Alexco Keno Hill Mining Corp.
Bellekeno Mine Operations

Groundwater Monitoring Plan

Water Use Licence QZ09-092

February 2011

Prepared by:

TABLE OF CONTENTS

1.0 INTRODUCTION....1
1.1 Purpose of Plan....1
2.0 MINE LOCATION AND DESCRIPTION....2
3.0 PREVIOUS GROUNDWATER STUDIES....4
4.0 REGIONAL GEOLOGY AND HYDROGEOLGICAL IMPLICATIONS....5
5.0 FLAME AND MOTH SITE GROUNDWATER MONITORING....7
5.1 Shallow Subsurface Conditions in the Flame and Moth Area....9
5.2 Bedrock Geology and Structure in the Flame and Moth Area....10
6.0 BELLEKENO NON-AML WASTE ROCK DISPOSAL AREA GROUNDWATER MONITORING....13
7.0 KENO CITY GROUNDWATER MONITORING....17
8.0 REVIEW OF RESULTS....19
9.0 GROUNDWATER MONITORING SCHEDULE....19
10.0 REPORTING....20
11.0 REFERENCES....20

LIST OF FIGURES

Figure 1 Flame and Moth Groundwater Monitoring Plan Site Map....3
Figure 2 Conceptual WRDA Groundwater Monitoring Well Locations....16
Figure 3 Keno City Groundwater Monitoring Wells....18

LIST OF TABLES

Table 1 Flame and Moth Site Groundwater Monitoring Well Summary....8
Table 2 General Subsurface Conditions for Gravel Area....10
Table 3 Borehole Depths at Bellekeno Site....14
Table 4 Bellekeno WRDA Groundwater Monitoring Well Summary....15
Table 5 Groundwater Monitoring Schedule....19

APPENDICES

Appendix A SRK Report 2010 Bellekeno Groundwater Program
Appendix B 2010 Flame and Moth Diamond Drill Logs
Appendix C Flame and Moth Site Geotechnical Borehole Logs

1.0 INTRODUCTION

1.1 *Purpose of Plan*

This plan is submitted to fulfill the conditions set out in Part H, Clauses 85, 86, and 87 of Water Licence QZ09-092 (hereafter referred to as the Licence) issued to Alexco Keno Hill Mining Corp (Alexco) on August 19th 2010:

85. Within six months of the effective date of this licence, the Licensee shall submit to the Board a Bellekeno Groundwater Monitoring Plan for both the Bellekeno Waste Rock Disposal Area and Flame and Moth Site and shall implement that plan.

86. The plan for the Waste Rock Disposal Area shall include the installation of at least four groundwater monitoring wells.

87. For the Flame and Moth Site, the plan shall be developed by considering existing knowledge of geological structures at the site and the consideration of groundwater table mapping based on sampling of KV -84, KV -85, KV -86, and KV -87. The developed plan shall include, but not necessarily be limited to the following:

a) Installing at least three multi-level groundwater monitoring wells down gradient of DSTF;

b) Where wells are installed into bedrock, the bedrock shall be cored'

c) Developing detailed geological logs for all new well installations including: identification of soil or rock types; soil condition or rock quality; and geological and hydrogeological features such as joints and fractures. The logs are also to include details of the well installations;

c) Based on baseline groundwater quality, development of trigger levels that would be used to enact the adaptive management strategy and provide early warning of the need for mitigative measures and/or changes in facility design/operations

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In addition, Part F Clauses 45 and 46 of the Licence provided additional guidance on the groundwater monitoring program:

45. Monitoring results should be reviewed after each sampling event to identify groundwater changes, should they occur.

46. Groundwater wells determined to be subject to seasonal freezing shall have pressure transducers installed when cleared of seasonal ice.

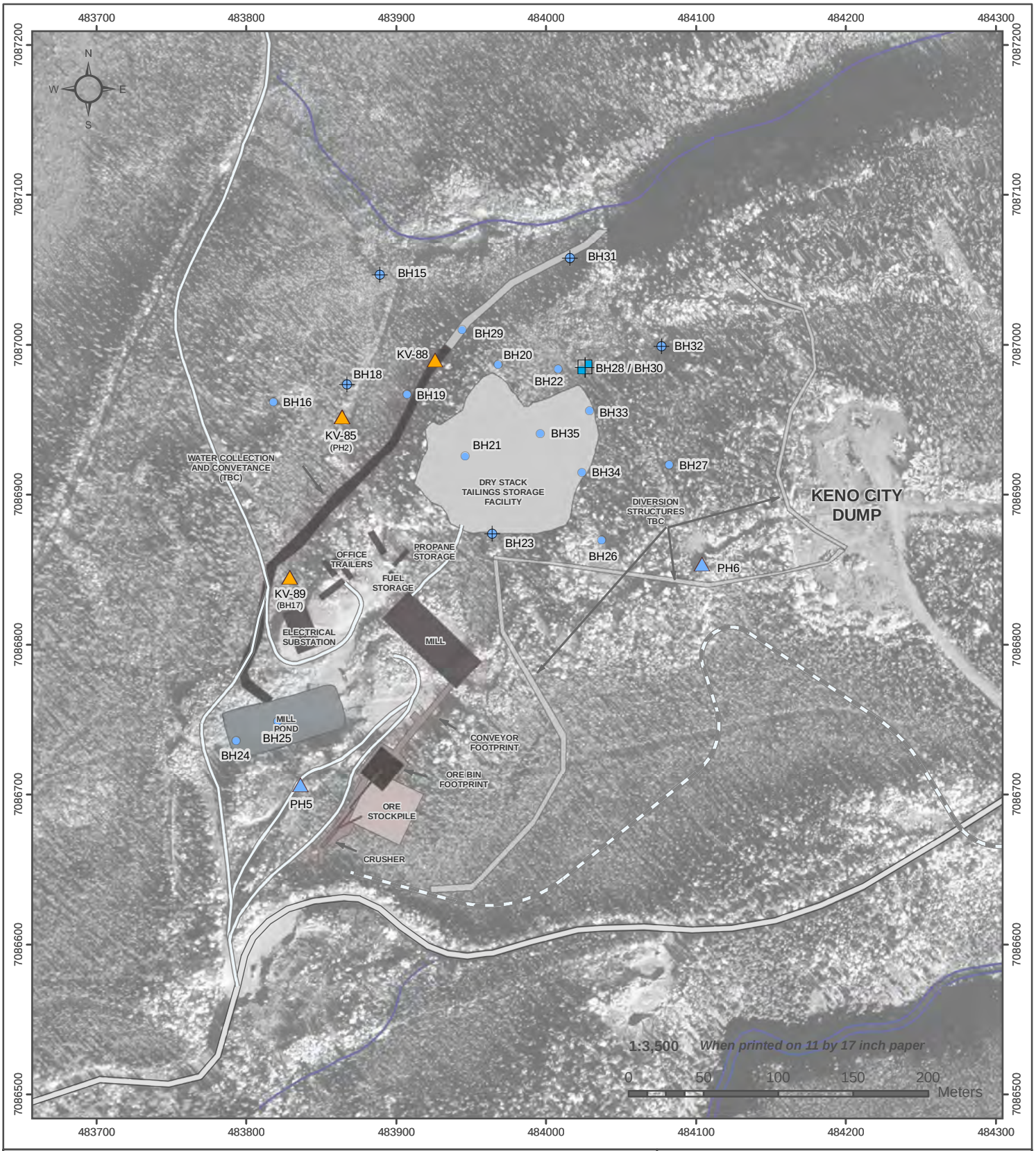
This plan outlines the groundwater monitoring strategy that will be used during mining operations at the Bellekeno Mine and Mill on Alexco's Keno Hill property.

2.0 MINE LOCATION AND DESCRIPTION

The Keno Hill Silver District is located in central Yukon Territory, 354 km (by air) due north of Whitehorse. The Bellekeno mine area is located approximately 3 km east of Keno City within the Keno Hill Silver District. The mill site and Dry Stack Tailings Facility (hereinafter referred to as the "DSTF") are located approximately 1 km west of Keno City.

The portal at Bellekeno East is located on a steep slope above Thunder Gulch, a narrow tributary of Lightning Creek, and the haul road access to the mill site is provided by an approximately 3 km access road which crosses Lightning Creek approximately 2200 meters downstream from the confluence of Thunder Gulch and Lightning Creek. Please refer to see Figure 1 for the site map.

The proposed Waste Rock Disposal Area (hereafter referred to as the WRDA) will be constructed as a wrap around dump and located along the northeast flank of Sourdough Hill, as shown on Figure 3.



- Monitoring Well
- Monitoring Well and Ground Temperature
- Proposed Monitoring Well
- Ground Temperature
- Slope Indicator
- Bore Hole
- Mill Access Road
- Haul Road
- Duncan Creek Road
- Major Contour (5 meter interval)
- Minor Contour (1 meter interval)

QZ09-092 GROUNDWATER MONITORING PLAN

FIGURE 1 - MILL SITE AREA BOREHOLE AND GROUNDWATER MONITORING LOCATIONS

AKHM ACCESS

Aerial photography flight date: July 13th 2006. Ortho-rectification produced by Challenger Geomatics Ltd. Site hydrography and contours derived from 2006 aerial imagery. Mill pond survey (Y.E.S. Sept 2010), mill structures, current DSTF footprint and roads survey (ACG, December 2011). Design data obtained from EBA.

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3.0 PREVIOUS GROUNDWATER STUDIES

SRK Consulting Canada Inc. (SRK) was retained by Alexco to investigate groundwater gradients in the vicinity of the mill site in relation to Keno City and Lightning Creek. Three groundwater monitoring wells were installed for this program (PH2, PH5 and PH6). These wells will be referred to in this plan according to their KV station numbers as listed in Schedule A of the Licence, KV-85, KV-86 and KV-87, respectively. Key findings of the SRK groundwater investigation (SRK, 2010) include:

- The water table within the bedrock aquifer under the site and within a relatively thick overburden aquifer to the south is at considerable depth (>25 m);
- Water level data from monitoring wells at site and Keno City indicate that groundwater flows from east to west, or from Keno City towards the mill site and Christal Lake;
- These water level data also indicate a shallow gradient between Lightning Creek towards Christal Lake;
- Water quality analyses of samples taken immediately following monitoring well development indicate that in general, concentrations of dissolved anions and metal are low;
- The only notable exceptions are elevated levels concentrations of chloride and sodium in KV-87, which is located downgradient and could be indicative of seepage from the Keno City dump and; elevated concentrations of sulphate in KV-86 and KV-87, which are deemed to be indicative of natural mineralization in this area;
- The likelihood of effects to groundwater quality in general related to the mill and DSTF are considered very low, due to site water management plans for seepage and runoff interception, and collection and treatment if necessary;
- Because groundwater extraction is not planned at the mill site, there will be no effects on the amount of water available for extraction from wells in Keno City, and;
- The chance of water quality being affected in wells in Keno City is considered insignificant due to current understanding of the local groundwater gradient and the large distance between the mill site and Keno City water wells.

The SRK groundwater report, entitled “Bellekeno Groundwater Program” was issued in May 2010, and was submitted to the Board as supplemental information in support of the application for QZ09-092 (Exhibit 1.12 of the public registry). This report is included as Appendix A. Prior to issuance of their 2010 Bellekeno Groundwater report, SRK was also retained to complete initial (desktop) assessments of potential impacts of the proposed mill and DSTF site on groundwater quantity and quality (SRK, 2009a; SRK, 2009b).

4.0 REGIONAL GEOLOGY AND HYDROGEOLGICAL IMPLICATIONS

Because of a long history of mine and exploration in the Keno Hill Silver District, regional geology is well studied. Although no comprehensive studies specific to groundwater have been completed in the district, a number of observations can be made relating to bedrock and surficial geology and their hydrogeological characteristics. Some background information pertinent to district geology and groundwater, are summarized below from the Environmental Conditions Report (ACG, 2009).

> The Keno Hill District is underlain primarily by Yukon Group metasedimentary rocks, locally divided into three formations; Upper Schist, Central Quartzite and Lower Schist. The Upper Schist (Hyland Group, pre-Cambrian to Cambrian age) overlies the quartzite in what is inferred to be a thrust contact (Robert Service Thrust) and consists of quartz-mica schist, quartzite, graphitic schist and minor limestone. The Central Quartzite (Keno Hill Quartzite, Mississippian age) contains thick-and thin-bedded quartzite, massive quartzite, graphitic phyllite, graphitic schist, calcareous schist and minor Triassic greenstone. This unit is approximately 700 m thick and is host to most of the past producing ore bodies. Structurally juxtaposed below the quartzite is the Lower Schist which has been correlated with the Devonian-Mississippian Earn Group. The Lower Schist includes graphitic schist, argillite, thin-bedded quartzite, calcareous schist, phyllite, slate, sericite schist, minor thick-bedded quartzite and locally significant intervals of Triassic greenstone. The greenstone forms sills and / or boudins and consists of metadiorite and metagabbro. The sills and boudins form bodies up to one kilometre long and thirty metres thick. Regional, greenschist facies metamorphism of all units is believed to have occurred in the Middle Cretaceous, about 105 million years ago.
>
> A number of quartz-feldspar porphyritic sills have intruded the stratigraphy parallel to schistosity. The sills are most common in the Lower and Upper Schists and can reach thicknesses of up to fifty metres; reports of occurrences in the Central Quartzite are inconclusive and vague. The quartz-porphyry sills are believed to be of Cretaceous age.

> Structurally, the property is characterized by four sets of faults; many of which have been filled by hydrothermal minerals, forming veins. The oldest fault set consists of south dipping structures that are generally parallel to foliation and are apparently associated with the Tombstone Thrust Fault since movement was contemporaneous or slightly later. Locally, brittle deformation has been observed along these structures. A second fault set, known as "longitudinal veins" strikes north east to east northeast and dips steeply southeast. The latest movement along these faults is sinistral with offsets locally reaching more than 150 metres; however, more than one episode of movement commonly is indicated. Depending on the competency of the host rock, longitudinal veins can be up to thirty metres wide in an anastomosing system of sub-veins. Essentially all mineralized rock was mined from these longitudinal veins. A third set of faults, known as "transverse faults", is north-west striking and dips steeply to the north. Transverse faults typically do not contain silver and lead mineralization but are commonly filled by quartz with trace to minor arsenopyrite, pyrite and jamesonite.
>
> A younger set of faults, known as cross faults, strike north to north west with a dip of sixty degrees west to south west and offset vein or longitudinal faults by up to 2,000 metres. In the western part of the property, dextral movement is the most recent event along these structures, whereas in the eastern part of the property sinistral movement with less magnitude prevails."

SRK (2009a) further described summarized the bedrock geology of the site as it relates to hydrogeological characteristics:

> "The bedrock geology of the area around Keno consists predominantly of layered metasedimentary rocks consisting mainly of quartzite, schist and phyllite. Unlike high yielding aquifer rocks such as sandstone, where groundwater can flow through connected 'pores' in the rock mass, the metasediments typically found in the Keno Hill district have a very low permeability, with little or no space between rock grains due to the metamorphosed character. The main medium through which water travels in these metasedimentary rocks therefore is via fractures and joints within the rock. The permeability of the rock (or the ease at which groundwater can flow through the rock formation) in this case is dependent on how many fractures are within the rock, and how well they are connected to each other, *and* how well connected to a water source (such as rainfall, a lake or a river) these fractures are."

SRK (2009a) also describes surficial sediments and their hydrology:

> "Shallow surficial sediments are found locally and typically are present in topographic lows which control surface drainage patterns. These overburden deposits have limited thickness and lateral extent, and likely form only small

> local aquifers. It is generally recognised that metasedimentary rocks do not commonly form high yielding aquifers. Fractures are not typically
> well connected and the resulting permeability is low. Evidence for this around Keno City can be seen in the characteristic marshy conditions seen in the area. The surface water found within these marshy areas is unable to drain easily down through the underlying rocks. The regional groundwater flowpaths can be generally described as mimicking surface water pathways."

It is further recognized in that the presence of complex glacial and glaciofluvial sediments present in the valley bottoms and along the margins of the hills produces complex overburden stratigraphy. Overburden thickness and composition are known to vary widely, which can result in complex hydrology (e.g. perched aquifers) and generally poor drainage and low permeability. Also, the ubiquitous presence of permafrost and, in some areas, massive ground ice further complicate near surface groundwater regimes. In general, surficial sediment drainage can be described as generally poor, and complex, while bedrock hydrogeology can be described as generally low permeability with groundwater flow controlled by fractures and joints.

5.0 FLAME AND MOTH SITE GROUNDWATER MONITORING

As per Clause 87a of the Licence, three multi-level groundwater monitoring wells are to be installed down gradient of the DSTF. Clause 87 specifies that three multi-level groundwater monitoring wells (e.g. Westbay type) are to be installed down gradient of the DSTF. However, because to the known challenges in the ground conditions near the DSTF (the presence of permafrost and massive ice, in some cases), Alexco believes that separate boreholes to monitor each potential groundwater zone (shallow overburden, and deep bedrock) are more likely to provide reliable results than complicated multi-level monitoring well systems, which are more likely to fail. The decision to use individual monitoring wells is also based on discussions with professional hydrogeologists experienced in monitoring well installations.

Alexco believes that the intention of Clause 87a was to ensure that three relatively shallow overburden monitoring wells and three deeper, bedrock groundwater monitoring points were installed down gradient of the DSTF to allow for monitoring of both shallow and deep groundwater. Alexco proposes to comply with Clause 87a through use of the following groundwater monitoring network as described below in Table 1 and shown on

Figure 1. The selection of these wells was based on a review of available geotechnical and hydrogeological information for the site and in discussion with EBA Engineering Consultants on the location of ground ice in this area.

Table 1 Flame and Moth Site Groundwater Monitoring Well Summary

Station #	Hole #	Purpose	Total Depth (m)	Depth in Overburden (m)	Depth in Bedrock (m)	Northing[1]	Easting[1]
KV-85	PH2	Deep bedrock groundwater monitoring	27.01	11.5	15.51	7086952	483864
	TBD[2]	Shallow or perched groundwater monitoring	5*	5*	-	TBD[2]	TBD[2]
KV-88	TBD[2]	Deep bedrock groundwater monitoring	35*	5*	30*	TBD[2]	TBD[2]
	TBD[2]	Shallow or perched groundwater monitoring	5*	5*	-		
KV-89	TBD[2]	Deep bedrock groundwater monitoring	35*	14.5*	20.5*	7086845	483829
	BH17	Shallow or perched groundwater monitoring	14.5	14.5	-		

[1]Coordinates are UTM Zone 8 NAD 1983
[2]TBD – "to be determined", station not established at this time.
*Estimated based on nearby wells or boreholes

PH2 and BH17 are monitoring wells already in place down gradient of the DSTF, and are proposed serve as one of the deep, and shallow groundwater monitoring locations.

In accordance with Clause 87c of the Licence, all new well installations will include collection of information on soil and rock types, soil condition or rock quality and geological and hydrogeological features such as joints or fractures where possible, and will include details of well installations.

Clause 46 of the Licence, states that all groundwater wells determined to be subject to seasonal freezing shall have pressure transducers installed. AHKM will install vibrating wire pressure transducers in groundwater wells deemed to be subject to seasonal freezing and these installations will be measured monthly for the first year (twelve monthly readings) as per Clause 44e and then quarterly for water level as per Schedule B Table 4.

Although Clause 87b, requires that where wells are installed into bedrock, the bedrock shall be cored, Alexco's preference is to complete these groundwater well installations (including bedrock holes) using more conventional drilling technology for the installation of monitoring wells (air-rotary, ODEX) for the following reasons:

- Air-rotary drilling is preferable to diamond drilling for monitoring well installation for a number of reasons including:
    1. More efficient drilling of both overburden and bedrock;
    2. Larger diameter borehole produced using an air-rotary drilling rig is preferable and reduces the chance of bridging during well completion;
- Alexco does not currently have a diamond drill program active at site, and;
- An air-rotary drilling rig will be on site in late February for other groundwater investigations related to District Closure, costs can be optimized if combined with this program.

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The Reasons for Decision document for the Licence does not provide additional information regarding Clause 87b; however, Alexco believes that the intent of this Clause was to ensure that adequate data and information regarding the subsurface conditions (overburden and especially bedrock and structural geology) of the DSTF and mill site area were collected to better inform Alexco's mill site area construction plans and ensure that the monitoring strategy was appropriate. Alexco believes that information collected in both the shallow subsurface soils and the deeper bedrock is sufficient to inform the groundwater monitoring plan. These data are presented in Sections 5.1 and 5.2 below.

5.1 Shallow Subsurface Conditions in the Flame and Moth Area

A considerable amount of geotechnical information has been collected from the mill site and the area beneath the DSTF during geotechnical studies in support of preliminary and final design of the DSTF, mill building, mill site pond, ancillary facilities, and site water management infrastructure. This work was carried out by EBA Engineering Consultants Ltd. A summary of the subsurface conditions of the DSTF, from the Preliminary Design Report (EBA, 2010):

> "Nine boreholes were drilled near the DSTF. Information gathered in these boreholes indicates two general soil profiles in the area:
>
> - glaciofluvial GRAVEL underlain by bedrock and
> - SILT and SAND till underlain by gravel and bedrock."

"The gravel was encountered along the ridge that crosses the site. The gravel in the area of the DSTF was found in both frozen and unfrozen states. It is typically sandy with trace silt, compact, medium grained, well graded, and brown, and it is underlain by a thin layer of silt and sand till and then bedrock. Bedrock encountered in testholes is a competent quartzite. Subsurface conditions for the gravel area are summarized in Table 2.

Table 2 General Subsurface Conditions for Gravel Area

Soil Unit	Min thickness (m)	Max Thickness (m)	Average Thickness (m)
Gravel	1.3	3.7	2.5
Silt and Sand till	0.2	1.3	1.0
Bedrock (quartzite	@2.1 mbgs*	@5.0 mbgs*	@3.4 mbgs*

*Meters below ground surface

All silt and sand till encountered in the area of the DSTF was frozen. The silt and sand till typically contains trace gravel and trace clay, is low to non-plastic, olive grey, is underlain by gravel seams within the till and then by quartzite bedrock. Two boreholes on the west side of the ridge, BH15 and BH17, were drilled through the silt and sand layer. The gravel seams were encountered below 16 m depth in BH15, and bedrock was encountered at 14.2 m depth in BH17. One borehole, BH23, was drilled through the till deposit on the east side of the ridge and gravel seams were encountered at 7.6 m depth. Two boreholes, BH24 and BH25, were drilled near a proposed water collection pond. The general soil conditions in this area are gravel fill over glaciofluvial gravel over silt and sand till over glaciofluvial gravel. The glaciofluvial gravel and silt and sand till are similar to the soils described above and are all unfrozen."

Borehole Logs for drilled in the vicinity of the mill site and DSTF area are attached as Appendix C. Ongoing work and additional drilling provided further information on subsurface conditions over the mill site area. Borehole logs for these additional holes are also included in Appendix C. All of this data was taken into consideration for the placement of the groundwater monitoring wells.

5.2 Bedrock Geology and Structure in the Flame and Moth Area

Exploration drilling in the vicinity of the DSTF by Alexco during the 2010 season has provided additional data from the deeper subsurface in the form of information on rock quality and geological features. This drilling was designed to investigate the historically known mineralisation about the Flame and Moth underground mine workings and comprised 13 holes for a total of 3,974 metres that were completed from five locations.

Basic rock quality designation (RQD) information that is routinely logged for exploration diamond drill core was supplemented with additional data including Rock Strength, Total

Fracture Count, Total Vein Count, Vein Strength and % Vein for some of the Flame and Moth holes.

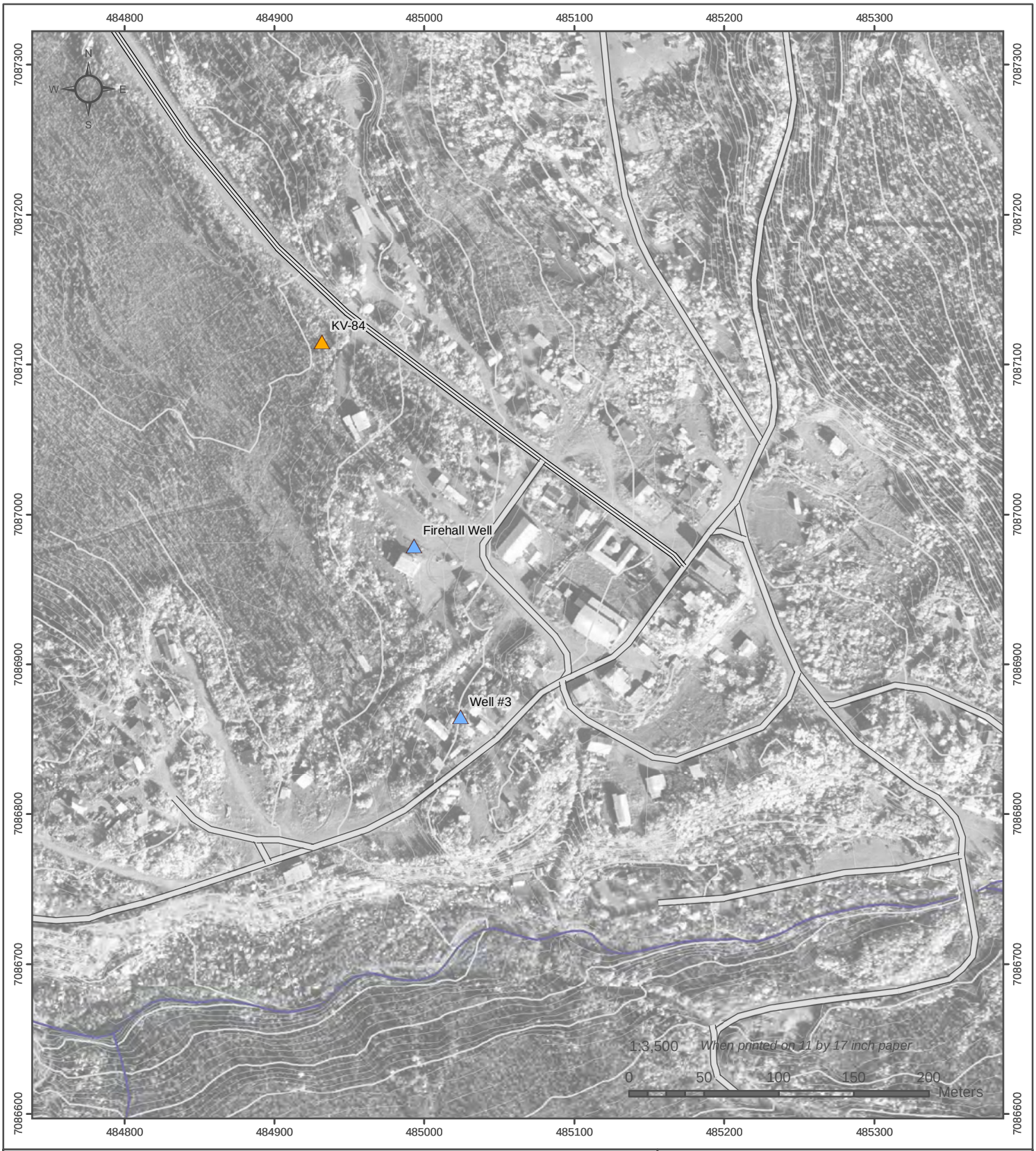
The details of location and orientation of the drill holes are shown in Table 3 while the RQD data, as well as the main rock types intercepted, is included in Appendix B.

Table 3 Details of Diamond Drill Hole at the Flame & Moth Prospect

Hole_ID	Total Depth (m)	UTM Easting (m)	UTM Northing (m)	Elevation (m)	Collar Azimuth	Collar Dip	Started	Completed	Core Size
K-10-0264	336.80	484131.84	7086649.76	927.98	306	-60	05/07/2010	20/07/2010	HQ
K-10-0271	347.47	484131.84	7086649.76	927.98	306	-70	21/07/2010	31/07/2010	HQ
K-10-0275	346.57	484131.54	7086649.51	927.98	328	-62	01/08/2010	24/08/2010	HQ
K-10-0285	324.31	484071.91	7086679.39	919.59	306	-50	25/08/2010	06/09/2010	HQ
K-10-0291	192.67	484101.25	7086870.75	936.78	285	-54	08/09/2010	13/09/2010	HQ
K-10-0295	313.94	484101.35	7086870.5	936.78	285	-80	13/09/2010	03/10/2010	HQ
K-10-0298	220.68	484101.5	7086870.4	936.78	250	-60	03/10/2010	11/10/2010	HQ
K-10-0299	306.32	484067.23	7086584.28	923.86	285	-68	05/10/2010	10/10/2010	HQ
K-10-0303	348.08	484067.96	7086584.23	923.85	285	-75	10/10/2010	19/10/2010	HQ
K-10-0304	252.07	484101.68	7086870.26	936.78	230	-75	11/10/2010	19/10/2010	HQ
K-10-0305	352.35	484076.44	7086582.7	924.14	340	-65	20/10/2010	30/10/2010	HQ
K-10-0312	388.93	484076.65	7086585.25	923.89	250	-55	30/10/2010	16/11/2010	HQ
K-10-0320	243.84	484076.45	7086586.09	923.99	290	-55	19/11/2010	26/11/2010	HQ

The interpreted surface geology of the Flame and Moth area is shown in Figure 2. The area is underlain by the Keno Hill Quartzite. Several distinctive east – west striking map units that dip moderately to the south are identified in this area:

- Upper Quartzite (Msq) - Comprising light to dark grey, platey quartzite with grey schist (phyllite) layers.
- Sericite Schist Marker (Mss) – Sericite +/-chlorite schist, schistose grit, minor light grey crystalline limestone.
- Graphitic Schist Marker (Msg) – Medium to dark grey schist (phyllite), locally calcareous.
- Basal Quartzite (Mkq) – Blocky buff, light to medium grey quartzite, locally calcareous. Thin graphitic schist bands are common.
- Greenstone (Trgn) – Chlorite-actinolite+/-calcite greenstone sills, locally with relict phaneritic texture.



Monitoring Well

Proposed Monitoring Well

Highway

Duncan Creek Road

Major Contour (5 meter interval)

Minor Contour (1 meter interval)

QZ09-092 GROUNDWATER MONITORING PLAN

FIGURE 2 - KENO CITY AREA BOREHOLE AND GROUNDWATER MONITORING LOCATIONS

AKHM

ACCESS CONSULTING GROUP

Aerial photography flight date: July 13th 2006. Ortho-rectification produced by Challenger Geomatics Ltd. Site hydrography and contours derived from 2006 aerial imagery obtained from Geodesy Remote Sensing Inc., Calgary Alberta.
Datum: NAD 83; Projection: UTM Zone 8N

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As the amount of surface outcrop in the area is poor, the distribution of these rock units as shown on the map is somewhat interpretative. There is however evidence of possibly two significant north-east trending fault structures (Moth and Flame Faults) that offset the stratigraphy and that also host mineralised veins.

There is currently no surface geologic evidence for the presence of any later cross-cutting north-west trending faults.

Two diamond drill holes (K-10-0291, K-10-0295) were completed beneath the footprint of the DSTF from a site that was essentially on outcropping Basal Quartzite. These holes were however drilled at an oblique angle to the dominant stratigraphic structure, and this may affected the quality of the RQD information.

In K-10-0291, two zones displayed increased density of fracture development:

- In quartzite between 88.85 – 96.32 m,
- In a faulted quartzite zone associated with minor mineralisation between 129.84 – 157.28 m.

In K-10-0295, much wider zones in the Basal Quartzite display increased density of fracture development associated:

- Between 8.23 – 87.48 m,
- Between 166.73 – end of hole at 313.94 m.

Some of these fracture zones are associated with minor mineralisation, but may also reflect the thin bedded nature of some of the units.

6.0 BELLEKENO NON-AML WASTE ROCK DISPOSAL AREA GROUNDWATER MONITORING

Preliminary engineering design based on 5 boreholes for the Bellekeno Non-Acidic/Metal Leaching Waste Rock Disposal Area (WRDA) was undertaken by EBA Engineering Consultants Ltd. in late 2008 (EBA, 2008). Additional work in support of final design is expected prior to construction. Relevant findings on the subsurface conditions at the proposed WRDA site are excerpted below:

Subsurface Conditions

The subsurface conditions at the site were determined through interpretation of data from the five boreholes advanced by EBA on October 30, 2008. The subsurface conditions consist of sand that is gravely and silty. Bedrock was not encountered in any of the boreholes. The drill lost circulation in the boreholes and prevented the return of cuttings to the surface. A summary of the boreholes and their respective depths is shown in Table [3].

Table 4 Borehole Depths at Bellekeno Site

Borehole Number	Termination Depth (m)
W14101178-BH11(1)	9.0
W14101178-BH12	18.0
W14101178-BH13	12.0
W14101178-BH14	6.0
W14101178-BH15	10.0

(1) Ground Temperature Cable installed to 8.0 m

Groundwater

Groundwater was not encountered in any of the boreholes at the Bellekeno site.

Permafrost

The moisture content testing completed on the samples collected indicates elevated moisture contents attributed to either the presence of permafrost or increased silt contents of the soils. A ground temperature cable was installed in W14101178-BH11 to 8.0 m. Preliminary readings taken from the ground temperature cable indicate the presence of warm permafrost (-1 to -0.5°C).

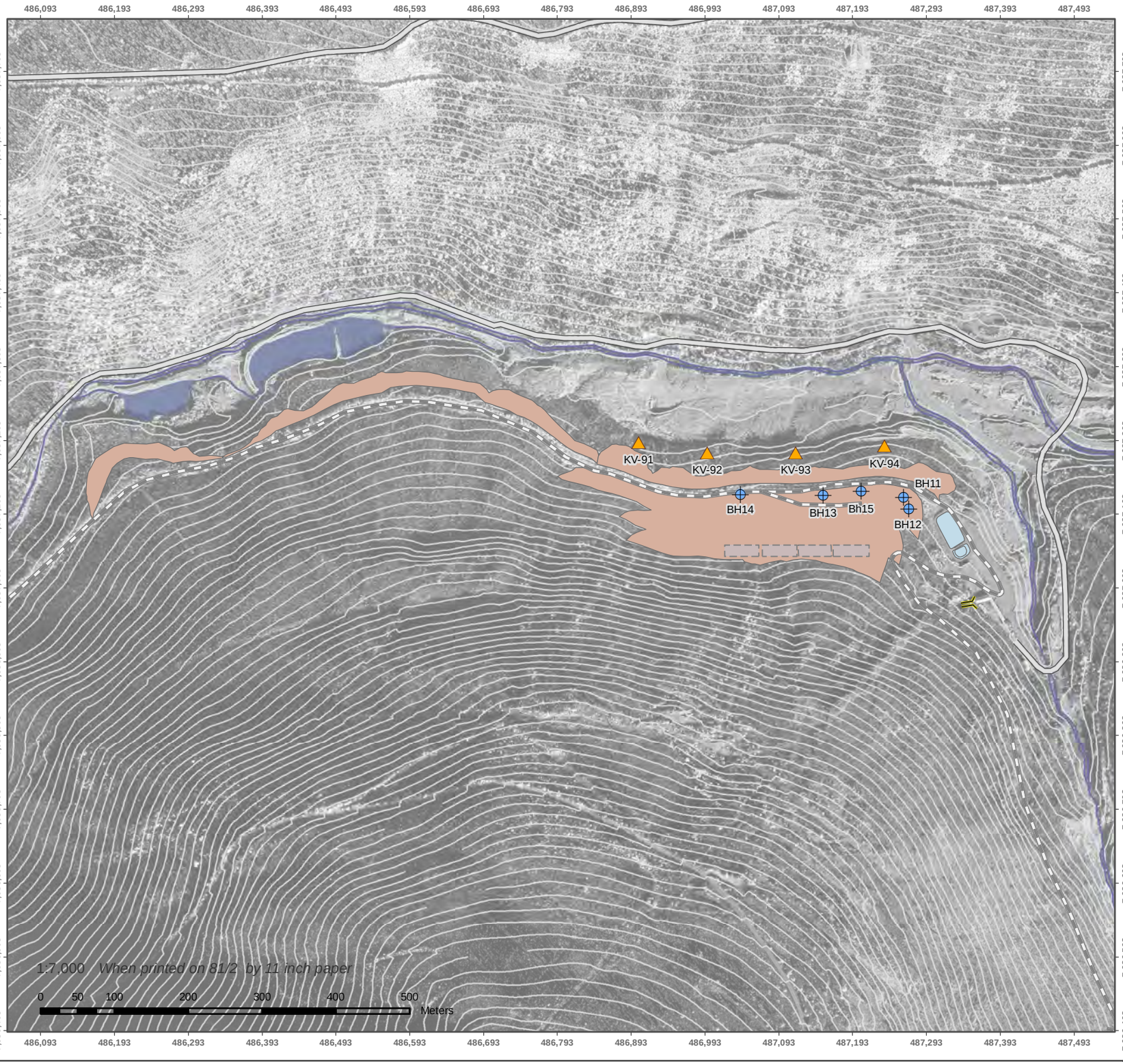
Commencement of construction of the (WRDA) is scheduled for Q2 2012. Four groundwater monitoring wells below the Bellekeno WRDA (as per Clause 86 of the Licence) will be installed according to WRDA final design. Due to the known presence of permafrost and sloping topography in the area beneath the proposed WRDA, Alexco expects any seepage to be deflected by the frozen layer, causing it to run downslope within the active layer. Because of this, relatively shallow monitoring wells are considered appropriate and most likely to intersect and monitor for any seepage from the WRDA. Proposed monitoring wells in the vicinity of the WRDA are summarized in Table 5.

Table 5 Bellekeno WRDA Groundwater Monitoring Well Summary

Station Number	Purpose	Estimated Total Depth (m)	Estimated Overburden Depth (m)	Northing[1]	Easting[1]
KV-91	Seepage/shallow groundwater monitoring	10	10	TBD[2]	TBD[2]
KV-92	Seepage/shallow groundwater monitoring	10	10	TBD[2]	TBD[2]
KV-93	Seepage/shallow groundwater monitoring	10	10	TBD[2]	TBD[2]
KV-94	Seepage/shallow groundwater monitoring	10	10	TBD[2]	TBD[2]

[1]Coordinates are UTM Zone 8 NAD 1983
[2]TBD – "to be determined", station not established at this time.

Appropriate layout and borehole locations for the WRDA monitoring wells will be selected based on field conditions prior to construction and will depend on final WRDA and with the input from design engineers. Conceptual WRDA monitoring well locations are shown on Figure 3.



