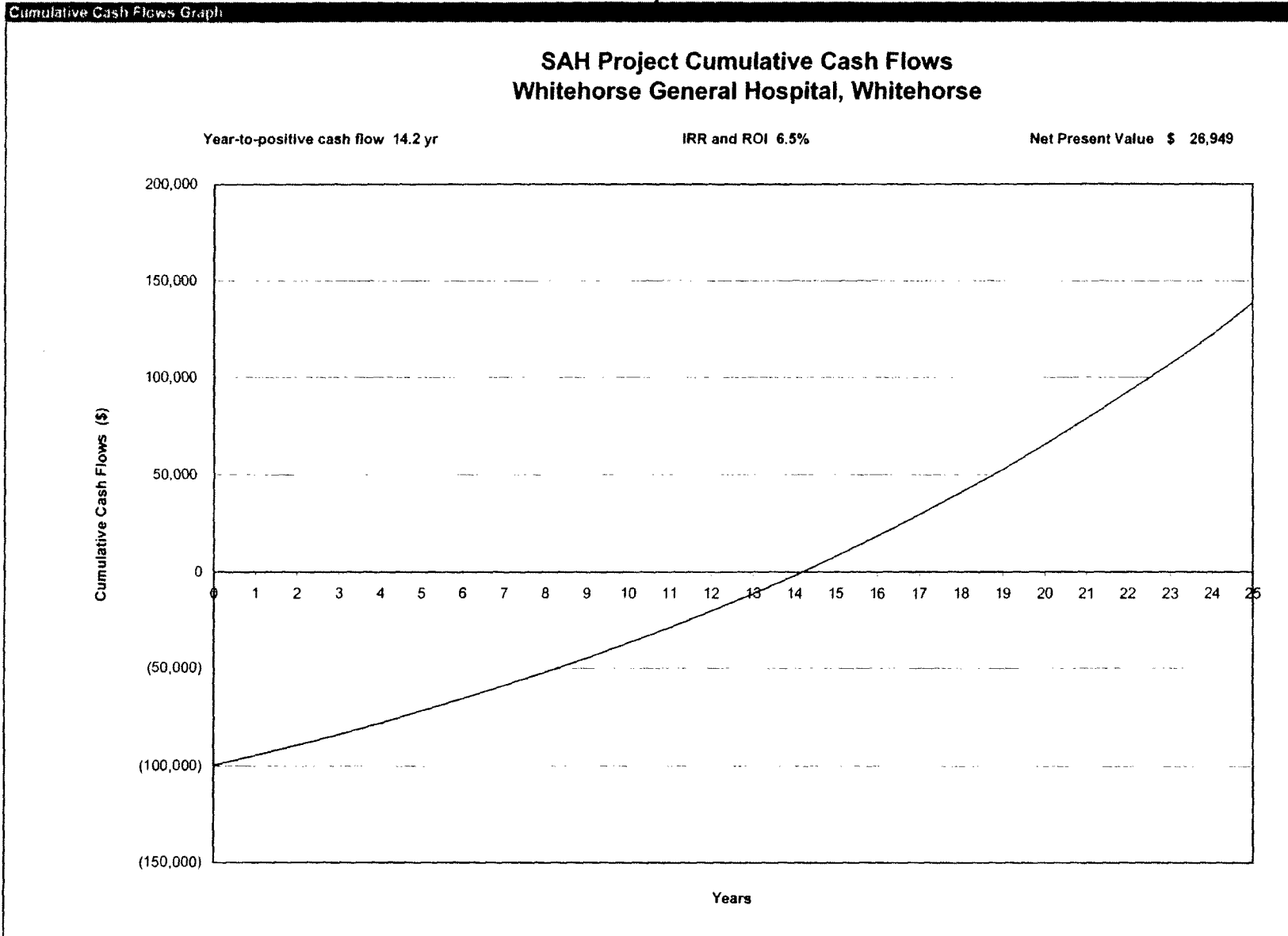
Financial Parameters				
Avoided cost of heating energy	\$/kWh	<input type="text" value="0.043"/>	Debt ratio	% <input type="text" value="0.0%"/>
GHG emission reduction credit	\$/t _{co2}	<input type="text" value="-"/>	Income tax analysis?	yes/no <input type="text" value="No"/>
Retail price of electricity	\$/kWh	0.131		
Energy cost escalation rate	%	<input type="text" value="5.0%"/>		
Inflation	%	<input type="text" value="3.0%"/>		
Discount rate	%	<input type="text" value="4.5%"/>		
Project life	yr	<input type="text" value="25"/>		

Project Costs and Savings				
Initial Costs			Annual Costs and Debt	
Feasibility study	0.0%	\$ -	O&M	\$ -
Development	0.0%	\$ -	Fuel/Electricity	\$ 284
Engineering	0.0%	\$ -		
RE equipment	90.9%	\$ 150,883	Annual Costs - Total	\$ 284
Balance of equipment	0.0%	\$ -		
Miscellaneous	9.1%	\$ 15,088	Annual Savings or Income	
Initial Costs - Total	100.0%	\$ 165,972	Heating energy savings/income	\$ 5,007
Incentives/Grants	\$	<input type="text" value="66,388"/>		
			Annual Savings - Total	\$ 5,007
Periodic Costs (Credits)			Schedule yr # 5,10,15,20,25	
Damper Motor	\$	(200)		
	\$	-		
	\$	-		
End of project life -	\$	-		