QZ09-092 GROUNDWATER MONITORING PLAN

FIGURE 3

WASTE ROCK STORAGE AREA GROUNDWATER MONITORING LOCATIONS

- Bellekeno 625 Adit
- Proposed Monitoring Well
- Existing Borehole
- Proposed AML Waste Rock Disposal Area
- Proposed Non AML Waste Rock Disposal Area
- Settling Pond
- Haul Road
- Local Road/Trail
- Major Contour (5 meter interval)

Aerial photography flight date: July 13th 2006. Ortho-rectification produced by Challenger Geomatics Ltd.Site hydrography and contours derived from 2006 aerial imagery obtained from Geodesy Remote Sensing Inc., Calgary Alberta.

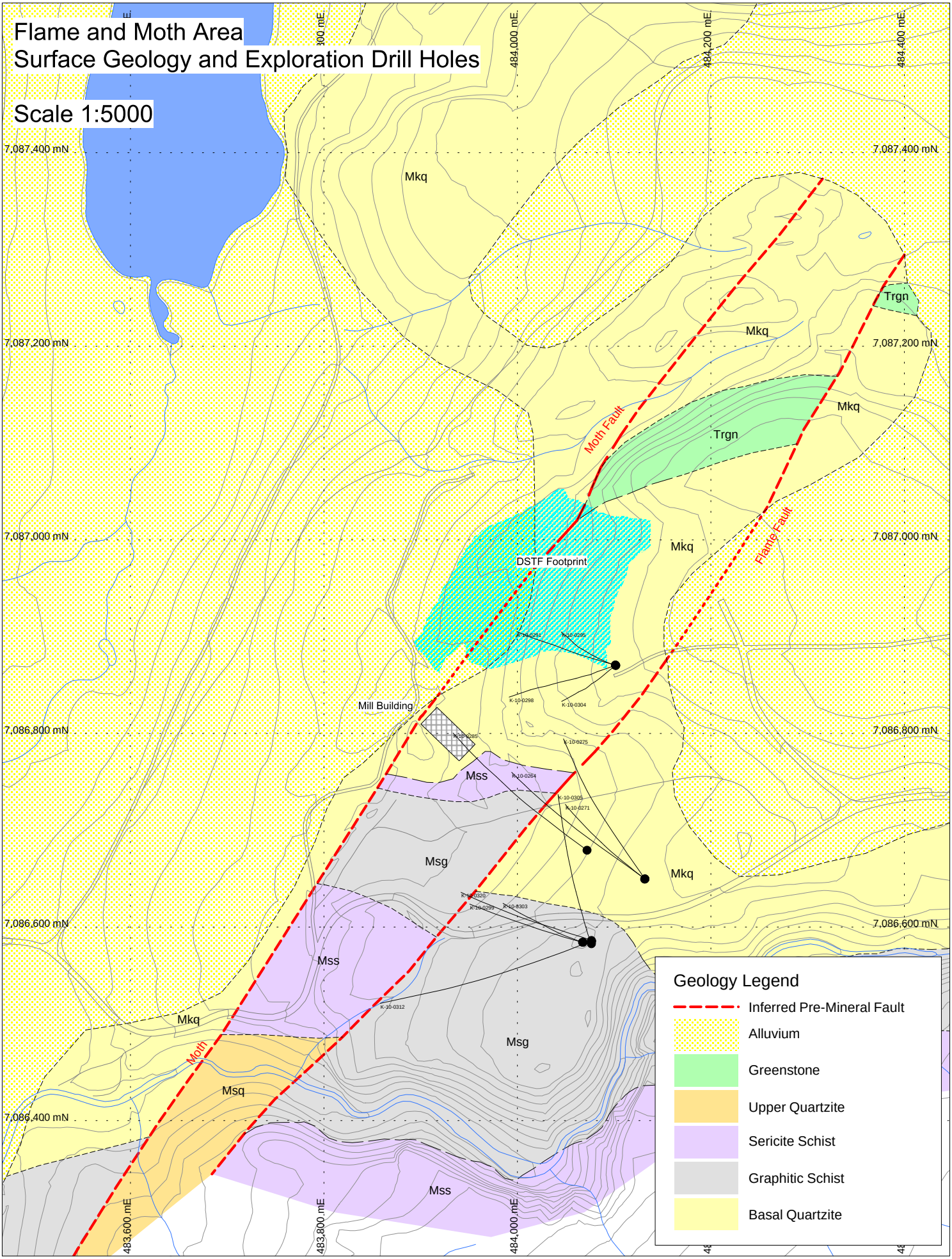
Datum: NAD 83; Projection: UTM Zone 8N

DRAWN BY MD	JAN 2011	VERIFIED BY EA

I:\ALEX-05-01\Bellekeno\GIS\mxd\Permitting\GroundwaterMonitoringPlan\Fig3_BKMine_20110125.mxd

7.0 KENO CITY GROUNDWATER MONITORING

The licence requirement for monitoring of KV-84 requires that a Keno City Well be monitored on a quarterly basis. This monitoring is also subject to Clause 44, requiring that all wells be sampled monthly for the first twelve months that they contain water. Initial sampling as reported in the SRK Bellekeno Groundwater Study (SRK, 2010) used Keno City Well #3 which is owned by a private resident of Keno City. Well #3 and the Keno City Firehall well have been sampled since issuance of the Licence in order to fulfill monitoring requirements for KV-84, but because of difficulties coordinating sampling, this is not viewed as a satisfactory solution for the duration of the Licence. Alexco, through part of the District Closure Planning, is currently planning installation of several wells around Keno City for a hydrogeology study as part of a hydrogeologic study of the Keno City area. It is anticipated that this work will be carried out during February 2011, and that once installed, one of these wells will be selected for reporting for KV-84. A notification will be submitted to the YWB and Water Resources in order to provide notification to regulators of the final sampling location of the Keno City well. The locations of the existing Keno City area wells including an approximate location for KV-84 are also shown on Figure 4


Flame and Moth Area
Surface Geology and Exploration Drill Holes
Scale 1:5000
7,087,400 mN
7,087,200 mN
7,087,000 mN
7,086,800 mN
7,086,600 mN
7,086,400 mN
483,600 mE
483,800 mE
484,000 mE
484,200 mE
484,400 mE
Mkq
Trgn
Msg
Mss
Msq
Moth Fault
Flame Fault
DSTF Footprint
Mill Building
K-10-0298
K-10-0304
K-10-0285
K-10-0275
K-10-0264
K-10-0305
K-10-0271
K-10-0320
K-10-0299
K-10-0303
K-10-0312
Geology Legend
Inferred Pre-Mineral Fault
Alluvium
Greenstone
Upper Quartzite
Sericite Schist
Graphitic Schist
Basal Quartzite

8.0 REVIEW OF RESULTS

Results of all groundwater monitoring activities will be subject to periodic review and interpretation by Alexco. This review and interpretation is key in identifying any potential changes in baseline conditions, and if necessary, trigger mitigation and/or adaptive management measures. The results of these reviews and analyses will be reported with the Annual Report.

9.0 GROUNDWATER MONITORING SCHEDULE

Groundwater monitoring will follow the schedule as described in Schedule B, Table 4 of the Licence, which is summarized below as Table 6.

Table 6 Groundwater Monitoring Schedule

Monitoring Station	Field Parameters			
	pH	Temp.	Cond.	Level
KV-84	Q*	Q*	Q*	Q*
KV-85	Q*	Q*	Q*	Q*
KV-86	Q*	Q*	Q*	Q*
KV-87	Q*	Q*	Q*	Q*
KV-88	Q*	Q*	Q*	Q*
KV-89	Q*	Q*	Q*	Q*
KV-90	Q*	Q*	Q*	Q*
KV-91	Q*	Q*	Q*	Q*
KV-92	Q*	Q*	Q*	Q*
KV-93	Q*	Q*	Q*	Q*
KV-94	Q*	Q*	Q*	Q*

*Represents monthly sampling for the first twelve months that they contain water based on Clause 44 of the Licence

Groundwater sampling and monitoring will be carried out by competent and trained field operators. The operators will also document the condition of the well at each location and record any non-standard observations (e.g. icing, blockage, physical damage to wellhead).

10.0 REPORTING

As per Clause 54 of Water Licence QZ09-092:

> *Unless otherwise specified in this licence, all monitoring data, reports, plans, studies, study results, designs or manual shall be submitted to the Board in the following format:*
>
> *a) All reports required to be submitted to the Board will be unbound and reproducible by standard photocopier, accompanied by one electronic copy on a CD/DVD.*
> *b) The Licensee shall provide to the Board 5 additional copies of all reports. The additional copies may be either 5 bound paper copies or 5 electronic copies on individual CDs/DVDs.*
> *c) Electronic copies shall be IBM compatible in one of the following formats: Word 97-2003, Excel 97-2003 workbooks, or Adobe .pdf format. Water quality results must be presented in Excel 97-2003 .xls format.*

The results of the weekly physical inspections will be summarized from the weekly inspection checklists and incorporated into the annual reports (as per section 55 of the licence). Requirements of the annual reports are outlined in sections 55 and 56 of the Licence.

11.0 REFERENCES

Access Consulting Group, 2009. Keno Hill Silver District Environmental Conditions Report Version 1. Report prepared for Alexco Resource Corp.

EBA Engineering Consultants Ltd. 2010. Preliminary Engineering Design and Management Plan, Dry-Stacked Tailings Facility, Bellekeno Mine Mill Site, Yukon. Report prepared for Alexco Keno Hill Mining Corp.

EBA Engineering Consultants Ltd. 2008. Geotechnical Evaluation – Potential Mill Sites Bellekeno Project near Keno City, Yukon. Letter to Alexco Resource Canada Corp.

SRK Consulting (Canada) Inc (2010) 2010 Bellekeno Groundwater Program. Report Prepared for Alexco Keno Hill Mining Corp. SRK Project # 1CA009.003.

SRK Consulting (Canada) Inc (2009a) Desktop review: Effects of Water Extraction at Christal Lake on Water Levels in the Keno City Community Well. Memorandum to Alexco Keno Hill Mining Corp. SRK Project # 1CE012.003.

SRK Consulting (Canada) Inc (2009b) Assessment of Potential Groundwater Impacts from the Bellekeno Mill Site and Dry Stack Tailings Facility. Letter to Alexco Resource Corp. SRK Project # 1CE012.003.

Alexco Keno Hill Mining Corp.

Groundwater Monitoring Plan

Water Use Licence QZ09-092

Appendix A

SRK 2010 Bellekeno Groundwater Report

2010 Bellekeno Groundwater Program





Prepared for:

Alexco Resource Corporation

Prepared by:

SRK Consulting
Engineers and Scientists

Project Reference Number
SRK 1CA009.003

May 2010

2010 Bellekeno Groundwater Program

Alexco Resource Corporation

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SRK Project Number 1CA009.003

May 2010

Executive Summary

Alexco Resources Corporation is proposing to construct the Bellekeno Mill and dry stack tailings facility (DSTF) at the Flame & Moth area approximately one kilometer west of Keno City, Yukon. SRK Consulting (Canada) Inc. was contracted by Alexco to plan and implement a groundwater investigation with the objectives of installing a groundwater monitoring system around the mill and DSTF sites, collecting information to update the conceptual model for groundwater flow, and assessing the potential for impacts to groundwater quality and quantity.

Three monitoring wells were drilled and completed in early February 2010 (PH2, PH5 and PH6). Drilling was conducted with an air-rotary drill and PVC monitoring wells were installed in each drill hole with sand packs and bentonite annular seals. Vibrating wire pressure transducers were attached to the outside of PH5 and PH6 to allow collection of water level data in the event the monitoring wells freeze closed.

In the DSTF area at the north end of the site, bedrock is found at relatively shallow depths, with the thickness of overburden materials increasing towards the marshy ground to the west of the site. Only minor groundwater was identified in overburden sediments; bedrock is the primary aquifer. On the southern edge of the site, below the proposed mill area, overburden is much thicker and significant flow was produced during drilling of PH5 (estimated at 15 L/s) suggesting that groundwater flow through these overburden materials is significant.

Water levels measured in the newly installed monitoring wells were compared to those in Well #3 in Keno City to determine groundwater flow directions. Well #3, which is about 80m south of the community supply well (the Firehall Well), was used to represent water levels in the Keno City area. The water level in the Firehall Well could not be measured due to the wellhead construction. Drill logs indicate that both Well #3 and the Firehall Well get water from bedrock. The water table drops by about 4 m between Keno City and PH6 on the eastern edge of the site, then drops steeply by another 20 or so meters under the site. The groundwater flow direction is from Keno City towards the site.

The water level in Well#3 was monitored continuously with a datalogger for a period of about 5 days during the investigation. During this period, it was reported by the Water Steward that approximately 4,000 imperial gallons of water were delivered to local residents. Well #3 water level data indicate no effects from pumping of the Firehall Well to replenish storage tanks, nor effects from day-to-day supply to the public shower and laundry facilities. These observations indicate that either the aquifer is not being significantly drawn down or that recharge is sufficient for the aquifer to quickly reciver from any periods of lower water levels.

Samples from the new monitoring wells were analysed for water quality. Results indicate higher concentrations of chloride, sulphate and dissolved zinc at PH6 relative to PH5. PH6 is located uphill of the proposed DSTF on the eastern edge of the site, closest to Keno City and down gradient of the

city dump. It is also in close proximity to the Flame & Moth vein fault and water quality may indicate the influence of the city dump or natural mineralization.

Potential effects on the groundwater system due to the site are limited to water quality. The current plans for mill water supply do not include groundwater extraction, thus there will be no effects on groundwater quantities. Water management structures planned as part of the mill and DSTF construction, including an underdrain for the DSTF and diversion ditches, are designed to intercept and convey any site runoff to a lined pond, from which water will be treated prior to discharge or re-used as part of the mill water supply. Leakage from or bypass of water management structures is the only potential pathway for effects to groundwater quality. These structures have been graded and designed to freely drain to the mill pond. The combination of compaction and sloping of the DSTF to promote runoff and the free-draining nature of the interception structures will all limit the chance of significant leakage.

The risk to water quality at the Keno City Firehall Well and other Keno City private wells is considered insignificant. Groundwater flows east to west, away from Keno City, and the water level in Well #3 is similar to the water level measured in the Firehall Well during construction in 1987, indicating that either there has been no significant drawdown of the Keno City bedrock aquifer or that it recovers from pumping during periods of relatively low extraction. In either case, the groundwater flow direction (i.e., the entire local water table) would have to be reversed for an extended period of time for water from the site to reach Keno City wells. Such a reversal would require pumping at rates many times greater than currently possible and over durations long enough to completely change the regional groundwater flow system.

It is recommended that groundwater quality and levels be monitored regularly:

- The groundwater monitoring wells should be sampled and water levels recorded twice annually, if not frozen and accessible. If frozen, the vibrating wire transducers on PH6 and PH5 should be monitored quarterly.
- If the monitoring wells are found to freeze and remain frozen, the wells should be freeze protected or alternate methods should be implemented to allow groundwater sampling.
- Following finalization of the mill and DSTF engineering, three monitoring points should be located within shallow sediments down gradient of the DSTF drainage ditches and mill pond to monitor for potential ditch leakage. These wells should be sampled twice during the summer.

Table of Contents

Executive Summary i

1 Introduction 1

2 Background 1
2.1 Flame & Moth Mill and DSTF Plan 1
2.2 Available Data 2
2.3 Previous Assessments of Potential Groundwater Impacts 3

3 Field Program 3
3.1 Site Reconnaissance and Initial Meeting with Keno City Residents 3
3.2 Drilling and Monitoring Well Installation 4
3.3 Water Level Data 5
3.4 Water Quality 7

4 Conceptual Model for Groundwater Flow 10

5 Updated Effects Assessment 11
5.1 Environmental Effects 11
5.2 Keno City Water Supply 12

6 Conclusions and Recommendations 12

7 References 13

List of Tables

Table 1: Monitoring Well Completion Information 5
Table 2: Depth to Water in Monitoring Wells 6
Table 3: Monitoring Well Development 7
Table 4: Water Quality Data 8

List of Figures

Figure 1: Bellekeno Site Map and Well Locations
Figure 2: Interpreted Water Table
Figure 3: Compensated Vibewire Measurements at Well#3
Figure 4: Interpreted Bedrock Surface
Figure 5: Location Map and Cross Section A
Figure 6: Cross Section B and C

List of Appendices

Appendix A1: Firehall Well Log
Appendix A2: Firehall Well Water Quality
Appendix A3: Review of Firehall Well and Water System

Appendix B: 2010 Drill Hole Logs

Appendix C: Vibrating Wire Calibration Sheets

Appendix D: 2010 Drill Hole Water Quality

1 Introduction

This report presents results of groundwater investigations at the proposed Bellekeno Flame and Moth mill site and dry stack tailings facility (DSTF). The work was completed by SRK Consulting (Canada) Inc. for Alexco Resources Corporation.

The scope of this program included:

- A review of available data and a meeting with Keno City residents to discuss groundwater issues related to the project.
- Design and implementation of a groundwater field program.
- Interpretation of field program results, an update of the conceptual model for groundwater flow and an updated assessment of potential effects to groundwater related to the proposed Flame and Moth mill and DSTF.
- Recommendations for future groundwater monitoring.

2 Background

As part of the proposed Bellekeno development, Alexco plans to build a mill and DSTF at the Flame and Moth site (the site), which is located approximately one kilometer west of Keno City, Yukon. The general site layout is shown in Figure 1. Groundwater characterization and monitoring will be required as part of the site operations and water management.

Keno City obtains potable water from groundwater extraction. Many residents and business' are supplied from the Firehall Well. Water is delivered by truck to those with storage tanks; and piped directly to the public laundry and restroom facilities. A tap is provided for general public use. Maintaining the quality and quantity of the groundwater resource is an important issue for residents. From the perspective of the environment, groundwater is primarily a pathway from the site.

Surface water quality and aquatic resources have also been identified as a valued component by local First Nations, governments and the local community. Potential effects to groundwater that could contribute to effects on Lightning Creek and the wetlands above Christal Lake are also considered.

2.1 Flame & Moth Mill and DSTF Plan

Ore from the Bellekeno underground development will be hauled to the mill site, where it will be ground and separated into concentrate and tailings. The general site layout is shown in Figure 1.

Tailings from the mill will be dewatered and managed in two streams:

1. High-pyrite tailings will be hauled back to the underground workings, mixed with cement and placed as backfill.

2. Low-pyrite tailings will be placed in the dry stack tailings facility, north of the mill at the Flame and Moth site. Low-pyrite tailings not placed in the DSTF will also be hauled to the underground workings.

Design of the surface water management infrastructure and DSTF has been completed by EBA Engineering (EBA 2010a, 2010b). Water management structures have been incorporated to minimize, divert or treat water contacting the DSTF and mill facilities. The DSTF will be located adjacent to the mill, on a westward facing slope. Low-pyrite tailings routed to the DSTF will be end-dumped, graded and compacted in lifts. Water management structures will include:

- An uphill berm to divert runoff around the DSTF.
- A 0.5 m drainage blanket beneath the entire DSTF for seepage interception.
- A series of runoff collection ditches along the toe of the DSTF.
- A runoff conveyance flume that will route water from the drainage blanket and collection ditches to the mill pond.
- Grading of the DSTF surface to increase runoff and minimize infiltration.
- Placement of a till cover over the DSTF to further reduce infiltration of precipitation, minimize dust and promote re-growth of vegetation.
- A low permeability till pad will be constructed underneath the ore stockpile, which will be milled at closure.

Site runoff and seepage from the DSTF will be collected in a lined runoff collection pond (i.e., the mill pond). The mill pond will be located in the topographically lowest area of the site, below the mill and DSTF. Water in the pond will be used to supplement mill water supply or treated, if necessary, and discharged.

Mill operations will use re-cycled process water with a freshwater "makeup", or supplement, of about 43 m^3/day (about 8 US gallons per minute). Freshwater will be supplied from the Galkeno 900 water treatment facility (WTF) and from the mill pond. Extraction from Cristal Lake or Cristal Creek will be used as a backup if necessary. Water from the Galkeno 900 WTF will be conveyed to the mill via an insulated, heat-traced pipeline. The current plan does not include a provision for groundwater extraction, but notes that if investigations indicate that groundwater can be extracted without impact to users or the environment, use may be assessed (Access, 2009).

2.2 Available Data

Data available at the commencement of this program included both site-specific data and general information on local and regional geology. Information on subsurface conditions included geotechnical drilling and test pit logs for the mill and DSTF site, subsurface temperature data from thermistor strings installed at the site and drill logs for a limited number of Keno City wells. Current water level data was only available from existing monitoring wells at the mill and DSTF site. The only water level data for Keno City was that collected during well installation and reported on well logs.

2.3 Previous Assessments of Potential Groundwater Impacts

SRK had previously completed initial assessments of potential impacts of the proposed mill and DSTF site on groundwater quantity and quality (SRK, 2009a; SRK, 2009b). At the time that those assessments were completed, there were no groundwater monitoring wells at the site and little information available about the Keno City water supply, thus, interpretations were based on available mine plans, hydrogeologic principles and previous work in the Keno Hill district and overall region.

The initial assessment indicate that the risks of impacts to the Keno City water supply were low, but that data on groundwater flow directions and Keno City water well pumping rates were needed before a definitive conclusion and be drawn available.

3 Field Program

3.1 Site Reconnaissance and Initial Meeting with Keno City Residents

Dan Mackie, Senior Consultant with SRK, inspected the site between January 14 and 19, 2010. The visit included a reconnaissance of potential drill hole locations and access, a tour and visual inspection of the Keno City water supply system, and a meeting with residents of Keno City. Findings included:

Keno City water supply – Residents, businesses and services not connected to a private well are supplied by Keno City. Keno City extracts groundwater from a well located next to the Keno City firehall. The well is called the Firehall well (Yukon Department of Environment Well ID 213140003) and has the following details:

- The well was drilled in 1987 to a total depth of 93 m. Bedrock was intersected at a depth of 55 m and steel casing was seated about 2 m into bedrock. The well is an open bedrock well from about 57 m to 93 m (i.e., there is no screen in the well). The well log does not include any information about a surface seal.
- The submersible pump is a Grundfos 15 SQ15C-290 with a rated capacity of 0.95 to 1.3 L/s (12.5 to 16.7 Igpm). The well is housed in an unlocked plywood box with ditching to divert runoff. The wellhead itself does not allow access for water level measurement; the access port typically used for a water level sounding tube is being used to run heat trace for the pump riser pipe.
- The static water level during drilling was reported as 55 m below ground, or at about the overburden – bedrock contact. Due to the wellhead construction, water levels cannot be measured without removing the heat trace or disassembling the wellhead. Both would probably require deactivation of the well and removal of the pump.
- The well and water quality are managed by the town Water Steward. Water is disinfected by chlorination within the firehall. Water is stored in multiple tanks and delivered to individual tanks with a dedicated water truck. Water quality data, including physical parameters, dissolved

anions and total metals are available since 1998; dissolved metals have been analyzed on occasion. Water quality has met the Guidelines for Canadian Drinking Water Quality for the majority of parameters, with occasional exceedances of iron and lead, though notes indicate the lead exceedance may have resulted from inappropriate sampling methods.

- Historically, water extraction rates have not been quantified. Deliveries are recorded and provide the only long term record of approximate water use. The supply system has a cumulative flow meter, but it has not been monitored regularly.

The well log is included in Appendix A1. Water quality data is included in Appendix A2. A review of the water supply system, completed in May 2002 by N.A. Jacobsen, P.Eng. is included as Appendix A3.

Meeting with Keno City residents – On January 15, 2010, Mr. Mackie met with residents of Keno City. The proposed water management plan was presented and historical observations of the Keno City groundwater system were discussed. Residents expressed concerns about potential impacts on water quality and provided input on requirements and locations for groundwater monitoring wells.

3.2 Drilling and Monitoring Well Installation

Three groundwater monitoring wells were installed between February 10th to February 15th, 2010. Monitoring well locations were positioned to provide information on groundwater flow directions and for use in long term monitoring. Drilling was completed by Geotech Drilling of Prince George, BC using ODEX air-rotary methods and a down-the-hole hammer. Jacek Scibek, an Intermediate Consultant with SRK, supervised the drilling, chip logging and the installation of the monitoring wells. All drill holes were vertical. Monitoring well locations are shown on Figure 1.

The following summarizes lithology and groundwater occurrences observed during drilling:

- PH2, located down gradient and west of the proposed DSTF, intersected a shallow layer of gravel and moist silt (till), solid ice between 4 and 6 m below ground surface, then 3 metres of frozen gravel and 2 metres of dry, gravelly silt (till) over bedrock. Bedrock was encountered from a depth of 11.3 to 43 m. Bedrock became moist at about 33 m and began producing about 0.3 L/s (5 USgpm) at about 41 m.
- PH5, located to the southwest of the mill between the mill and Duncan Creek Road, intersected moist, gravelly to clayey, silt (till) with occasional gravel lenses to a depth of about 29 m, then water bearing gravel and sand to the end of the hole at 36 m. Within the lower gravel to coarse sand unit, water was produced at estimated rates of up to 15 L/s (> 200 USgpm). Drill casing could not be pushed past this point and this drill hole did not intersect bedrock.
- PH6, located at the approximate eastern extent of the proposed DSTF and at roughly 40 m higher elevation than the mill pad, intersected bedrock at a depth of 2.7 m below ground surface. The thin layer of overburden was not recovered. The drill-hole ended at 57 metres in a water producing section of bedrock. Water was only produced after shutting down the drill and

allowing the water levels to recover. Total volumes on the order of 10 to 20 litres were observed when air was pumped down the drill hole, but these volumes were not sustained.

PVC monitoring wells were completed in each of the drill holes. Monitoring wells in PH2 and PH5 have 5 cm (2-inch) construction and the monitoring well in PH6 has 2.5 cm (1-inch) construction. All wells were constructed with threaded, flush joint Schedule 40 PVC and a three metre length of slotted PVC for the well screen. Filter sand was used around the screen zones, topped with a layer of bentonite chips or pellets. The drillhole was then grouted to surface using a bentonite grout. Completion information for the new wells, as well as for the Firehall Well and Well #3 are provided in Table 1. Completion logs for the three new wells are provided in Appendix B.

Table 1: Monitoring Well Completion Information

Drill Hole ID	Easting	Northing	Installed On	Drill Hole Depth (mbgs)	Screen Depth (mbgs)	Stick-Up (m)
PH2	483864	7086952	15-Feb-10	42.7	38.1 to 41.1	0.85
PH5	483836	7086707	12-Feb-10	36.0	31.1 to 34.1	0.45
PH6	484104	7086854	11-Feb-10	57.9	53.3 to 56.4	1.16
Well #3 Yukon ID: 213140005	485024	7086865	21-Aug-83	67.1	Open Hole	At ground surface
Firehall Yukon ID: 213140003	484993	7086979	22-Aug-87	92.9	Open Hole	n/a

Coordinates are NAD 83, UTM Zone 8V – all coordinates taken with hand-held Garmin GPSmap 60Cx.
mbgs = metres below ground surface.
masl = meters above sea level.
Open hole = well was cased through overburden and left open in bedrock.

Vibrating wire pressure transducers (vibe wires) were installed on the outside of monitoring wells PH5 and PH6 to allow the measurement of water level in the event that water within the wells froze near surface.

The vibe wires are model VW2100-0.7 (0.7 MPa range) produced by RST Instruments of Coquitlam, B.C. Each transducer has a 60 m long communication cable. The transducer and cable was taped to the outside of the monitoring well PVC as it was installed. The transducer itself is within the sand pack of the monitoring well screen zone. A RST VW2106 portable readout unit was used to take readings and left at site for future use. Calibration and information sheets for the vibe wires and readout unit are provided in Appendix C.

3.3 Water Level Data

Water levels were measured in the three new monitoring wells and Well #3 to establish groundwater flow directions. Well #3 is located approximately 80 m to the south of the Firehall Well (Figure 1). Water level data was collected from Well #3 in Keno City and not the Firehall Well due to the well access issues described in section 3.1. Water level data are presented in Table 2.

Table 2: Depth to Water in Monitoring Wells

Drill Hole ID	Date	Depth to Water (m below top of casing)	Stick-Up (m)	Depth to Water (mbgs)	Ground Elevation (masl)	Water Level Elevation (masl)
Well #3	11-Feb-10	42.83	0	42.83	940.3	897.5
PH2	15-Feb-10	27.86	0.85	27.01	898.5	871.5
PH5	14-Feb-10	28.45	1.05	27.4	900.0	872.6
PH6	14-Feb-10	44.31	0.95	43.36	937.0	893.6

Well #3 had been reported as going dry during the summer of 2008, but the owners provided authorization to access and recheck the well. A hole was drilled in the top of the wellhead to allow access as, similar to the Firehall Well, the port for a water level sounding tube has been used for heat trace. Water level soundings indicated that there was a water column of about 20 m, suggesting that either the well has recovered since it went dry or that the pump may have failed and been interpreted as the water level dropping below the pump. The hole drilled for water level access was fitted with a removable plug.

Figure 3 is a water table map inferred from the above data. Water level elevations indicate an overall east to west flow direction, from the Keno City area towards the site. The water table drops steeply westward at the site.

In an effort to assess the radius of influence of the Firehall Well when pumping, a water level datalogger was installed in Well #3 between February 10 and 15. The Firehall Well and Well #3 are both designed to extract water from bedrock and are relatively close together. Mr. Jim Milley, the Water Steward, reported that during the monitoring period:

- The potable water storage tank was cleaned on February 10, thus empty;
- Deliveries of 2000 imperial gallons were made on the February 11 and 12; and
- The pump runs every day to supply water to the public laundry and shower facilities.

Using the maximum design pumping rate of about 17 Igpm for the Firehall Well pump, the pump would have to run for about 100 minutes to provide 2000 Igpm.

Figure 4 shows water level data for Well #3 for the monitoring period. The water level in Well #3 was approximately the same as the water level measured in the Firehall Well in 1988, indicating that either the aquifer has not been significantly drawn down or that recharge is sufficient to reverse any periods of lower water levels. Water levels fluctuated by less than 5 cm during the monitoring period and show no drawdown or recovery characteristics that would indicate effects of pumping in the Firehall Well. The cyclic variation in water level coincides more closely to changes in atmospheric pressure.

At a distance of 80m, Well #3 is not influenced by day-to-day operation of the Firehall Well, even during the winter season when groundwater inflows would be low. These results suggest that normal operation of the Firehall Well are unlikely to cause a significant change in the local water table.

3.4 Water Quality

Following installation, each of the three new monitoring wells were developed and sampled for water quality analyses. The wells were developed by pumping out at least three well volumes of water using a Waterra Hydrolift pump, or by hand. Field measurements of pH and electrical conductivity were used to assess the progress of development. Once these field parameters had stabilised, samples were collected. For quality assurance, a duplicate sample was collected from PH5, as well as a field blank, though the field blank appears to not have been submitted to the laboratory for analyses. Table 3 summarizes well development information.

Table 3: Monitoring Well Development

Drill Hole ID	Date of Development	Total Volume Pumped (L)	Duration of Pumping (min)	Final Temperature (deg C)	Final Electrical Conductivity (µS/cm)	Final pH
PH2	15-Feb-10	120	15	0.5	1830	7.10
PH5	14-Feb-10	200	25	0.7	690	6.70
PH6	14-Feb-10	620	180	0.9	2360	6.89

Samples for water quality were field filtered, stabilized and stored in a refrigerator at the Alexco office in Elsa. Samples were submitted by Alexco staff to Exova Group Ltd of Surrey, BC. Four samples were analysed, including the duplicate from PH5. The sample from PH2 was of limited volume due to difficulties encountered while pumping; following development, sufficient sample could not be collected for the full suite of analyses due to a pump failure and subsequent freezing of the sampling line. As a result, only pH and electrical conductivity were tested for that sample. The sample analysis results are presented in Table 4, along with the most recent water quality data from the Keno City Firehall Well for comparison. The complete laboratory report is included in Appendix D.

Table 4: Water Quality Data

Drill Hole ID		Drinking Water Guideline	Guideline Note	Firehall	PH6	PH5	PH5-Dupl.	PH2
Date of Sample	**Unit**			**18-Apr-08**	**14-Feb-10**	**14-Feb-10**	**14-Feb-10**	**15-Feb-10**
Field Parameters								
pH		-	-	-	6.89	6.7	6.7	7.1
Electrical Conductivity	µS/cm	-	-	-	2360	690	690	1830
Physical Parameters (lab)								
pH		6.5-8.5	1	7.72	7.1	6.85	6.79	7.28
Electrical Conductivity	µS/cm	-		562	2280	693	700	1770
Total Dissolved Solids	mg/L	5001	1	386	1850	422	428	-
Anions								
T-Alkalinity	mg/L	-	-	147	482	93	93	-
Hardness as $CaCO_3$	mg/L	-	-	281	1650	359	358	-
Chloride	mg/L	250	1	6.26	9.18	0.54	0.58	-
Sulfate (SO_4)	mg/L	500	1,5	129	953	229	236	-
Total Metals								
Aluminum	mg/L	-	-	0.036	15.1	0.038	0.035	-
Antimony	mg/L	0.006	4,5	<0.001	0.024	<0.0002	<0.0002	-
Arsenic	mg/L	0.01	-	0.005	0.048	0.0012	0.0012	-
Barium	mg/L	1	-	0.14	0.1	0.051	0.049	-
Boron	mg/L	5	4	<0.05	<0.02	<0.005	<0.005	-
Cadmium	mg/L	0.006	-	0.0009	0.00008	0.00037	0.00038	-
Calcium	mg/L	-	-	80.4	493	118	117	-
Chromium	mg/L	0.05	-	<0.001	0.0098	<0.0004	<0.0004	-
Copper	mg/L	1	1,6	0.18	0.006	0.002	0.001	-
Iron	mg/L	0.3	1	0.42	12.4	0.157	0.149	-
Lead	mg/L	0.01	6,5	<0.001	0.01	0.0005	0.0004	-
Magnesium	mg/L	-	-	21.6	136	32.3	32	-
Manganese	mg/L	0.05	1	0.004	1.39	0.0209	0.0191	-
Potassium	mg/L	-	-	0.3	5.4	0.5	0.6	-
Selenium	mg/L	0.01	-	0.002	<0.003	<0.0006	<0.0006	-
Sodium	mg/L	200	1	2.43	19.5	1.6	1.59	-
Uranium	mg/L	0.02	4	0.0067	0.167	0.0034	0.0034	-
Zinc	mg/L	5	1,6	0.16	0.37	0.042	0.038	-
Dissolved Metals								
Aluminum	mg/L	-	-	-	<0.005	<0.005	<0.005	-
Antimony	mg/L	-	-	-	0.0407	<0.0002	<0.0002	-
Arsenic	mg/L	0.025	6	-	0.0192	0.0003	0.0004	-
Barium	mg/L	1	-	-	0.02	0.048	0.048	-
Boron	mg/L	5	6	-	<0.004	<0.004	<0.004	-
Cadmium	mg/L	0.005	-	-	<0.00001	0.00033	0.00035	-
Calcium	mg/L	-	-	-	425	99.2	99.1	-
Chromium	mg/L	0.05	-	-	<0.0004	<0.0004	<0.0004	-
Copper	mg/L	1	1,3	-	<0.001	0.001	0.001	-
Iron	mg/L	0.3	1	-	<0.01	<0.01	<0.01	-
Lead	mg/L	0.01	3,7	-	<0.0001	<0.0001	<0.0001	-
Magnesium	mg/L	-	-	-	144	27	27	-
Manganese	mg/L	0.05	1	-	1.09	0.0148	0.0152	-
Potassium	mg/L	-	-	-	2.1	0.3	0.3	-
Selenium	mg/L	0.01	-	-	<0.0006	0.0006	0.0007	-
Sodium	mg/L	200	1	-	15.5	1.4	1.4	-
Uranium	mg/L	0.1	-	-	0.142	0.0031	0.0031	-
Zinc	mg/L	5	1,3	-	0.064	0.036	0.037	-

Water quality data provide an initial sense of local variability in water quality. While only a single sample has been collected from two wells, drill holes were completed with air-rotary methods and well developed, thus, the data are considered representative.

Firehall Water Quality

A water sample collected from the Firehall well in April 2008 was slightly alkaline (lab pH 7.72) and had an Electrical Conductivity (EC) of 562 µS/cm. Total Dissolved Solids (TDS) was 386 mg/L, and chloride concentration was 6.3 mg/L. Sulphate, bicarbonate, calcium and magnesium were the most abundant ions measured, although it should be noted that metal analyses are reported as Total Metals only.

PH2 Water Quality

A water sample collected from PH2 in February 2009 had neutral pH (field pH 7.1) and EC of 1830 µS/cm. No results for metals or anions are available from PH2. The EC value for PH2 indicates that TDS in this sample were intermediate between the PH5 and PH6 samples from the same monitoring round.

PH5 Water Quality

A water sample collected from PH5 in February 2009 had near-neutral pH (field pH 6.7) and EC of 690 µS/cm. Total Dissolved Solids (TDS) was 422 mg/L. Sulphate and calcium were the most abundant ions measured. The chloride concentration was low (0.54 mg/L)

Both total and dissolved metals samples were collected. Based on the higher total metal concentrations (e.g. iron and aluminum), it appears that some sediment was entrained during sample collection and the reported total metal results reflect the influence of both dissolved metals and of suspended solids.

Dissolved trace metal concentrations were generally low (<0.05 mg/L). The slightly elevated sulphate level may be an indication that the water has contacted naturally mineralized material.

Field duplicate samples from this station returned acceptable results, with duplicate values for all parameters having relative percent differences (RPDs) less than 10% for all parameters where concentrations were at least five times higher than the method detection limit. Based on these results, the water quality analyses are considered to be representative and reliable.

PH6 Water Quality

A water sample collected from PH6 in February 2009 had neutral pH (field pH 6.89) and EC of 2360 µS/cm. Total Dissolved Solids (TDS) was 1850 mg/L, and the chloride concentration was elevated (9.18 mg/L). Sulphate, bicarbonate, calcium and magnesium were the major ions measured. Sulphate is elevated and total arsenic, antimony, iron and manganese exceed drinking water guidelines.

Both total and dissolved metals samples were collected. The high total iron and aluminum, concentrations clearly indicate that some sediment was entrained during sample collection.

Dissolved trace metal concentrations were low (generally <0.05 mg/L, with the exception of uranium (0.142 mg/L)). As shown in Figure 1, PH6 appears to be situated downgradient of the Keno City landfill, and it may be that the elevated chloride and sodium concentrations in PH6 may reflect the influence of leaching from the landfill. Elevated metals in PH6 may also be due to proximity to known mineralized structures in the area (Figure 1). The elevated uranium concentration should be checked in subsequent sampling and analysis.

4 Conceptual Model for Groundwater Flow

A conceptual model for groundwater flow in the area of the mill, DSTF and Keno City, or a "picture" of how the groundwater system works, has been developed from the available information. Figures 5 and 6 present cross-sections through the site, including generalized geology and the inferred water table. Cross-section locations are shown on Figure 5. The following points summarize the conceptual model:

- Groundwater is present in both overburden and bedrock aquifers. In areas where bedrock is close to ground surface, shallow groundwater may be present, probably within depths that freeze or thaw seasonally. A thicker overburden aquifer is present to the south of the site. The relatively thick overburden sequence encountered at PH5 likely represents sediments and old stream channels deposited during glaciations. Groundwater flow within this thicker aquifer is probably significant, as indicated by the volume of water encountered during drilling. A bedrock aquifer is apparent both below the site and at Keno City. Groundwater flow within this aquifer will be controlled by the presence of fractures and geologic structures, though different lithologies and mineralized zones may create areas of higher porosity. Bedrock permeability within the vicinity of Keno City is thought to be generally low, as indicated by low yield observed during the drilling of PH6. Geologic structures cross the site, but none have been mapped as connecting the site and Keno City. The bedrock aquifer probably has a lower capacity to transmit water than the thick overburden aquifer to the south of the site.
- The measured water level elevations and the inferred water table shown in Figure 3 indicate that the overall groundwater flow direction is from east to west, or from the area of Keno City towards the site. Available data suggests that the water table is relatively flat between Well #3 and PH6, dropping only about 4 m. The water table drops significantly more to the west under the site, by about 20m between PH6 and both PH5 and PH2. The water table in vicinity of Keno City is more than 20m higher in elevation than the water table down gradient of the mill and DSTF.
- The groundwater system at the site is likely recharged by runoff from the surrounding mountains, infiltration of direct precipitation and, possibly, leakage from Lightning Creek, which is higher than the measured groundwater levels. Shallow groundwater probably discharges to a limited degree to low elevation marshes and Christal Lake, while deeper groundwater within overburden sediments and bedrock will flow parallel to the Duncan Creek and Christal Creek drainages.

5 Updated Effects Assessment

5.1 Environmental Effects

The current mill and DSTF plan includes no provision for groundwater extraction, thus there will be no effects on groundwater flows. The potential for effects to groundwater quality and either the lower elevation marshy areas or Lightning Creek will be controlled through the mill and DSTF water management plans.

As described in section 2.1, the water management plan includes surface water diversion structures, drainage ditches and a drainage blanket under the DSTF. The purpose of this system is to intercept site runoff and seepage though the DSTF and re-direct it to the lined mill pond, for treatment and discharge. The only pathway for affected waters to reach the groundwater system will be via leakage from these structures.

The significance of leakage from the water management structures will be a function of the quality and volume of leakage. The potential volume of leakage will be minimized in a number of ways:

- A diversion berm will be constructed uphill of the DSTF to divert clean runoff around the DSTF.
- During operations, the DSTF surface will be progressively graded and compacted to enhance runoff, or limit the amount of water infiltrating into the tailings. The compacted tailings will have a low permeability (estimated at approximatley7x10-7 m/s by Alexco), thus promoting runoff and decreasing infiltration or displacement of pore water.
- During progressive closure and reclamation annually during operations, a 0.5 m thick cover will be placed over the DSTF, graded and re-vegetated.
- Any water that does flow into and through the tailings will be collected by the underdrain, which will itself be graded to drain to collection ditches and the lined mill pond. The conveyance flume and mill pond will be lined with a geosynthetic liner, the type of which has not yet been chosen (EBA, 2010a).

Flows within diversion ditches will most likely be seasonal, primarily related to freshet and significant rain events. Any water that may leak from ditches or the mill pond into shallow, unfrozen overburden materials will flow east (downhill) towards organic-rich soils in the marshy ground near Christal Creek. Natural attenuation mechanisms in peat and other organic-rich soils have been observed to remove metals from mine-impacted water at other locations in the Keno Hill district and elsewhere in Yukon (e.g., Valley Tailings Facility (Elsa); Rose Creek Valley Tailings Facility (Faro)) (SRK, 2009c).

The groundwater flow direction under the site is generally east to west, towards marshy ground. To the south of the site, water level data from PH5 indicates that the groundwater table is lower than Lightning Creek. While the groundwater table may merge with Lightning Creek downstream, the site water management controls, the east to west flow direction, the long groundwater flow path and the high flow in Lightning Creek make the likelihood of water quality impacts to Lightning Creek very low.

5.2 Keno City Water Supply

The current plan does not use groundwater extraction for freshwater supply to the mill, thus there will be no effects on the amount of water that can be extracted by the Firehall Well or other Keno City private wells.

The risk that water quality at the Firehall Well or other Keno City private wells will be affected by the mill or DSTF is insignificant. First, as discussed above:

- Seepage from the DSTF is very unlikely to reach the bedrock groundwater system.
- Second, pumping at the Firehall Well would have to lower the water table *in the area of PH6* by over 20m to reverse the groundwater flow direction from underneath the site towards Keno City. Such a decline in water table elevation at a distance of over one kilometre down gradient of the pumping well would require the entire local water table to be changed by a similar or greater magnitude. Currently, the aquifer appears to recharge during the low extraction season and effectively recover completely from higher extraction periods, thus indicating that wholesale lowering of the area water table is not occurring, or recovering on an annual basis.

6 Conclusions and Recommendations

Results from the groundwater investigation reported herein indicate that the water table within the bedrock aquifer under the site and within a relatively thick overburden aquifer to the south is at considerable depth. Water level data from monitoring wells at site and that collected from Well #3 in Keno City, the only well that could be accessed, indicate that groundwater flows from east to west, or from Keno City towards the site and Christal Lake, not towards Keno City or Lightning Creek from the site.

Water quality analyses of samples taken immediately following monitoring well development indicate that, in general, concentrations of dissolved anions and metals are low. The only notable exceptions are elevated concentrations of chloride and sodium in PH6, which is located down could be indicative of seepage from the city dump and elevated concentrations of sulphate in PH5 and PH6, which could be indicative of natural mineralization.

The likelihood of effects to groundwater quality in general related to the mill and DSTF are considered very low, due primarily to the site water management plans for seepage interception and diversion. Leakage from water management structures represents the only source of impacted waters to the environment.

The current plan for the mill does not involve groundwater extraction, thus there will be no effects on the amount of water available for extraction from the Keno City water supply well. The chance of water quality at the supply well or other Keno City private wells being affected by site outflow is considered insignificant due to the direction of the groundwater gradient and the large distance between the site and the supply well.

The following recommendations are presented:

- The groundwater monitoring wells should be checked monthly for the first year to determine if they remain accessible and not frozen.
- The groundwater monitoring wells should be sampled and water levels recorded twice annually, if not frozen. If frozen, the vibe wire transducers on PH6 and PH5 should be monitored quarterly.
- If the monitoring wells are found to freeze and remain frozen, the wells should be freeze protected or alternate methods should be implemented to allow groundwater monitoring.
- Following finalization of the mill and DSTF engineering, three monitoring points should be located within shallow sediments down gradient of the DSTF drainage ditches and mill pond to monitor for potential ditch leakage. These wells should be sampled twice during the summer.
- Samples should be analyzed for dissolved metals, anions and physical parameters.

7 References

Access (2009). Bellekeno Project, Mill Development and Operations Plan, Quartz Mining License QML-0009. Report prepared by Access Consulting Group for Alexco Keno Hill Mining Corp.

EBA (2010a). Preliminary Engineering Design and Management Plan, Dry-Stacked Tailings Facility, Bellekeno Mine Mill Site, Yukon. Report prepared for Alexco Resource Corp. EBA File # W14101178.003

EBA (2010b). Response to Water Board Questions, Water Management Preliminary Designs. Letter prepared for Alexco Resources Corp. EBA File # W14101178.003.

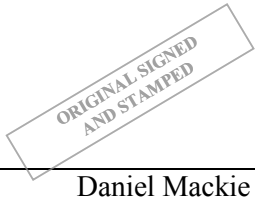
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SRK Consulting (Canada) Inc. (2009b). Assessment of Potential Groundwater Impacts from the Bellekeno Mill Site and Dry Stack Tailings Facility. Letter to Alexco Resource Corp. SRK Project # 1CE012.003.

SRK Consulting (Canada) Inc. (2009c). 2007/08 Geochemical Studies, Keno Hill Silver District, YT. Report prepared for Elsa Reclamation and Development Company Ltd. SRK Project # 1CE012.001.

This report **"2010 Bellekeno Groundwater Program"**, has been prepared by SRK Consulting (Canada) Inc.

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Reviewed by



Daryl Hockley
Principal

All data used as source material plus the text, tables, figures, and attachments of this document have been reviewed and prepared in accordance with generally accepted professional engineering and environmental practices.

Figures

Galkeno 900 Adit
and
Water Treatment Plant

Crystal
Lake

Trend of Flamed Moth Vein

Silver Trail Highway

Onek Mine

Hinton Creek

C-D Fault

BH15

BH18

BH16

BH20

BH22

BH19

BH21

PH2

BH23

PH6

City Dump

BH17

Mineral Creek

E Fault

BH25

BH24

PH5

Flamed & Moth Vein Fault

Duncan Creek Road

Lightning Creek

Keno City

Keno City Firehall Well

Keno Hotel Well

Well #1

Well #2

Well #3

Note:
Structures from Phillips (2002)
Fault and vein trends approximate

N

Meters

0 50 100 150 200

LEGEND

- New monitoring wells (Feb 2010)
- Keno City wells
- EBA geotechnical boreholes
- Thermistor Drillhole
- Tailings (Year 4)
- Ditch (Year 4)
- Roads
- Elevation (masl)

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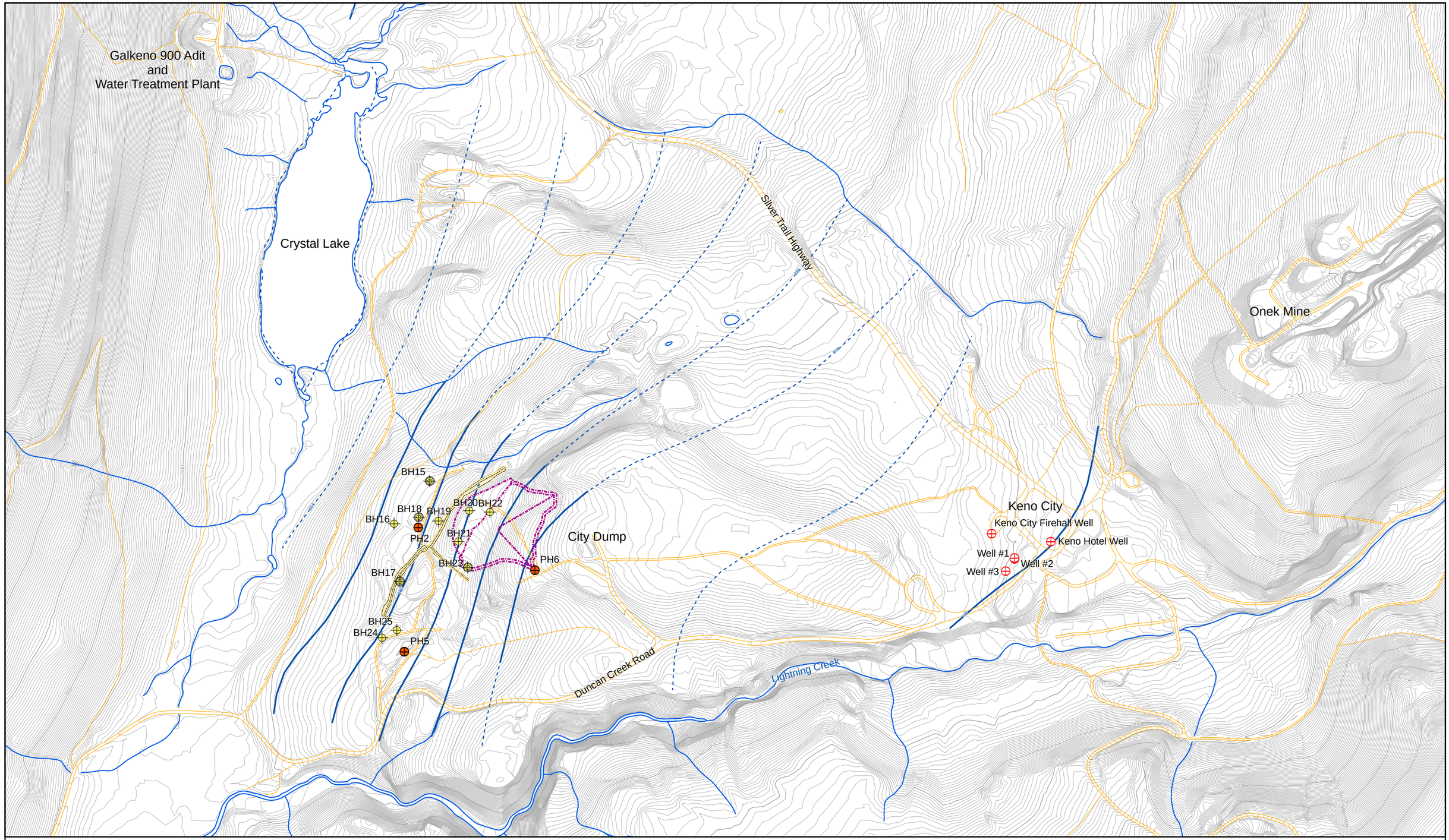
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SCALE:	1 inch = 583.3 feet			DATE:	03/16/2010
FILE NAME:	Fig1 - Bellekeno - Site Location map.mxd				

ALEXCO

Bellekeno Mine Project

DRAWING TITLE:	**Bellekeno Site Map And Well Locations**
ISSUED FOR:	**ALEXCO**
Revision No	**1**
SRK JOB NO.	**1CA009.003**
FIGURE	1



N

Meters

0 50 100 150 200

LEGEND

- New monitoring wells (Feb 2010)
- Keno City wells
- EBA geotechnical boreholes
- Thermistor Drillhole
- Tailings (Year 4)
- Ditch (Year 4)
- Water table (masl)
- Inferred water table (masl)
- Elevation (masl)

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UTM Zone 8N

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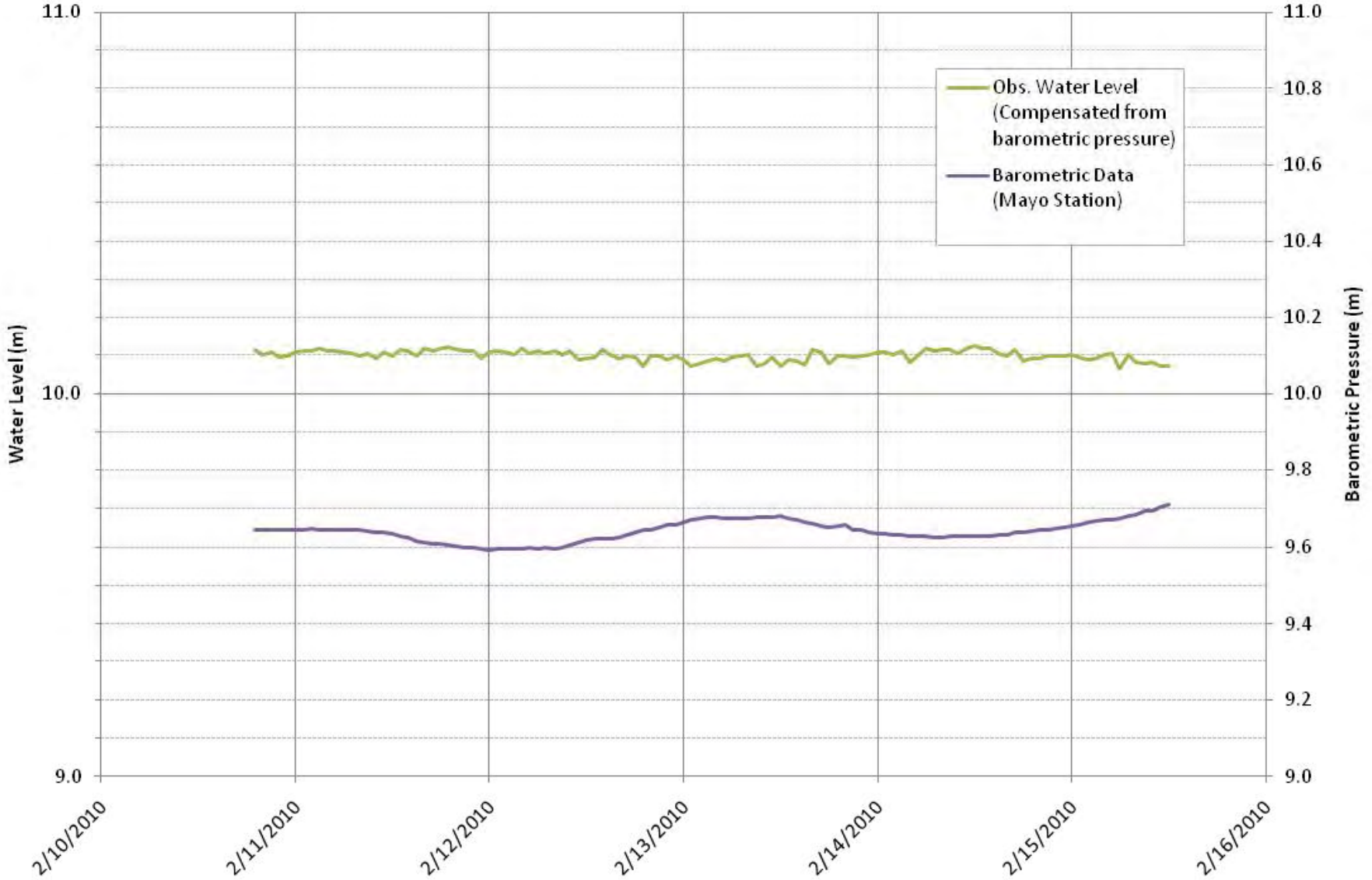
ALEXCO

Bellekeno Mine Project

DRAWING TITLE: **Interpreted Water Table**

ISSUED FOR:	ALEXCO	
Revision No	1	FIGURE 2
SRK JOB NO.	1CA009.003	

Path:



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ALEXCO

Compensated Vibewire Measurements at Well#3

Job No: 1CA009.003
Filename: Fig3_Well#3 monitoring GWL Observation.ppt

Bellekeno Mine Project

Date: March 2010
Approved: DM
Figure: 3

Galkeno 900 Adit
and
Water Treatment Plant

Cristal
Lake

Silver Trail Highway

Onek Mine

Keno City

Keno City Firehall Well

Keno Hotel Well

Well #1

Well #2

Well #3

BH15

BH16

BH17

BH18

BH19

BH20

BH21

BH22

BH23

BH24

BH25

PH2

PH5

PH6

City Dump

Duncan Creek Road

Lightning Creek

Bedrock surface

980 masl

830 masl

Bedrock surface shown as shaded relief under topographic contour lines. Bedrock surface interpreted from drill holes, observable ground features and local geology.

N

Meters

0 50 100 150 200

LEGEND

- New monitoring wells (Feb 2010)
- Keno City wells
- EBA geotechnical boreholes
- Thermistor Drillhole
- Tailings (Year 4)
- Ditch (Year 4)
- Elevation (masl)
- NE-SW Structures

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UTM Zone 8N

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SCALE:	1 inch = 583.3 feet			DATE:	03/16/2010
FILE NAME:	Fig4 - Bellekeno - Interp bedrock surface.mxd				

ALEXCO

Bellekeno Mine Project

DRAWING TITLE:	**Interpreted Bedrock Surface**
ISSUED FOR:	**ALEXCO**
Revision No	**1**
SRK JOB NO.	**1CA009.003**
FIGURE	4

Path:

Galkeno 300 Adit and Water Treatment Facility

+/-859.3

Crystal Lake

McLeod Creek

Silver Trail Highway

Onek 400 Adit

Onek Mine

Dry Stack Tailings Facility Footprint

PH2

PH6

PH5

Mill

Mill Pond

Mill Pad

Duncan Road Creek

Flow Direction

Lightning Creek

Firehall Well

Well #3

Keno Hill

Flow Direction

A

A'

B

B'

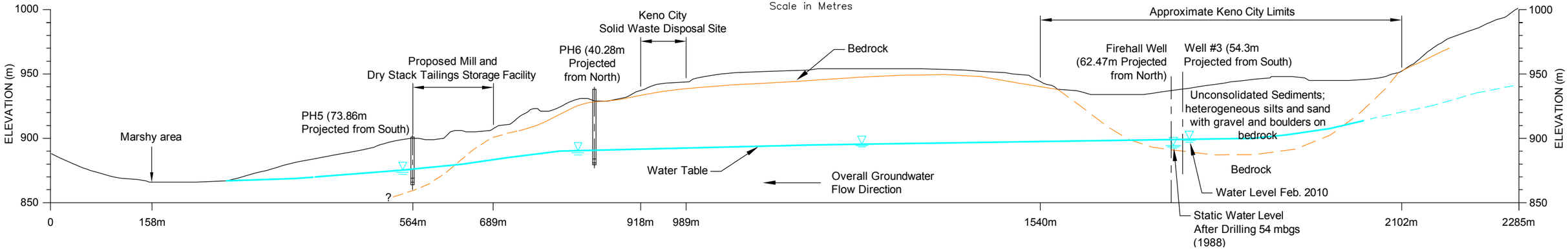
C

6

Plan View

0 100 200 300 400 500

Scale in Metres



CROSS SECTION A - A'

A

0 60 120 180 240 300

Horizontal Scale in Metres
Vertical Exaggeration X2

LEGEND

- Flow Direction
- Water Table Contour

NOTES

1. All units in metres
2. Coordinate system is NAD83, UTM Zone 8.
3. Water table contours from Figure 3.

SRK Consulting Engineers and Scientists Vancouver B.C.

SRK JOB NO.: 1CA009.003

FILE NAME: Bellekeno Plan Sec.dwg

ALEXCO

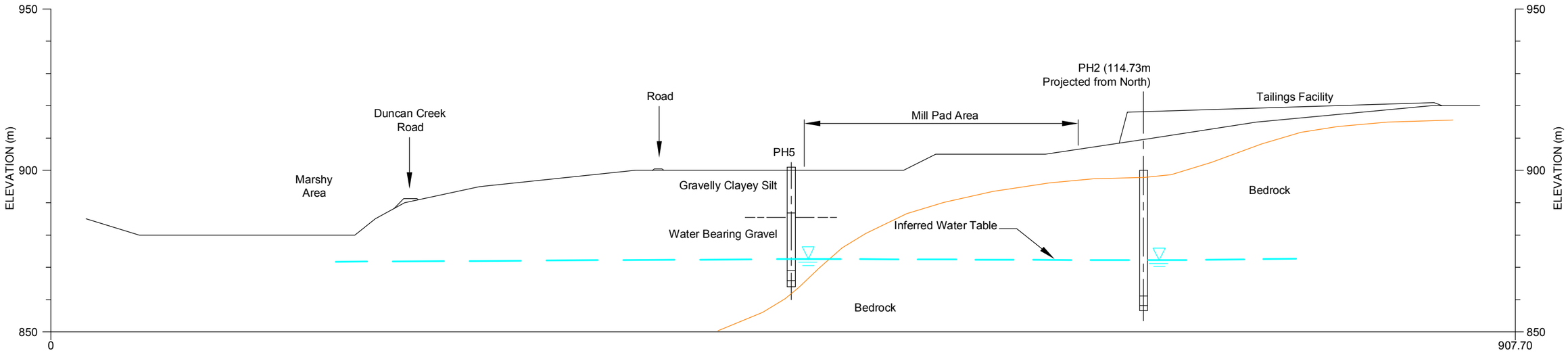
Bellekeno Mine Project

2010 Bellekeno Groundwater Investigation

Location Map and Cross Section A

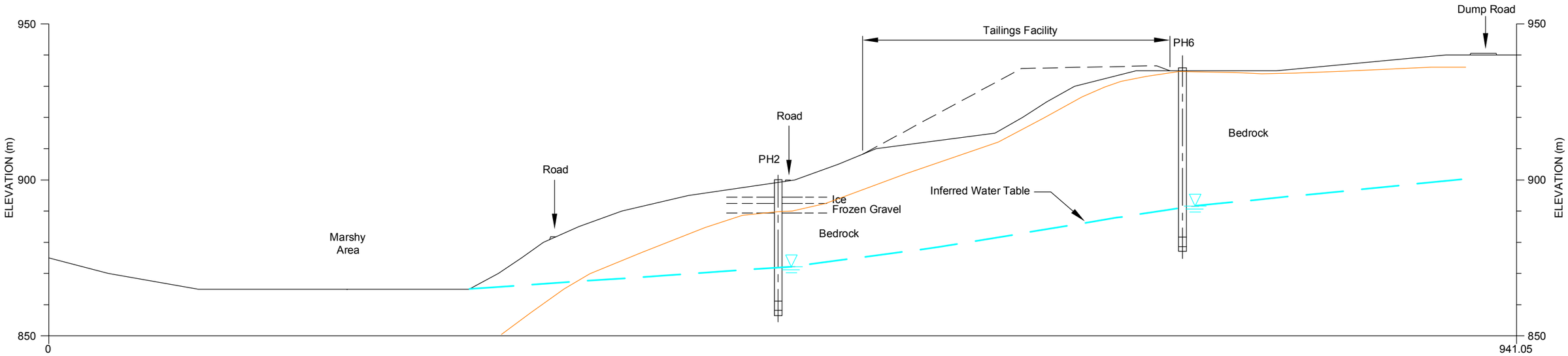
DATE:	APPROVED:	FIGURE:
Apr. 2010	DM	5

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B 5 CROSS SECTION B - B'

Vertical Exaggeration X2



C 5 CROSS SECTION C - C'

Vertical Exaggeration X2

NOTES

1. All units in metres
2. Coordinate system is NAD83, UTM Zone 8.

0 20 40 60 80 100

Scale in Metres

SRK Consulting Engineers and Scientists Vancouver B.C.

SRK JOB NO.: 1CA009.003

FILE NAME: Bellekeno Plan Sec.dwg

ALEXCO

Bellekeno Mine Project

2010 Bellekeno Groundwater Investigation

Cross Section B and C

DATE:	APPROVED:	FIGURE:
Apr. 2010	DM	6

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Appendices

Appendix A1
Firehall Well Log

Department of Environment

Water Resources Section
Yukon Water Well Registry
Box 1703, Whitehorse, Yukon, Y1A 2C6

WATER WELL DRILLING REPORT

Well ID: 213140003
Assigned by Dept. of Environment

The data contained in this report is supplied by the Driller. The Territory disclaims responsibility for its accuracy.
The information contained in this "Water Well Drilling Report" is unverified by YTG Yukon Water Resources Section.
If fields are empty, then no information was provided by the driller.

WELL LOCATION

Well Name: Keno City Firehall Well

The well name is simply an informal name given to a well upon it's completion.

Street Address of Well Location: Lot 48

Town/Village/Area/Lot#: KENO - Keno

UTM Coordinates of Well Location: 484993 m E 7086979 m N

NAD83 Zone 8

Accuracy of Well Location: 5 +/- m

Given that the well location may not be accurate, the above accuracy value represents the approximate error that might be associated with the actual well location.

Sketch of Well Location

This sketch has been provided by the driller and should be considered as an approximation of well location only.

The well was drilled for the following purpose: Commercial

Date the well was completed: 1987/08/22

The method used to drill the well: Rotary air

LOG OF OVERBURDEN AND BEDROCK MATERIALS

The following section describes the geological materials (as recorded by the driller) that were encountered when the well was first drilled.

Depth (m) From	Depth (m) To	General Colour	Most Common Material	Secondary Materials	General Description
0	4.267		SILT	Sand	
4.2672	14.02		SILT	Gravel and Cobbles	
14.021	23.77		SAND	Gravel and Cobbles	
23.774	33.22		SILT		
33.223	38.1		SAND	Gravel and Cobbles	
38.1	55.17		TILL	Cobbles and Boulders	
55.169	92.96		BEDROCK		

While drilling the well, was permafrost encountered? ☐ **If yes, the depth interval was:** from: m to m

WELL CONSTRUCTION

The following section provides information about the well construction details.

Monitor ID: 2131400031
For administrative purposes only

In what geological material (i.e. sand and gravel or bedrock) is the water producing zone of the well completed?

The outside diameter of the well casing: 152.4 cm

The casing material is made out of: Steel

The casing wall thickness is: mm

The casing extends in a depth below ground surface of: 57.3024 m

Other comments that were provided by the driller regarding the casing: Water from 190'; more from 298' to 301' and very loose ground

Surface/Environmental Seal A surface seal provides an impermeable seal between the casing and the ground in the upper 3 metres. This seal helps prevent surface water from leaking downward and into the well water.

Seal Material Type: **Diameter of Seal:** m **Seal Depth from:** m **Seal Depth to:** m

Gravel Pack A gravel pack is sometimes installed by the driller around the well screen. The purpose of a gravel pack could be to reduce sand production in the well water or to increase well yield.

Is there a gravel pack on the well? ☐

Gravel pack details (as provided by the driller):

Well Screen Infromation

Screened Interval from: 57.3024 m **to:** 92.964 m

The outside diameter of the screen is: 152.4 mm

Screen 1 Length: 35.6616 m **Slot Size 1:** thou. inch

The screen is made of:

Screen 2 Length: m **Slot Size 2:** thou. inch

The type of screen is: None

Screen 3 Length: m **Slot Size 3:** thou. inch

There are many types of well screens on the market. Wells with no screens or wells constructed in bedrock are called "OPEN HOLE".

Other useful comments about the screen:

WELL DEVELOPMENT AND STATUS

Following well construction, the well is developed or clean-out until clear groundwater is produced. Depending on the well yield and water quality, the well status is determined (i.e. the well is put into production or the well is abandoned). The following section provides information about Well Development and Status.

The well was developed by: Air surging

Once the well was constructed the following completion or "tie in" was constructed: None

The height of the well casing above ground surface construction (i.e. Well Stick-up) is: 0 m AGS

The static water level (i.e. non pumping condition) below top of casing is: 54.864 m

The estimated yield or production rate of the well is: 1.5154 L/s

After constructing and developing the well, the Well Status was: New, in use for intended purpose

If the well was abandoned, was the well properly filled (i.e. sealed) with bentonite grout? ☐ **If YES, date:**

Method used to estimate the well yield: Air lifting

PUMPING TEST RECORD AND GROUNDWATER QUALITY

Following well construction, the well may have been assessed for quality and/or tested to determine well yield or production rate. The following section provides this information if such assessment was done.

Pumping Test Information

Pumping Test Start Date:

Static Water Level (SWL): m

Pump was set at a depth of: m

Duration of pumping test: min

Final Water Level (FWL) at end of pumping test: m

Recommended Pump Depth and Flow Rate

Pump depth: m

Pump rate: L/s

Well Water Level Drawdown Data

Drawdown	
Time (min)	Level (m

If the well is flowing naturally under artesian pressure, the flow rate is: L/s

Groundwater Quality

Electrical Conductivity: uS pH: Temperature: C

Date Measurements Taken:

Was Bacteria Testing Conducted? ☐ Date Sample Taken Laboratory that conducted analysis:

Was Chemical Analysis Conducted? ☐ Date Sample Taken Laboratory that conducted analysis:

Groundwater Type (i.e. salty, rotten egg smell, iron staining):

Turbidity/sand content after development:

Well Disinfection:

Following well construction the well should be disinfected. Above briefly describes the method of disinfection.

WELL CONTRACTOR

The well contractor that drilled and constructed the well.

Name of Contractor/Drilling Company: Midnight Sun Drilling Company Limited

Name of Driller(s):

CONSULTANT

Consultants that may have been associated with the drilling/well construction.

Company Name:

Company Address:

Report Reference:

Appendix A2
Firehall Well Water Quality

Keno City Fire Hall Drinking Water Quality
(305' deep well - pump at 298')

Parameter	Units	04-Aug-99	04-Dec-99	24-Oct-00	19-Dec-01	23-Aug-02	16-Sep-03	02-Jul-04	16-Jun-05	20-Jun-06	18-Apr-08	GCDWQ	
Physical Tests													
Colour	CU	< 5	< 5	< 5	< 5	<5	<5	<5	<5	<5	<5	15	1
Conductivity	umhos/cm	411	385	384	358	440	569	559	535	527	562		
Total Dissolved Solids	mg/L	267	238	234	234	331	414	360	356	378	380	500	1
Hardness	mg/L $CaCO_3$	215	202	184	184	206	297	297	288	284	281	-	2
pH		7.69	7.67	7.91	8.08	7.93	8.17	7.85	7.83	8.08	7.72	6.5 - 8.5	1
Turbidity	NTU	0.8	0.4	0.6	<0.1	0.7	0.3	0.26	0.72	2.68	3.5	5	1,6
Dissolved Anions													
Alkalinity - Total	mg/L	122	112	122	111	125	168	166	156	148	147		
Chloride	mg/L	5.9	5	5.2	6.2	6.4	9.1	9.6	7.56	8.38	6.26	250	1
Fluoride	mg/L	0.07	0.09	0.2	0.03	0.04	0.04	0.038	0.053	0.046	<.1	1.5	
Sulphate	mg/L	82	70	70	67	88	136	120	121	123	129	500	1,5
Nutrients													
Nitrate Nitrogen	mg/L	1.9	1.7	1.6	1.67	1.6	1.6	1.68	1.55	1.83	1.61	10	
Nitrite Nitrogen	mg/L	< 0.1	< 0.1	< 0.1	<0.001	<0.1	<0.1	<0.1	<.001	<.001	<.002	1	
Total Metals													
Aluminum	mg/L	< 0.2	< 0.005	< 0.005	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	0.036		
Antimony	mg/L				<0.0005	<0.0005	<0.0005	<0.0005	<0.0005	<0.0005	<.001	0.006	4,5
Arsenic	mg/L	0.0027	0.0051	0.0055	0.003	0.002	0.001	0.003	0.00187	0.00238	0.005	0.01	
Barium	mg/L	0.11	0.144	0.122	0.11	0.12	0.15	0.157	0.139	0.134	0.14	1	
Boron	mg/L	< 0.1	< 0.05	< 0.05	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<.05	5	4
Cadmium	mg/L	0.0007	0.0007	0.0008	0.0007	0.0008	0.0011	0.00099	0.00094	0.00095	0.0009	0.005	
Calcium	mg/L	62.6	59.4	54.8	55.9	58.6	88.7	88	79.8	86.2	80.4		
Chromium	mg/L	< 0.01	< 0.001	< 0.001	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<.001	0.05	
Copper	mg/L	0.02	0.154	1.16[7]	<0.01	<0.01	<0.01	<0.01	0.0043	0.103	0.18	1	1,6
Iron	mg/L	0.11	0.03	0.09	<0.03	0.05	0.17	<0.03	0.071	1.98	0.42	0.3	1
Lead	mg/L	< 0.001	0.010	0.048[7]	<0.001	<0.001	<0.001	<0.001	<0.001	0.0015	<.001	0.01	5,6
Magnesium	mg/L	14.4	13.1	11.4	11.6	14.3	19.5	18.7	17.3	19.1	21.6		
Manganese	mg/L	< 0.005	< 0.001	0.002	0.002	<0.002	0.005	0.0025	0.0036	<0.002	0.004	0.05	1
Mercury	mg/L	< 0.00005	< 0.00005	< 0.00005	< 0.0002	<0.0002	<0.0002	<0.0002	<0.0002	<0.0002	<.02	0.001	
Potassium	mg/L	< 2	0.3	0.24	0.3	0.3	0.3	0.35	0.31	0.32	0.3		
Selenium	mg/L	0.002	0.002	< 0.003	0.002	0.002	0.002	0.0037	0.002	0.002	0.002	0.01	
Sodium	mg/L	2	1.8	1.96	2.1	2	3	2.6	2.3	2.4	2.43	200	1
Uranium	mg/L	0.00462	0.00478	0.00465	0.0037	0.0054	0.0125	0.0116	0.00959	0.00965	0.0067	0.02	4
Zinc	mg/L	0.510	0.159	0.383	0.47	0.26	0.31	0.224	0.135	0.183	0.16	5	1, 6
Dissolved Metals													
Aluminum	mg/L			< 0.005	<0.01								
Antimony	mg/L				<0.0005								
Arsenic	mg/L			0.0052	0.002							0.025	8
Barium	mg/L			0.122	0.11							1	
Boron	mg/L			< 0.05	<0.1							5	9
Cadmium	mg/L			0.0008	0.0007							0.005	
Calcium	mg/L			54.8	54.7								
Chromium	mg/L			< 0.001	<0.002							0.05	
Copper	mg/L			0.905	0.006							1	1,3
Iron	mg/L			0.06	<0.03							0.3	1
Lead	mg/L			0.035[6]	<0.001							0.01	3,7
Magnesium	mg/L			11.4	11.6								
Manganese	mg/L			0.002	<0.002							0.05	1
Mercury	mg/L			< 0.00005	<0.0002							0.001	
Potassium	mg/L			0.26	0.3								
Selenium	mg/L			< 0.003	0.002							0.01	
Sodium	mg/L			1.98	2.1							200	1
Uranium	mg/L			0.00458	0.0037							0.1	
Zinc	mg/L			0.356	0.43							5	1, 3

Notes:
< = less than the detection limit indicated.
GCDWQ = Guidelines for Canadian Drinking Water Quality.
All limits are Maximum Acceptable Concentration (MAC) unless otherwise indicated.
1. Aesthetic Objective (AO) (taste, odour, appearance, etc.)
2. 1 NTU maximum allowed for water entering distribution systems.
3. There may be a laxative effect in some individuals when sulphate levels exceed 500 mg/L.
4. Interim Maximum Acceptable Concentration (IMAC).
5. First drawn water may be high, flush system before sampling (MAC).
6. At point of consumption.
7. Dec 12/00 resampled: Cu 0.011mg/L, Lead <0.001mg/L. Taken at point of consumption (truck fill point).
Oct. 24/00 sample was collected as an attempt to collect untreated well water - not from a proper sample port.
Suspect the sample location was not properly flushed so that sediment in the pipe caused high levels of lead and copper.

Appendix A3
Review of Firehall Well and Water System

4.5 KENO CITY

4.5.1 GENERAL

Community Status: Unincorporated

Owner of System: Government of the Yukon

Location: The water system is located within the fire hall at the community.

System Description: In general, the system consists of a deep well, which supplies water to a steel storage reservoir in the fire hall where the water is batch-chlorinated. A service pump delivers from the reservoir to a second elevated reservoir located below the ceiling of the truck bay where water gravity discharges into the water truck. Water is delivered to 19 or 20 residents in the community. Some Elsa residents travel to Keno City for water pickup.