Financial Feasibility				
Pre-tax IRR and ROI	%	6.5%	Calculate GHG reduction cost?	yes/no <input type="text" value="No"/>
After-tax IRR and ROI	%	6.5%		
Simple Payback	yr	21.1	Project equity	\$ 165,972
Year-to-positive cash flow	yr	14.2		
Net Present Value - NPV	\$	26,949		
Annual Life Cycle Savings	\$	1,817		
Profitability Index - PI	-	0.16		

Yearly Cash Flows			
Year #	Pre-tax \$	After-tax \$	Cumulative \$
0	(99,584)	(99,584)	(99,584)
1	4,960	4,960	(94,624)
2	5,208	5,208	(89,416)
3	5,468	5,468	(83,948)
4	5,742	5,742	(78,206)
5	6,260	6,260	(71,946)
6	6,330	6,330	(65,616)
7	6,647	6,647	(58,970)
8	6,979	6,979	(51,991)
9	7,328	7,328	(44,663)
10	7,963	7,963	(36,700)
11	8,079	8,079	(28,621)
12	8,483	8,483	(20,138)
13	8,907	8,907	(11,231)
14	9,352	9,352	(1,879)
15	10,132	10,132	8,253
16	10,311	10,311	18,563
17	10,826	10,826	29,390
18	11,368	11,368	40,758
19	11,936	11,936	52,694
20	12,894	12,894	65,588
21	13,160	13,160	78,748
22	13,818	13,818	92,565
23	14,508	14,508	107,074
24	15,234	15,234	122,308
25	16,414	16,414	138,722

Secondary Sales



RETScreen® Cost Analysis - Solar Air Heating P

Type of project:

Initial Costs (Credits)		Unit	
Feasibility Study			
Other		Cost	
Sub-total :			
Development			
Other		Cost	
Sub-total :			
Engineering			
Other		Cost	
Sub-total :			
Renewable Energy (RE) Equipment			
Solar collector materials		m ²	
Equipment installation		m ²	
Cladding material credit		m ²	
Cladding labour credit		m ²	
Incremental transportation		project	
Other		Cost	
Sub-total :			
Balance of Equipment			
Fans and ducting materials		L/s	
Fans and ducting labour		L/s	
Fan and duct mat'l credit		L/s	
Fan and duct labour credit		L/s	
Incremental transportation		project	
Other		Cost	
Sub-total :			
Miscellaneous			
Overhead		%	
Training		p-h	
Contingencies		%	
Sub-total :			
Initial Costs - Total			

Annual Costs (Credits)		Unit	
O&M			
Property taxes/Insurance		project	
O&M labour		project	
Travel and accommodation		p-trip	
Other		Cost	
Contingencies		%	
Sub-total :			
Fuel/Electricity		kWh	
Annual Costs - Total			

Periodic Costs (Credits)		Unit	
Damper Motor			
End of project life			

RETScreen® Financial Summary - Solar Air Heating Project *(Adjusted) FO Heating*

Annual Energy Balance				
Project name	Whitehorse General Hospital	Electricity required	MWh	1.2
Project location	Whitehorse			
Renewable energy delivered	MWh 80.4	GHG analysis sheet used?	yes/no	Yes
		Net GHG emission reduction	t _{CO2} /yr	27
		Net GHG emission reduction - 25 yrs	t _{CO2}	676
Heating fuel displaced	- Diesel (#2 oil)			