A second service pump supplies water to the nearby Community Centre through a buried, insulated water line. The Community Centre houses washrooms, showers and laundry facilities, which are used by local residents and summer visitors.

Contacts:

Owner: Engineering and Development Branch
Government of the Yukon
P. O. Box 2703, Whitehorse, Yukon Y1A 2C6

Ph. (867) 667-5195 Fax (867) 393-6216

Attention: Georgi Pearson, Manager, Community Operations
Dave Albisser, Community Services Officer

Operator: Mike Kokanov
Site 1, Box 22, Keno City, Yukon Y0B 1M0

Ph. (867) 995-2409 (c/o Mike Mancini)

4.5.2 WATER SOURCE

Water is obtained from a deep, drilled well located approximately 15 m from the fire hall. Well information is as follows:

Date of Construction: 1987 (by Midnight Sun Drilling Co. Ltd.)

Depth: 93 m (305 ft.)

Casing: Steel – 203 mm (8 in.) dia. to 36 m (117 ft.) and 152 mm (6 in.) casing into bedrock. Bedrock was located at 55 m (180 ft.).

Screen: No screen in bedrock

Static Level: 55 m (180 ft.)

Pump Location: 91 m (299 ft.)

Pump Specifications: Grundfos 15 SQ15C–290
1.5 hp (estimated)

Capacity: 0.95 to 1.3 L/s (12.5 to 16.7 Igpm.) discharge rate into reservoir

Wellhead Construction: The well casing terminates in an insulated and heated box of PWF construction. The discharge line from the cap extends into an insulated utilidor, which connects to the fire hall (see photos). The pump discharge pipe is heat-traced.

Observations and Comments: The wellhead appears to be fairly well constructed and properly protected from freezing. The box is in good condition and the metal cladding in the lid offers adequate protection from the elements. Past problems with runoff accumulating around the wellhead has resulted in some flooding within the box and around the wellhead. Evidence of this can be seen in the photo of the wellhead box interior. Ditching around the box has alleviated this problem by routing the runoff around and past the box. However, problems may again arise in the future if the ditch fills up with silt and allows water to enter the box again. A more permanent solution may be to install a french drain to collect drainage and carry it to an open discharge point.

The box has no means of locking it from unauthorized entry at present. As such, security should be improved.

The in-ground septic system is located on the opposite side of the fire hall, about 45 to 50 m from the well. As such, it does not meet the current requirement of 60 m separation.

4.5.3 WATER STORAGE, PUMPING AND TREATMENT FACILITIES

The current water supply facilities were constructed with the fire hall in 1988. The key system components include water storage, service pump to an overhead tank for trucked water, and a second service pump, which supplies piped water to the Community Centre. See Fig. 4.5.1 and photos.

4.5.3.1 Water Storage

Water from the well discharges through a 32 mm (1.25 in.) dia. plastic line into the floor-mounted reservoir at the end of the truck bay in the fire hall. The well pump is activated by reservoir float controls.

Primary Tank Description: Plywood reinforced fibreglass, 3.7 m (12 ft.) x 1.9 m (6.3 ft.) x 1.9 m (6.3 ft.) high, complete with access through a 610x610 (24 in. x 24 in.) square opening in the top. The total tank capacity is approximately 13,300 L (2,925 Igal.) and the normal high level volume, at 230 mm (9 in.) below the top, is about 11,700 L (2,574 Igal.).

FLOOR TANK FIRE

A second storage tank is situated below the ceiling and is filled by the service pump. A valve on the discharge line below the tank is used to fill the water truck by gravity.

Elevated Tank Description: Fibreglass – 5,455 L (1,200 Igal.). Access is provided at the top of the tank.

POTABLE WATER TANK

Observations and Comments: The elevated tank is difficult to access for cleaning and there are reports of past leaks, which have subsequently been repaired, having occurred in the tank.

4.5.3.2 Service Pumps (P–1 and P–2)

The service pump (P–1) draws chlorinated water from the storage tank and fills the elevated tank through a 50 mm (2 in.) dia. line. Pump specifications are as follows:

SAME

Specification: 1.5 hp Leroy Somer, Model 145JH (Centrifugal)

A similar pump (P–2) supplies water to an elevated tank in the adjacent fire truck bay. These pumps can function as standby pumps for each other, since each of them can serve both the water truck and fire truck tanks through appropriate valving.

4.5.3.3 Service Pump (P–3)

This pump draws chlorinated water from the storage tank and pumps it through a 50 mm (2 in.) dia. P.E. line to the Community Centre. It has the following characteristics:

SAME

Specification: 1.5 hp Armstrong 3/4 B (Centrifugal)

Capacity: 1.5 L/s @ 23 m TDH (24 USgpm @ 75 ft. TDH)

Water is obtained from a deep, drilled well located approximately 15 m from the fire hall. Well information is as follows:

Date of Construction: 1987 (by Midnight Sun Drilling Co. Ltd.)

Depth: 93 m (305 ft.)

Casing: Steel – 203 mm (8 in.) dia. to 36 m (117 ft.) and 152 mm (6 in.) casing into bedrock. Bedrock was located at 55 m (180 ft.).

Screen: No screen in bedrock

Static Level: 55 m (180 ft.)

Pump Location: 91 m (299 ft.)

Pump Specifications: Grundfos 15 SQ15C-290
1.5 hp (estimated)

Capacity: 0.95 to 1.3 L/s (12.5 to 16.7 Igpm.) discharge rate into reservoir

Wellhead Construction: The well casing terminates in an insulated and heated box of PWF construction. The discharge line from the cap extends into an insulated utilidor, which connects to the fire hall (see photos). The pump discharge pipe is heat-traced.

Observations and Comments: The wellhead appears to be fairly well constructed and properly protected from freezing. The box is in good condition and the metal cladding in the lid offers adequate protection from the elements. Past problems with runoff accumulating around the wellhead has resulted in some flooding within the box and around the wellhead. Evidence of this can be seen in the photo of the wellhead box interior. Ditching around the box has alleviated this problem by routing the runoff around and past the box. However, problems may again arise in the future if the ditch fills up with silt and allows water to enter the box again. A more permanent solution may be to install a french drain to collect drainage and carry it to an open discharge point.

The box has no means of locking it from unauthorized entry at present. As such, security should be improved.

The in-ground septic system is located on the opposite side of the fire hall, about 45 to 50 m from the well. As such, it does not meet the current requirement of 60 m separation.

Appendix B
2010 Drill Hole Logs

SRK Consulting
Engineers and Scientists

BOREHOLE LOG

PROJECT No: 1CA009.003
SITE: Bellekeno
CLIENT: Alexco Resource Corp.

DATE: Feb. 2010
LOGGED BY: Jacek Scibek
DRILL HOLE: PH2

EASTING: 483864
NORTHING: 7086952
ELEVATION: 898.5 masl

DEPTH (m)	ELEV (masl)	WELL	DESCRIPTION	LITHO SYMBOL	DETAILED LITHOGRAPHY	COMMENTS
0	898.5				Ground Surface	
			0.85 m stickup		Gravel	
	895.0				Till some water	
5			2" PVC		Ice	
					Gravel no water, frozen?	
	890.0					
10					Till dry	
					Bedrock	
	885.0					
15			bentonite chips to surface			
	880.0					
20						
	875.0					
25		27.86 m below TOC				
	870.0					
30						
	865.0		bentonite pellets			
35			sand			
	860.0		screen			39.6 m Producing water up to 20 L/min
40						
	855.0					
45						

NOTES: Coordinates are +/- 5m, they are from a handheld GPS. Elevations are +/- 1m, they are taken from a topo map.

	Reviewed By:	FILE

SRK Consulting
Engineers and Scientists

BOREHOLE LOG

PROJECT No: 1CA009.003
SITE: Bellekeno
CLIENT: Alexco Resource Corp.

DATE: Feb. 2010
LOGGED BY: Jacek Scibek
DRILL HOLE: PH5

EASTING: 483836
NORTHING: 7086707
ELEVATION: 900 masl

DEPTH (m)	ELEV (masl)	WELL	DESCRIPTION	LITHO SYMBOL	DETAILED LITHOGRAPHY	COMMENTS
-1	900.0		1.05 m stickup		Ground Surface	
					Gravel and Silt (till) dry, fine - coarse ang/sub ang, grey	
4	895.0		2" PVC			
					Silt with fine gravel (till) dark grey moist	
9	890.0				**Silt (clayey) and gravel (till)** dark grey moist	
14	885.0		bentonite pellets to surface		**Boulder** till with cobbles	
					Gravelly till with cobbles dry, then moist at 60 ft	
19	880.0					
					Hard till with gravel layers	
24	875.0					
					Gravel (fine-coarse) dry grey-brown	
					Silt and gravel (till) dark grey moist	
29	870.0		sand		**Gravel with silt (till)** wet	**30.5 m to 35.1 m producing water up to 15 L/min**
			screen		**Fine gravel and coarse sand** clean, angular, some Qz, still see sub-round f. gravel	
34	865.0	28.45 m below TOC			**Clean gravel**	**35.1 m to 36.0 m water producing**
39	860.0					

NOTES: Coordinates are +/- 5m, they are from a handheld GPS. Elevations are +/- 1m, they are taken from a topo map.

	Reviewed By:	FILE

SRK Consulting
Engineers and Scientists

BOREHOLE LOG

PROJECT No: 1CA009.003
SITE: Bellekeno
CLIENT: Alexco Resource Corp.

DATE: Feb. 2010
LOGGED BY: Jacek Scibek
DRILL HOLE: PH6

EASTING: 484104
NORTHING: 7086854
ELEVATION: 937.0 masl

DEPTH (m)	ELEV (masl)	WELL	DESCRIPTION	LITHO SYMBOL	DETAILED LITHOGRAPHY	COMMENTS
0	937.0		0.95 m stickup		Ground Surface	
					Overburden	
5	935.0				Bedrock	
	930.0		1" PVC			
10	925.0					
15	920.0					
20	915.0		grout to surface			
25	910.0					
30	905.0					
35	900.0					
40	895.0	44.31 m below TOC				
45	890.0					48.8 m a few liters of water were blown out after 30 min of recovery
50			bentonite chips			50.3 m a few liters blown out
	885.0		sand filter			53.3 m approx. 12 L blown out
55			screen			56.4 m approx. 20 L blown out after 2 min of recovery
	880.0					

NOTES: Coordinates are +/- 5m, they are from a handheld GPS. Elevations are +/- 1m, they are taken from a topo map.

	Reviewed By:	FILE

Appendix C
Vibrating Wire Calibration Sheets

rst INSTRUMENTS

Calibration Record

200 - 2050 Hartley Ave., Coquitlam, British Columbia, Canada V3K 6W5
Tel: 604.540.1100 • Fax: 604.540.1005 • Toll Free: 1.800.665.5599 (North America only)
e-mail: info@rstinstruments.com • Website: www.rstinstruments.com

IN

PH5

Vibrating Wire Piezometer

Customer:	ALEXCO RESOURCE CORPORATION	
Model:		VW2100-0.7
Serial Number:		**VW13099**
Mfg Number:		0927952
Range:		700.0 kPa
Temperature:		24.5 °C
Barometric Pressure:		999.6 millibars
W.O. Number:		Q015395
Cable Length:		60 meters
Cable Colour Code:	Red / Black (Coil)	Green / White (Thermistor)
Cable Type:		EL380004
Thermistor Type:		3 Kohms

Applied Pressure (kPa)	First Reading (B units)	Applied Pressure (kPa)	Second Reading (B units)	Average Pressure (kPa)	Average Readings (B units)	Calculated Linear (kPa)	Linearity F.S. Error (%)	Polynomial Fit (% FS)
0.0	9039	0.0	9040	0.0	9040	1.2	0.17	-0.02
140.0	8279	140.0	8281	140.0	8280	139.9	-0.01	0.03
280.0	7519	280.0	7519	280.0	7519	279.0	-0.15	0.00
420.0	6753	420.0	6753	420.0	6753	418.9	-0.16	-0.01
560.0	5983	560.0	5983	560.0	5983	559.5	-0.07	-0.03
700.0	5206	700.0	5206	700.0	5206	701.5	0.21	0.02
						Max. Error (%):	0.21	0.03

Linear Calibration Factor:	C.F.=	0.18267 kPa/B unit
Regression Zero:	At Calibration =	9046.1 B unit
Temperature Correction Factor:	Tk =	0.0740 kPa/°C rise

Polynomial Gage Factors (kPa) A: -6.8580E-07 B: -0.17290 C: 1618.8

Pressure is calculated with the following equations:
Linear, P(kPa) = C.F. X (Li - Lc) - [Tk (Ti - Tc)] + [0.10 (Bi - Bc)]
Polynomial: $P(kPa)=A(Lc)^2+BLc+C+Tk(Tc-Ti)-[0.10(Bc-Bi)]$

	Date (dd/mm/yr)	VW Readout Pos. B (Li)	Temp °C (Ti)	Baro (Bi)
Shipped Zero Readings:	19-Jan-10	9051	19.6	1085.4

Li, Lc = initial (at installation) and current readings
Ti, Tc = initial (at installation) and current temperature, in °C
Bi, Bc = initial (at installation) and current barometric pressure readings, in millibars
B units = B scale output of VW 2102, VW 2104, VW 2106 and DT 2011 readouts
B units = Hz^2 / 1000 ie: 1700Hz = 2890 B units

Technician: H. Chang Date: 19-Jan-10

This instrument has been calibrated using standards traceable to the NIST in compliance with ANSI Z540-1

Applied Science Technologists and Technicians of British Columbia
22724
A. C.
AL CULLEY
ASCT

Document Number.: ELL0130J

MIG0106A

rst INSTRUMENTS

Calibration Record

200 - 2050 Hartley Ave., Coquitlam, British Columbia, Canada V3K 6W5
Tel: 604.540.1100 • Fax: 604.540.1005 • Toll Free: 1.800.665.5599 (North America only)
e-mail: info@rstinstruments.com • Website: www.rstinstruments.com

Vibrating Wire Piezometer

19
PH6

Customer:	ALEXCO RESOURCE CORPORATION	
Model:	VW2100-0.7	
Serial Number:	**VW13100**	
Mfg Number:	0927953	
Range:	700.0	kPa
Temperature:	24.5	°C
Barometric Pressure:	999.6	millibars
W.O. Number:	Q015395	
Cable Length:	60	meters
Cable Colour Code:	Red / Black (Coil)	Green / White (Thermistor)
Cable Type:	EL380004	
Thermistor Type:	3	Kohms

Applied Pressure (kPa)	First Reading (B units)	Applied Pressure (kPa)	Second Reading (B units)	Average Pressure (kPa)	Average Readings (B units)	Calculated Linear (kPa)	Linearity F.S. Error (%)	Polynomial Fit (% FS)
0.0	8878	0.0	8880	0.0	8879	1.1	0.16	-0.01
140.0	8102	140.0	8103	140.0	8103	139.7	-0.04	0.00
280.0	7320	280.0	7321	280.0	7321	279.4	-0.09	0.04
420.0	6539	420.0	6540	420.0	6540	418.8	-0.16	-0.03
560.0	5751	560.0	5751	560.0	5751	559.6	-0.05	-0.02
700.0	4958	700.0	4958	700.0	4958	701.2	0.18	0.01
						Max. Error (%):	0.18	0.04

Linear Calibration Factor:	**C.F.=**	**0.17857 kPa/B unit**
Regression Zero:	**At Calibration =**	**8885.1** B unit
Temperature Correction Factor:	**Tk =**	**0.0542 kPa/°C rise**

Polynomial Gage Factors (kPa) **A:** -5.6285E-07 **B:** -0.17078 **C:** 1560.6

Pressure is calculated with the following equations:
Linear, P(kPa) = C.F. X (Li - Lc) - [Tk (Ti - Tc)] + [0.10 (Bi - Bc)]
Polynomial: $P(kPa)=A(Lc)^2+BLc+C+Tk(Tc-Ti)-[0.10(Bc-Bi)]$

	Date (dd/mm/yr)	VW Readout Pos. B (Li)	Temp °C (Ti)	Baro (Bi)
Shipped Zero Readings:	19-Jan-10	8890	19.6	1085.4

Li, Lc = initial (at installation) and current readings
Ti, Tc = initial (at installation) and current temperature, in °C
Bi, Bc = initial (at installation) and current barometric pressure readings, in millibars
B units = B scale output of VW 2102, VW 2104, VW 2106 and DT 2011 readouts
B units = Hz^2 / 1000 ie: 1700Hz = 2890 B units

Technician: H. Chang Date: 19-Jan-10

This instrument has been calibrated using standards traceable to the NIST in compliance with ANSI Z540-1

Applied Science Technologists and Technicians of British Columbia
22724
AL CULLEY
ASCT

Document Number.: ELL0130J

MIG0106A

Appendix D
2010 Drill Hole Water Quality

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Report Transmission Cover Page

Bill To:	Alexco Resource Corp.	Project:	
Report To:	Access Mining Consultants Ltd.	ID:	
	# 3 Calcite Business Centre	Name:	
	151 Industrial Road	Location:	
	Whitehorse, YT, Canada	LSD:	
	Y1A 2V3	P.O.:	
Attn:	Scott Keesey	Acct code:	ALEXCO 2701
Sampled By:	Jacek Sciber		
Company:	SRK		

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

Contact & Affiliation	Address	Delivery Commitments
Scott Keesey Access Mining Consultants Ltd.	151 Industrial Road, # 3 Calcite Business Whitehorse, Yukon Territory Y1A 2V3 Phone: (867) 668-6463 Fax: (867) 667-6680 Email: scott@accessconsulting.ca	On [Lot Verification] send (COA) by Email - Single Report On [Report Approval] send (COC, Test Report) by Email - Merge Reports On [Report Approval] send (Test Report) by Email - Single Report
Durand Cornett Access Mining Consultants Ltd.	151 Industrial Road, # 3 Calcite Business Whitehorse, Yukon Territory Y1A 2V3 Phone: (867) 668-6463 Fax: (867) 667-6680 Email: durand@accessconsulting.ca	On [Lot Verification] send (COA) by Email - Single Report On [Report Approval] send (COC, Test Report) by Email - Merge Reports On [Report Approval] send (Test Report) by Email - Single Report
Derek Meneghin Alexco Resource Corp.	1920 - 200 Granville Street Vancouver, British Columbia V6C 1S4 Phone: (604) 633-4888 Fax: null Email: dmeneghin@alexcoresource.com	On [Lot Approval and Final Test Report Approval] send (Invoice) by Email - Single Report
Tiffany Lunday Access Mining Consultants Ltd.	Suite 1150 - 200 Granville Street, Vancouver Vancouver, British Columbia V6C 1S4 Phone: (604) 633-4888 Fax: (604) 633-4887 Email: tlunday@alexcoresource.com	On [Report Approval] send (COC, Test Report) by Email - Merge Reports On [Report Approval] send (Test Report) by Email - Single Report
Ethan Allen Samplers Account	Whitehorse, Yukon Territory Y1A 2V3 Phone: (867) 668-6463 Fax: null Email: eallen@accessconsulting.ca	On [Report Approval] send (Test Report, COC) by Email - Merge Reports

Notes To Clients:

- Analysis was performed on samples 1-3 that exceeded the recommended holding time for pH, nitrate and nitrite analysis.

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Sample Custody

Bill To:	Alexco Resource Corp.	Project:	
Report To:	Access Mining Consultants Ltd.	ID:	
	# 3 Calcite Business Centre	Name:	
	151 Industrial Road	Location:	
	Whitehorse, YT, Canada	LSD:	
	Y1A 2V3	P.O.:	
Attn:	Scott Keesey	Acct code:	ALEXCO 2701
Sampled By:	Jacek Sciber		
Company:	SRK		

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

Sample Disposal Date: March 28, 2010

All samples will be stored until this date unless other instructions are received. Please indicate other requirements below and return this form to the address or fax number on the top of this page.

☐ Extend Sample Storage Until _____ (MM/DD/YY)

The following charges apply to extended sample storage:

Storage for an additional 30 days	$ 2.50 per sample
Storage for an additional 60 days	$ 5.00 per sample
Storage for an additional 90 days	$ 7.50 per sample

☐ Return Sample, collect, to the address below via:

- ☐ Greyhound
- ☐ DHL
- ☐ Purolator
- ☐ Other (specify) _____

Name _____
Company _____
Address _____
_____
Phone _____
Fax _____

Signature _____

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Analytical Report

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	Whitehorse, YT, Canada	LSD:	
	Y1A 2V3	P.O.:	
Attn:	Scott Keesey	Acct code:	ALEXCO 2701
Sampled By:	Jacek Sciber		
Company:	SRK		

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

Reference Number	727339-1	727339-2
Sample Date	Feb 14, 2010	Feb 14, 2010
Sample Time	NA	NA
Sample Location		
Sample Description	PH6-1	PH5-1
Matrix	Water	Water

Analyte		Units	Results	Results	Results	Nominal Detection Limit
Inorganic Nonmetallic Parameters						
Organic Carbon	Total Nonpurgeable	mg/L	1.4	1.2		0.5
Organic Carbon	Dissolved Nonpurgeable	mg/L	1.0	<0.5		0.5

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3 Calcite Business Centre
151 Industrial Road
Whitehorse, YT, Canada
Y1A 2V3
Attn: Scott Keesey
Sampled By: Jacek Sciber
Company: SRK

Project:
ID:
Name:
Location:
LSD:
P.O.:
Acct code: ALEXCO 2701

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

		Reference Number	727339-1	727339-2	727339-3	
		Sample Date	Feb 14, 2010	Feb 14, 2010	Feb 14, 2010	
		Sample Time	NA	NA	NA	
		Sample Location				
		Sample Description	PH6-1	PH5-1	Ph5-2	
		Matrix	Water	Water	Water	
Analyte		**Units**	**Results**	**Results**	**Results**	Nominal Detection Limit
Metals Dissolved						
Mercury	Total Dissolved	ug/L	<0.01	<0.01	<0.01	0.01
Aluminum	Dissolved	mg/L	<0.005	<0.005	<0.005	0.005
Antimony	Dissolved	mg/L	0.0407	<0.0002	<0.0002	0.0002
Arsenic	Dissolved	mg/L	0.0192	0.0003	0.0004	0.0002
Barium	Dissolved	mg/L	0.020	0.048	0.048	0.001
Beryllium	Dissolved	mg/L	<0.00004	<0.00004	<0.00004	0.00004
Bismuth	Dissolved	mg/L	<0.001	<0.001	<0.001	0.001
Boron	Dissolved	mg/L	<0.004	<0.004	<0.004	0.004
Cadmium	Dissolved	mg/L	<0.00001	0.00033	0.00035	0.00001
Chromium	Dissolved	mg/L	<0.0004	<0.0004	<0.0004	0.0004
Cobalt	Dissolved	mg/L	0.01890	0.00025	0.00026	0.00002
Copper	Dissolved	mg/L	<0.001	0.001	0.001	0.001
Iron	Dissolved	mg/L	<0.01	<0.01	<0.01	0.01
Lead	Dissolved	mg/L	<0.0001	<0.0001	<0.0001	0.0001
Lithium	Dissolved	mg/L	0.035	0.009	0.01	0.001
Manganese	Dissolved	mg/L	1.090	0.0148	0.0152	0.0002
Molybdenum	Dissolved	mg/L	0.0048	<0.0001	<0.0001	0.0001
Nickel	Dissolved	mg/L	0.078	0.005	0.006	0.001
Selenium	Dissolved	mg/L	<0.0006	0.0006	0.0007	0.0006
Silver	Dissolved	mg/L	<0.00001	<0.00001	<0.00001	0.00001
Strontium	Dissolved	mg/L	1.380	0.246	0.252	0.001
Sulfur	Dissolved	mg/L	318	76.5	78.6	0.2
Thallium	Dissolved	mg/L	<0.00001	<0.00001	<0.00001	0.00001
Thorium	Dissolved	mg/L	<0.0004	<0.0004	<0.0004	0.0004
Tin	Dissolved	mg/L	<0.0001	<0.0001	<0.0001	0.0001
Titanium	Dissolved	mg/L	0.0006	<0.0004	<0.0004	0.0004
Uranium	Dissolved	mg/L	0.1420	0.0031	0.0031	0.0004
Vanadium	Dissolved	mg/L	0.0002	<0.0001	<0.0001	0.0001
Zinc	Dissolved	mg/L	0.064	0.036	0.037	0.001
Zirconium	Dissolved	mg/L	0.0030	<0.0001	<0.0001	0.0001
Metals Total						
Aluminum	Total	mg/L	15.1	0.038	0.035	0.005
Antimony	Total	mg/L	0.024	<0.0002	<0.0002	0.0002
Arsenic	Total	mg/L	0.048	0.0012	0.0012	0.0002
Barium	Total	mg/L	0.10	0.051	0.049	0.001
Beryllium	Total	mg/L	0.0017	<0.00004	<0.00004	0.00004

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Analytical Report

Bill To: Alexco Resource Corp.
Report To: Access Mining Consultants Ltd.
3 Calcite Business Centre
151 Industrial Road
Whitehorse, YT, Canada
Y1A 2V3
Attn: Scott Keesey
Sampled By: Jacek Sciber
Company: SRK

Project:
ID:
Name:
Location:
LSD:
P.O.:
Acct code: ALEXCO 2701

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

		Reference Number	727339-1	727339-2	727339-3	
		Sample Date	Feb 14, 2010	Feb 14, 2010	Feb 14, 2010	
		Sample Time	NA	NA	NA	
		Sample Location				
		Sample Description	PH6-1	PH5-1	Ph5-2	
		Matrix	Water	Water	Water	
Analyte		**Units**	**Results**	**Results**	**Results**	Nominal Detection Limit
Metals Total - Continued						
Bismuth	Total	mg/L	<0.005	<0.001	<0.001	0.001
Boron	Total	mg/L	<0.02	<0.005	<0.005	0.004
Cadmium	Total	mg/L	0.00008	0.00037	0.00038	0.00001
Calcium	Total	mg/L	493	118	117	0.05
Chromium	Total	mg/L	0.0098	<0.0004	<0.0004	0.0004
Cobalt	Total	mg/L	0.0221	0.00032	0.00030	0.00002
Copper	Total	mg/L	0.006	0.002	0.001	0.001
Iron	Total	mg/L	12.4	0.157	0.149	0.01
Lead	Total	mg/L	0.010	0.0005	0.0004	0.0001
Lithium	Total	mg/L	0.04	0.01	0.01	0.001
Magnesium	Total	mg/L	136	32.3	32.0	0.05
Manganese	Total	mg/L	1.39	0.0209	0.0191	0.0002
Molybdenum	Total	mg/L	0.004	<0.0001	<0.0001	0.0001
Nickel	Total	mg/L	0.085	0.005	0.006	0.001
Phosphorus	Total	mg/L	0.10	<0.010	<0.010	0.01
Potassium	Total	mg/L	5.4	0.5	0.6	0.1
Selenium	Total	mg/L	<0.003	<0.0006	<0.0006	0.0006
Silicon	Total	mg/L	35.0	3.39	3.37	0.05
Silver	Total	mg/L	<0.00005	<0.00001	<0.00001	0.00001
Sodium	Total	mg/L	19.5	1.60	1.59	0.02
Strontium	Total	mg/L	1.36	0.256	0.251	0.001
Sulfur	Total	mg/L	404	96.4	99.0	0.1
Tellurium	Total	mg/L	<0.0005	<0.0001	<0.0001	0.0001
Thallium	Total	mg/L	0.00018	<0.00001	<0.00001	0.00001
Thorium	Total	mg/L	0.011	<0.0004	<0.0004	0.0004
Tin	Total	mg/L	<0.0005	<0.0001	<0.0001	0.0001
Uranium	Total	mg/L	0.167	0.0034	0.0034	0.0004
Vanadium	Total	mg/L	0.011	<0.0001	0.0001	0.0001
Zinc	Total	mg/L	0.37	0.042	0.038	0.001
Zirconium	Total	mg/L	0.0098	<0.0001	<0.0001	0.0001
Titanium	Total	mg/L	0.072	<0.001	0.002	0.001
Routine Water						
pH	@ 25 °C		7.10	6.85	6.79	
Electrical Conductivity		µS/cm at 25 C	2280	693	700	1
Calcium	Dissolved	mg/L	425	99.2	99.1	0.1
Magnesium	Dissolved	mg/L	144	27.0	27.0	0.1

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Analytical Report

Bill To:	Alexco Resource Corp.	Project:	
Report To:	Access Mining Consultants Ltd.	ID:	
	# 3 Calcite Business Centre	Name:	
	151 Industrial Road	Location:	
	Whitehorse, YT, Canada	LSD:	
	Y1A 2V3	P.O.:	
Attn:	Scott Keesey	Acct code:	ALEXCO 2701
Sampled By:	Jacek Sciber		
Company:	SRK		

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

Reference Number	727339-1	727339-2	727339-3
Sample Date	Feb 14, 2010	Feb 14, 2010	Feb 14, 2010
Sample Time	NA	NA	NA
Sample Location			
Sample Description	PH6-1	PH5-1	Ph5-2
Matrix	Water	Water	Water

Analyte		Units	Results	Results	Results	Nominal Detection Limit
Routine Water - Continued						
Phosphorus	Dissolved	mg/L	<0.01	0.01	<0.01	0.01
Potassium	Dissolved	mg/L	2.1	0.3	0.3	0.1
Silicon	Dissolved	mg/L	3.78	2.68	2.71	0.05
Sodium	Dissolved	mg/L	15.5	1.4	1.4	0.1
Bicarbonate		mg/L	590	100	100	5
Carbonate		mg/L	<6	<6	<6	6
Hydroxide		mg/L	<5	<5	<5	5
P-Alkalinity	as CaCO3	mg/L	<5	<5	<5	5
T-Alkalinity	as CaCO3	mg/L	482	93	93	5
Chloride	Dissolved	mg/L	9.18	0.54	0.58	0.02
Nitrate - N	Dissolved	mg/L	<0.01	0.16	0.15	0.01
Nitrite - N	Dissolved	mg/L	<0.01	<0.01	<0.01	0.01
Sulfate (SO4)	Dissolved	mg/L	953	229	236	0.6
Hardness	as CaCO3	mg/L	1650	359	358	5
Total Dissolved Solids	Calculated Value	mg/L	1850	422	428	1

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	# 3 Calcite Business Centre	Name:	
	151 Industrial Road	Location:	
	Whitehorse, YT, Canada	LSD:	
	Y1A 2V3	P.O.:	
Attn:	Scott Keesey	Acct code:	ALEXCO 2701
Sampled By:	Jacek Sciber		
Company:	SRK		

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

Reference Number	727339-4
Sample Date	Feb 15, 2010
Sample Time	NA
Sample Location	
Sample Description	PH2-1
Matrix	Water

Analyte		Units	Results	Results	Results	Nominal Detection Limit
Routine Water						
pH	@ 25 °C		7.28			
Electrical Conductivity		µS/cm at 25 C	1770			1

Approved by:

Andrew Garrard, BSc, PChem
General Manager

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Methodology and Notes

Bill To:	Alexco Resource Corp.	Project:	
Report To:	Access Mining Consultants Ltd.	ID:	
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	Whitehorse, YT, Canada	LSD:	
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Sampled By:	Jacek Sciber		
Company:	SRK		

Lot ID: **727339**
Control Number:
Date Received: Feb 18, 2010
Date Reported: Feb 26, 2010
Report Number: 1298606

Method of Analysis

Method Name	Reference		Method	Date Analysis Started	Location
Alk, pH, EC, Turb in water	APHA	*	Alkalinity - Titration Method, 2320 B	22-Feb-10	Exova Surrey
Alk, pH, EC, Turb in water	APHA	*	Conductivity, 2510	22-Feb-10	Exova Surrey
Alk, pH, EC, Turb in water	APHA	*	pH - Electrometric Method, 4500-H+ B	22-Feb-10	Exova Surrey
Anions by IEC in water (Surrey)	APHA	*	Ion Chromatography with Chemical Suppression of Eluent Cond., 4110 B	19-Feb-10	Exova Surrey
Carbon Organic (Dissolved) in water (DOC)	APHA		High-Temperature Combustion Method, 5310 B	22-Feb-10	Exova Edmonton
Carbon Organic (Total) in water (TOC)	APHA		High-Temperature Combustion Method, 5310 B	22-Feb-10	Exova Edmonton
Mercury Low Level (Total) in water	EPA	*	Mercury in Water by Cold Vapor Atomic Fluorescence Spectrometry, 245.7	22-Feb-10	Exova Surrey
Metals SemiTrace (Dissolved) in water	US EPA	*	Metals & Trace Elements by ICP-AES, 6010C	22-Feb-10	Exova Surrey
Metals SemiTrace (Total) in Water	US EPA	*	Metals & Trace Elements by ICP-AES, 6010C	22-Feb-10	Exova Surrey
Trace Metals (dissolved) in Water	US EPA	*	Determination of Trace Elements in Waters and Wastes by ICP-MS, 200.8	22-Feb-10	Exova Surrey
Trace Metals (dissolved) in Water	US EPA	*	Metals & Trace Elements by ICP-AES, 6010C	22-Feb-10	Exova Surrey
Trace Metals (Total) in Water	US EPA	*	Determination of Trace Elements in Waters and Wastes by ICP-MS, 200.8	22-Feb-10	Exova Surrey
Trace Metals (Total) in Water	US EPA	*	Metals & Trace Elements by ICP-AES, 6010C	22-Feb-10	Exova Surrey

** Reference Method Modified*

References

APHA	Standard Methods for the Examination of Water and Wastewater
EPA	Environmental Protection Agency Test Methods - US
US EPA	US Environmental Protection Agency Test Methods

Comments:

- Analysis was performed on samples 1-3 that exceeded the recommended holding time for pH, nitrate and nitrite analysis.

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Methodology and Notes

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UPDATED

Lab Copy

Chain-of-Custody Record - Analytical Request Form

From:	Send Samples For Analysis To:	eMail Confirmation and Results To:	Send Original Signed Lab Reports To:	Send Invoice To:
		dmackie@srk.com	SRK Consulting	SRK Consulting
Address:	Address:	eallen@accessconsulting.ca	Address: 2200 - 1066 West Hastings, Vancouver, BC, V6E 3X2	Address: 2200 - 1066 West Hastings, Vancouver, BC, V6E 3X2
Telephone:	Telephone:		Phone: (604) 681 4196	Phone: (604) 681 4196
Fax:	Fax:		Fax: (604) 687 5532	Fax: (604) 687 5532
Contact:	Contact:		Attn: Dan Mackie	Attn: Dan Mackie
Email:	Email:		Email: dmackie@srk.com	Email: dmackie@srk.com

Fields Notes:

All monitoring wells purged with waterra tubes and hydrolift until field parameters (EC, pH, Temp) stable and water clear, or not clearing any further.

Note: sample PH2-1 was from well not developed completely.

Sampled water was cold, close to 0 C, and stored for short time in +5C in vehicle.

FIELD SAMPLE INFORMATION | ***REQUESTED LAB SUITES (see reverse side for details)***

	G = Grab or C = Composite	Number of Containers	Conductivity & pH	TOC, DOC, Sulphide	Nutrients	Major Ions (incl. Alkalinity)	Physical Parameters (TDS, TSS)	Low Detection Total Metals	Total Metals	Low Detection Dissolved Metals	Dissolved Metals	Oil and Grease	Total Cyanide	Total Ammonia	Dissolved Arsenic by GFAA	Total Arsenic by GFAA	Speciation	Ra226	Total As, Cu, Pb, Ni, Zn	Dissolved As, Cu, Pb, Ni, Zn	Sample Control Number	Lab Sample ID	Sample Date (dd-mmm-yy)	Sample Time (hh:mm)	Matrix	Laboratory Comments	Sampler Comments
√ = Preserved :											√																
√ = Field Filtered :											√																
√ = 1-Day Rush :																											
		3	√	√		√			√		√									√		PH6-1	14-Feb-10	14:00		Diss Metals sample filtered .45 um filter + preserved with HCl	clear
		3	√	√		√			√		√									√		PH5-1	14-Feb-10	16:45		Diss Metals sample filtered .45 um filter + preserved with HCl	clear
		2	√						√		√											PH5-2	14-Feb-10	16:45		Diss Metals sample filtered .45 um filter + preserved with HCl	clear
		1	√																			PH2-1	15-Feb-10	10:00			cloudy grey

Relinquished by (Sampler Signature):	Date/Time:	Company:	Received by (Signature):	Company:
Jacek Scibek	Feb 15, 2010	SRK Consulting		
Relinquished by (Signature):	Date/Time:	Company:	Received by (Signature):	Company:

Sampler (Printed Name):	Sample Storage Temperature prior to Shipping (deg. C):	Sample Receipt Temperature (deg. C):	SAMPLE CONDITION (lab use only) Samples Received in Good Condition? Yes / No (If no, provide details.)
Jacek Scibek			

Lab Copy

Chain-of-Custody Record - Analytical Request Form

From: Alexco Resources

Address: #2 Calcite Business Centre	
Telephone:	
Fax:	
Contact:	
Email:	

Send Samples For Analysis To:

Address:	
Telephone:	
Fax:	
Contact:	
Email:	

eMail Confirmation and Results To:

dmackie@srk.com
eallen@accessconsulting.ca

Send Original Signed Lab Reports To:

Access Consulting Group
Address: #3 Calcite Business Centre, 151 Industrial Road, Whitehorse, Yukon Y1A 2V3
Phone: (867) 668-6463
Fax: (867) 667-6680
Attn: Ethan Allen
Email: eallen@accessconsulting.ca

Send Invoice To:

Access Consulting Group
Address: #3 Calcite Business Centre, 151 Industrial Road, Whitehorse, Yukon Y1A 2V3
Phone:
Fax:
Attn:
Email:

RECEIVED
FEB 18 2010

FIELD SAMPLE INFORMATION

Fields Notes:

All monitoring wells purged with waterra tubes and hydrolift until field parameters (EC, pH, Temp) stable and water clear, or not clearing any further.

Exception is PH2-1, where 160 liters of water was purged due to hydrolift failure. Water was clearing up and field parameters stable.

Sampled water was cold, close to 0 C, and stored for short time in +5C in vehicle.