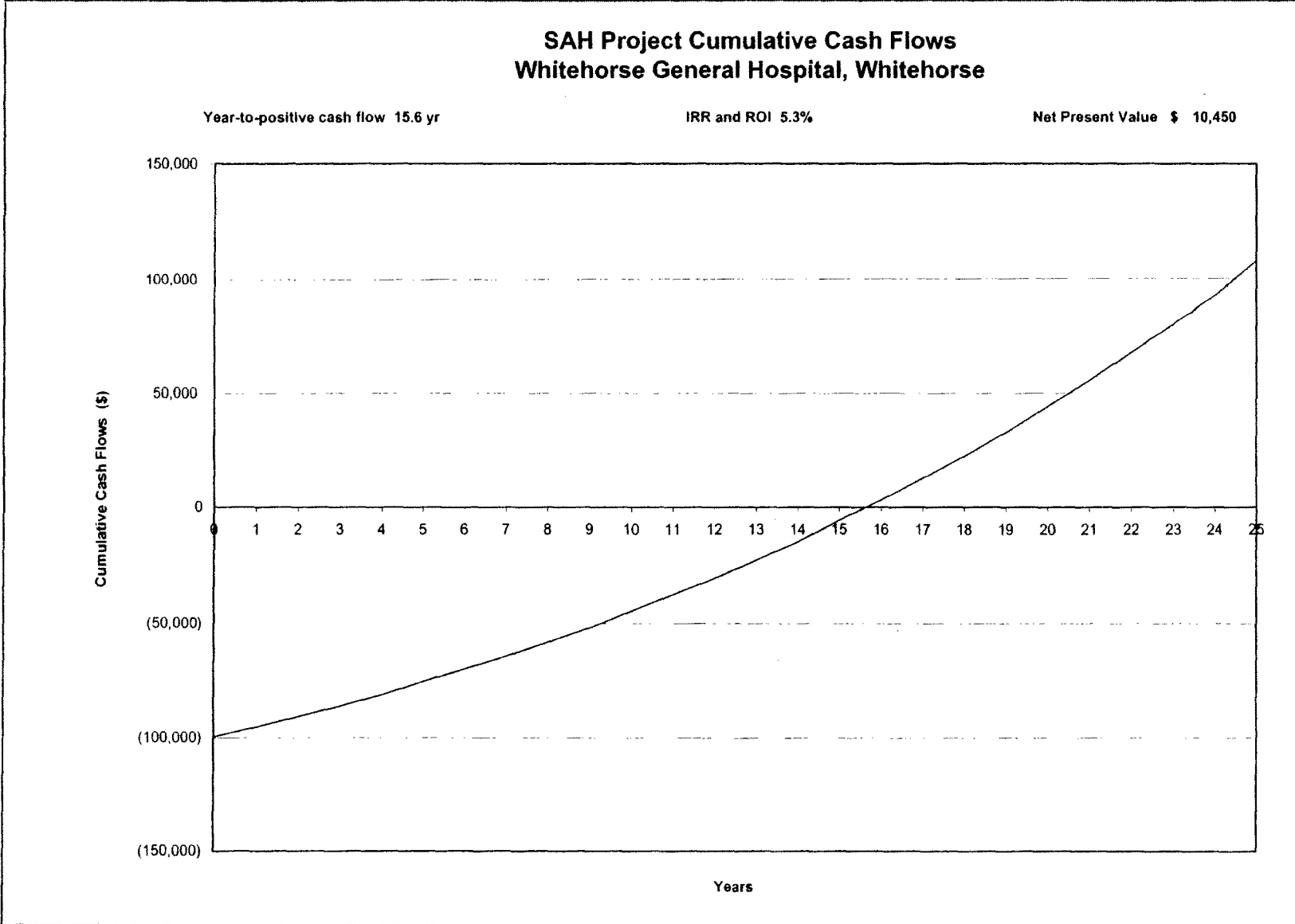
Financial Parameters				
Avoided cost of heating energy	\$/L	<input type="text" value="0.450"/>	Debt ratio	% <input type="text" value="0.0%"/>
GHG emission reduction credit	\$/t _{CO2}	<input type="text" value="-"/>	Income tax analysis?	yes/no <input type="text" value="No"/>
Retail price of electricity	\$/kWh	0.131		
Energy cost escalation rate	%	<input type="text" value="5.0%"/>		
Inflation	%	<input type="text" value="3.0%"/>		
Discount rate	%	<input type="text" value="4.5%"/>		
Project life	yr	<input type="text" value="25"/>		

Project Costs and Savings						
Initial Costs		Annual Costs and Debt				
Feasibility study	0.0%	\$	-	O&M	\$	-
Development	0.0%	\$	-	Fuel/Electricity	\$	151
Engineering	0.0%	\$	-			
RE equipment	90.9%	\$	150,883	Annual Costs - Total	\$	151
Balance of equipment	0.0%	\$	-			
Miscellaneous	9.1%	\$	15,088	Annual Savings or Income		
Initial Costs - Total	100.0%	\$	165,972	Heating energy savings/income	\$	4,209
Incentives/Grants		\$	<input type="text" value="66,388"/>	Annual Savings - Total	\$	4,209
Periodic Costs (Credits)				Schedule yr # 5, 10, 15, 20, 25		
Damper Motor		\$	(500)			
		\$	-			
		\$	-			
End of project life -		\$	-			

Financial Feasibility				
Pre-tax IRR and ROI	%	5.3%	Calculate GHG reduction cost?	yes/no <input type="text" value="No"/>
After-tax IRR and ROI	%	5.3%		
Simple Payback	yr	24.5	Project equity	\$ 165,972
Year-to-positive cash flow	yr	15.6		
Net Present Value - NPV	\$	10,450		
Annual Life Cycle Savings	\$	705		
Profitability Index - PI	-	0.06		

Yearly Cash Flows			
Year	Pre-tax	After-tax	Cumulative
#	\$	\$	\$
0	(99,584)	(99,584)	(99,584)
1	4,261	4,261	(95,323)
2	4,474	4,474	(90,849)
3	4,698	4,698	(86,151)
4	4,933	4,933	(81,218)
5	5,759	5,759	(75,459)
6	5,438	5,438	(70,021)
7	5,710	5,710	(64,311)
8	5,996	5,996	(58,316)
9	6,295	6,295	(52,020)
10	7,282	7,282	(44,738)
11	6,941	6,941	(37,797)
12	7,288	7,288	(30,510)
13	7,652	7,652	(22,858)
14	8,035	8,035	(14,823)
15	9,215	9,215	(5,608)
16	8,858	8,858	3,251
17	9,301	9,301	12,552
18	9,766	9,766	22,318
19	10,254	10,254	32,572
20	11,670	11,670	44,243
21	11,306	11,306	55,548
22	11,871	11,871	67,419
23	12,464	12,464	79,883
24	13,088	13,088	92,971
25	14,789	14,789	107,760

Cumulative Cash Flows Graph



RETScreen® Cost Analysis - Solar Air Heating Project *(Adjusted) Secondary Sales*

Type of project:

Currency:

Cost references:

Initial Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
Feasibility Study							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%		
Development							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%		
Engineering							
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%		
Renewable Energy (RE) Equipment							
Solar collector materials	m ²	248	\$ 608	\$ 150,883	-	-	-
Equipment installation	m ²	248	\$ -	\$ -	-	-	-
Cladding material credit	m ²	-248	\$ -	\$ -	-	-	-
Cladding labour credit	m ²	-248	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ 150,883	90.9%		
Balance of Equipment							
Fans and ducting materials	L/s	8,817	\$ -	\$ -	-	-	-
Fans and ducting labour	L/s	8,817	\$ -	\$ -	-	-	-
Fan and duct mat'l credit	L/s	-8,817	\$ -	\$ -	-	-	-
Fan and duct labour credit	L/s	-8,817	\$ -	\$ -	-	-	-
Incremental transportation	project	0	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Sub-total :				\$ -	0.0%		
Miscellaneous							
Overhead	%	0%	\$ 150,883	\$ -	-	-	-
Training	p-h	0	\$ -	\$ -	-	-	-
Contingencies	%	10%	\$ 150,883	\$ 15,088	-	-	-
Sub-total :				\$ 15,088	9.1%		
Initial Costs - Total				\$ 165,972	100.0%		

Annual Costs (Credits)	Unit	Quantity	Unit Cost	Amount	Relative Costs	Quantity Range	Unit Cost Range
O&M							
Property taxes/Insurance	project	1	\$ -	\$ -	-	-	-
O&M labour	project	0	\$ -	\$ -	-	-	-
Travel and accommodation	p-trip	1	\$ -	\$ -	-	-	-
Other	Cost	0	\$ -	\$ -	-	-	-
Contingencies	%	0%	\$ 150,883	\$ -	-	-	-
Sub-total :				\$ -	0.0%		
Fuel/Electricity	kWh	1,156	\$ 0.1305	\$ 151	100.0%	-	-
Annual Costs - Total				\$ 151	100.0%		

Periodic Costs (Credits)	Period	Unit Cost	Amount	Interval Range	Unit Cost Range
Damper motor	5 yr	\$ 500	\$ (500)	-	-
		\$ -	\$ -	-	-
		\$ -	\$ -	-	-
End of project life	-	\$ -	\$ -	-	-

Go to GHG Analysis sheet

(Adjusted) Secondary Sales

Annual Energy Balance					
Project name	Whitehorse General Hospital		Electricity required	MWh	1.2
Project location	Whitehorse				
Renewable energy delivered	MWh	80.4	GHG analysis sheet used?	yes/no	Yes
			Net GHG emission reduction	t _{CO2} /yr	0
			Net GHG emission reduction - 25 yrs	t _{CO2}	0
Heating fuel displaced	-	Electricity			

Financial Parameters					
Avoided cost of heating energy	\$/kWh	<input type="text" value="0.043"/>	Debt ratio	%	<input type="text" value="0.0%"/>
GHG emission reduction credit	\$/t _{CO2}	<input type="text" value="-"/>	Income tax analysis?	yes/no	<input type="text" value="No"/>
Retail price of electricity	\$/kWh	0.131			
Energy cost escalation rate	%	<input type="text" value="5.0%"/>			
Inflation	%	<input type="text" value="3.0%"/>			
Discount rate	%	<input type="text" value="4.5%"/>			
Project life	yr	<input type="text" value="25"/>			

Project Costs and Savings				
Initial Costs			Annual Costs and Debt	
Feasibility study	0.0%	\$ -	O&M	\$ -
Development	0.0%	\$ -	Fuel/Electricity	\$ 151
Engineering	0.0%	\$ -		
RE equipment	90.9%	\$ 150,883	Annual Costs - Total	\$ 151
Balance of equipment	0.0%	\$ -		
Miscellaneous	9.1%	\$ 15,088	Annual Savings or Income	
Initial Costs - Total	100.0%	\$ 165,972	Heating energy savings/income	\$ 3,464
Incentives/Grants		\$ <input type="text" value="66,388"/>	Annual Savings - Total	\$ 3,464
Periodic Costs (Credits)			Schedule yr # 5,10,15,20,25	
Damper motor		\$ (500)		
		\$ -		
		\$ -		
End of project life -		\$ -		

Financial Feasibility					
Pre-tax IRR and ROI	%	3.7%	Calculate GHG reduction cost?	yes/no	<input type="text" value="No"/>
After-tax IRR and ROI	%	3.7%			
Simple Payback	yr	30.1	Project equity	\$	165,972
Year-to-positive cash flow	yr	18.0			
Net Present Value - NPV	\$	(9,387)			
Annual Life Cycle Savings	\$	(633)			
Profitability Index - PI	-	(0.06)			

Yearly Cash Flows			
Year	Pre-tax	After-tax	Cumulative
#	\$	\$	\$
0	(99,584)	(99,584)	(99,584)
1	3,478	3,478	(96,105)
2	3,652	3,652	(92,453)
3	3,835	3,835	(88,618)
4	4,027	4,027	(84,591)
5	4,808	4,808	(79,784)
6	4,439	4,439	(75,344)
7	4,661	4,661	(70,683)
8	4,894	4,894	(65,788)
9	5,139	5,139	(60,649)
10	6,068	6,068	(54,581)
11	5,666	5,666	(48,915)
12	5,949	5,949	(42,966)
13	6,247	6,247	(36,719)
14	6,559	6,559	(30,160)
15	7,666	7,666	(22,494)
16	7,231	7,231	(15,263)
17	7,593	7,593	(7,670)
18	7,973	7,973	302
19	8,371	8,371	8,674
20	9,693	9,693	18,366
21	9,229	9,229	27,596
22	9,691	9,691	37,286
23	10,175	10,175	47,461
24	10,684	10,684	58,145
25	12,265	12,265	70,410