REQUESTED LAB SUITES (see reverse side for details)

	G = Grab or C = Composite	Number of Containers	Conductivity & pH	TOC, DOC, Sulphide	Nutrients	Major Ions	Physical Parameters	Low Detection Total Metals	Total Metals	Low Detection Dissolved Metals	Dissolved Metals	Oil and Grease	Total Cyanide	Total Ammonia	Dissolved Arsenic by GFAA	Total Arsenic by GFAA	Speciation	Ra226	Total As, Cu, Pb, Ni, Zn	Dissolved As, Cu, Pb, Ni, Zn
√ = Preserved :											√									
√ = Field Filtered :											√									
√ = 1-Day Rush :																				

Sample Control Number	Lab Sample ID	Sample Date (dd-mmm-yy)	Sample Time (hh:mm)	Matrix	Laboratory Comments	Sampler Comments
	PH6-1	14-Feb-10	14:00		Diss Metals sample filtered .45 um filter + preserved with HCl	clear
	PH5-1	14-Feb-10	16:45		Diss Metals sample filtered .45 um filter + preserved with HCl	clear
	PH5-2	14-Feb-10	16:45		Diss Metals sample filtered .45 um filter + preserved with HCl	clear
	~~PH2-1~~	~~13-Feb-10~~	9:55			cloudy, only 160 liters of well purging

Relinquished by (Sampler Signature): Jacek Scibek	Date/Time: Feb 15, 2010	Company: SRK Consulting	Received by (Signature):
Relinquished by (Signature):	Date/Time:	Company:	Received by (Signature):
Sampler (Printed Name): Jacek Scibek	Sample Storage Temperature prior to Shipping (deg. C):	Sample Receipt Temperature (deg. C):	SAMPLE CONDITION (lab use only) Samples Received in Good Condition? Yes / No (If no, provide details.)

Company:

Company:

Alexco Keno Hill Mining Corp.

Groundwater Monitoring Plan

Water Use Licence QZ09-092

Appendix B

Flame and Moth 2010 Diamond Drill Logs

Flame and Moth Prospect
Diamond Drill Hole Details - 2010 Exploration

Hole_ID	Total Depth (m)	UTM Easting (m)	UTM Northing (m)	Elevation (m)	Collar Azimuth	Collar Dip	Date_Started	Date_Completed	Core_Size
K-10-0264	336.80	484131.84	7086649.76	927.98	306	-60	05/07/2010	20/07/2010	HQ
K-10-0271	347.47	484131.84	7086649.76	927.98	306	-70	21/07/2010	31/07/2010	HQ
K-10-0275	346.57	484131.54	7086649.51	927.98	328	-62	01/08/2010	24/08/2010	HQ
K-10-0285	324.31	484071.91	7086679.39	919.59	306	-50	25/08/2010	06/09/2010	HQ
K-10-0291	192.67	484101.25	7086870.75	936.78	285	-54	08/09/2010	13/09/2010	HQ
K-10-0295	313.94	484101.35	7086870.5	936.78	285	-80	13/09/2010	03/10/2010	HQ
K-10-0298	220.68	484101.5	7086870.4	936.78	250	-60	03/10/2010	11/10/2010	HQ
K-10-0299	306.32	484067.23	7086584.28	923.86	285	-68	05/10/2010	10/10/2010	HQ
K-10-0303	348.08	484067.96	7086584.23	923.85	285	-75	10/10/2010	19/10/2010	HQ
K-10-0304	252.07	484101.68	7086870.26	936.78	230	-75	11/10/2010	19/10/2010	HQ
K-10-0305	352.35	484076.44	7086582.7	924.14	340	-65	20/10/2010	30/10/2010	HQ
K-10-0312	388.93	484076.65	7086585.25	923.89	250	-55	30/10/2010	16/11/2010	HQ
K-10-0320	243.84	484076.45	7086586.09	923.99	290	-55	19/11/2010	26/11/2010	HQ

Lithology Descriptions

CHSCH	Chloritic Schist	Green, well foliated schist as described below (Schist). Similar in colour to typical greenstone.
CQTZT	Calcareous Quartzite	Quartzite, as described below, with carbonate as a main constituent.
CSCH	Calcareous Schist	Schist, as described below, with carbonate as the main constituent.
FLT	Fault	
GNST	Greenstone	Grayish green to dark green, schistose rocks commonly having a jointed, slabby appearance.
GSCH	Graphitic Schist	Grey to dark gray to black Schist, as described below, with graphite as a main constituent.
ICQS	Iintercalated carbonaceous quartzite schist	Very thinly bedded quartzite with regular dark, carbonaceous, mud-rich horizons or graphitic schist bands. Well-defined schistose fabric. Quartzite bands regularly greater than 1cm wide (3 or 4 cm is common). Has a greater proportion of quartzite and is more competent than graphitic schist; often breaks across foliation.
LMST	Limestone	Gray to black in colour when fresh, sometimes banded with irregular lense-like layers of white or buff carbonate. At times schistose in appearance.
MCQ	Massive carbonaceous quartzite	Very dark grey to black carbonaceous quartzite, usually massive.
OVB	Overburden	
PHY	Phyllite	Most are gray to black when fresh, and display a silky sheen on cleavage surfaces. They may show weak undulations on surfaces but generally cleave into plates better than do the schists. Quartz stringers and boudins may be present but are not nearly as abundant as in the schists.
QFP	Quartz Feldspar Porphyry	
QTZT	Quartzite	Fresh colours range from white to bluish grey. Bedding may be visible throughout, giving the unit a somewhat gneissoid (foliated) appearance. Some are very fine grained, with a sugary texture and resemble re-crystallized cherts. SCH may be interbedded throughout, but must comprise less than 10% of the unit in order to be considered massive Quartzite.
SCH	Schist, undivided	Fresh colours range from light to dark greyish black or green depending on the dominant mineral content. Fracture surfaces generally have a metallic sheen and show well developed schistose foliation. They contain plications, wrinkle laminations, small drag folds and crenulations. Most contain irregular masses of quartz as stringers or boudins. stringers or boudins. QTZT may be interbedded throughout, but must comprise less than 10% of the unit in order to be considered massive Schist.
SM	Stringer Mineralization	
SSCH	Sericite Schist	Light green Schist with sericite as the main constituent.
TQTZT	Thin bedded Quartzite	<30 cm thick bands or beds of QTZT, SCH or mixture
VM	Vein Mineralized	
VN	Vein	
VNLT	Veinlet	

Geotechnical Core Logging Guide

RQD (Rock Quality Data)

The sum of the length of all core pieces greater than 10 cm in length.

Rock Strength

R0	Extremely weak	Indented by thumbnail
R1	Very weak	Crumbles under firm blow of geology hammer, Peeled by pocket knife
R2	Weak	Shallow indentation under firm blow of geology hammer
R3	Medium strong	Fractured with single blow of geology hammer
R4	Strong	Requires more than one blow of geology hammer to fracture
R5	Very strong	Requires many blows of geology hammer to fracture
R6	Extremely strong	Can only be chipped with strong blows of geology hammer

Cemented Joint/Vein Strength

Drop test from knee height defects

1	Strong	- never breaks
2	Moderate	- sometimes breaks
3	Weak	- always breaks

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0264	0.00	46.02	OVB
K-10-0264	46.02	53.05	QTZT
K-10-0264	53.05	53.84	FLT
K-10-0264	53.84	55.17	QTZT
K-10-0264	55.17	58.08	QTZT
K-10-0264	58.08	59.85	ICQS
K-10-0264	59.85	65.28	TQTZT
K-10-0264	65.28	70.39	QTZT
K-10-0264	70.39	71.25	ICQS
K-10-0264	71.25	71.80	QTZT
K-10-0264	71.80	73.41	CHSCH
K-10-0264	73.41	73.95	GSCH
K-10-0264	73.95	74.95	CHSCH
K-10-0264	74.95	82.65	ICQS
K-10-0264	82.65	86.38	QTZT
K-10-0264	86.38	89.38	FLT
K-10-0264	89.38	91.03	TQTZT
K-10-0264	91.03	92.60	QTZT
K-10-0264	92.60	94.49	TQTZT
K-10-0264	94.49	102.29	QTZT
K-10-0264	102.29	106.41	TQTZT
K-10-0264	106.41	109.93	QTZT
K-10-0264	109.93	111.87	TQTZT
K-10-0264	111.87	114.12	QTZT
K-10-0264	114.12	120.42	CQTZT
K-10-0264	120.42	122.55	QTZT
K-10-0264	122.55	124.42	CQTZT
K-10-0264	124.42	128.49	QTZT
K-10-0264	128.49	129.54	CQTZT
K-10-0264	129.54	136.07	TQTZT
K-10-0264	136.07	136.88	ICQS
K-10-0264	136.88	138.84	QTZT
K-10-0264	138.84	141.08	CQTZT
K-10-0264	141.08	142.33	QTZT
K-10-0264	142.33	142.60	TQTZT
K-10-0264	142.60	143.01	CQTZT
K-10-0264	143.01	145.10	QTZT
K-10-0264	145.10	146.21	CQTZT
K-10-0264	146.21	152.12	ICQS
K-10-0264	152.12	157.44	CQTZT
K-10-0264	157.44	162.53	GNST
K-10-0264	162.53	164.52	QTZT
K-10-0264	164.52	165.70	ICQS
K-10-0264	165.70	167.80	QTZT
K-10-0264	167.80	168.58	ICQS
K-10-0264	168.58	170.67	QTZT
K-10-0264	170.67	171.62	TQTZT
K-10-0264	171.62	174.20	CQTZT
K-10-0264	174.20	176.74	TQTZT
K-10-0264	176.74	178.09	CHSCH
K-10-0264	178.09	185.69	QTZT
K-10-0264	185.69	189.70	ICQS
K-10-0264	189.70	195.05	TQTZT
K-10-0264	195.05	199.95	CQTZT
K-10-0264	199.95	204.01	TQTZT
K-10-0264	204.01	209.97	QTZT
K-10-0264	209.97	216.74	QTZT
K-10-0264	216.74	248.44	GNST
K-10-0264	248.44	251.87	VM
K-10-0264	251.87	254.59	VM
K-10-0264	254.59	254.99	VM
K-10-0264	254.99	256.41	TQTZT
K-10-0264	256.41	256.81	VN
K-10-0264	256.81	259.03	TQTZT
K-10-0264	259.03	263.51	ICQS
K-10-0264	263.51	270.20	QTZT
K-10-0264	270.20	271.46	GSCH
K-10-0264	271.46	282.12	TQTZT
K-10-0264	282.12	283.84	ICQS
K-10-0264	283.84	289.50	QTZT
K-10-0264	289.50	293.16	ICQS
K-10-0264	293.16	300.60	QTZT
K-10-0264	300.60	301.76	ICQS
K-10-0264	301.76	305.05	QTZT
K-10-0264	305.05	306.70	TQTZT
K-10-0264	306.70	316.07	QTZT
K-10-0264	316.07	319.02	TQTZT
K-10-0264	319.02	321.11	QTZT
K-10-0264	321.11	323.75	GSCH
K-10-0264	323.75	326.91	TQTZT
K-10-0264	326.91	328.49	GSCH
K-10-0264	328.49	336.80	QTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0264	47.55	49.07	1.52	1.13	74.34	0.00	0.00	HQ					
K-10-0264	49.07	50.60	1.53	1.41	92.16	0.48	31.37	HQ					
K-10-0264	50.60	52.12	1.52	1.30	85.53	0.28	18.42	HQ					
K-10-0264	52.12	53.64	1.52	1.34	88.16	0.00	0.00	HQ					
K-10-0264	53.64	55.17	1.53	1.40	91.50	0.61	39.87	HQ					
K-10-0264	55.17	56.69	1.52	1.26	82.89	0.23	15.13	HQ					
K-10-0264	56.69	58.22	1.53	1.23	80.39	0.41	26.80	HQ					
K-10-0264	58.22	59.74	1.52	1.45	95.39	0.26	17.11	HQ					
K-10-0264	59.74	60.05	0.31	0.46	148.39	0.33	106.45	HQ					
K-10-0264	60.05	61.26	1.21	0.80	66.12	0.00	0.00	HQ					
K-10-0264	61.26	62.79	1.53	1.50	98.04	0.93	60.78	HQ					
K-10-0264	62.79	64.47	1.68	1.52	90.48	0.69	41.07	HQ					
K-10-0264	64.47	65.84	1.37	1.28	93.43	0.53	38.69	HQ					
K-10-0264	65.84	68.88	3.04	3.02	99.34	2.53	83.22	HQ					
K-10-0264	68.88	71.93	3.05	2.72	89.18	1.19	39.02	HQ					
K-10-0264	71.93	74.98	3.05	2.98	97.70	0.52	17.05	HQ					
K-10-0264	74.98	77.42	2.44	2.41	98.77	0.24	9.84	HQ					
K-10-0264	77.42	78.03	0.61	0.51	83.61	0.00	0.00	HQ					
K-10-0264	78.03	81.08	3.05	2.84	93.11	1.23	40.33	HQ					
K-10-0264	81.08	83.52	2.44	2.27	93.03	0.72	29.51	HQ					
K-10-0264	83.52	84.12	0.60	0.51	85.00	0.28	46.67	HQ					
K-10-0264	84.12	85.95	1.83	2.24	122.40	0.70	38.25	HQ					
K-10-0264	85.95	87.17	1.22	0.58	47.54	0.15	12.30	HQ					
K-10-0264	87.17	88.39	1.22	0.37	30.33	0.00	0.00	HQ					
K-10-0264	88.39	90.22	1.83	1.57	85.79	0.13	7.10	HQ					
K-10-0264	90.22	92.66	2.44	2.18	89.34	0.60	24.59	HQ					
K-10-0264	92.66	93.57	0.91	0.35	38.46	0.00	0.00	HQ					
K-10-0264	93.57	95.10	1.53	1.77	115.69	0.50	32.68	HQ					
K-10-0264	95.10	96.32	1.22	0.82	67.21	0.32	26.23	HQ					
K-10-0264	96.32	98.15	1.83	1.86	101.64	0.38	20.77	HQ					
K-10-0264	98.15	99.36	1.21	1.01	83.47	0.50	41.32	HQ					
K-10-0264	99.36	100.74	1.38	1.22	88.41	0.83	60.14	HQ					
K-10-0264	100.74	102.41	1.67	1.51	90.42	0.45	26.95	HQ					
K-10-0264	102.41	104.24	1.83	1.65	90.16	0.42	22.95	HQ					
K-10-0264	104.24	105.46	1.22	1.00	81.97	0.00	0.00	HQ					
K-10-0264	105.46	106.22	0.76	0.42	55.26	0.00	0.00	HQ					
K-10-0264	106.22	108.51	2.29	1.97	86.03	0.47	20.52	HQ					
K-10-0264	108.51	111.56	3.05	2.65	86.89	1.06	34.75	HQ					
K-10-0264	111.56	114.60	3.04	2.77	91.12	1.41	46.38	HQ					
K-10-0264	114.60	117.65	3.05	2.90	95.08	2.15	70.49	HQ					
K-10-0264	117.65	117.96	0.31	0.36	116.13	0.33	106.45	HQ					
K-10-0264	117.96	118.87	0.91	0.99	108.79	0.73	80.22	HQ					
K-10-0264	118.87	120.70	1.83	0.54	29.51	0.31	16.94	NQ					
K-10-0264	120.70	123.44	2.74	2.86	104.38	1.96	71.53	NQ					
K-10-0264	123.44	126.49	3.05	2.87	94.10	1.96	64.26	NQ					
K-10-0264	126.49	129.54	3.05	3.01	98.69	2.51	82.30	NQ					
K-10-0264	129.54	132.74	3.20	2.91	90.94	1.33	41.56	NQ					
K-10-0264	132.74	135.79	3.05	3.03	99.34	1.92	62.95	NQ					
K-10-0264	135.79	138.84	3.05	2.90	95.08	1.97	64.59	NQ					
K-10-0264	138.84	141.88	3.04	2.87	94.41	2.39	78.62	NQ					
K-10-0264	141.88	144.93	3.05	2.86	93.77	1.70	55.74	NQ					
K-10-0264	144.93	147.98	3.05	2.80	91.80	0.72	23.61	NQ					
K-10-0264	147.98	151.03	3.05	2.90	95.08	1.14	37.38	NQ					
K-10-0264	151.03	153.31	2.28	2.56	112.28	1.52	66.67	NQ					
K-10-0264	153.31	154.08	0.77	0.24	31.17	0.20	25.97	NQ					
K-10-0264	154.08	157.28	3.20	2.40	75.00	1.15	35.94	NQ					
K-10-0264	157.28	160.32	3.04	3.05	100.33	2.68	88.16	NQ					
K-10-0264	160.32	163.37	3.05	2.90	95.08	2.45	80.33	NQ					
K-10-0264	163.37	166.42	3.05	2.83	92.79	1.46	47.87	NQ					
K-10-0264	166.42	169.47	3.05	2.90	95.08	2.23	73.11	NQ					
K-10-0264	169.47	172.52	3.05	3.05	100.00	2.15	70.49	NQ					
K-10-0264	172.52	175.52	3.00	2.85	95.00	1.87	62.33	NQ					
K-10-0264	175.52	178.61	3.09	2.90	93.85	1.36	44.01	NQ					
K-10-0264	178.61	181.66	3.05	2.92	95.74	2.08	68.20	NQ					
K-10-0264	181.66	184.71	3.05	2.81	92.13	1.23	40.33	NQ					
K-10-0264	184.71	187.76	3.05	2.90	95.08	1.58	51.80	NQ					
K-10-0264	187.76	188.52	0.76	0.58	76.32	0.12	15.79	NQ					
K-10-0264	188.52	190.80	2.28	1.95	85.53	0.26	11.40	NQ					
K-10-0264	190.80	192.02	1.22	0.70	57.38	0.00	0.00	NQ					
K-10-0264	192.02	193.85	1.83	1.32	72.13	0.31	16.94	NQ					
K-10-0264	193.85	196.29	2.44	2.00	81.97	0.62	25.41	NQ					
K-10-0264	196.29	199.34	3.05	3.07	100.66	1.58	51.80	NQ					
K-10-0264	199.34	199.95	0.61	0.65	106.56	0.00	0.00	NQ					
K-10-0264	199.95	203.00	3.05	2.90	95.08	1.46	47.87	NQ					
K-10-0264	203.00	206.04	3.04	3.00	98.68	2.60	85.53	NQ					
K-10-0264	206.04	209.09	3.05	3.05	100.00	2.60	85.25	NQ					
K-10-0264	209.09	212.14	3.05	2.95	96.72	1.50	49.18	NQ					
K-10-0264	212.14	215.19	3.05	3.00	98.36	2.24	73.44	NQ					
K-10-0264	215.19	218.24	3.05	3.00	98.36	2.48	81.31	NQ					
K-10-0264	218.24	221.28	3.04	3.05	100.33	2.97	97.70	NQ					
K-10-0264	221.28	224.33	3.05	3.08	100.98	2.97	97.38	NQ					
K-10-0264	224.33	227.38	3.05	2.90	95.08	2.90	95.08	NQ					
K-10-0264	227.38	230.43	3.05	3.10	101.64	3.04	99.67	NQ					
K-10-0264	230.43	233.48	3.05	3.08	100.98	2.08	68.20	NQ					
K-10-0264	233.48	236.52	3.04	3.00	98.68	2.70	88.82	NQ					
K-10-0264	236.52	239.57	3.05	3.05	100.00	2.98	97.70	NQ					
K-10-0264	239.57	242.62	3.05	3.00	98.36	3.00	98.36	NQ					
K-10-0264	242.62	245.67	3.05	3.00	98.36	1.79	58.69	NQ					
K-10-0264	245.67	248.72	3.05	3.00	98.36	2.26	74.10	NQ					
K-10-0264	248.72	251.76	3.04	3.02	99.34	2.55	83.88	NQ					
K-10-0264	251.76	254.81	3.05	3.00	98.36	2.80	91.80	NQ					
K-10-0264	254.81	257.86	3.05	2.90	95.08	1.26	41.31	NQ					
K-10-0264	257.86	260.91	3.05	3.03	99.34	0.82	26.89	NQ					
K-10-0264	260.91	263.96	3.05	2.90	95.08	0.74	24.26	NQ					
K-10-0264	263.96	265.18	1.22	1.07	87.70	0.73	59.84	NQ					
K-10-0264	265.18	266.79	1.61	1.60	99.38	0.50	31.06	NQ					
K-10-0264	266.79	267.00	0.21	0.09	42.86	0.00	0.00	NQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0264	267.00	270.05	3.05	2.83	92.79	2.09	68.52	NQ					
K-10-0264	270.05	273.10	3.05	2.80	91.80	0.96	31.48	NQ					
K-10-0264	273.10	276.15	3.05	2.86	93.77	0.77	25.25	NQ					
K-10-0264	276.15	277.37	1.22	0.72	59.02	0.00	0.00	NQ					
K-10-0264	277.37	279.20	1.83	1.35	73.77	0.10	5.46	NQ					
K-10-0264	279.20	282.24	3.04	2.80	92.11	0.70	23.03	NQ					
K-10-0264	282.24	285.29	3.05	2.86	93.77	0.55	18.03	NQ					
K-10-0264	285.29	288.34	3.05	2.90	95.08	1.69	55.41	NQ					
K-10-0264	288.34	291.39	3.05	3.00	98.36	1.15	37.70	NQ					
K-10-0264	291.39	294.28	2.89	2.40	83.04	0.80	27.68	NQ					
K-10-0264	294.28	297.33	3.05	3.05	100.00	1.86	60.98	NQ					
K-10-0264	297.33	297.48	0.15	0.18	120.00	0.14	93.33	NQ					
K-10-0264	297.48	298.18	0.70	0.85	121.43	0.55	78.57	NQ					
K-10-0264	298.18	300.53	2.35	2.00	85.11	0.90	38.30	NQ					
K-10-0264	300.53	303.58	3.05	3.00	98.36	1.22	40.00	NQ					
K-10-0264	303.58	306.63	3.05	3.00	98.36	1.44	47.21	NQ					
K-10-0264	306.63	309.68	3.05	3.05	100.00	1.98	64.92	NQ					
K-10-0264	309.68	312.72	3.04	3.05	100.33	1.87	61.51	NQ					
K-10-0264	312.72	315.77	3.05	2.80	91.80	1.78	58.36	NQ					
K-10-0264	315.77	318.82	3.05	2.75	90.16	1.00	32.79	NQ					
K-10-0264	318.82	321.87	3.05	3.00	98.36	1.55	50.82	NQ					
K-10-0264	321.87	324.92	3.05	2.85	93.44	0.50	16.39	NQ					
K-10-0264	324.92	327.05	2.13	1.70	79.81	0.61	28.64	NQ					
K-10-0264	327.05	330.71	3.66	2.33	63.66	0.99	27.05	NQ					
K-10-0264	330.71	333.76	3.05	2.82	92.46	1.34	43.93	NQ					
K-10-0264	333.76	336.79	3.03	2.95	97.36	0.54	17.82	NQ					

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0271	0.00	12.55	OVB
K-10-0271	12.55	14.07	CQTZT
K-10-0271	14.07	16.58	TQTZT
K-10-0271	16.58	18.68	TQTZT
K-10-0271	18.68	28.57	TQTZT
K-10-0271	28.57	31.85	TQTZT
K-10-0271	31.85	33.62	ICQS
K-10-0271	33.62	34.86	QTZT
K-10-0271	34.86	37.55	TQTZT
K-10-0271	37.55	39.23	ICQS
K-10-0271	39.23	39.62	SSCH
K-10-0271	39.62	40.67	GSCH
K-10-0271	40.67	42.67	FLT
K-10-0271	42.67	44.55	GSCH
K-10-0271	44.55	45.00	QTZT
K-10-0271	45.00	47.90	TQTZT
K-10-0271	47.90	52.68	QTZT
K-10-0271	52.68	59.20	TQTZT
K-10-0271	59.20	66.34	QTZT
K-10-0271	66.34	69.30	SSCH
K-10-0271	69.30	72.10	ICQS
K-10-0271	72.10	79.20	TQTZT
K-10-0271	79.20	81.42	FLT
K-10-0271	81.42	91.33	TQTZT
K-10-0271	91.33	92.03	FLT
K-10-0271	92.03	93.10	CQTZT
K-10-0271	93.10	95.53	ICQS
K-10-0271	95.53	96.98	CQTZT
K-10-0271	96.98	100.42	QTZT
K-10-0271	100.42	101.25	ICQS
K-10-0271	101.25	105.25	QTZT
K-10-0271	105.25	108.35	CQTZT
K-10-0271	108.35	109.98	GSCH
K-10-0271	109.98	118.50	QTZT
K-10-0271	118.50	119.74	ICQS
K-10-0271	119.74	125.90	CQTZT
K-10-0271	125.90	126.80	FLT
K-10-0271	126.80	130.89	TQTZT
K-10-0271	130.89	132.32	ICQS
K-10-0271	132.32	142.60	TQTZT
K-10-0271	142.60	144.33	ICQS
K-10-0271	144.33	150.10	GNST
K-10-0271	150.10	151.13	ICQS
K-10-0271	151.13	152.90	QTZT
K-10-0271	152.90	159.68	TQTZT
K-10-0271	159.68	166.73	QTZT
K-10-0271	166.73	167.35	GNST
K-10-0271	167.35	170.48	TQTZT
K-10-0271	170.48	178.03	QTZT
K-10-0271	178.03	183.73	TQTZT
K-10-0271	183.73	188.50	CQTZT
K-10-0271	188.50	190.61	TQTZT
K-10-0271	190.61	192.12	ICQS
K-10-0271	192.12	197.42	QTZT
K-10-0271	197.42	198.46	QTZT
K-10-0271	198.46	202.60	ICQS
K-10-0271	202.60	251.23	GNST
K-10-0271	251.23	254.57	CHSCH
K-10-0271	254.57	255.40	SSCH
K-10-0271	255.40	264.78	GNST
K-10-0271	264.78	278.33	TQTZT
K-10-0271	278.33	281.88	GNST
K-10-0271	281.88	281.99	VM
K-10-0271	281.99	286.07	GNST
K-10-0271	286.07	288.07	ICQS
K-10-0271	288.07	291.67	TQTZT
K-10-0271	291.67	310.14	ICQS
K-10-0271	310.14	318.30	TQTZT
K-10-0271	318.30	319.03	VN
K-10-0271	319.03	322.10	VM
K-10-0271	322.10	324.32	VM
K-10-0271	324.32	327.00	VM
K-10-0271	327.00	332.12	VM
K-10-0271	332.12	335.17	VM
K-10-0271	335.17	335.96	VN
K-10-0271	335.96	339.14	GNST
K-10-0271	339.14	342.62	QTZT
K-10-0271	342.62	347.47	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0271	0.00	5.79	5.79					HQ					
K-10-0271	5.79	7.62	1.83					HQ					
K-10-0271	7.62	8.84	1.22					HQ					
K-10-0271	8.84	9.14	0.30					HQ					
K-10-0271	9.14	9.75	0.61					HQ					
K-10-0271	9.75	10.97	1.22					HQ					
K-10-0271	10.97	12.50	1.53					HQ					
K-10-0271	12.50	14.02	1.52	1.48	97.37	0.31	20.39	HQ					
K-10-0271	14.02	17.07	3.05	2.99	98.03	0.87	28.52	HQ					
K-10-0271	17.07	18.59	1.52	1.61	105.92	0.92	60.53	HQ					
K-10-0271	18.59	20.12	1.53	1.47	96.08	0.35	22.88	HQ					
K-10-0271	20.12	21.64	1.52	1.60	105.26	0.95	62.50	HQ					
K-10-0271	21.64	23.16	1.52	1.50	98.68	0.53	34.87	HQ					
K-10-0271	23.16	26.21	3.05	3.10	101.64	2.10	68.85	HQ					
K-10-0271	26.21	29.26	3.05	3.11	101.97	1.37	44.92	HQ					
K-10-0271	29.26	32.31	3.05	3.08	100.98	1.58	51.80	HQ					
K-10-0271	32.31	35.36	3.05	2.93	96.07	0.98	32.13	HQ					
K-10-0271	35.36	37.80	2.44	2.73	111.89	0.42	17.21	HQ					
K-10-0271	37.80	38.40	0.60	0.60	100.00	0.14	23.33	HQ					
K-10-0271	38.40	39.93	1.53	1.54	100.65	0.00	0.00	HQ					
K-10-0271	39.93	41.45	1.52	1.58	103.95	0.10	6.58	HQ					
K-10-0271	41.45	42.67	1.22	1.15	94.26	0.00	0.00	HQ					
K-10-0271	42.67	44.50	1.83	1.57	85.79	0.10	5.46	HQ					
K-10-0271	44.50	47.55	3.05	2.96	97.05	0.00	0.00	HQ					
K-10-0271	47.55	50.66	3.11	3.01	96.78	0.12	3.86	HQ					
K-10-0271	50.66	53.64	2.98	3.24	108.72	0.63	21.14	HQ					
K-10-0271	53.64	56.69	3.05	3.08	100.98	1.19	39.02	HQ					
K-10-0271	56.69	59.44	2.75	2.96	107.64	0.63	22.91	HQ					
K-10-0271	59.44	62.48	3.04	3.26	107.24	0.73	24.01	HQ					
K-10-0271	62.48	65.68	3.20	3.12	97.50	0.37	11.56	HQ					
K-10-0271	65.68	65.99	0.31	0.32	103.23	0.00	0.00	HQ					
K-10-0271	65.99	67.21	1.22	0.93	76.23	0.25	20.49	HQ					
K-10-0271	67.21	68.88	1.67	1.90	113.77	0.22	13.17	HQ					
K-10-0271	68.88	70.87	1.99	2.19	110.05	0.13	6.53	HQ					
K-10-0271	70.87	71.93	1.06	0.94	88.68	0.00	0.00	HQ					
K-10-0271	71.93	74.68	2.75	2.64	96.00	0.52	18.91	HQ					
K-10-0271	74.68	74.98	0.30	0.25	83.33	0.00	0.00	HQ					
K-10-0271	74.98	76.99	2.01	2.10	104.48	0.73	36.32	HQ					
K-10-0271	76.99	78.03	1.04	1.03	99.04	0.00	0.00	HQ					
K-10-0271	78.03	79.25	1.22	0.97	79.51	0.12	9.84	HQ					
K-10-0271	79.25	80.62	1.37	1.50	109.49	0.00	0.00	HQ					
K-10-0271	80.62	81.08	0.46	0.40	86.96	0.00	0.00	HQ					
K-10-0271	81.08	82.69	1.61	1.77	109.94	0.00	0.00	HQ					
K-10-0271	82.69	84.12	1.43	1.39	97.20	0.13	9.09	HQ					
K-10-0271	84.12	87.17	3.05	3.25	106.56	0.44	14.43	HQ					
K-10-0271	87.17	89.15	1.98	2.20	111.11	0.30	15.15	HQ					
K-10-0271	89.15	90.22	1.07	1.05	98.13	0.25	23.36	HQ					
K-10-0271	90.22	91.74	1.52	1.55	101.97	0.13	8.55	HQ					
K-10-0271	91.74	92.84	1.10	1.12	101.82	0.10	9.09	HQ					
K-10-0271	92.84	93.27	0.43	0.44	102.33	0.00	0.00	HQ					
K-10-0271	93.27	95.10	1.83	1.89	103.28	0.30	16.39	HQ					
K-10-0271	95.10	96.32	1.22	1.28	104.92	0.20	16.39	HQ					
K-10-0271	96.32	99.36	3.04	2.90	95.39	0.46	15.13	HQ					
K-10-0271	99.36	101.65	2.29	2.54	110.92	0.69	30.13	HQ					
K-10-0271	101.65	102.41	0.76	0.69	90.79	0.54	71.05	HQ					
K-10-0271	102.41	105.46	3.05	3.12	102.30	0.48	15.74	HQ					
K-10-0271	105.46	108.51	3.05	3.04	99.67	0.92	30.16	HQ					
K-10-0271	108.51	111.51	3.00	3.04	101.33	0.90	30.00	HQ					
K-10-0271	111.51	114.60	3.09	3.05	98.71	1.51	48.87	HQ					
K-10-0271	114.60	117.65	3.05	3.12	102.30	0.81	26.56	HQ					
K-10-0271	117.65	118.87	1.22	1.25	102.46	0.29	23.77	NQ					
K-10-0271	118.87	120.70	1.83	1.60	87.43	0.00	0.00	NQ					
K-10-0271	120.70	123.74	3.04	2.93	96.38	1.52	50.00	NQ					
K-10-0271	123.74	126.80	3.06	2.65	86.60	1.62	52.94	NQ					
K-10-0271	126.80	129.54	2.74	2.50	91.24	1.98	72.26	NQ					
K-10-0271	129.54	129.84	0.30	0.37	123.33	0.12	40.00	NQ					
K-10-0271	129.84	132.89	3.05	3.05	100.00	1.96	64.26	NQ					
K-10-0271	132.89	135.94	3.05	2.80	91.80	1.95	63.93	NQ					
K-10-0271	135.94	138.99	3.05	3.05	100.00	2.22	72.79	NQ					
K-10-0271	138.99	142.04	3.05	2.95	96.72	2.25	73.77	NQ					
K-10-0271	142.04	145.08	3.04	2.90	95.39	1.22	40.13	NQ					
K-10-0271	145.08	148.13	3.05	3.03	99.34	2.36	77.38	NQ					
K-10-0271	148.13	151.18	3.05	2.95	96.72	1.84	60.33	NQ					
K-10-0271	151.18	154.23	3.05	2.77	90.82	1.71	56.07	NQ					
K-10-0271	154.23	157.28	3.05	2.80	91.80	2.09	68.52	NQ					
K-10-0271	157.28	159.59	2.31	2.00	86.58	0.82	35.50	NQ					
K-10-0271	159.59	160.32	0.73	0.70	95.89	0.33	45.21	NQ					
K-10-0271	160.32	163.37	3.05	3.05	100.00	1.50	49.18	NQ					
K-10-0271	163.37	166.42	3.05	2.45	80.33	0.57	18.69	NQ					
K-10-0271	166.42	166.73	0.31	0.15	48.39	0.00	0.00	NQ					
K-10-0271	166.73	169.47	2.74	2.80	102.19	2.43	88.69	NQ					
K-10-0271	169.47	172.52	3.05	2.95	96.72	2.18	71.48	NQ					
K-10-0271	172.52	175.56	3.04	2.70	88.82	0.83	27.30	NQ					
K-10-0271	175.56	176.48	0.92	0.46	50.00	0.24	26.09	NQ					
K-10-0271	176.48	177.39	0.91	0.87	95.60	0.41	45.05	NQ					
K-10-0271	177.39	178.61	1.22	0.82	67.21	0.32	26.23	NQ					
K-10-0271	178.61	180.29	1.68	1.35	80.36	0.45	26.79	NQ					
K-10-0271	180.29	181.66	1.37	1.40	102.19	0.69	50.36	NQ					
K-10-0271	181.66	184.71	3.05	3.03	99.34	1.31	42.95	NQ					
K-10-0271	184.71	187.76	3.05	3.05	100.00	2.68	87.87	NQ					
K-10-0271	187.76	190.80	3.04	2.93	96.38	1.26	41.45	NQ					
K-10-0271	190.80	193.85	3.05	3.00	98.36	2.00	65.57	NQ					
K-10-0271	193.85	196.90	3.05	2.95	96.72	2.40	78.69	NQ					
K-10-0271	196.90	199.95	3.05	3.00	98.36	1.09	35.74	NQ					
K-10-0271	199.95	203.00	3.05	3.05	100.00	3.02	99.02	NQ					
K-10-0271	203.00	206.04	3.04	3.05	100.33	2.92	96.05	NQ					
K-10-0271	206.04	208.33	2.29	2.38	103.93	2.31	100.87	NQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0271	208.33	209.09	0.76	0.65	85.53	0.44	57.89	NQ					
K-10-0271	209.09	212.14	3.05	3.01	98.69	2.74	89.84	NQ					
K-10-0271	212.14	215.19	3.05	3.06	100.33	2.94	96.39	NQ					
K-10-0271	215.19	218.24	3.05	3.20	104.92	1.98	64.92	NQ					
K-10-0271	218.24	221.18	2.94	3.15	107.14	2.05	69.73	NQ					
K-10-0271	221.18	224.33	3.15	3.02	95.87	3.02	95.87	NQ					
K-10-0271	224.33	227.38	3.05	3.05	100.00	2.94	96.39	NQ					
K-10-0271	227.38	230.43	3.05	3.15	103.28	2.92	95.74	NQ					
K-10-0271	230.43	233.48	3.05	3.04	99.67	2.96	97.05	NQ					
K-10-0271	233.48	236.52	3.04	3.06	100.66	2.90	95.39	NQ					
K-10-0271	236.52	239.57	3.05	3.02	99.02	2.61	85.57	NQ					
K-10-0271	239.57	242.62	3.05	2.98	97.70	2.00	65.57	NQ					
K-10-0271	242.62	245.67	3.05	3.12	102.30	2.63	86.23	NQ					
K-10-0271	245.67	248.71	3.04	3.04	100.00	2.46	80.92	NQ					
K-10-0271	248.71	251.77	3.06	2.97	97.06	2.03	66.34	NQ					
K-10-0271	251.77	254.81	3.04	3.03	99.67	1.50	49.34	NQ					
K-10-0271	254.81	257.86	3.05	3.02	99.02	1.83	60.00	NQ					
K-10-0271	257.86	260.91	3.05	3.05	100.00	1.55	50.82	NQ					
K-10-0271	260.91	263.96	3.05	2.85	93.44	1.92	62.95	NQ					
K-10-0271	263.96	264.87	0.91	0.81	89.01	0.34	37.36	NQ					
K-10-0271	264.87	267.00	2.13	2.02	94.84	0.41	19.25	NQ					
K-10-0271	267.00	270.05	3.05	3.06	100.33	1.10	36.07	NQ					
K-10-0271	270.05	271.27	1.22	1.45	118.85	0.91	74.59	NQ					
K-10-0271	271.27	273.10	1.83	1.07	58.47	0.37	20.22	NQ					
K-10-0271	273.10	274.32	1.22	1.45	118.85	0.54	44.26	NQ					
K-10-0271	274.32	276.15	1.83	1.17	63.93	0.30	16.39	NQ					
K-10-0271	276.15	279.20	3.05	3.07	100.66	0.68	22.30	NQ					
K-10-0271	279.20	280.29	1.09	1.36	124.77	0.28	25.69	NQ					
K-10-0271	280.29	281.29	1.00	1.00	100.00	0.32	32.00	NQ					
K-10-0271	281.29	282.24	0.95	0.89	93.68	0.00	0.00	NQ					
K-10-0271	282.24	285.29	3.05	3.30	108.20	1.31	42.95	NQ					
K-10-0271	285.29	288.34	3.05	3.19	104.59	0.13	4.26	NQ					
K-10-0271	288.34	290.47	2.13	2.27	106.57	0.35	16.43	NQ					
K-10-0271	290.47	291.39	0.92	0.80	86.96	0.13	14.13	NQ					
K-10-0271	291.39	293.22	1.83	2.14	116.94	0.29	15.85	NQ					
K-10-0271	293.22	294.44	1.22	1.10	90.16	0.59	48.36	NQ					
K-10-0271	294.44	297.48	3.04	3.19	104.93	0.76	25.00	NQ					
K-10-0271	297.48	300.53	3.05	3.10	101.64	0.64	20.98	NQ					
K-10-0271	300.53	303.58	3.05	3.04	99.67	1.63	53.44	NQ					
K-10-0271	303.58	306.63	3.05	3.13	102.62	1.01	33.11	NQ					
K-10-0271	306.63	309.68	3.05	3.10	101.64	1.65	54.10	NQ					
K-10-0271	309.68	312.72	3.04	3.00	98.68	0.65	21.38	NQ					
K-10-0271	312.72	315.77	3.05	3.16	103.61	0.14	4.59	NQ					
K-10-0271	315.77	318.82	3.05	3.07	100.66	0.52	17.05	NQ					
K-10-0271	318.82	321.87	3.05	3.04	99.67	1.73	56.72	NQ					
K-10-0271	321.87	324.92	3.05	3.06	100.33	1.26	41.31	NQ					
K-10-0271	324.92	326.59	1.67	1.76	105.39	0.33	19.76	NQ					
K-10-0271	326.59	327.70	1.11	0.45	40.54	0.10	9.01	NQ					
K-10-0271	327.70	327.96	0.26	0.30	115.38	0.10	38.46	NQ					
K-10-0271	327.96	331.01	3.05	2.92	95.74	0.94	30.82	NQ					
K-10-0271	331.01	334.06	3.05	2.26	74.10	0.00	0.00	NQ					
K-10-0271	334.06	337.11	3.05	2.86	93.77	0.92	30.16	NQ					
K-10-0271	337.11	340.16	3.05	3.14	102.95	1.00	32.79	NQ					
K-10-0271	340.16	343.20	3.04	3.03	99.67	0.96	31.58	NQ					
K-10-0271	343.20	346.25	3.05	3.05	100.00	1.30	42.62	NQ					
K-10-0271	346.25	347.17	0.92	1.10	119.57	0.46	50.00	NQ					
K-10-0271	347.17	347.47	0.30	0.41	136.67	0.27	90.00	NQ					