(Adjusted) Secondary Sales

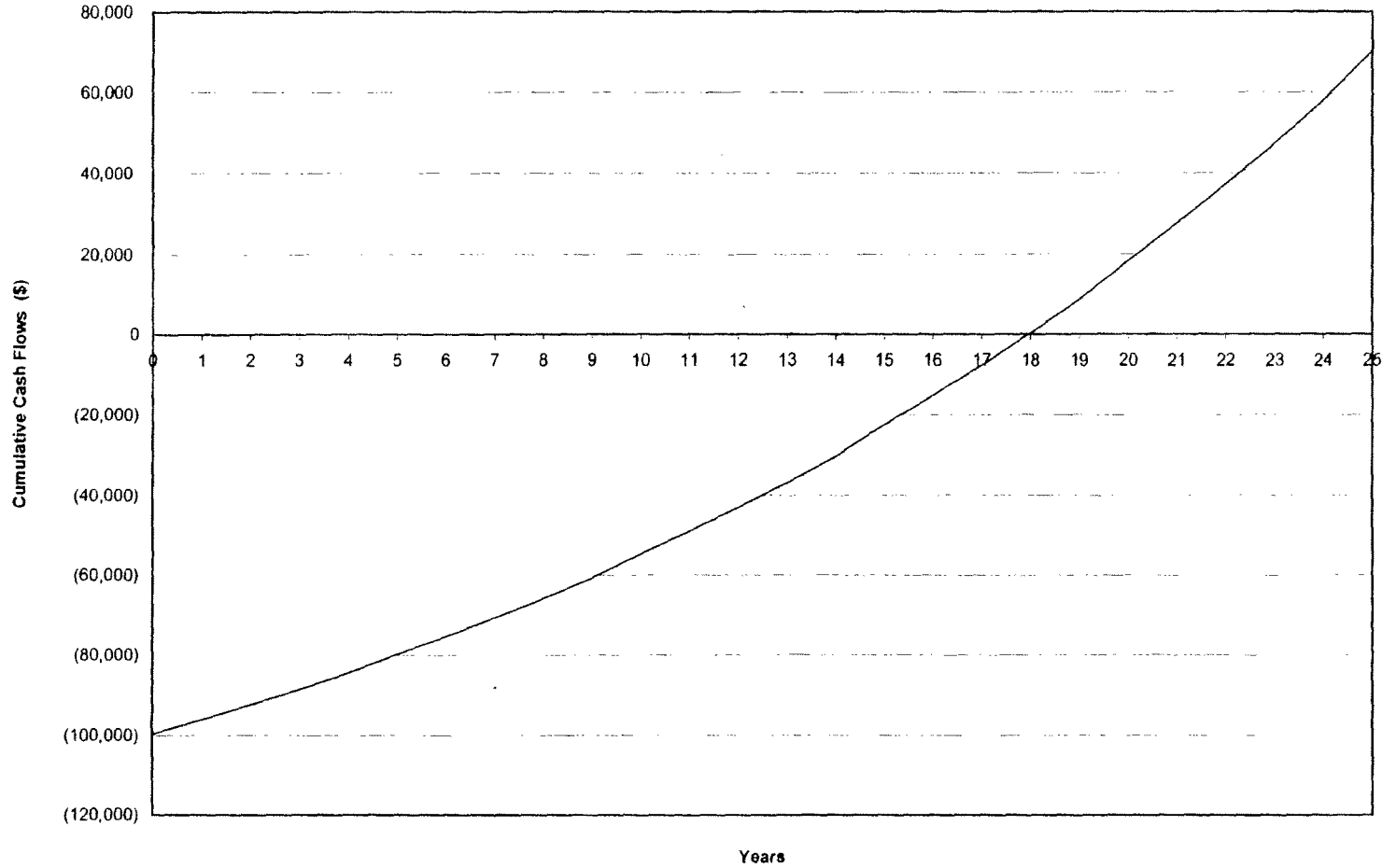
Cumulative Cash Flows Graph

SAH Project Cumulative Cash Flows Whitehorse General Hospital, Whitehorse

Year-to-positive cash flow 18 yr

IRR and ROI 3.7%

Net Present Value \$ (9,387)