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0275	0.00	10.92	OVB
K-10-0275	10.92	20.99	ICQS
K-10-0275	20.99	24.28	FLT
K-10-0275	24.28	28.92	ICQS
K-10-0275	28.92	30.31	FLT
K-10-0275	30.31	31.95	QTZT
K-10-0275	31.95	34.04	FLT
K-10-0275	34.04	34.75	SSCH
K-10-0275	34.75	36.13	FLT
K-10-0275	36.13	37.27	GSCH
K-10-0275	37.27	39.75	ICQS
K-10-0275	39.75	49.24	QTZT
K-10-0275	49.24	51.51	TQTZT
K-10-0275	51.51	52.96	ICQS
K-10-0275	52.96	54.91	TQTZT
K-10-0275	54.91	60.68	QTZT
K-10-0275	60.68	60.99	GSCH
K-10-0275	60.99	61.21	FLT
K-10-0275	61.21	62.82	SSCH
K-10-0275	62.82	67.55	GSCH
K-10-0275	67.55	68.68	QTZT
K-10-0275	68.68	72.00	GSCH
K-10-0275	72.00	73.54	QTZT
K-10-0275	73.54	75.13	ICQS
K-10-0275	75.13	78.91	TQTZT
K-10-0275	78.91	80.91	ICQS
K-10-0275	80.91	82.25	QTZT
K-10-0275	82.25	83.23	ICQS
K-10-0275	83.23	86.39	QTZT
K-10-0275	86.39	88.65	GSCH
K-10-0275	88.65	94.98	QTZT
K-10-0275	94.98	95.60	GSCH
K-10-0275	95.60	99.15	QTZT
K-10-0275	99.15	104.50	CQTZT
K-10-0275	104.50	104.93	GSCH
K-10-0275	104.93	110.53	QTZT
K-10-0275	110.53	114.72	CQTZT
K-10-0275	114.72	117.90	ICQS
K-10-0275	117.90	119.25	CQTZT
K-10-0275	119.25	121.05	ICQS
K-10-0275	121.05	131.48	CQTZT
K-10-0275	131.48	137.58	ICQS
K-10-0275	137.58	139.34	QTZT
K-10-0275	139.34	139.75	ICQS
K-10-0275	139.75	141.04	QTZT
K-10-0275	141.04	147.04	GNST
K-10-0275	147.04	149.34	QTZT
K-10-0275	149.34	151.42	GNST
K-10-0275	151.42	152.75	ICQS
K-10-0275	152.75	155.68	TQTZT
K-10-0275	155.68	159.78	CQTZT
K-10-0275	159.78	160.80	QTZT
K-10-0275	160.80	161.86	ICQS
K-10-0275	161.86	163.28	QTZT
K-10-0275	163.28	167.13	TQTZT
K-10-0275	167.13	169.69	QTZT
K-10-0275	169.69	171.85	ICQS
K-10-0275	171.85	175.62	CQTZT
K-10-0275	175.62	178.00	GSCH
K-10-0275	178.00	182.93	CQTZT
K-10-0275	182.93	183.53	ICQS
K-10-0275	183.53	188.89	QTZT
K-10-0275	188.89	191.78	ICQS
K-10-0275	191.78	193.72	QTZT
K-10-0275	193.72	252.66	GNST
K-10-0275	252.66	258.26	CHSCH
K-10-0275	258.26	260.93	GNST
K-10-0275	260.93	265.64	GSCH
K-10-0275	265.64	268.04	CQTZT
K-10-0275	268.04	277.94	GNST
K-10-0275	277.94	278.41	GNST
K-10-0275	278.41	281.80	GSCH
K-10-0275	281.80	282.09	FLT
K-10-0275	282.09	282.62	GSCH
K-10-0275	282.62	285.39	ICQS
K-10-0275	285.39	286.12	QTZT
K-10-0275	286.12	289.79	GSCH
K-10-0275	289.79	290.05	FLT
K-10-0275	290.05	292.76	GSCH
K-10-0275	292.76	294.10	FLT

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0275	294.10	299.39	VL
K-10-0275	299.39	303.32	SM
K-10-0275	303.32	303.98	VM
K-10-0275	303.98	305.41	SM
K-10-0275	305.41	307.82	QTZT
K-10-0275	307.82	312.34	FLT
K-10-0275	312.34	312.86	GSCH
K-10-0275	312.86	314.91	QTZT
K-10-0275	314.91	317.06	QTZT
K-10-0275	317.06	321.65	TQTZT
K-10-0275	321.65	322.48	ICQS
K-10-0275	322.48	331.07	GNST
K-10-0275	331.07	334.20	TQTZT
K-10-0275	334.20	340.06	QTZT
K-10-0275	340.06	342.77	GSCH
K-10-0275	342.77	346.55	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0275	0.00	3.99	3.99	0.70	17.54	0.00	0.00	HQ					
K-10-0275	3.99	5.18	1.19	0.33	27.73	0.10	8.40	HQ					
K-10-0275	5.18	5.79	0.61	0.61	100.00	0.00	0.00	HQ					
K-10-0275	5.79	10.06	4.27	0.89	20.84	0.26	6.09	HQ					
K-10-0275	10.06	10.37	0.31	0.31	100.00	0.00	0.00	HQ					
K-10-0275	10.37	14.02	3.65	1.37	37.53	0.32	8.77	HQ					
K-10-0275	14.02	15.85	1.83	1.80	98.36	0.25	13.66	HQ					
K-10-0275	15.85	16.46	0.61	0.51	83.61	0.13	21.31	HQ					
K-10-0275	16.46	19.51	3.05	2.26	74.10	0.56	18.36	HQ					
K-10-0275	19.51	21.33	1.82	1.49	81.87	0.00	0.00	HQ					
K-10-0275	21.33	24.38	3.05	0.65	21.31	0.00	0.00	HQ					
K-10-0275	24.38	25.60	1.22	0.72	59.02	0.15	12.30	HQ					
K-10-0275	25.60	28.65	3.05	0.81	26.56	0.00	0.00	HQ					
K-10-0275	28.65	31.78	3.13	3.05	97.44	0.00	0.00	HQ					
K-10-0275	31.78	32.61	0.83	0.92	110.84	0.70	84.34	HQ					
K-10-0275	32.61	34.14	1.53	1.14	74.51	0.38	24.84	HQ					
K-10-0275	34.14	34.75	0.61	0.43	70.49	0.00	0.00	HQ					
K-10-0275	34.75	37.79	3.04	2.87	94.41	0.53	17.43	HQ					
K-10-0275	37.79	39.32	1.53	1.32	86.27	0.22	14.38	HQ					
K-10-0275	39.32	40.84	1.52	1.32	86.84	0.66	43.42	HQ					
K-10-0275	40.84	42.85	2.01	1.85	92.04	0.48	23.88	HQ					
K-10-0275	42.85	43.89	1.04	0.95	91.35	0.29	27.88	HQ					
K-10-0275	43.89	46.94	3.05	2.85	93.44	2.10	68.85	HQ					
K-10-0275	46.94	49.99	3.05	2.65	86.89	0.77	25.25	HQ					
K-10-0275	49.99	53.03	3.04	2.97	97.70	0.81	26.64	HQ					
K-10-0275	53.03	54.25	1.22	1.08	88.52	0.42	34.43	HQ					
K-10-0275	54.25	55.47	1.22	1.23	100.82	0.44	36.07	HQ					
K-10-0275	55.47	56.08	0.61	0.42	68.85	0.10	16.39	HQ					
K-10-0275	56.08	59.13	3.05	2.96	97.05	1.19	39.02	HQ					
K-10-0275	59.13	62.28	3.15	2.80	88.89	0.63	20.00	HQ					
K-10-0275	62.28	65.23	2.95	2.46	83.39	0.74	25.08	HQ					
K-10-0275	65.23	68.27	3.04	2.76	90.79	0.67	22.04	HQ					
K-10-0275	68.27	70.71	2.44	2.00	81.97	0.83	34.02	HQ					
K-10-0275	70.71	71.47	0.76	0.44	57.89	0.00	0.00	HQ					
K-10-0275	71.47	72.54	1.07	0.67	62.62	0.10	9.35	HQ					
K-10-0275	72.54	74.37	1.83	1.30	71.04	0.00	0.00	HQ					
K-10-0275	74.37	77.42	3.05	2.17	71.15	0.33	10.82	HQ					
K-10-0275	77.42	80.47	3.05	2.21	72.46	0.55	18.03	HQ					
K-10-0275	80.47	83.51	3.04	3.16	103.95	1.18	38.82	HQ					
K-10-0275	83.51	86.56	3.05	2.67	87.54	1.04	34.10	HQ					
K-10-0275	86.56	89.61	3.05	1.82	59.67	0.76	24.92	HQ					
K-10-0275	89.61	92.66	3.05	2.26	74.10	0.54	17.70	HQ					
K-10-0275	92.66	95.71	3.05	2.03	66.56	0.45	14.75	HQ					
K-10-0275	95.71	98.75	3.04	2.49	81.91	1.59	52.30	HQ					
K-10-0275	98.75	99.97	1.22	1.26	103.28	0.28	22.95	HQ					
K-10-0275	99.97	101.80	1.83	1.61	87.98	1.45	79.23	HQ					
K-10-0275	101.80	104.85	3.05	2.63	86.23	1.72	56.39	HQ					
K-10-0275	104.85	107.90	3.05	2.96	97.05	2.13	69.84	HQ					
K-10-0275	107.90	110.65	2.75	2.80	101.82	1.94	70.55	HQ					
K-10-0275	110.65	113.38	2.73	2.45	89.74	2.09	76.56	HQ					
K-10-0275	113.38	116.43	3.05	2.99	98.03	1.80	59.02	HQ					
K-10-0275	116.43	118.26	1.83	1.55	84.70	0.99	54.10	HQ					
K-10-0275	118.26	120.09	1.83	1.81	98.91	0.79	43.17	HQ					
K-10-0275	120.09	123.14	3.05	2.95	96.72	2.63	86.23	HQ					
K-10-0275	123.14	126.19	3.05	2.85	93.44	2.09	68.52	HQ					
K-10-0275	126.19	129.23	3.04	2.97	97.70	2.71	89.14	HQ					
K-10-0275	129.23	132.28	3.05	3.05	100.00	2.02	66.23	HQ					
K-10-0275	132.28	135.33	3.05	3.10	101.64	1.16	38.03	HQ					
K-10-0275	135.33	138.38	3.05	3.02	99.02	1.97	64.59	HQ					
K-10-0275	138.38	141.43	3.05	3.07	100.66	2.43	79.67	HQ					
K-10-0275	141.43	144.47	3.04	2.96	97.37	2.82	92.76	HQ					
K-10-0275	144.47	147.52	3.05	3.07	100.66	2.79	91.48	HQ					
K-10-0275	147.52	150.57	3.05	2.94	96.39	2.60	85.25	HQ					
K-10-0275	150.57	153.62	3.05	2.90	95.08	2.52	82.62	HQ					
K-10-0275	153.62	156.67	3.05	2.90	95.08	2.50	81.97	HQ					
K-10-0275	156.67	159.72	3.05	2.92	95.74	1.73	56.72	HQ					
K-10-0275	159.72	162.76	3.04	2.80	92.11	1.79	58.88	HQ					
K-10-0275	162.76	165.81	3.05	2.93	96.07	1.85	60.66	HQ					
K-10-0275	165.81	167.64	1.83	1.86	101.64	1.44	78.69	HQ					
K-10-0275	167.64	168.86	1.22	1.13	92.62	0.97	79.51	HQ					
K-10-0275	168.86	171.91	3.05	3.02	99.02	2.25	73.77	HQ					
K-10-0275	171.91	174.96	3.05	3.07	100.66	1.32	43.28	HQ					
K-10-0275	174.96	178.00	3.04	3.06	100.66	0.00	0.00	HQ					
K-10-0275	178.00	181.05	3.05	3.06	100.33	1.49	48.85	HQ					
K-10-0275	181.05	184.10	3.05	3.10	101.64	1.59	52.13	HQ					
K-10-0275	184.10	187.15	3.05	3.11	101.97	2.46	80.66	HQ					
K-10-0275	187.15	190.20	3.05	3.08	100.98	2.32	76.07	HQ					
K-10-0275	190.20	193.24	3.04	3.03	99.67	1.84	60.53	HQ					
K-10-0275	193.24	196.29	3.05	3.05	100.00	2.62	85.90	HQ					
K-10-0275	196.29	199.34	3.05	3.02	99.02	2.81	92.13	HQ					
K-10-0275	199.34	202.39	3.05	3.11	101.97	3.05	100.00	HQ					
K-10-0275	202.39	205.49	3.10	3.05	98.39	2.46	79.35	HQ					
K-10-0275	205.49	208.48	2.99	3.03	101.34	3.03	101.34	HQ					
K-10-0275	208.48	211.53	3.05	2.90	95.08	2.68	87.87	HQ					
K-10-0275	211.53	214.58	3.05	2.96	97.05	2.80	91.80	HQ					
K-10-0275	214.58	217.63	3.05	3.09	101.31	2.82	92.46	HQ					
K-10-0275	217.63	220.68	3.05	3.07	100.66	2.46	80.66	HQ					
K-10-0275	220.68	223.72	3.04	3.07	100.99	2.86	94.08	HQ					
K-10-0275	223.72	226.77	3.05	2.93	96.07	2.93	96.07	HQ					
K-10-0275	226.77	229.82	3.05	3.02	99.02	2.88	94.43	HQ					
K-10-0275	229.82	232.87	3.05	3.07	100.66	2.75	90.16	HQ					
K-10-0275	232.87	235.92	3.05	3.10	101.64	3.00	98.36	HQ					
K-10-0275	235.92	238.96	3.04	3.06	100.66	2.50	82.24	HQ					
K-10-0275	238.96	242.01	3.05	3.04	99.67	2.90	95.08	HQ					
K-10-0275	242.01	245.06	3.05	3.11	101.97	2.84	93.11	HQ					
K-10-0275	245.06	248.11	3.05	2.98	97.70	2.68	87.87	HQ					
K-10-0275	248.11	251.16	3.05	3.08	100.98	2.91	95.41	HQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0275	251.16	254.20	3.04	3.04	100.00	2.62	86.18	HQ					
K-10-0275	254.20	257.25	3.05	3.04	99.67	1.42	46.56	HQ					
K-10-0275	257.25	260.30	3.05	3.18	104.26	1.77	58.03	HQ					
K-10-0275	260.30	263.35	3.05	3.14	102.95	0.87	28.52	HQ					
K-10-0275	263.35	266.40	3.05	3.08	100.98	0.00	0.00	HQ					
K-10-0275	266.40	269.44	3.04	3.15	103.62	1.37	45.07	HQ					
K-10-0275	269.44	272.49	3.05	3.04	99.67	2.76	90.49	HQ					
K-10-0275	272.49	275.54	3.05	3.05	100.00	3.05	100.00	HQ					
K-10-0275	275.54	278.59	3.05	3.01	98.69	2.30	75.41	HQ					
K-10-0275	278.59	281.64	3.05	3.06	100.33	0.27	8.85	HQ					
K-10-0275	281.64	284.68	3.04	3.00	98.68	0.00	0.00	HQ					
K-10-0275	284.68	287.73	3.05	3.09	101.31	0.34	11.15	HQ					
K-10-0275	287.73	290.78	3.05	2.99	98.03	0.84	27.54	HQ					
K-10-0275	290.78	293.83	3.05	2.85	93.44	0.00	0.00	HQ					
K-10-0275	293.83	296.88	3.05	2.82	92.46	1.64	53.77	HQ					
K-10-0275	296.88	299.92	3.04	2.99	98.36	1.90	62.50	HQ					
K-10-0275	299.92	300.84	0.92	0.87	94.57	0.33	35.87	HQ					
K-10-0275	300.84	302.97	2.13	2.09	98.12	0.59	27.70	HQ					
K-10-0275	302.97	305.41	2.44	2.40	98.36	1.37	56.15	HQ					
K-10-0275	305.41	306.02	0.61	0.63	103.28	0.00	0.00	HQ					
K-10-0275	306.02	309.07	3.05	2.57	84.26	1.15	37.70	HQ					
K-10-0275	309.07	310.13	1.06	0.27	25.47	0.00	0.00	HQ					
K-10-0275	310.13	310.74	0.61	0.10	16.39	0.00	0.00	HQ					
K-10-0275	310.74	311.51	0.77	0.20	25.97	0.00	0.00	HQ					
K-10-0275	311.51	311.96	0.45	0.32	71.11	0.00	0.00	HQ					
K-10-0275	311.96	312.12	0.16	0.13	81.25	0.00	0.00	HQ					
K-10-0275	312.12	313.18	1.06	1.15	108.49	0.41	38.68	HQ					
K-10-0275	313.18	315.16	1.98	1.89	95.45	1.37	69.19	HQ					
K-10-0275	315.16	318.21	3.05	3.05	100.00	1.40	45.90	HQ					
K-10-0275	318.21	321.26	3.05	3.00	98.36	0.89	29.18	HQ					
K-10-0275	321.26	324.31	3.05	3.03	99.34	1.51	49.51	HQ					
K-10-0275	324.31	327.36	3.05	3.01	98.69	2.84	93.11	HQ					
K-10-0275	327.36	330.40	3.04	3.04	100.00	2.72	89.47	HQ					
K-10-0275	330.40	333.45	3.05	2.96	97.05	1.63	53.44	HQ					
K-10-0275	333.45	336.50	3.05	3.00	98.36	1.83	60.00	HQ					
K-10-0275	336.50	339.50	3.00	3.24	108.00	1.51	50.33	HQ					
K-10-0275	339.50	342.60	3.10	2.84	91.61	0.26	8.39	HQ					
K-10-0275	342.60	345.64	3.04	3.09	101.64	1.51	49.67	HQ					
K-10-0275	345.64	346.55	0.91	0.91	100.00	0.00	0.00						

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0285	0.00	64.24	OVB
K-10-0285	64.24	68.88	CHSCH
K-10-0285	68.88	72.05	GSCH
K-10-0285	72.05	75.54	QTZT
K-10-0285	75.54	77.94	TQTZT
K-10-0285	77.94	81.69	FLT
K-10-0285	81.69	84.77	QTZT
K-10-0285	84.77	87.41	TQTZT
K-10-0285	87.41	93.64	QTZT
K-10-0285	93.64	98.09	TQTZT
K-10-0285	98.09	101.25	CQTZT
K-10-0285	101.25	103.13	GSCH
K-10-0285	103.13	112.12	QTZT
K-10-0285	112.12	113.05	ICQS
K-10-0285	113.05	122.77	QTZT
K-10-0285	122.77	130.63	TQTZT
K-10-0285	130.63	146.43	QTZT
K-10-0285	146.43	147.65	FLT
K-10-0285	147.65	158.28	QTZT
K-10-0285	158.28	162.12	TQTZT
K-10-0285	162.12	162.82	GSCH
K-10-0285	162.82	164.31	GNST
K-10-0285	164.31	169.61	QTZT
K-10-0285	169.61	170.44	FLT
K-10-0285	170.44	170.61	VN
K-10-0285	170.61	172.88	QTZT
K-10-0285	172.88	175.11	GSCH
K-10-0285	175.11	176.14	QTZT
K-10-0285	176.14	181.35	TQTZT
K-10-0285	181.35	184.71	TQTZT
K-10-0285	184.71	186.23	NR
K-10-0285	186.23	188.95	TQTZT
K-10-0285	188.95	199.47	QTZT
K-10-0285	199.47	199.71	VM
K-10-0285	199.71	203.16	QTZT
K-10-0285	203.16	209.98	GNST
K-10-0285	209.98	210.84	GNST
K-10-0285	210.84	211.91	VM
K-10-0285	211.91	216.75	GNST
K-10-0285	216.75	218.85	FLT
K-10-0285	218.85	220.07	NR
K-10-0285	220.07	220.56	FLT
K-10-0285	220.56	221.49	VM
K-10-0285	221.49	225.19	QTZT
K-10-0285	225.19	228.38	TQTZT
K-10-0285	228.38	230.86	TQTZT
K-10-0285	230.86	232.60	GSCH
K-10-0285	232.60	236.48	CQTZT
K-10-0285	236.48	237.30	GSCH
K-10-0285	237.30	242.52	QTZT
K-10-0285	242.52	260.00	TQTZT
K-10-0285	260.00	261.52	GSCH
K-10-0285	261.52	267.58	TQTZT
K-10-0285	267.58	268.07	GSCH
K-10-0285	268.07	270.48	QTZT
K-10-0285	270.48	271.04	FLT
K-10-0285	271.04	275.97	GSCH
K-10-0285	275.97	280.09	QTZT
K-10-0285	280.09	282.72	TQTZT
K-10-0285	282.72	283.41	GSCH
K-10-0285	283.41	287.41	ICQS
K-10-0285	287.41	291.01	GNST
K-10-0285	291.01	309.61	QTZT
K-10-0285	309.61	324.31	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0285	64.24	64.31	0.07	0.08	114.29	0.00	0.00	HQ					
K-10-0285	64.31	65.53	1.22	1.03	84.43	0.25	20.49	HQ					
K-10-0285	65.53	68.88	3.35	1.31	39.10	0.00	0.00	HQ					
K-10-0285	68.88	69.95	1.07	0.86	80.37	0.00	0.00	NQ					
K-10-0285	69.95	71.63	1.68	1.77	105.36	0.00	0.00	NQ					
K-10-0285	71.63	71.93	0.30	0.21	70.00	0.00	0.00	NQ					
K-10-0285	71.93	74.52	2.59	1.63	62.93	0.00	0.00	NQ					
K-10-0285	74.52	74.98	0.46	0.27	58.70	0.00	0.00	NQ					
K-10-0285	74.98	76.35	1.37	0.95	69.34	0.00	0.00	NQ					
K-10-0285	76.35	78.02	1.67	1.44	86.23	0.00	0.00	NQ					
K-10-0285	78.02	81.08	3.06	1.17	38.24	0.00	0.00	NQ					
K-10-0285	81.08	81.69	0.61	0.52	85.25	0.00	0.00	NQ					
K-10-0285	81.69	82.30	0.61	0.53	86.89	0.00	0.00	NQ					
K-10-0285	82.30	83.97	1.67	1.36	81.44	0.38	22.75	NQ					
K-10-0285	83.97	85.19	1.22	1.19	97.54	0.00	0.00	NQ					
K-10-0285	85.19	85.80	0.61	0.46	75.41	0.25	40.98	NQ					
K-10-0285	85.80	86.56	0.76	0.93	122.37	0.00	0.00	NQ					
K-10-0285	86.56	87.17	0.61	0.50	81.97	0.00	0.00	NQ					
K-10-0285	87.17	88.70	1.53	0.55	35.95	0.00	0.00	NQ					
K-10-0285	88.70	89.92	1.22	1.45	118.85	0.10	8.20	NQ					
K-10-0285	89.92	90.53	0.61	0.50	81.97	0.00	0.00	NQ					
K-10-0285	90.53	91.14	0.61	0.89	145.90	0.00	0.00	NQ					
K-10-0285	91.14	93.27	2.13	1.95	91.55	0.40	18.78	NQ					
K-10-0285	93.27	96.32	3.05	2.95	96.72	1.38	45.25	NQ					
K-10-0285	96.32	96.62	0.30	0.20	66.67	0.00	0.00	NQ					
K-10-0285	96.62	98.15	1.53	1.25	81.70	0.00	0.00	NQ					
K-10-0285	98.15	99.36	1.21	1.10	90.91	0.55	45.45	NQ					
K-10-0285	99.36	102.41	3.05	2.90	95.08	0.86	28.20	NQ					
K-10-0285	102.41	105.46	3.05	2.80	91.80	1.82	59.67	NQ					
K-10-0285	105.46	108.51	3.05	3.05	100.00	2.05	67.21	NQ					
K-10-0285	108.51	111.56	3.05	3.05	100.00	2.47	80.98	NQ					
K-10-0285	111.56	112.93	1.37	1.50	109.49	0.50	36.50	NQ					
K-10-0285	112.93	114.60	1.67	1.70	101.80	0.80	47.90	NQ					
K-10-0285	114.60	117.65	3.05	3.08	100.98	1.52	49.84	NQ					
K-10-0285	117.65	120.70	3.05	3.08	100.98	1.88	61.64	NQ					
K-10-0285	120.70	123.75	3.05	3.00	98.36	1.02	33.44	NQ					
K-10-0285	123.75	126.80	3.05	3.00	98.36	1.95	63.93	NQ					
K-10-0285	126.80	129.84	3.04	3.00	98.68	2.25	74.01	NQ					
K-10-0285	129.84	132.89	3.05	3.00	98.36	1.42	46.56	NQ					
K-10-0285	132.89	135.94	3.05	3.00	98.36	1.30	42.62	NQ					
K-10-0285	135.94	138.99	3.05	2.90	95.08	1.86	60.98	NQ					
K-10-0285	138.99	142.04	3.05	3.07	100.66	1.48	48.52	NQ					
K-10-0285	142.04	143.26	1.22	1.80	147.54	0.64	52.46	NQ					
K-10-0285	143.26	145.08	1.82	1.07	58.79	0.00	0.00	NQ					
K-10-0285	145.08	148.13	3.05	3.08	100.98	0.90	29.51	NQ					
K-10-0285	148.13	151.18	3.05	2.93	96.07	1.95	63.93	NQ					
K-10-0285	151.18	154.23	3.05	2.93	96.07	1.46	47.87	NQ					
K-10-0285	154.23	157.28	3.05	3.08	100.98	1.75	57.38	NQ					
K-10-0285	157.28	160.32	3.04	2.90	95.39	1.57	51.64	NQ					
K-10-0285	160.32	162.76	2.44	2.20	90.16	0.41	16.80	NQ					
K-10-0285	162.76	163.37	0.61	0.45	73.77	0.00	0.00	NQ					
K-10-0285	163.37	166.42	3.05	2.80	91.80	0.63	20.66	NQ					
K-10-0285	166.42	167.34	0.92	0.79	85.87	0.30	32.61	NQ					
K-10-0285	167.34	169.47	2.13	2.26	106.10	0.60	28.17	NQ					
K-10-0285	169.47	172.52	3.05	2.55	83.61	0.00	0.00	NQ					
K-10-0285	172.52	175.56	3.04	2.86	94.08	0.58	19.08	NQ					
K-10-0285	175.56	178.61	3.05	2.79	91.48	1.40	45.90	NQ					
K-10-0285	178.61	181.66	3.05	3.04	99.67	0.66	21.64	NQ					
K-10-0285	181.66	184.25	2.59	2.52	97.30	0.54	20.85	NQ					
K-10-0285	184.25	184.71	0.46	0.30	65.22	0.00	0.00	NQ					
K-10-0285	184.71	186.23	1.52	0.00	0.00	0.00	0.00	NQ					
K-10-0285	186.23	187.76	1.53	1.18	77.12	0.11	7.19	NQ					
K-10-0285	187.76	190.80	3.04	2.92	96.05	0.66	21.71	NQ					
K-10-0285	190.80	193.85	3.05	2.50	81.97	0.88	28.85	NQ					
K-10-0285	193.85	196.90	3.05	2.93	96.07	0.92	30.16	NQ					
K-10-0285	196.90	199.95	3.05	2.73	89.51	0.86	28.20	NQ					
K-10-0285	199.95	204.06	4.11	2.05	49.88	0.26	6.33	NQ					
K-10-0285	204.06	206.04	1.98	0.92	46.46	0.23	11.62	NQ					
K-10-0285	206.04	207.26	1.22	0.54	44.26	0.00	0.00	NQ					
K-10-0285	207.26	209.09	1.83	0.91	49.73	0.22	12.02	NQ					
K-10-0285	209.09	212.14	3.05	2.49	81.64	0.69	22.62	NQ					
K-10-0285	212.14	215.19	3.05	2.42	79.34	0.87	28.52	NQ					
K-10-0285	215.19	216.10	0.91	0.72	79.12	0.15	16.48	NQ					
K-10-0285	216.10	218.23	2.13	2.06	96.71	0.49	23.00	NQ					
K-10-0285	218.23	218.85	0.62	0.20	32.26	0.00	0.00	NQ					
K-10-0285	218.85	219.76	0.91	0.00	0.00	0.00	0.00	NQ					
K-10-0285	219.76	220.07	0.31	0.00	0.00	0.00	0.00	NQ					
K-10-0285	220.07	221.28	1.21	1.09	90.08	0.38	31.40	NQ					
K-10-0285	221.28	224.33	3.05	2.94	96.39	2.19	71.80	NQ					
K-10-0285	224.33	227.38	3.05	2.97	97.38	2.06	67.54	NQ					
K-10-0285	227.38	230.43	3.05	2.95	96.72	2.16	70.82	NQ					
K-10-0285	230.43	233.48	3.05	3.00	98.36	1.95	63.93	NQ					
K-10-0285	233.48	236.52	3.04	2.95	97.04	2.15	70.72	NQ					
K-10-0285	236.52	239.57	3.05	2.98	97.70	1.78	58.36	NQ					
K-10-0285	239.57	242.62	3.05	2.93	96.07	1.03	33.77	NQ					
K-10-0285	242.62	245.67	3.05	1.20	39.34	0.81	26.56	NQ					
K-10-0285	245.67	248.72	3.05	2.90	95.08	1.25	40.98	NQ					
K-10-0285	248.72	249.94	1.22	1.29	105.74	0.77	63.11	NQ					
K-10-0285	249.94	251.76	1.82	1.44	79.12	0.62	34.07	NQ					
K-10-0285	251.76	253.44	1.68	1.71	101.79	0.36	21.43	NQ					
K-10-0285	253.44	254.81	1.37	1.16	84.67	0.87	63.50	NQ					
K-10-0285	254.81	256.79	1.98	1.76	88.89	0.65	32.83	NQ					
K-10-0285	256.79	257.86	1.07	1.16	108.41	0.00	0.00	NQ					
K-10-0285	257.86	260.91	3.05	2.93	96.07	0.97	31.80	NQ					
K-10-0285	260.91	261.52	0.61	0.72	118.03	0.27	44.26	NQ					
K-10-0285	261.52	263.96	2.44	2.32	95.08	0.71	29.10	NQ					
K-10-0285	263.96	267.00	3.04	2.88	94.74	0.96	31.58	NQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0285	267.00	268.07	1.07	1.14	106.54	0.16	14.95	NQ					
K-10-0285	268.07	270.05	1.98	1.68	84.85	0.78	39.39	NQ					
K-10-0285	270.05	273.10	3.05	2.94	96.39	0.40	13.11	NQ					
K-10-0285	273.10	275.53	2.43	1.98	81.48	1.11	45.68	NQ					
K-10-0285	275.53	276.15	0.62	0.83	133.87	0.40	64.52	NQ					
K-10-0285	276.15	279.20	3.05	3.05	100.00	1.58	51.80	NQ					
K-10-0285	279.20	280.26	1.06	1.17	110.38	0.52	49.06	NQ					
K-10-0285	280.26	282.24	1.98	1.92	96.97	0.22	11.11	NQ					
K-10-0285	282.24	285.29	3.05	3.05	100.00	1.00	32.79	NQ					
K-10-0285	285.29	288.34	3.05	3.05	100.00	1.05	34.43	NQ					
K-10-0285	288.34	291.39	3.05	2.95	96.72	2.09	68.52	NQ					
K-10-0285	291.39	294.44	3.05	3.05	100.00	2.05	67.21	NQ					
K-10-0285	294.44	297.48	3.04	2.75	90.46	0.25	8.22	NQ					
K-10-0285	297.48	300.53	3.05	3.05	100.00	2.10	68.85	NQ					
K-10-0285	300.53	303.58	3.05	3.05	100.00	1.27	41.64	NQ					
K-10-0285	303.58	306.32	2.74	2.80	102.19	1.16	42.34	NQ					
K-10-0285	306.32	306.63	0.31	0.25	80.65	0.13	41.94	NQ					
K-10-0285	306.63	309.68	3.05	3.05	100.00	2.25	73.77	NQ					
K-10-0285	309.68	311.20	1.52	1.52	100.00	0.96	63.16	NQ					
K-10-0285	311.20	312.72	1.52	1.20	78.95	0.12	7.89	NQ					
K-10-0285	312.72	315.77	3.05	2.28	74.75	0.86	28.20	NQ					
K-10-0285	315.77	318.82	3.05	3.05	100.00	1.70	55.74	NQ					
K-10-0285	318.82	321.87	3.05	3.05	100.00	1.92	62.95	NQ					
K-10-0285	321.87	324.15	2.28	2.45	107.46	0.94	41.23	NQ					
K-10-0285	324.15	324.31	0.16	0.19	118.75	0.00	0.00	NQ					