RETScreen® Financial Summary - Solar Air Heating Project (DOE Database) Fuel Oil

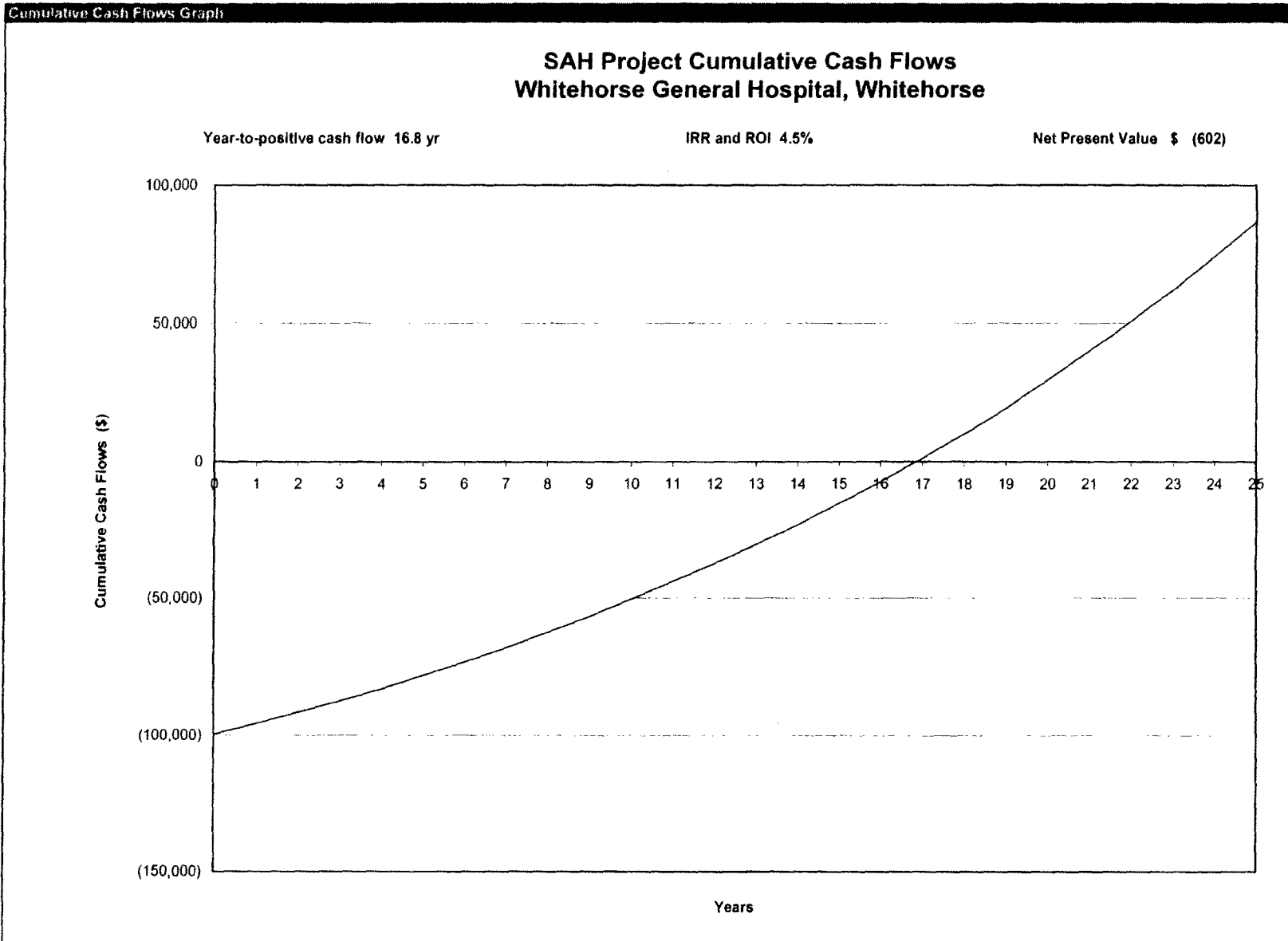
Annual Energy Balance					
Project name	Whitehorse General Hospital		Electricity required	MWh	2.2
Project location	Whitehorse				
Renewable energy delivered	MWh	72.7	GHG analysis sheet used?	yes/no	Yes
			Net GHG emission reduction	t _{CO2} /yr	24
			Net GHG emission reduction - 25 yrs	t _{CO2}	611
Heating fuel displaced	-	Diesel (#2 oil)			

Financial Parameters					
Avoided cost of heating energy	\$/L	<input type="text" value="0.450"/>	Debt ratio	%	<input type="text" value="0.0%"/>
GHG emission reduction credit	\$/t _{CO2}	<input type="text" value="-"/>	Income tax analysis?	yes/no	<input type="text" value="No"/>
Retail price of electricity	\$/kWh	0.054			
Energy cost escalation rate	%	<input type="text" value="5.0%"/>			
Inflation	%	<input type="text" value="3.0%"/>			
Discount rate	%	<input type="text" value="4.5%"/>			
Project life	yr	<input type="text" value="25"/>			

Project Costs and Savings					
Initial Costs			Annual Costs and Debt		
Feasibility study	0.0%	\$ -	O&M	\$	-
Development	0.0%	\$ -	Fuel/Electricity	\$	117
Engineering	0.0%	\$ -			
RE equipment	90.9%	\$ 150,883	Annual Costs - Total	\$	117
Balance of equipment	0.0%	\$ -			
Miscellaneous	9.1%	\$ 15,088	Annual Savings or Income		
Initial Costs - Total	100.0%	\$ 165,972	Heating energy savings/income	\$	3,806
Incentives/Grants		\$ <input type="text" value="66,388"/>			
			Annual Savings - Total	\$	3,806
Periodic Costs (Credits)			Schedule yr # 5,10,15,20,25		
Damper Motor		\$ (200)			
		\$ -			
		\$ -			
End of project life -		\$ -			

Financial Feasibility					
Pre-tax IRR and ROI	%	4.5%	Calculate GHG reduction cost?	yes/no	<input type="text" value="No"/>
After-tax IRR and ROI	%	4.5%			
Simple Payback	yr	27.0	Project equity	\$	165,972
Year-to-positive cash flow	yr	16.8			
Net Present Value - NPV	\$	(602)			
Annual Life Cycle Savings	\$	(41)			
Profitability Index - PI	-	(0.00)			