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0291	0.00	2.10	OVB
K-10-0291	2.10	10.20	CQTZT
K-10-0291	10.20	14.47	ICQS
K-10-0291	14.47	18.64	QTZT
K-10-0291	18.64	20.44	ICQS
K-10-0291	20.44	24.85	QTZT
K-10-0291	24.85	25.20	ICQS
K-10-0291	25.20	28.14	QTZT
K-10-0291	28.14	31.40	ICQS
K-10-0291	31.40	32.81	QTZT
K-10-0291	32.81	33.94	ICQS
K-10-0291	33.94	34.65	TQTZT
K-10-0291	34.65	39.58	QTZT
K-10-0291	39.58	41.45	ICQS
K-10-0291	41.45	42.87	QTZT
K-10-0291	42.87	47.78	ICQS
K-10-0291	47.78	52.20	QTZT
K-10-0291	52.20	53.36	ICQS
K-10-0291	53.36	53.90	SSCH
K-10-0291	53.90	64.50	QTZT
K-10-0291	64.50	66.64	TQTZT
K-10-0291	66.64	66.99	SSCH
K-10-0291	66.99	69.29	QTZT
K-10-0291	69.29	70.60	TQTZT
K-10-0291	70.60	73.16	CQTZT
K-10-0291	73.16	74.98	CQTZT
K-10-0291	74.98	77.87	CQTZT
K-10-0291	77.87	79.35	TQTZT
K-10-0291	79.35	80.95	GNST
K-10-0291	80.95	86.68	QTZT
K-10-0291	86.68	88.18	GSCH
K-10-0291	88.18	88.85	FLT
K-10-0291	88.85	92.33	TQTZT
K-10-0291	92.33	94.11	GSCH
K-10-0291	94.11	99.21	CQTZT
K-10-0291	99.21	100.57	GSCH
K-10-0291	100.57	116.00	QTZT
K-10-0291	116.00	117.65	SM
K-10-0291	117.65	118.92	QTZT
K-10-0291	118.92	119.10	VL
K-10-0291	119.10	121.04	QTZT
K-10-0291	121.04	122.95	VM
K-10-0291	122.95	125.26	SM
K-10-0291	125.26	133.60	GNST
K-10-0291	133.60	135.46	FLT
K-10-0291	135.46	136.55	FLT
K-10-0291	136.55	139.93	FLT
K-10-0291	139.93	141.05	SM
K-10-0291	141.05	145.32	FLT
K-10-0291	145.32	149.89	ICQS
K-10-0291	149.89	157.54	TQTZT
K-10-0291	157.54	158.66	GSCH
K-10-0291	158.66	160.76	SSCH
K-10-0291	160.76	165.20	VL
K-10-0291	165.20	173.36	TQTZT
K-10-0291	173.36	176.60	GSCH
K-10-0291	176.60	178.40	ICQS
K-10-0291	178.40	185.09	TQTZT
K-10-0291	185.09	186.00	ICQS
K-10-0291	186.00	188.30	QTZT
K-10-0291	188.30	192.67	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0291	1.98	3.35	1.37	1.13	82.48	0.88	64.23	HQ	4	R5	3	1	
K-10-0291	3.35	4.42	1.07	1.04	97.20	0.57	53.27	HQ	2	R5	4	1	
K-10-0291	4.42	4.57	0.15	0.15	100.00	0.11	73.33	HQ	4	R5	1	1	
K-10-0291	4.57	5.18	0.61	0.61	100.00	0.20	32.79	HQ	7	R5	1	1	
K-10-0291	5.18	7.92	2.74	2.74	100.00	2.37	86.50	HQ	6	R5	3	1	
K-10-0291	7.92	9.14	1.22	1.07	87.70	0.90	73.77	HQ	2	R5	0		
K-10-0291	9.14	10.97	1.83	1.71	93.44	0.88	48.09	HQ	10	R4	0		
K-10-0291	10.97	11.77	0.80	0.72	90.00	0.22	27.50	HQ	8	R3	0		
K-10-0291	11.77	14.02	2.25	2.40	106.67	1.12	49.78	HQ	9	R2	0		
K-10-0291	14.02	17.07	3.05	2.93	96.07	2.64	86.56	HQ	5	R5	1	1	
K-10-0291	17.07	20.12	3.05	2.79	91.48	2.07	67.87	HQ	6	R5	0		
K-10-0291	20.12	23.16	3.04	3.04	100.00	2.42	79.61	HQ	6	R5	0		
K-10-0291	23.16	26.21	3.05	3.02	99.02	2.31	75.74	HQ	8	R4	1	1	
K-10-0291	26.21	28.35	2.14	2.00	93.46	1.33	62.15	HQ	7	R5	2	1	
K-10-0291	28.35	29.26	0.91	0.69	75.82	0.12	13.19	HQ	8	R3	0		
K-10-0291	29.26	32.31	3.05	2.88	94.43	1.90	62.30	HQ	11	R4	3	1	
K-10-0291	32.31	35.36	3.05	3.05	100.00	2.37	77.70	HQ	8	R3	0		
K-10-0291	35.36	35.66	0.30	0.34	113.33	0.22	73.33	HQ	1	R5	0		
K-10-0291	35.66	38.40	2.74	2.72	99.27	1.98	72.26	HQ	4	R5	0		
K-10-0291	38.40	41.45	3.05	3.00	98.36	2.00	65.57	HQ	7	R4	1	1	
K-10-0291	41.45	44.50	3.05	2.98	97.70	2.31	75.74	HQ	5	R4	0		
K-10-0291	44.50	47.54	3.04	2.91	95.72	2.28	75.00	HQ	6	R3	0		
K-10-0291	47.54	50.60	3.06	3.05	99.67	2.34	76.47	HQ	5	R5	0		
K-10-0291	50.60	52.12	1.52	1.58	103.95	0.98	64.47	HQ	11	R5	1	1	
K-10-0291	52.12	53.64	1.52	1.26	82.89	0.61	40.13	HQ	5	R3	0		
K-10-0291	53.64	56.69	3.05	2.93	96.07	2.01	65.90	HQ	4	R5	0		
K-10-0291	56.69	59.74	3.05	2.96	97.05	1.78	58.36	HQ	7	R5	4	1	
K-10-0291	59.74	60.20	0.46	0.62	134.78	0.62	134.78	HQ	1	R5	1	1	
K-10-0291	60.20	62.79	2.59	2.34	90.35	1.39	53.67	HQ	5	R5	2	1	
K-10-0291	62.79	65.84	3.05	3.01	98.69	2.39	78.36	HQ	4	R5	1	1	
K-10-0291	65.84	68.88	3.04	2.85	93.75	1.19	39.14	HQ	6	R5	0		
K-10-0291	68.88	70.71	1.83	1.47	80.33	0.70	38.25	HQ	15	R5	0		
K-10-0291	70.71	71.93	1.22	1.18	96.72	0.56	45.90	HQ	7	R5	0		
K-10-0291	71.93	74.98	3.05	3.03	99.34	1.89	61.97	HQ	10	R5	0		
K-10-0291	74.98	78.03	3.05	3.05	100.00	2.72	89.18	HQ	4	R5	0		
K-10-0291	78.03	81.07	3.04	3.04	100.00	2.09	68.75	HQ	6	R5	1	1	
K-10-0291	81.07	81.38	0.31	0.25	80.65	0.25	80.65	HQ	0	R4	0		
K-10-0291	81.38	84.12	2.74	2.74	100.00	1.69	61.68	HQ	9	R5	0		
K-10-0291	84.12	87.17	3.05	3.05	100.00	2.02	66.23	HQ	10	R3	2	1	
K-10-0291	87.17	88.85	1.68	1.56	92.86	0.69	41.07	HQ	8	R2	1	1	
K-10-0291	88.85	90.07	1.22	1.06	86.89	0.24	19.67	HQ	24	R5	0		
K-10-0291	90.07	90.68	0.61	0.61	100.00	0.00	0.00	HQ	20	R5	0		
K-10-0291	90.68	91.74	1.06	0.99	93.40	0.00	0.00	HQ	25	R5	0		
K-10-0291	91.74	92.35	0.61	0.56	91.80	0.00	0.00	HQ	18	R5	0		
K-10-0291	92.35	93.27	0.92	0.35	38.04	0.12	13.04	HQ	6	R3	0		
K-10-0291	93.27	96.32	3.05	3.05	100.00	1.46	47.87	HQ	16	R4	1	1	
K-10-0291	96.32	97.23	0.91	0.91	100.00	0.18	19.78	HQ	6	R5	0		
K-10-0291	97.23	99.36	2.13	1.71	80.28	0.91	42.72	HQ	10	R4	0		
K-10-0291	99.36	102.41	3.05	3.00	98.36	2.05	67.21	HQ	8	R3	0		
K-10-0291	102.41	102.71	0.30	0.23	76.67	0.14	46.67	HQ	0	R5	0		
K-10-0291	102.71	104.85	2.14	2.14	100.00	1.62	75.70	HQ	10	R5	0		
K-10-0291	104.85	105.46	0.61	0.60	98.36	0.25	40.98	HQ	3	R5	0		
K-10-0291	105.46	108.51	3.05	2.97	97.38	2.45	80.33	HQ	4	R5	6	1	
K-10-0291	108.51	111.56	3.05	2.95	96.72	2.62	85.90	HQ	6	R5	4	1	
K-10-0291	111.56	114.60	3.04	3.04	100.00	3.04	100.00	HQ	2	R5	9	1	
K-10-0291	114.60	117.65	3.05	2.97	97.38	2.73	89.51	HQ	4	R5	1	1	
K-10-0291	117.65	120.70	3.05	3.05	100.00	2.93	96.07	HQ	2	R5	9	1	
K-10-0291	120.70	123.75	3.05	2.99	98.03	2.53	82.95	HQ	2	R4	9	2	
K-10-0291	123.75	126.60	2.85	2.80	98.25	2.62	91.93	HQ	1	R5	9	2	
K-10-0291	126.60	129.84	3.24	2.92	90.12	2.54	78.40	HQ	1	R5	8	2	
K-10-0291	129.84	132.89	3.05	3.05	100.00	1.41	46.23	HQ	19	R5	2	1	
K-10-0291	132.89	134.87	1.98	1.19	60.10	0.57	28.79	HQ	16	R5	2	2	
K-10-0291	134.87	135.94	1.07	0.70	65.42	0.38	35.51	HQ	18	R3	0		
K-10-0291	135.94	136.55	0.61	0.56	91.80	0.32	52.46	HQ	2	R3	1	2	
K-10-0291	136.55	138.99	2.44	2.37	97.13	1.35	55.33	HQ	14	R2	3	2	
K-10-0291	138.99	142.04	3.05	2.95	96.72	1.47	48.20	HQ	24	R2	4	2	
K-10-0291	142.04	143.87	1.83	1.76	96.17	1.07	58.47	HQ	18	R2	2	2	
K-10-0291	143.87	145.08	1.21	1.15	95.04	0.54	44.63	HQ	10	R1	1	1	
K-10-0291	145.08	148.13	3.05	3.05	100.00	1.77	58.03	HQ	16	R5	5	1	
K-10-0291	148.13	148.74	0.61	0.57	93.44	0.51	83.61	HQ	2	R5	0		
K-10-0291	148.74	151.18	2.44	2.40	98.36	1.43	58.61	HQ	17	R5	3	1	
K-10-0291	151.18	154.23	3.05	3.05	100.00	1.78	58.36	HQ	12	R4	4	1	
K-10-0291	154.23	157.28	3.05	3.00	98.36	1.78	58.36	HQ	12	R4	5	1	
K-10-0291	157.28	160.32	3.04	2.92	96.05	2.03	66.78	HQ	6	R3	7	2	
K-10-0291	160.32	163.37	3.05	2.75	90.16	2.45	80.33	HQ	4	R5	7	1	
K-10-0291	163.37	166.42	3.05	3.05	100.00	2.63	86.23	HQ	7	R4	3	1	
K-10-0291	166.42	169.47	3.05	2.94	96.39	2.56	83.93	HQ	8	R5	4	1	
K-10-0291	169.47	172.52	3.05	3.05	100.00	2.30	75.41	HQ	8	R5	4	2	
K-10-0291	172.52	175.56	3.04	3.02	99.34	2.01	66.12	HQ	7	R3	2	1	
K-10-0291	175.56	178.61	3.05	3.00	98.36	2.05	67.21	HQ	9	R3	0		
K-10-0291	178.61	181.66	3.05	2.96	97.05	2.09	68.52	HQ	7	R3	0		
K-10-0291	181.66	184.71	3.05	3.05	100.00	2.23	73.11	HQ	11	R4	0		
K-10-0291	184.71	187.76	3.05	2.78	91.15	1.71	56.07	HQ	14	R4	1	1	
K-10-0291	187.76	190.80	3.04	2.81	92.43	1.72	56.58	HQ	8	R3	1	1	
K-10-0291	190.80	192.67	1.87	1.62	86.63	1.48	79.14	HQ	6	R4	2	1	

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0295	0.00	2.44	OVB
K-10-0295	2.44	8.65	CQTZT
K-10-0295	8.65	15.42	TQTZT
K-10-0295	15.42	17.74	ICQS
K-10-0295	17.74	19.35	QTZT
K-10-0295	19.35	20.48	GSCH
K-10-0295	20.48	22.34	CQTZT
K-10-0295	22.34	27.13	GSCH
K-10-0295	27.13	33.48	QTZT
K-10-0295	33.48	41.08	TQTZT
K-10-0295	41.08	46.48	CQTZT
K-10-0295	46.48	47.85	GSCH
K-10-0295	47.85	48.13	SSCH
K-10-0295	48.13	61.53	QTZT
K-10-0295	61.53	61.94	SSCH
K-10-0295	61.94	69.24	TQTZT
K-10-0295	69.24	70.40	SSCH
K-10-0295	70.40	73.67	TQTZT
K-10-0295	73.67	75.82	GSCH
K-10-0295	75.82	78.41	CQTZT
K-10-0295	78.41	81.38	GSCH
K-10-0295	81.38	86.00	CQTZT
K-10-0295	86.00	87.48	GSCH
K-10-0295	87.48	107.53	CQTZT
K-10-0295	107.53	110.77	TQTZT
K-10-0295	110.77	110.98	GNST
K-10-0295	110.98	113.53	GSCH
K-10-0295	113.53	115.81	TQTZT
K-10-0295	115.81	153.30	GNST
K-10-0295	153.30	159.95	CHSCH
K-10-0295	159.95	163.28	QTZT
K-10-0295	163.28	167.38	QTZT
K-10-0295	167.38	181.36	TQTZT
K-10-0295	181.36	182.71	GNST
K-10-0295	182.71	186.17	FLT
K-10-0295	186.17	190.20	ICQS
K-10-0295	190.20	196.22	TQTZT
K-10-0295	196.22	197.22	ICQS
K-10-0295	197.22	198.57	QTZT
K-10-0295	198.57	200.93	SM
K-10-0295	200.93	204.70	TQTZT
K-10-0295	204.70	212.32	SM
K-10-0295	212.32	215.49	TQTZT
K-10-0295	215.49	221.03	QTZT
K-10-0295	221.03	231.67	TQTZT
K-10-0295	231.67	232.93	ICQS
K-10-0295	232.93	239.65	GNST
K-10-0295	239.65	244.74	QTZT
K-10-0295	244.74	248.00	TQTZT
K-10-0295	248.00	252.29	QTZT
K-10-0295	252.29	259.69	TQTZT
K-10-0295	259.69	266.70	QTZT
K-10-0295	266.70	269.02	TQTZT
K-10-0295	269.02	275.47	QTZT
K-10-0295	275.47	280.60	ICQS
K-10-0295	280.60	285.09	TQTZT
K-10-0295	285.09	288.58	ICQS
K-10-0295	288.58	306.63	QTZT
K-10-0295	306.63	307.43	GNST
K-10-0295	307.43	313.94	ICQS

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0295	2.44	4.11	1.67	1.34	80.24	0.46	27.54	HQ	1	R5	1	1	0.0
K-10-0295	4.11	5.18	1.07	0.96	89.72	0.91	85.05	HQ	4	R5	0	1	0.0
K-10-0295	5.18	8.23	3.05	2.77	90.82	2.64	86.56	HQ	10	R4	4	1	0.0
K-10-0295	8.23	11.28	3.05	2.80	91.80	0.87	28.52	HQ	34	R4	10	2	2.0
K-10-0295	11.28	14.33	3.05	2.91	95.41	1.65	54.10	HQ	27	R4	13	3	1.0
K-10-0295	14.33	17.37	3.04	2.88	94.74	1.48	48.68	HQ	31	R4	15	2	20.0
K-10-0295	17.37	20.42	3.05	2.86	93.77	1.71	56.07	HQ	41	R4	20	3	4.0
K-10-0295	20.42	23.47	3.05	2.91	95.41	2.31	75.74	HQ	23	R4	28	1	0.5
K-10-0295	23.47	26.52	3.05	3.01	98.69	1.40	45.90	HQ	41	R4	27	2	2.0
K-10-0295	26.52	29.57	3.05	2.98	97.70	2.26	74.10	HQ	27	R5	62	2	8.0
K-10-0295	29.57	32.61	3.04	3.01	99.01	2.85	93.75	HQ	17	R5	54	2	3.0
K-10-0295	32.61	35.66	3.05	2.94	96.39	2.23	73.11	HQ	18	R4	23	1	0.1
K-10-0295	35.66	38.71	3.05	2.86	93.77	1.67	54.75	HQ	32	R3	21	2	5.0
K-10-0295	38.71	41.76	3.05	3.06	100.33	1.92	62.95	HQ	29	R4	24	2	2.0
K-10-0295	41.76	44.81	3.05	3.00	98.36	2.68	87.87	HQ	15	R5	17	2	0.5
K-10-0295	44.81	46.63	1.82	1.86	102.20	0.93	51.10	HQ	19	R5	17	2	0.1
K-10-0295	46.63	47.85	1.22	1.07	87.70	0.20	16.39	HQ	29	R3	3	2	0.1
K-10-0295	47.85	50.90	3.05	3.04	99.67	2.03	66.56	HQ	29	R6	26	2	2.0
K-10-0295	50.90	53.95	3.05	2.96	97.05	2.23	73.11	HQ	20	R6	3	1	1.0
K-10-0295	53.95	54.78	0.83	0.96	115.66	0.84	101.20	HQ	8	R5	10	1	1.0
K-10-0295	54.78	57.00	2.22	2.06	92.79	1.14	51.35	HQ	22	R5	11	2	2.0
K-10-0295	57.00	60.05	3.05	3.01	98.69	2.80	91.80	HQ	9	R5	5	3	1.0
K-10-0295	60.05	63.09	3.04	2.86	94.08	1.43	47.04	HQ	39	R3	17	2	0.0
K-10-0295	63.09	66.14	3.05	2.97	97.38	1.22	40.00	HQ	37	R3	8	2	0.1
K-10-0295	66.14	69.19	3.05	2.19	71.80	0.96	31.48	HQ	54	R3	6	2	0.0
K-10-0295	69.19	72.24	3.05	3.10	101.64	1.41	46.23	HQ	39	R4	16	2	4.0
K-10-0295	72.24	75.29	3.05	3.02	99.02	1.34	43.93	HQ	43	R3	19	2	10.0
K-10-0295	75.29	76.35	1.06	0.82	77.36	0.00	0.00	HQ	38	R2	1	3	0.0
K-10-0295	76.35	77.72	1.37	1.02	74.45	0.00	0.00	HQ	24	R3	1	3	0.0
K-10-0295	77.72	78.33	0.61	0.27	44.26	0.13	21.31	HQ	6	R4	0	1	0.0
K-10-0295	78.33	81.38	3.05	1.89	61.97	0.57	18.69	NQ	27	R4	11	2	4.0
K-10-0295	81.38	84.43	3.05	2.95	96.72	2.24	73.44	NQ	22	R4	4	1	1.0
K-10-0295	84.43	87.48	3.05	3.07	100.66	1.20	39.34	NQ	58	R2	20	3	2.0
K-10-0295	87.48	90.53	3.05	3.08	100.98	2.50	81.97	NQ	17	R6	2	1	0.0
K-10-0295	90.53	93.57	3.04	2.95	97.04	2.95	97.04	NQ	8	R6	9	1	0.2
K-10-0295	93.57	96.62	3.05	2.94	96.39	2.80	91.80	NQ	12	R6	10	2	0.1
K-10-0295	96.62	99.67	3.05	2.92	95.74	2.37	77.70	NQ	20	R6	5	3	0.0
K-10-0295	99.67	102.72	3.05	3.01	98.69	2.44	80.00	NQ	13	R6	8	2	3.0
K-10-0295	102.72	105.77	3.05	3.04	99.67	1.56	51.15	NQ	28	R5	12	2	1.0
K-10-0295	105.77	108.81	3.04	3.08	101.32	1.80	59.21	NQ	36	R5	7	2	1.0
K-10-0295	108.81	111.86	3.05	2.90	95.08	1.56	51.15	NQ	5	R4	5	3	2.0
K-10-0295	111.86	113.39	1.53	1.53	100.00	0.93	60.78	NQ	6	R3	0	2	0.0
K-10-0295	113.39	114.91	1.52	1.39	91.45	1.15	75.66	NQ	3	R4	2	3	3.0
K-10-0295	114.91	117.65	2.74	2.78	101.46	2.40	87.59	NQ	2	R4	4	3	1.0
K-10-0295	117.65	118.87	1.22	1.42	116.39	1.42	116.39	NQ	0	R4	3	3	2.0
K-10-0295	118.87	121.01	2.14	1.78	83.18	1.76	82.24	NQ	0	R4	5	3	2.0
K-10-0295	121.01	124.05	3.04	3.05	100.33	3.05	100.33	NQ	1	R4	6	2	1.0
K-10-0295	124.05	127.10	3.05	3.05	100.00	3.05	100.00	NQ	0	R4	9	2	1.0
K-10-0295	127.10	130.15	3.05	3.05	100.00	3.05	100.00	NQ	0	R4	6	2	1.0
K-10-0295	130.15	133.20	3.05	3.05	100.00	3.05	100.00	NQ	0	R4	5	2	0.1
K-10-0295	133.20	136.25	3.05	3.05	100.00	3.05	100.00	NQ	0	R4	0		0.0
K-10-0295	136.25	139.29	3.04	3.00	98.68	3.00	98.68	NQ	0	R4	2	2	0.5
K-10-0295	139.29	142.34	3.05	2.93	96.07	2.93	96.07	NQ	0	R4	2	3	0.1
K-10-0295	142.34	145.39	3.05	3.05	100.00	3.05	100.00	NQ	0	R4	4	3	0.1
K-10-0295	145.39	148.44	3.05	3.05	100.00	3.05	100.00	NQ	0	R4	2	3	0.1
K-10-0295	148.44	151.49	3.05	3.05	100.00	3.05	100.00	NQ	0	R4	5	3	0.0
K-10-0295	151.49	154.53	3.04	3.05	100.33	2.85	93.75	NQ	2	R4	5	3	0.0
K-10-0295	154.53	157.58	3.05	3.05	100.00	2.78	91.15	NQ	5	R4	11	2	4.0
K-10-0295	157.58	160.63	3.05	2.90	95.08	2.08	68.20	NQ	3	R3	7	2	3.0
K-10-0295	160.63	163.68	3.05	3.05	100.00	2.87	94.10	NQ	2	R5	14	2	3.0
K-10-0295	163.68	166.73	3.05	3.05	100.00	2.92	95.74	NQ	6	R5	19	2	10.0
K-10-0295	166.73	170.08	3.35	3.05	91.04	1.11	33.13	NQ	37	R3	6	2	1.0
K-10-0295	170.08	172.82	2.74	2.38	86.86	1.16	42.34	NQ	22	R4	12	3	2.0
K-10-0295	172.82	174.65	1.83	1.72	93.99	1.43	78.14	NQ	24	R3	9	3	2.0
K-10-0295	174.65	175.87	1.22	0.82	67.21	0.00	0.00	NQ	19	R5	1	3	0.1
K-10-0295	175.87	176.17	0.30	0.22	73.33	0.00	0.00	NQ	5	R3	0	3	0.0
K-10-0295	176.17	178.92	2.75	2.34	85.09	1.10	40.00	NQ	20	R3	9	2	3.0
K-10-0295	178.92	179.71	0.79	0.46	58.23	0.00	0.00	NQ	13	R3	4	2	8.0
K-10-0295	179.71	181.23	1.52	1.57	103.29	0.90	59.21	NQ	19	R4	7	2	2.0
K-10-0295	181.23	181.96	0.73	0.70	95.89	0.11	15.07	NQ	13	R4	4	2	2.0
K-10-0295	181.96	184.10	2.14	1.87	87.38	0.93	43.46	NQ			10		6.0
K-10-0295	184.10	185.01	0.91	0.80	87.91	0.00	0.00	NQ					
K-10-0295	185.01	186.23	1.22	1.12	91.80	0.00	0.00	NQ					
K-10-0295	186.23	187.15	0.92	0.49	53.26	0.00	0.00	NQ	11	R1	2	3	1.0
K-10-0295	187.15	188.06	0.91	0.73	80.22	0.11	12.09	NQ	13	R2	3	3	1.0
K-10-0295	188.06	190.20	2.14	1.30	60.75	0.00	0.00	NQ		R1	3	3	1.0
K-10-0295	190.20	191.11	0.91	0.80	87.91	0.62	68.13	NQ	14	R3	9	2	1.0
K-10-0295	191.11	192.94	1.83	1.70	92.90	1.47	80.33	NQ	25	R3	9	2	2.0
K-10-0295	192.94	194.17	1.23	1.05	85.37	0.42	34.15	NQ	18	R3	4	3	9.0
K-10-0295	194.17	197.21	3.04	2.77	91.12	1.37	45.07	NQ	30	R3	6	2	6.0
K-10-0295	197.21	199.95	2.74	2.59	94.53	1.14	41.61	NQ	25	R3	11	3	15.0
K-10-0295	199.95	200.25	0.30	0.40	133.33	0.30	100.00	NQ	2	R4	5	2	3.0
K-10-0295	200.25	202.35	2.10	2.20	104.76	0.89	42.38	NQ	32	R4	18	2	10.0
K-10-0295	202.35	203.30	0.95	0.59	62.11	0.15	15.79	NQ	16	R3	6	2	10.0
K-10-0295	203.30	204.70	1.40	1.24	88.57	0.18	12.86	NQ	32	R4	7	2	5.0
K-10-0295	204.70	206.35	1.65	1.65	100.00	0.30	18.18	NQ	42	R4	9	2	40.0
K-10-0295	206.35	207.14	0.79	0.46	58.23	0.00	0.00	NQ	13	R4	8	2	15.0
K-10-0295	207.14	209.40	2.26	1.39	61.50	0.35	15.49	NQ	34	R4	5	2	3.0
K-10-0295	209.40	210.01	0.61	0.49	80.33	0.00	0.00	NQ	20	R4	10	2	6.0
K-10-0295	210.01	212.32	2.31	1.93	83.55	0.63	27.27	NQ	43	R4	34	2	2.0
K-10-0295	212.32	212.45	0.13	0.13	100.00	0.13	100.00	NQ	3	R5	1	3	1.0
K-10-0295	212.45	214.88	2.43	2.24	92.18	1.05	43.21	NQ	38	R4	5	3	2.0
K-10-0295	214.88	215.49	0.61	0.61	100.00	0.00	0.00	NQ	44	R4	7	2	0.3
K-10-0295	215.49	216.10	0.61	0.51	83.61	0.28	45.90	NQ	6	R5	6	1	5.0
K-10-0295	216.10	217.20	1.10	0.85	77.27	0.72	65.45	NQ	4	R5	17	2	20.0
K-10-0295	217.20	218.54	1.34	1.24	92.54	1.02	76.12	NQ	12	R5	10	2	50.0
K-10-0295	218.54	221.59	3.05	2.97	97.38	1.89	61.97	NQ	34	R5	22	2	25.0

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0295	221.59	223.11	1.52	1.12	73.68	0.20	13.16	NQ	26	R4	7	2	2.0
K-10-0295	223.11	224.64	1.53	1.30	84.97	0.20	13.07	NQ	33	R4	5	2	5.0
K-10-0295	224.64	227.69	3.05	2.38	78.03	0.84	27.54	NQ	47	R4	5	2	1.0
K-10-0295	227.69	228.30	0.61	0.25	40.98	0.00	0.00	NQ	8	R4	2	2	10.0
K-10-0295	228.30	230.72	2.42	2.42	100.00	0.87	35.95	NQ	44	R4	10	2	20.0
K-10-0295	230.72	233.30	2.58	2.36	91.47	0.59	22.87	NQ	70	R3	13	1	3.0
K-10-0295	233.30	236.83	3.53	2.95	83.57	2.42	68.56	NQ	22	R3	22	2	1.0
K-10-0295	236.83	239.88	3.05	2.95	96.72	2.57	84.26	NQ	28	R5	2	1	20.0
K-10-0295	239.88	242.50	2.62	2.60	99.24	1.63	62.21	NQ	34	R6	3	2	2.0
K-10-0295	242.50	242.93	0.43	0.44	102.33	0.33	76.74	NQ	8	R5	0	1	0.0
K-10-0295	242.93	245.55	2.62	2.26	86.26	1.19	45.42	NQ	27	R5	4	1	5.0
K-10-0295	245.55	245.97	0.42	0.24	57.14	0.13	30.95	NQ	5	R3	0	1	0.0
K-10-0295	245.97	246.77	0.80	0.99	123.75	0.75	93.75	NQ	12	R4	1	2	3.0
K-10-0295	246.77	249.02	2.25	2.10	93.33	1.32	58.67	NQ	21	R4	5	2	3.0
K-10-0295	249.02	249.94	0.92	1.06	115.22	0.33	35.87	NQ	17	R5	3	1	2.0
K-10-0295	249.94	252.07	2.13	2.09	98.12	1.86	87.32	NQ	11	R6	0	1	0.0
K-10-0295	252.07	254.20	2.13	2.08	97.65	1.42	66.67	NQ	22	R4	6	1	4.0
K-10-0295	254.20	255.12	0.92	0.72	78.26	0.10	10.87	NQ	20	R3	0	1	0.0
K-10-0295	255.12	256.34	1.22	1.13	92.62	0.81	66.39	NQ	13	R4	2	1	20.0
K-10-0295	256.34	256.95	0.61	0.55	90.16	0.26	42.62	NQ	13	R5	0	1	0.0
K-10-0295	256.95	257.25	0.30	0.31	103.33	0.00	0.00	NQ	8	R4	0	1	0.0
K-10-0295	257.25	258.17	0.92	0.59	64.13	0.00	0.00	NQ	20	R4	1	1	5.0
K-10-0295	258.17	259.69	1.52	1.47	96.71	0.34	22.37	NQ	35	R4	3	2	3.0
K-10-0295	259.69	261.21	1.52	1.51	99.34	1.12	73.68	NQ	14	R5	4	2	2.0
K-10-0295	261.21	262.43	1.22	1.21	99.18	0.40	32.79	NQ	21	R4	3	2	2.0
K-10-0295	262.43	264.26	1.83	1.00	54.64	0.14	7.65	NQ	26	R4	2	2	3.0
K-10-0295	264.26	265.79	1.53	1.55	101.31	1.22	79.74	NQ	24	R4	0	1	0.0
K-10-0295	265.79	266.09	0.30	0.14	46.67	0.14	46.67	NQ	4	R5	0	1	0.0
K-10-0295	266.09	266.70	0.61	0.64	104.92	0.56	91.80	NQ	9	R5	2	1	2.0
K-10-0295	266.70	269.75	3.05	3.00	98.36	2.00	65.57	NQ	31	R6	8	1	5.0
K-10-0295	269.75	272.80	3.05	3.06	100.33	2.77	90.82	NQ	15	R5	4	1	3.0
K-10-0295	272.80	275.84	3.04	2.98	98.03	2.44	80.26	NQ	22	R4	3	2	2.0
K-10-0295	275.84	276.45	0.61	0.49	80.33	0.00	0.00	NQ	17	R3	0	1	0.0
K-10-0295	276.45	279.50	3.05	3.03	99.34	0.21	6.89	NQ	70	R3	2	3	1.0
K-10-0295	279.50	282.55	3.05	3.06	100.33	1.42	46.56	NQ	52	R4	6	2	5.0
K-10-0295	282.55	285.60	3.05	2.92	95.74	2.35	77.05	NQ	23	R5	14	1	15.0
K-10-0295	285.60	288.65	3.05	3.05	100.00	0.74	24.26	NQ	44	R3	4	2	5.0
K-10-0295	288.65	291.69	3.04	3.09	101.64	2.46	80.92	NQ	22	R5	6	2	3.0
K-10-0295	291.69	294.74	3.05	3.06	100.33	1.00	32.79	NQ	53	R4	1	1	2.0
K-10-0295	294.74	297.79	3.05	3.05	100.00	1.57	51.48	NQ	37	R5	1	1	1.0
K-10-0295	297.79	300.84	3.05	3.10	101.64	2.00	65.57	NQ	31	R4	6	1	20.0
K-10-0295	300.84	303.89	3.05	2.97	97.38	1.91	62.62	NQ	28	R5	2	1	1.0
K-10-0295	303.89	306.63	2.74	2.85	104.01	2.47	90.15	NQ	23	R5	12	1	20.0
K-10-0295	306.63	309.68	3.05	3.00	98.36	1.02	33.44	NQ	50	R3	6	2	5.0
K-10-0295	309.68	312.42	2.74	2.79	101.82	0.26	9.49	NQ	65	R3	2	2	2.0
K-10-0295	312.42	313.94	1.52	1.22	80.26	0.70	46.05	NQ	22	R3	3	2	3.0

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0298	2.13	12.56	CQTZT
K-10-0298	12.56	13.87	TQTZT
K-10-0298	13.87	26.86	CQTZT
K-10-0298	26.86	30.10	TQTZT
K-10-0298	30.10	34.14	QTZT
K-10-0298	34.14	36.39	TQTZT
K-10-0298	36.39	43.19	QTZT
K-10-0298	43.19	53.40	TQTZT
K-10-0298	53.40	58.67	CQTZT
K-10-0298	58.67	60.48	SSCH
K-10-0298	60.48	63.99	SSCH
K-10-0298	63.99	66.55	SSCH
K-10-0298	66.55	69.49	QTZT
K-10-0298	69.49	71.93	TQTZT
K-10-0298	71.93	80.01	QTZT
K-10-0298	80.01	84.37	GSCH
K-10-0298	84.37	93.87	QTZT
K-10-0298	93.87	96.67	SSCH
K-10-0298	96.67	100.11	QTZT
K-10-0298	100.11	101.56	TQTZT
K-10-0298	101.56	107.93	QTZT
K-10-0298	107.93	112.20	ICQS
K-10-0298	112.20	116.74	CQTZT
K-10-0298	116.74	121.16	ICQS
K-10-0298	121.16	126.92	CQTZT
K-10-0298	126.92	131.49	ICQS
K-10-0298	131.49	134.43	QTZT
K-10-0298	134.43	135.24	SM
K-10-0298	135.24	148.28	QTZT
K-10-0298	148.28	151.42	ICQS
K-10-0298	151.42	155.66	VM
K-10-0298	155.66	156.05	SM
K-10-0298	156.05	156.62	SSCH
K-10-0298	156.62	157.44	GSCH
K-10-0298	157.44	158.14	SM
K-10-0298	158.14	162.33	QTZT
K-10-0298	162.33	163.80	TQTZT
K-10-0298	163.80	166.31	GNST
K-10-0298	166.31	172.52	TQTZT
K-10-0298	172.52	175.52	SM
K-10-0298	175.52	177.88	CHSCH
K-10-0298	177.88	179.75	FLT
K-10-0298	179.75	184.56	ICQS
K-10-0298	184.56	186.04	QTZT
K-10-0298	186.04	189.00	ICQS
K-10-0298	189.00	192.14	TQTZT
K-10-0298	192.14	195.38	VL
K-10-0298	195.38	197.45	QTZT
K-10-0298	197.45	198.33	VL
K-10-0298	198.33	199.37	QTZT
K-10-0298	199.37	201.51	TQTZT
K-10-0298	201.51	204.34	ICQS
K-10-0298	204.34	206.50	QTZT
K-10-0298	206.50	220.68	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0298	0.00	4.88	4.88	1.71	35.04	0.55	11.27	HQ	26	R6	0	1	0
K-10-0298	4.88	6.40	1.52	1.47	96.71	1.30	85.53	HQ	8	R6	0	1	0
K-10-0298	6.40	7.93	1.53	1.41	92.16	1.22	79.74	HQ	6	R6	0	1	0
K-10-0298	7.93	9.45	1.52	1.56	102.63	0.78	51.32	HQ	18	R5	0	1	0
K-10-0298	9.45	10.36	0.91	1.06	116.48	0.77	84.62	HQ	12	R5	0	1	0
K-10-0298	10.36	10.97	0.61	0.52	85.25	0.13	21.31	HQ	6	R5	0	1	0
K-10-0298	10.97	13.41	2.44	2.73	111.89	1.17	47.95	HQ	51	R4	3	3	2
K-10-0298	13.41	14.02	0.61	0.40	65.57	0.13	21.31	HQ	12	R4	0	1	0
K-10-0298	14.02	17.07	3.05	3.09	101.31	2.12	69.51	HQ	36	R5	3	2	4
K-10-0298	17.07	19.51	2.44	2.30	94.26	1.56	63.93	HQ	24	R6	1	2	2
K-10-0298	19.51	20.12	0.61	0.42	68.85	0.21	34.43	HQ	7	R5	1	2	20
K-10-0298	20.12	23.17	3.05	2.94	96.39	2.39	78.36	HQ	25	R6	1	1	2
K-10-0298	23.17	26.21	3.04	3.01	99.01	2.80	92.11	HQ	12	R6	1	1	1
K-10-0298	26.21	29.26	3.05	2.90	95.08	1.69	55.41	HQ	38	R4	2	1	4
K-10-0298	29.26	32.31	3.05	3.12	102.30	2.11	69.18	HQ	30	R6	2	1	4
K-10-0298	32.31	35.36	3.05	2.98	97.70	1.71	56.07	HQ	28	R4	1	2	2
K-10-0298	35.36	38.41	3.05	3.02	99.02	2.54	83.28	HQ	25	R4	1	2	5
K-10-0298	38.41	39.93	1.52	1.55	101.97	1.39	91.45	HQ	7	R6	0	1	0
K-10-0298	39.93	40.59	0.66	0.56	84.85	0.30	45.45	HQ	6	R5	0	1	0
K-10-0298	40.59	41.45	0.86	1.07	124.42	0.90	104.65	HQ	9	R5	1	1	2
K-10-0298	41.45	44.50	3.05	3.08	100.98	2.35	77.05	HQ	28	R5	1	1	1
K-10-0298	44.50	47.55	3.05	2.95	96.72	2.14	70.16	HQ	25	R4	2	2	1
K-10-0298	47.55	50.60	3.05	2.98	97.70	2.24	73.44	HQ	23	R4	4	2	2
K-10-0298	50.60	51.51	0.91	0.57	62.64	0.00	0.00	HQ	14	R4	0	1	0
K-10-0298	51.51	53.65	2.14	2.22	103.74	1.15	53.74	HQ	35	R4	1	2	2
K-10-0298	53.65	56.69	3.04	3.04	100.00	2.17	71.38	HQ	38	R5	1	1	1
K-10-0298	56.69	58.67	1.98	1.73	87.37	0.93	46.97	HQ	18	R5	0	1	0
K-10-0298	58.67	59.47	0.80	1.01	126.25	0.10	12.50	HQ	24	R4	1	1	2
K-10-0298	59.47	61.57	2.10	1.80	85.71	1.43	68.10	HQ	18	R4	1	1	2
K-10-0298	61.57	62.48	0.91	1.07	117.58	0.42	46.15	HQ	15	R4	1	1	1
K-10-0298	62.48	65.23	2.75	2.61	94.91	1.72	62.55	HQ	20	R4	3	2	2
K-10-0298	65.23	66.45	1.22	1.24	101.64	1.05	86.07	HQ	3	R5	4	1	6
K-10-0298	66.45	68.88	2.43	2.60	107.00	2.60	107.00	HQ	8	R5	5	1	5
K-10-0298	68.88	70.71	1.83	1.81	98.91	1.55	84.70	HQ	5	R5	2	2	5
K-10-0298	70.71	71.93	1.22	1.10	90.16	0.45	36.89	HQ	3	R4	3	3	3
K-10-0298	71.93	73.76	1.83	1.80	98.36	1.37	74.86	HQ	11	R4	2	2	5
K-10-0298	73.76	74.98	1.22	1.19	97.54	1.19	97.54	HQ	2	R6	1	1	2
K-10-0298	74.98	77.72	2.74	2.66	97.08	2.39	87.23	HQ	11	R6	2	2	1
K-10-0298	77.72	80.01	2.29	2.34	102.18	1.69	73.80	HQ	16	R5	0	1	0
K-10-0298	80.01	81.08	1.07	1.17	109.35	0.76	71.03	HQ	9	R3	0	1	0
K-10-0298	81.08	84.13	3.05	2.80	91.80	2.04	66.89	HQ	19	R3	4	3	2
K-10-0298	84.13	85.34	1.21	1.33	109.92	1.01	83.47	HQ	5	R5	1	1	1
K-10-0298	85.34	87.17	1.83	1.68	91.80	1.40	76.50	HQ	9	R5	0	1	0
K-10-0298	87.17	88.09	0.92	0.92	100.00	0.92	100.00	HQ	3	R5	0		0
K-10-0298	88.09	90.22	2.13	2.13	100.00	1.64	77.00	HQ	14	R5	1	1	1
K-10-0298	90.22	92.81	2.59	2.59	100.00	1.88	72.59	HQ	25	R5	0		0
K-10-0298	92.81	93.27	0.46	0.35	76.09	0.14	30.43	HQ	0	R5	0		0
K-10-0298	93.27	95.10	1.83	1.74	95.08	0.96	52.46	HQ	17	R4	0		0
K-10-0298	95.10	96.01	0.91	0.90	98.90	0.27	29.67	HQ	9	R4	1	1	2
K-10-0298	96.01	99.06	3.05	2.66	87.21	1.84	60.33	HQ	18	R6	2	1	3
K-10-0298	99.06	99.37	0.31	0.23	74.19	0.23	74.19	HQ	0	R6	0		0
K-10-0298	99.37	100.13	0.76	0.76	100.00	0.66	86.84	HQ	5	R6	0		0
K-10-0298	100.13	102.11	1.98	1.80	90.91	1.08	54.55	HQ	14	R4	2	2	2
K-10-0298	102.11	102.41	0.30	0.30	100.00	0.30	100.00	HQ	0	R5	1	2	20
K-10-0298	102.41	103.78	1.37	1.34	97.81	0.32	23.36	HQ	12	R5	3	2	5
K-10-0298	103.78	105.46	1.68	1.63	97.02	0.11	6.55	HQ	16	R4	2	2	3
K-10-0298	105.46	107.29	1.83	1.83	100.00	1.37	74.86	HQ	11	R5	3	1	2
K-10-0298	107.29	108.51	1.22	1.20	98.36	0.47	38.52	HQ	12	R4	3	2	2
K-10-0298	108.51	110.03	1.52	1.44	94.74	1.22	80.26	HQ	7	R3	0	1	0
K-10-0298	110.03	111.56	1.53	1.47	96.08	1.01	66.01	HQ	9	R3	0	1	0
K-10-0298	111.56	112.17	0.61	0.61	100.00	0.14	22.95	HQ	6	R3	0	1	0
K-10-0298	112.17	113.39	1.22	0.94	77.05	0.00	0.00	HQ	11	R5	0	1	0
K-10-0298	113.39	114.15	0.76	0.76	100.00	0.46	60.53	HQ	8	R4	0	1	0
K-10-0298	114.15	115.06	0.91	0.80	87.91	0.41	45.05	HQ	6	R4	0	1	0
K-10-0298	115.06	116.74	1.68	1.57	93.45	1.06	63.10	HQ	10	R5	2	1	2
K-10-0298	116.74	118.26	1.52	1.52	100.00	0.76	50.00	HQ	13	R3	2	2	3
K-10-0298	118.26	119.18	0.92	0.92	100.00	0.39	42.39	HQ	8	R3	1	1	1
K-10-0298	119.18	121.62	2.44	2.14	87.70	1.55	63.52	HQ	15	R3	1	3	2
K-10-0298	121.62	122.23	0.61	0.51	83.61	0.15	24.59	HQ	5	R5	0	1	0
K-10-0298	122.23	122.53	0.30	0.30	100.00	0.11	36.67	HQ	3	R5	0	1	0
K-10-0298	122.53	123.75	1.22	1.11	90.98	0.75	61.48	HQ	6	R5	0	1	0
K-10-0298	123.75	124.21	0.46	0.46	100.00	0.14	30.43	HQ	11	R4	0	1	0
K-10-0298	124.21	125.88	1.67	1.62	97.01	0.87	52.10	HQ	7	R4	0	1	0
K-10-0298	125.88	126.80	0.92	0.84	91.30	0.70	76.09	HQ	3	R5	0	1	0
K-10-0298	126.80	129.85	3.05	3.04	99.67	1.86	60.98	HQ	15	R3	0	1	0
K-10-0298	129.85	131.06	1.21	1.21	100.00	0.37	30.58	HQ	7	R3	0	1	0
K-10-0298	131.06	132.04	0.98	0.98	100.00	0.92	93.88	HQ	9	R4	1	1	1
K-10-0298	132.04	132.89	0.85	0.22	25.88	0.16	18.82	HQ	1	R5	1	1	1
K-10-0298	132.89	135.48	2.59	2.59	100.00	2.33	89.96	HQ	11	R6	5	1	4
K-10-0298	135.48	135.94	0.46	0.29	63.04	0.14	30.43	HQ	2	R6	0	1	0
K-10-0298	135.94	138.68	2.74	2.74	100.00	2.10	76.64	HQ	12	R6	0	1	0
K-10-0298	138.68	138.99	0.31	0.26	83.87	0.26	83.87	HQ	0	R6	0	1	0
K-10-0298	138.99	140.21	1.22	1.22	100.00	0.93	76.23	HQ	7	R6	0	1	0
K-10-0298	140.21	142.04	1.83	1.79	97.81	1.39	75.96	HQ	7	R6	0	1	0
K-10-0298	142.04	143.56	1.52	1.52	100.00	1.24	81.58	HQ	10	R6	0	1	0
K-10-0298	143.56	145.09	1.53	1.28	83.66	0.93	60.78	HQ	4	R6	0	1	0
K-10-0298	145.09	147.22	2.13	2.06	96.71	0.97	45.54	HQ	15	R4	1	2	1
K-10-0298	147.22	148.13	0.91	0.79	86.81	0.33	36.26	HQ	7	R6	0	1	0
K-10-0298	148.13	150.11	1.98	1.98	100.00	0.40	20.20	HQ	22	R4	1	2	1
K-10-0298	150.11	151.18	1.07	0.99	92.52	0.32	29.91	HQ	12	R4	2	2	1
K-10-0298	151.18	151.94	0.76	0.68	89.47	0.35	46.05	HQ	16	R2	0		0
K-10-0298	151.94	153.62	1.68	1.59	94.64	0.95	56.55	HQ	18	R3	3	2	30
K-10-0298	153.62	154.23	0.61	0.41	67.21	0.24	39.34	HQ	9	R2	0		0
K-10-0298	154.23	155.14	0.91	0.86	94.51	0.21	23.08	HQ	20	R2	3	1	2
K-10-0298	155.14	156.97	1.83	1.53	83.61	0.44	24.04	HQ	24	R3	4	2	3
K-10-0298	156.97	157.28	0.31	0.29	93.55	0.00	0.00	HQ	3	R4	0		0
K-10-0298	157.28	158.95	1.67	1.63	97.60	1.05	62.87	HQ	8	R6	3	2	1

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0298	158.95	160.33	1.38	1.24	89.86	0.96	69.57	HQ	6	R6	4	1	5
K-10-0298	160.33	161.54	1.21	1.29	106.61	0.72	59.50	HQ	11	R6	3	2	1
K-10-0298	161.54	163.07	1.53	1.39	90.85	0.80	52.29	HQ	10	R5	0		0
K-10-0298	163.07	163.32	0.25	0.16	64.00	0.00	0.00	HQ	4	R3	0		0
K-10-0298	163.32	163.98	0.66	0.62	93.94	0.11	16.67	HQ	10	R5	5	2	2
K-10-0298	163.98	165.81	1.83	1.61	87.98	0.78	42.62	HQ	18	R4	11	2	40
K-10-0298	165.81	166.42	0.61	0.52	85.25	0.34	55.74	HQ	5	R4	6	2	10
K-10-0298	166.42	168.10	1.68	1.40	83.33	0.47	27.98	HQ	23	R4	14	2	30
K-10-0298	168.10	169.47	1.37	1.32	96.35	0.20	14.60	HQ	18	R3	5	2	5
K-10-0298	169.47	170.84	1.37	1.41	102.92	0.54	39.42	HQ	21	R3	5	2	20
K-10-0298	170.84	172.52	1.68	1.38	82.14	0.57	33.93	HQ	19	R4	0		0
K-10-0298	172.52	175.41	2.89	2.73	94.46	0.83	28.72	HQ	32	R5	8	2	3
K-10-0298	175.41	176.48	1.07	0.39	36.45	0.00	0.00	HQ	16	R2	0		0
K-10-0298	176.48	178.00	1.52	0.97	63.82	0.00	0.00	HQ	36	R2	0		0
K-10-0298	178.00	178.61	0.61	0.28	45.90	0.00	0.00	HQ	9	R1	0		0
K-10-0298	178.61	180.14	1.53	1.46	95.42	0.23	15.03	HQ	32	R2	2	2	3
K-10-0298	180.14	181.66	1.52	1.28	84.21	0.15	9.87	HQ	36	R2	2	2	1
K-10-0298	181.66	183.49	1.83	1.83	100.00	0.00	0.00	HQ	42	R2	8	2	4
K-10-0298	183.49	184.71	1.22	1.01	82.79	0.21	17.21	HQ	20	R3	2	2	2
K-10-0298	184.71	185.93	1.22	1.22	100.00	0.26	21.31	HQ	37	R3	4	2	2
K-10-0298	185.93	186.54	0.61	0.56	91.80	0.00	0.00	HQ	11	R3	1	1	1
K-10-0298	186.54	187.45	0.91	0.79	86.81	0.00	0.00	HQ	28	R2	4	2	3
K-10-0298	187.45	187.76	0.31	0.28	90.32	0.00	0.00	HQ	10	R2	3	2	2
K-10-0298	187.76	188.37	0.61	0.53	86.89	0.00	0.00	HQ	11	R3	1	1	1
K-10-0298	188.37	190.04	1.67	1.52	91.02	0.30	17.96	HQ	25	R3	3	1	2
K-10-0298	190.04	190.81	0.77	0.58	75.32	0.27	35.06	HQ	17	R3	4	1	2
K-10-0298	190.81	193.24	2.43	1.89	77.78	0.73	30.04	HQ	36	R3	5	2	5
K-10-0298	193.24	193.85	0.61	0.39	63.93	0.00	0.00	HQ	16	R2	0		0
K-10-0298	193.85	195.07	1.22	1.11	90.98	0.26	21.31	HQ	35	R3	4	2	15
K-10-0298	195.07	195.38	0.31	0.24	77.42	0.00	0.00	HQ	4	R3	1	2	25
K-10-0298	195.38	195.53	0.15	0.12	80.00	0.00	0.00	HQ	5	R3	0		0
K-10-0298	195.53	196.90	1.37	1.17	85.40	0.80	58.39	HQ	15	R4	8	2	10
K-10-0298	196.90	199.03	2.13	2.11	99.06	0.65	30.52	HQ	23	R3	12	2	30
K-10-0298	199.03	199.95	0.92	0.82	89.13	0.21	22.83	HQ	19	R3	3	1	5
K-10-0298	199.95	201.17	1.22	1.22	100.00	0.55	45.08	HQ	18	R4	5	1	10
K-10-0298	201.17	202.84	1.67	1.42	85.03	0.43	25.75	HQ	25	R3	9	1	5
K-10-0298	202.84	204.22	1.38	1.36	98.55	0.66	47.83	HQ	26	R3	4	2	5
K-10-0298	204.22	206.05	1.83	1.63	89.07	1.13	61.75	HQ	19	R4	11	1	15
K-10-0298	206.05	206.50	0.45	0.38	84.44	0.13	28.89	HQ	5	R4	3	1	2
K-10-0298	206.50	207.42	0.92	0.86	93.48	0.21	22.83	HQ	13	R3	4	2	10
K-10-0298	207.42	209.09	1.67	1.45	86.83	0.68	40.72	HQ	17	R3	16	2	5
K-10-0298	209.09	209.40	0.31	0.24	77.42	0.00	0.00	HQ	9	R2	0		0
K-10-0298	209.40	211.68	2.28	2.23	97.81	0.81	35.53	HQ	17	R4	6	2	25
K-10-0298	211.68	212.14	0.46	0.26	56.52	0.00	0.00	HQ	5	R4	0		0
K-10-0298	212.14	213.66	1.52	1.49	98.03	0.41	26.97	HQ	20	R5	4	1	5
K-10-0298	213.66	215.19	1.53	1.35	88.24	0.32	20.92	HQ	19	R4	14	2	10
K-10-0298	215.19	215.80	0.61	0.60	98.36	0.11	18.03	HQ	17	R4	2	1	1
K-10-0298	215.80	217.37	1.57	1.50	95.54	0.53	33.76	HQ	18	R4	14	1	30
K-10-0298	217.37	218.24	0.87	0.83	95.40	0.12	13.79	HQ	12	R3	3	1	2
K-10-0298	218.24	220.37	2.13	2.07	97.18	0.75	35.21	HQ	23	R4	6	1	10
K-10-0298	220.37	220.67	0.30	0.28	93.33	0.10	33.33	HQ	2	R5	0		0

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0299	0.00	7.13	OVB
K-10-0299	7.13	15.77	ICQS
K-10-0299	15.77	18.67	GSCH
K-10-0299	18.67	21.28	ICQS
K-10-0299	21.28	22.10	SSCH
K-10-0299	22.10	26.93	TQTZT
K-10-0299	26.93	31.13	TQTZT
K-10-0299	31.13	32.26	QTZT
K-10-0299	32.26	35.45	QTZT
K-10-0299	35.45	39.36	TQTZT
K-10-0299	39.36	41.15	QTZT
K-10-0299	41.15	44.53	QTZT
K-10-0299	44.53	46.12	TQTZT
K-10-0299	46.12	48.82	ICQS
K-10-0299	48.82	50.71	QTZT
K-10-0299	50.71	52.37	TQTZT
K-10-0299	52.37	66.91	TQTZT
K-10-0299	66.91	74.68	ICQS
K-10-0299	74.68	78.84	QTZT
K-10-0299	78.84	81.02	TQTZT
K-10-0299	81.02	83.13	ICQS
K-10-0299	83.13	85.83	TQTZT
K-10-0299	85.83	92.59	QTZT
K-10-0299	92.59	96.72	TQTZT
K-10-0299	96.72	100.83	ICQS
K-10-0299	100.83	104.09	SSCH
K-10-0299	104.09	105.07	ICQS
K-10-0299	105.07	108.49	QTZT
K-10-0299	108.49	110.02	ICQS
K-10-0299	110.02	118.70	TQTZT
K-10-0299	118.70	120.81	QTZT
K-10-0299	120.81	128.11	TQTZT
K-10-0299	128.11	130.61	TQTZT
K-10-0299	130.61	138.86	QTZT
K-10-0299	138.86	139.82	ICQS
K-10-0299	139.82	142.58	SSCH
K-10-0299	142.58	151.57	ICQS
K-10-0299	151.57	154.99	TQTZT
K-10-0299	154.99	172.34	TQTZT
K-10-0299	172.34	173.41	TQTZT
K-10-0299	173.41	174.80	QTZT
K-10-0299	174.80	177.24	QTZT
K-10-0299	177.24	180.93	TQTZT
K-10-0299	180.93	181.62	ICQS
K-10-0299	181.62	186.78	QTZT
K-10-0299	186.78	187.68	ICQS
K-10-0299	187.68	188.62	ICQS
K-10-0299	188.62	190.95	QTZT
K-10-0299	190.95	192.36	QTZT
K-10-0299	192.36	198.68	ICQS
K-10-0299	198.68	199.64	QTZT
K-10-0299	199.64	201.30	TQTZT
K-10-0299	201.30	202.00	NR
K-10-0299	202.00	203.10	QTZT
K-10-0299	203.10	204.66	ICQS
K-10-0299	204.66	207.80	QTZT
K-10-0299	207.80	209.44	TQTZT
K-10-0299	209.44	213.44	TQTZT
K-10-0299	213.44	218.66	TQTZT
K-10-0299	218.66	219.96	TQTZT
K-10-0299	219.96	223.74	ICQS
K-10-0299	223.74	227.03	QTZT
K-10-0299	227.03	228.73	TQTZT
K-10-0299	228.73	229.56	ICQS
K-10-0299	229.56	231.36	ICQS
K-10-0299	231.36	235.06	TQTZT
K-10-0299	235.06	235.53	VL
K-10-0299	235.53	236.78	TQTZT
K-10-0299	236.78	237.66	VM
K-10-0299	237.66	239.46	VM
K-10-0299	239.46	241.43	VM
K-10-0299	241.43	242.22	VM
K-10-0299	242.22	242.75	SM
K-10-0299	242.75	243.29	VL
K-10-0299	243.29	243.85	SM
K-10-0299	243.85	245.36	SM
K-10-0299	245.36	246.61	SM
K-10-0299	246.61	247.18	SM
K-10-0299	247.18	247.68	VM
K-10-0299	247.68	248.41	VM

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0299	248.41	248.67	GNST
K-10-0299	248.67	256.20	TQTZT
K-10-0299	256.20	258.05	ICQS
K-10-0299	258.05	261.14	QTZT
K-10-0299	261.14	262.32	TQTZT
K-10-0299	262.32	266.30	GNST
K-10-0299	266.30	270.12	TQTZT
K-10-0299	270.12	270.96	ICQS
K-10-0299	270.96	271.84	TQTZT
K-10-0299	271.84	273.80	SM
K-10-0299	273.80	277.91	SM
K-10-0299	277.91	281.30	SM
K-10-0299	281.30	282.20	FLT
K-10-0299	282.20	282.76	QTZT
K-10-0299	282.76	285.46	ICQS
K-10-0299	285.46	286.03	QTZT
K-10-0299	286.03	286.51	ICQS
K-10-0299	286.51	287.03	TQTZT
K-10-0299	287.03	289.90	FLT
K-10-0299	289.90	291.00	SM
K-10-0299	291.00	292.44	SM
K-10-0299	292.44	293.47	SM
K-10-0299	293.47	294.18	ICQS
K-10-0299	294.18	295.70	SM
K-10-0299	295.70	296.29	ICQS
K-10-0299	296.29	297.37	SM
K-10-0299	297.37	298.17	ICQS
K-10-0299	298.17	298.63	TQTZT
K-10-0299	298.63	299.37	ICQS
K-10-0299	299.37	300.42	TQTZT
K-10-0299	300.42	302.83	QTZT
K-10-0299	302.83	305.39	TQTZT
K-10-0299	305.39	306.32	QTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0299	0.00	3.05	3.05	0.64	20.98	0.00	0.00	HTW	0	R0	0		
K-10-0299	3.05	4.57	1.52	0.37	24.34	0.00	0.00	HTW	0	R0	0		
K-10-0299	4.57	6.10	1.53	0.54	35.29	0.00	0.00	HTW	0	R0	0		
K-10-0299	6.10	7.62	1.52	0.62	40.79	0.49	32.24	HTW	3	R3	2	1	2
K-10-0299	7.62	9.14	1.52	1.52	100.00	1.38	90.79	HTW	9	R3	2	1	1
K-10-0299	9.14	10.67	1.53	1.45	94.77	1.40	91.50	HTW	9	R3	2	1	0.5
K-10-0299	10.67	12.19	1.52	1.10	72.37	0.57	37.50	HTW	18	R4	2	2	2
K-10-0299	12.19	13.72	1.53	1.52	99.35	0.73	47.71	HTW	29	R4	1	1	0.5
K-10-0299	13.72	15.24	1.52	1.43	94.08	0.74	48.68	NTW	22	R4	3	1	4
K-10-0299	15.24	16.76	1.52	1.27	83.55	0.00	0.00	NTW	34	R2	1	1	2
K-10-0299	16.76	18.26	1.50	1.33	88.67	0.22	14.67	NTW	43	R2	0		0
K-10-0299	18.26	19.81	1.55	1.52	98.06	0.84	54.19	NTW	21	R3	2	2	1
K-10-0299	19.81	21.34	1.53	1.49	97.39	1.22	79.74	NTW	13	R3	4	1	5
K-10-0299	21.34	22.86	1.52	1.52	100.00	1.00	65.79	NTW	20	R3	3	1	1
K-10-0299	22.86	24.38	1.52	1.52	100.00	1.33	87.50	NTW	16	R3	3	1	4
K-10-0299	24.38	25.91	1.53	1.41	92.16	1.16	75.82	NTW	14	R4	2	1	0.5
K-10-0299	25.91	27.43	1.52	1.49	98.03	1.02	67.11	NTW	23	R3	1	1	0.5
K-10-0299	27.43	28.96	1.53	1.52	99.35	0.53	34.64	NTW	31	R2	0		0
K-10-0299	28.96	30.48	1.52	1.46	96.05	0.47	30.92	NTW	16	R3	2	1	1
K-10-0299	30.48	32.00	1.52	1.12	73.68	0.34	22.37	NTW	25	R3	0		0
K-10-0299	32.00	33.53	1.53	1.45	94.77	0.78	50.98	NTW	18	R3	3	1	3
K-10-0299	33.53	35.05	1.52	1.37	90.13	0.77	50.66	NTW	15	R2	4	1	5
K-10-0299	35.05	36.58	1.53	1.41	92.16	0.84	54.90	NTW	16	R3	7	1	3
K-10-0299	36.58	38.10	1.52	1.35	88.82	0.89	58.55	NTW	10	R4	3	1	1
K-10-0299	38.10	39.62	1.52	1.52	100.00	0.97	63.82	NTW	12	R3	2	1	1
K-10-0299	39.62	41.15	1.53	1.48	96.73	0.92	60.13	NTW	9	R3	0		0
K-10-0299	41.15	42.67	1.52	1.43	94.08	1.14	75.00	NTW	9	R3	1	1	0.5
K-10-0299	42.67	44.20	1.53	1.50	98.04	1.20	78.43	NTW	8	R3	4	2	2
K-10-0299	44.20	45.72	1.52	1.46	96.05	0.67	44.08	NTW	16	R2	6	1	3
K-10-0299	45.72	47.24	1.52	1.31	86.18	0.32	21.05	NTW	37	R1	2	1	1
K-10-0299	47.24	48.77	1.53	1.49	97.39	0.76	49.67	NTW	20	R2	1	1	0.5
K-10-0299	48.77	50.29	1.52	1.48	97.37	0.34	22.37	NTW	15	R3	5	1	1
K-10-0299	50.29	51.82	1.53	1.47	96.08	0.62	40.52	NTW	27	R3	7	1	3
K-10-0299	51.82	53.34	1.52	1.33	87.50	0.59	38.82	NTW	25	R3	3	1	0.5
K-10-0299	53.34	54.86	1.52	1.42	93.42	0.71	46.71	NTW	19	R3	8	1	3
K-10-0299	54.86	56.39	1.53	1.21	79.08	0.25	16.34	NTW	26	R3	2	1	1
K-10-0299	56.39	57.91	1.52	1.41	92.76	0.76	50.00	NTW	22	R2	3	1	1
K-10-0299	57.91	59.44	1.53	1.44	94.12	0.43	28.10	NTW	23	R2	2	1	0.5
K-10-0299	59.44	60.96	1.52	1.24	81.58	0.71	46.71	NTW	14	R2	2	1	0.5
K-10-0299	60.96	62.48	1.52	1.33	87.50	0.76	50.00	NTW	28	R2	3	1	0.5
K-10-0299	62.48	64.01	1.53	1.50	98.04	0.28	18.30	NTW	21	R1	4	1	1
K-10-0299	64.01	65.53	1.52	1.52	100.00	0.28	18.42	NTW	36	R1	3	1	2
K-10-0299	65.53	67.06	1.53	1.39	90.85	0.59	38.56	NTW	27	R2	4	1	1
K-10-0299	67.06	68.58	1.52	1.33	87.50	0.55	36.18	NTW	21	R2	4	1	2
K-10-0299	68.58	70.10	1.52	1.49	98.03	1.18	77.63	NTW	12	R2	7	1	2
K-10-0299	70.10	71.63	1.53	1.30	84.97	0.45	29.41	NTW	13	R2	6	1	3
K-10-0299	71.63	73.15	1.52	1.46	96.05	0.96	63.16	NTW	8	R2	11	1	2
K-10-0299	73.15	74.68	1.53	1.34	87.58	0.17	11.11	NTW	39	R1	5	1	1
K-10-0299	74.68	76.20	1.52	1.10	72.37	0.35	23.03	NTW	31	R2	2	1	0.5
K-10-0299	76.20	77.72	1.52	0.61	40.13	0.00	0.00	NTW	0	R1	0		
K-10-0299	77.72	79.25	1.53	1.31	85.62	0.56	36.60	NTW	21	R3	3	1	1
K-10-0299	79.25	80.77	1.52	1.47	96.71	0.86	56.58	NTW	14	R3	5	1	2
K-10-0299	80.77	82.30	1.53	1.48	96.73	1.23	80.39	NTW	9	R3	4	1	1
K-10-0299	82.30	83.82	1.52	1.43	94.08	1.12	73.68	NTW	9	R3	11	2	5
K-10-0299	83.82	85.34	1.52	1.44	94.74	1.08	71.05	NTW	8	R4	5	2	2
K-10-0299	85.34	86.87	1.53	1.39	90.85	0.78	50.98	NTW	12	R4	3	1	1
K-10-0299	86.87	88.39	1.52	1.46	96.05	1.26	82.89	NTW	7	R4	6	1	4
K-10-0299	88.39	89.92	1.53	1.47	96.08	1.16	75.82	NTW	9	R4	3	1	2
K-10-0299	89.92	91.44	1.52	1.39	91.45	0.99	65.13	NTW	7	R4	4	1	2
K-10-0299	91.44	92.96	1.52	1.44	94.74	1.11	73.03	NTW	10	R4	15	1	20
K-10-0299	92.96	94.49	1.53	1.43	93.46	0.67	43.79	NTW	12	R4	1	1	0.5
K-10-0299	94.49	96.01	1.52	1.42	93.42	0.65	42.76	NTW	11	R4	6	1	3
K-10-0299	96.01	97.54	1.53	1.50	98.04	0.85	55.56	NTW	14	R3	8	1	5
K-10-0299	97.54	99.06	1.52	1.51	99.34	0.86	56.58	NTW	24	R3	14	1	7
K-10-0299	99.06	100.58	1.52	1.33	87.50	0.69	45.39	NTW	21	R2	12	1	3
K-10-0299	100.58	102.11	1.53	1.46	95.42	0.93	60.78	NTW	19	R3	16	1	5
K-10-0299	102.11	103.63	1.52	1.43	94.08	0.78	51.32	NTW	16	R3	5	1	8
K-10-0299	103.63	105.16	1.53	1.27	83.01	0.69	45.10	NTW	14	R3	4	1	2
K-10-0299	105.16	106.58	1.42	1.41	99.30	0.89	62.68	NTW	9	R4	8	1	4
K-10-0299	106.58	108.20	1.62	1.36	83.95	0.98	60.49	NTW	9	R4	4	1	2
K-10-0299	108.20	109.73	1.53	1.52	99.35	0.45	29.41	NTW	13	R3	5	1	2
K-10-0299	109.73	111.25	1.52	1.36	89.47	0.80	52.63	NTW	11	R4	6	1	3
K-10-0299	111.25	112.78	1.53	1.40	91.50	0.90	58.82	NTW	9	R5	5	1	2
K-10-0299	112.78	114.30	1.52	1.39	91.45	0.77	50.66	NTW	12	R5	6	2	2
K-10-0299	114.30	115.82	1.52	1.40	92.11	1.16	76.32	NTW	7	R5	5	2	5
K-10-0299	115.82	117.35	1.53	1.52	99.35	1.33	86.93	NTW	8	R4	2	2	2
K-10-0299	117.35	118.87	1.52	1.49	98.03	1.18	77.63	NTW	7	R4	8	2	5
K-10-0299	118.87	120.04	1.17	1.17	100.00	0.88	75.21	NTW	5	R5	2	1	2
K-10-0299	120.04	121.92	1.88	1.40	74.47	0.96	51.06	NTW	7	R4	5	1	3
K-10-0299	121.92	123.44	1.52	1.37	90.13	0.50	32.89	NTW	11	R5	25	2	1
K-10-0299	123.44	124.97	1.53	1.43	93.46	0.84	54.90	NTW	12	R5	5	1	4
K-10-0299	124.97	126.49	1.52	1.44	94.74	0.92	60.53	NTW	10	R3	7	2	5
K-10-0299	126.49	128.02	1.53	1.49	97.39	1.20	78.43	NTW	6	R5	7	1	20
K-10-0299	128.02	129.54	1.52	1.47	96.71	0.88	57.89	NTW	9	R5	12	2	30
K-10-0299	129.54	131.00	1.46	1.44	98.63	0.64	43.84	NTW	15	R5	7	2	40
K-10-0299	131.00	132.59	1.59	1.38	86.79	0.93	58.49	NTW	7	R6	3	1	5
K-10-0299	132.59	134.11	1.52	1.44	94.74	1.02	67.11	NTW	9	R6	6	2	7
K-10-0299	134.11	135.64	1.53	1.37	89.54	0.91	59.48	NTW	6	R4	13	2	25
K-10-0299	135.64	137.16	1.52	1.41	92.76	1.00	65.79	NTW	9	R5	10	2	40
K-10-0299	137.16	138.68	1.52	1.45	95.39	1.41	92.76	NTW	3	R6	2	2	1
K-10-0299	138.68	140.21	1.53	1.26	82.35	0.52	33.99	NTW	15	R4	6	1	10
K-10-0299	140.21	141.73	1.52	1.43	94.08	1.18	77.63	NTW	7	R5	18	1	20
K-10-0299	141.73	143.26	1.53	1.48	96.73	0.76	49.67	NTW	11	R3	8	2	8
K-10-0299	143.26	144.78	1.52	1.38	90.79	0.42	27.63	NTW	18	R3	9	1	5
K-10-0299	144.78	146.30	1.52	1.46	96.05	0.60	39.47	NTW	15	R3	5	2	5
K-10-0299	146.30	147.83	1.53	1.49	97.39	1.10	71.90	NTW	7	R3	4	2	20
K-10-0299	147.83	149.35	1.52	1.30	85.53	0.74	48.68	NTW	10	R3	7	1	10

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0299	149.35	150.88	1.53	1.29	84.31	0.19	12.42	NTW	26	R3	6	1	3
K-10-0299	150.88	152.40	1.52	1.38	90.79	1.26	82.89	NTW	8	R4	9	1	2
K-10-0299	152.40	153.92	1.52	1.42	93.42	0.55	36.18	NTW	13	R5	7	1	5
K-10-0299	153.92	155.45	1.53	1.36	88.89	0.91	59.48	NTW	9	R4	4	2	5
K-10-0299	155.45	156.97	1.52	1.49	98.03	0.56	36.84	NTW	11	R3	5	2	2
K-10-0299	156.97	158.50	1.53	1.37	89.54	0.86	56.21	NTW	14	R4	6	1	4
K-10-0299	158.50	160.02	1.52	1.38	90.79	0.87	57.24	NTW	10	R4	4	2	10
K-10-0299	160.02	161.54	1.52	1.40	92.11	0.90	59.21	NTW	11	R4	6	2	5
K-10-0299	161.54	163.07	1.53	1.33	86.93	0.74	48.37	NTW	11	R3	8	2	20
K-10-0299	163.07	164.59	1.52	1.29	84.87	0.61	40.13	NTW	16	R3	2	1	2
K-10-0299	164.59	166.12	1.53	1.44	94.12	0.33	21.57	NTW	24	R3	9	2	5
K-10-0299	166.12	167.64	1.52	1.32	86.84	0.12	7.89	NTW	27	R3	8	2	15
K-10-0299	167.64	169.16	1.52	1.20	78.95	0.27	17.76	NTW	29	R2	10	2	10
K-10-0299	169.16	170.69	1.53	1.40	91.50	0.59	38.56	NTW	20	R3	5	2	5
K-10-0299	170.69	172.21	1.52	1.42	93.42	0.75	49.34	NTW	19	R4	7	2	5
K-10-0299	172.21	173.74	1.53	1.24	81.05	0.67	43.79	NTW	14	R3	6	1	2
K-10-0299	173.74	175.26	1.52	1.40	92.11	0.97	63.82	NTW	8	R4	2	1	1
K-10-0299	175.26	176.78	1.52	1.22	80.26	0.48	31.58	NTW	13	R3	0		0
K-10-0299	176.78	178.31	1.53	1.47	96.08	0.22	14.38	NTW	21	R3	7	2	3
K-10-0299	178.31	179.83	1.52	1.37	90.13	0.81	53.29	NTW	17	R3	3	2	2
K-10-0299	179.83	181.36	1.53	1.48	96.73	0.53	34.64	NTW	15	R3	6	1	4
K-10-0299	181.36	182.88	1.52	1.41	92.76	0.69	45.39	NTW	13	R4	3	1	2
K-10-0299	182.88	184.40	1.52	1.43	94.08	1.07	70.39	NTW	4	R6	4	1	5
K-10-0299	184.40	185.93	1.53	1.51	98.69	1.10	71.90	NTW	12	R5	3	1	3
K-10-0299	185.93	187.45	1.52	1.46	96.05	0.65	42.76	NTW	10	R5	6	2	5
K-10-0299	187.45	188.98	1.53	1.47	96.08	1.11	72.55	NTW	11	R3	7	2	20
K-10-0299	188.98	190.50	1.52	1.41	92.76	1.01	66.45	NTW	10	R3	7	3	20
K-10-0299	190.50	192.02	1.52	1.19	78.29	0.61	40.13	NTW	27	R3	5	1	3
K-10-0299	192.02	193.55	1.53	1.46	95.42	1.03	67.32	NTW	9	R3	8	2	20
K-10-0299	193.55	195.07	1.52	1.41	92.76	0.53	34.87	NTW	32	R2	4	1	3
K-10-0299	195.07	196.60	1.53	1.38	90.20	0.00	0.00	NTW	36	R2	3	2	2
K-10-0299	196.60	198.12	1.52	1.36	89.47	0.81	53.29	NTW	10	R3	15	1	10
K-10-0299	198.12	199.64	1.52	1.19	78.29	0.47	30.92	NTW	18	R3	5	2	10
K-10-0299	199.64	201.17	1.53	1.21	79.08	0.12	7.84	NTW	33	R2	2	2	2
K-10-0299	201.17	202.69	1.52	0.83	54.61	0.00	0.00	NTW	25	R2	1	1	2
K-10-0299	202.69	204.22	1.53	1.46	95.42	1.21	79.08	NTW	8	R3	6	2	5
K-10-0299	204.22	205.74	1.52	1.37	90.13	0.76	50.00	NTW	6	R4	4	1	10
K-10-0299	205.74	207.26	1.52	1.47	96.71	0.57	37.50	NTW	7	R5	14	2	15
K-10-0299	207.26	208.79	1.53	1.09	71.24	0.21	13.73	NTW	31	R3	10	2	10
K-10-0299	208.79	210.31	1.52	1.37	90.13	0.73	48.03	NTW	13	R4	1	1	1
K-10-0299	210.31	211.84	1.53	1.36	88.89	0.68	44.44	NTW	12	R4	1	1	2
K-10-0299	211.84	213.36	1.52	1.14	75.00	0.00	0.00	NTW	33	R3	2	1	2
K-10-0299	213.36	214.88	1.52	1.52	100.00	0.27	17.76	NTW	44	R2	1	1	1
K-10-0299	214.88	216.41	1.53	1.47	96.08	0.98	64.05	NTW	17	R3	6	2	2
K-10-0299	216.41	217.93	1.52	1.39	91.45	0.56	36.84	NTW	18	R3	4	2	2
K-10-0299	217.93	219.46	1.53	1.58	103.27	0.31	20.26	NTW	40	R3	4	1	1
K-10-0299	219.46	220.98	1.52	1.47	96.71	0.62	40.79	NTW	25	R4	15	2	15
K-10-0299	220.98	222.50	1.52	1.48	97.37	0.16	10.53	NTW	31	R2	5	2	5
K-10-0299	222.50	224.03	1.53	1.31	85.62	0.20	13.07	NTW	38	R3	3	2	5
K-10-0299	224.03	225.55	1.52	1.02	67.11	0.38	25.00	NTW	23	R3	2	2	2
K-10-0299	225.55	227.08	1.53	1.33	86.93	0.61	39.87	NTW	27	R3	4	1	2
K-10-0299	227.08	228.60	1.52	1.45	95.39	0.25	16.45	NTW	21	R3	1	1	1
K-10-0299	228.60	230.12	1.52	1.40	92.11	0.62	40.79	NTW	17	R3	6	1	5
K-10-0299	230.12	231.65	1.53	1.46	95.42	0.51	33.33	NTW	13	R3	4	2	2
K-10-0299	231.65	233.17	1.52	1.43	94.08	0.68	44.74	NTW	17	R4	6	1	1
K-10-0299	233.17	234.70	1.53	1.36	88.89	0.22	14.38	NTW	20	R4	5	2	5
K-10-0299	234.70	236.22	1.52	1.37	90.13	0.38	25.00	NTW	21	R4	7	1	20
K-10-0299	236.22	237.44	1.22	1.22	100.00	0.82	67.21	NTW	21	R5	6	2	40
K-10-0299	237.44	239.27	1.83	1.48	80.87	1.43	78.14	NTW	5	R5	13	2	70
K-10-0299	239.27	240.79	1.52	1.50	98.68	1.50	98.68	NTW	3	R5	11	2	70
K-10-0299	240.79	242.32	1.53	1.49	97.39	1.03	67.32	NTW	6	R4	14	2	70
K-10-0299	242.32	243.84	1.52	1.49	98.03	1.34	88.16	NTW	5	R5	8	2	50
K-10-0299	243.84	245.36	1.52	1.48	97.37	1.28	84.21	NTW	2	R5	15	2	40
K-10-0299	245.36	246.89	1.53	1.44	94.12	1.23	80.39	NTW	6	R5	5	1	10
K-10-0299	246.89	248.41	1.52	1.31	86.18	0.97	63.82	NTW	9	R4	8	2	25
K-10-0299	248.41	249.94	1.53	1.50	98.04	0.86	56.21	NTW	15	R4	6	1	10
K-10-0299	249.94	251.46	1.52	1.44	94.74	1.07	70.39	NTW	10	R5	7	2	10
K-10-0299	251.46	252.98	1.52	1.45	95.39	1.17	76.97	NTW	12	R5	5	1	5
K-10-0299	252.98	254.51	1.53	1.46	95.42	0.98	64.05	NTW	15	R4	5	1	2
K-10-0299	254.51	256.03	1.52	1.41	92.76	0.71	46.71	NTW	14	R4	2	2	1
K-10-0299	256.03	257.56	1.53	1.47	96.08	0.52	33.99	NTW	22	R3	11	2	5
K-10-0299	257.56	259.08	1.52	1.42	93.42	0.57	37.50	NTW	21	R3	5	1	5
K-10-0299	259.08	260.60	1.52	1.40	92.11	1.00	65.79	NTW	9	R5	2	1	1
K-10-0299	260.60	262.13	1.53	1.44	94.12	1.08	70.59	NTW	10	R4	8	2	5
K-10-0299	262.13	263.65	1.52	1.52	100.00	1.40	92.11	NTW	3	R6	0		0
K-10-0299	263.65	265.18	1.53	1.41	92.16	1.15	75.16	NTW	2	R6	2	1	1
K-10-0299	265.18	266.70	1.52	1.49	98.03	1.10	72.37	NTW	7	R6	8	2	10
K-10-0299	266.70	268.22	1.52	1.44	94.74	0.71	46.71	NTW	11	R5	4	2	5
K-10-0299	268.22	269.75	1.53	1.25	81.70	0.83	54.25	NTW	12	R5	7	2	10
K-10-0299	269.75	271.27	1.52	1.41	92.76	0.66	43.42	NTW	11	R4	7	1	5
K-10-0299	271.27	272.80	1.53	1.36	88.89	0.63	41.