Yearly Cash Flows			
Year #	Pre-tax \$	After-tax \$	Cumulative \$
0	(99,584)	(99,584)	(99,584)
1	3,873	3,873	(95,711)
2	4,067	4,067	(91,644)
3	4,270	4,270	(87,374)
4	4,483	4,483	(82,891)
5	4,939	4,939	(77,952)
6	4,943	4,943	(73,009)
7	5,190	5,190	(67,819)
8	5,450	5,450	(62,369)
9	5,722	5,722	(56,647)
10	6,277	6,277	(50,370)
11	6,308	6,308	(44,062)
12	6,624	6,624	(37,438)
13	6,955	6,955	(30,483)
14	7,303	7,303	(23,180)
15	7,980	7,980	(15,200)
16	8,051	8,051	(7,149)
17	8,454	8,454	1,305
18	8,877	8,877	10,182
19	9,321	9,321	19,502
20	10,148	10,148	29,650
21	10,276	10,276	39,926
22	10,790	10,790	50,715
23	11,329	11,329	62,045
24	11,896	11,896	73,940
25	12,909	12,909	86,849



RETScreen® Financial Summary - Solar Air Heating Project (DOE Database) Secondary Sales

Annual Energy Balance				
Project name	Whitehorse General Hospital	Electricity required	MWh	2.2
Project location	Whitehorse			
Renewable energy delivered	MWh	72.7	GHG analysis sheet used?	yes/no Yes
			Net GHG emission reduction	t _{co2} /yr 0
			Net GHG emission reduction - 25 yrs	t _{co2} 0
Heating fuel displaced	-	Electricity		

Financial Parameters				
Avoided cost of heating energy	\$/kWh	0.043	Debt ratio	% 0.0%
GHG emission reduction credit	\$/t _{co2}	-	Income tax analysis?	yes/no No
Retail price of electricity	\$/kWh	0.054	<i>(note elect costs adjusted to reflect ROE total cost of elect)</i>	
Energy cost escalation rate	%	5.0%		
Inflation	%	3.0%		
Discount rate	%	4.5%		
Project life	yr	25		

Project Costs and Savings				
Initial Costs			Annual Costs and Debt	
Feasibility study	0.0%	\$ -	O&M	\$ -
Development	0.0%	\$ -	Fuel/Electricity	\$ 117
Engineering	0.0%	\$ -		
RE equipment	90.9%	\$ 150,883	Annual Costs - Total	\$ 117
Balance of equipment	0.0%	\$ -		
Miscellaneous	9.1%	\$ 15,088	Annual Savings or Income	
Initial Costs - Total	100.0%	\$ 165,972	Heating energy savings/income	\$ 3,125
Incentives/Grants	\$	66,388	Annual Savings - Total	\$ 3,125
Periodic Costs (Credits)			Schedule yr #	5, 10, 15, 20, 25
Damper Motor	\$	(200)		
	\$	-		
	\$	-		
End of project life -	\$	-		

Financial Feasibility				
Pre-tax IRR and ROI	%	2.9%	Calculate GHG reduction cost?	yes/no No
After-tax IRR and ROI	%	2.9%		
Simple Payback	yr	33.1	Project equity	\$ 165,972
Year-to-positive cash flow	yr	19.3		
Net Present Value - NPV	\$	(18,732)		
Annual Life Cycle Savings	\$	(1,263)		
Profitability Index - PI	-	(0.11)		

Yearly Cash Flows			
Year #	Pre-tax \$	After-tax \$	Cumulative \$
0	(99,584)	(99,584)	(99,584)
1	3,158	3,158	(96,426)
2	3,316	3,316	(93,110)
3	3,481	3,481	(89,629)
4	3,655	3,655	(85,974)
5	4,070	4,070	(81,904)
6	4,030	4,030	(77,874)
7	4,232	4,232	(73,642)
8	4,443	4,443	(69,199)
9	4,665	4,665	(64,534)
10	5,167	5,167	(59,367)
11	5,143	5,143	(54,223)
12	5,401	5,401	(48,823)
13	5,671	5,671	(43,152)
14	5,954	5,954	(37,198)
15	6,563	6,563	(30,634)
16	6,564	6,564	(24,070)
17	6,893	6,893	(17,177)
18	7,237	7,237	(9,940)
19	7,599	7,599	(2,341)
20	8,340	8,340	6,000
21	8,378	8,378	14,378
22	8,797	8,797	23,175
23	9,237	9,237	32,412
24	9,699	9,699	42,111
25	10,602	10,602	52,713

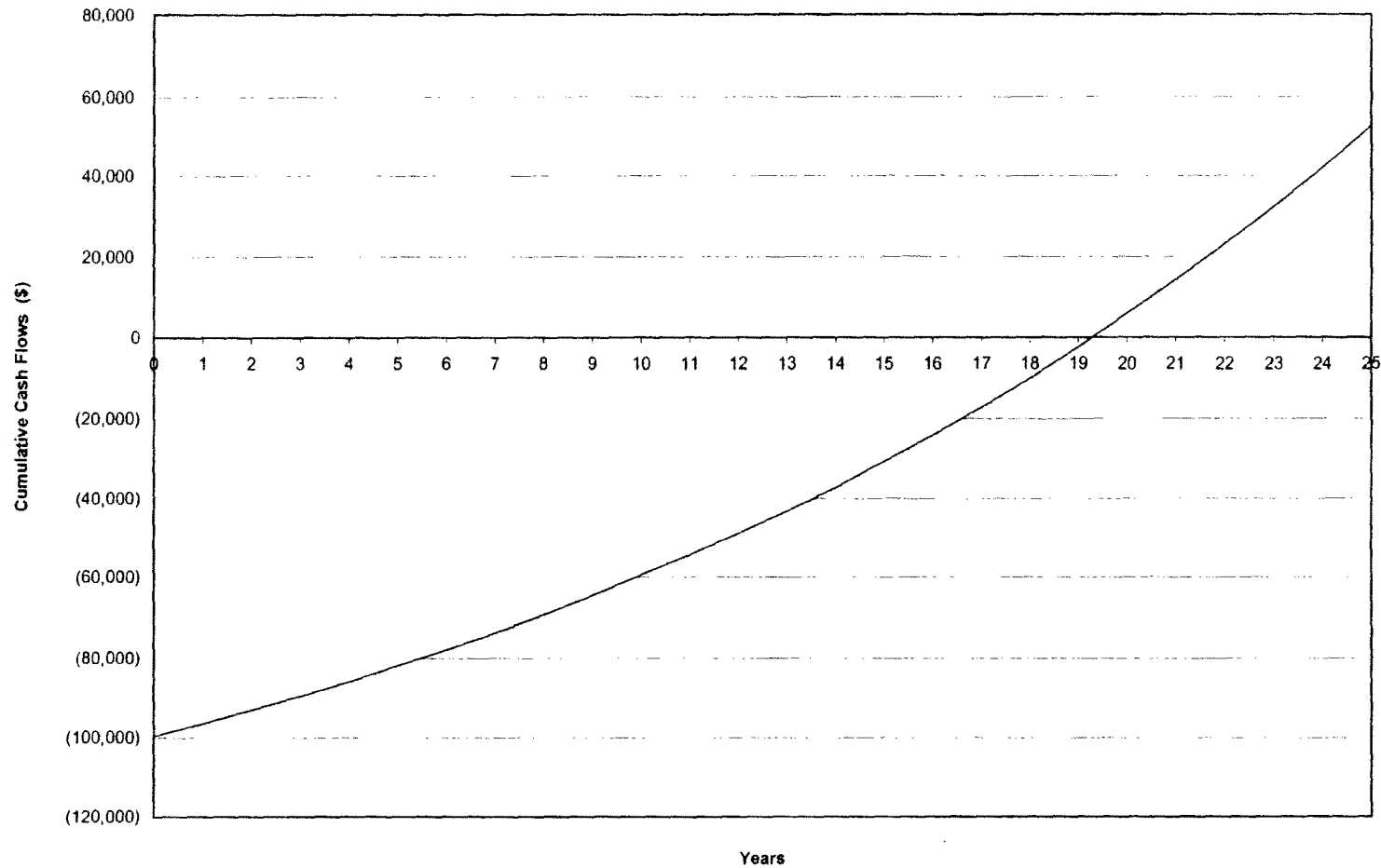
Cumulative Cash Flows Graph

SAH Project Cumulative Cash Flows Whitehorse General Hospital, Whitehorse

Year-to-positive cash flow 19.3 yr

IRR and ROI 2.9%

Net Present Value \$ (18,732)



SWIFT ENERGY SAVINGS ANALYSIS

PROJECT INFORMATION

CLIENT		DEALER / SIMULATOR	
Name:	ESC-Whitehorse General Hospital	Name:	
Job:	2002-4110.22	Address:	
Address:	Whitehorse, YT Canada,	Telephone:	
Telephone:		Fax:	
Fax:		E-mail:	
E-mail:		Website:	
Contact:			

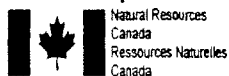
ANNUAL RESULTS

System	Size (m ²)	Energy Savings (GJ)	Fuel Savings	Cost Savings (\$)
Wall 1	248.20	450.0	14478.8 Oil (1)	6515.48
Total	248.20	450.0		6515.48

FINANCIAL RESULTS

COSTS		BENEFITS/PAYBACK	
Capital Costs	\$	165971	Simple Payback (yrs) 15.3
Grant / Subsidy	\$	66389	Internal Rate of Return (%/yr) 7.3
Capital Cost Credits	\$	0	Life Cycle Savings (\$) 36128
Net Cost	\$	99583	Reduced CO2 Emissions (tonnes/yr) 41.2

SWift was produced by:



SWIFT ENERGY SAVINGS ANALYSIS

PROJECT INFORMATION

CLIENT	DEALER / SIMULATOR
Name: ESC-Whitehorse General Hospital	Name:
Job: 2002-4110.22	Address:
Address: Whitehorse, YT Canada,	Telephone:
Telephone:	Fax:
Fax:	E-mail:
E-mail:	Website:
Contact:	

ANNUAL RESULTS

System	Size (m ²)	Energy Savings (GJ)	Fuel Savings	Cost Savings (\$)
Wall 1	248.20	450.0	125000.8 Elec. (kWh)	5375.04
Total	248.20	450.0		5375.04

FINANCIAL RESULTS

COSTS		BENEFITS/PAYBACK	
Capital Costs	\$ 165971	Simple Payback (yrs)	18.5
Grant / Subsidy	\$ 66389	Internal Rate of Return (%/yr)	5.5
Capital Cost Credits	\$ 0	Life Cycle Savings (\$)	12374
Net Cost	\$ 99583	Reduced CO2 Emissions (tonnes/yr)	0.0

SWift was produced by:

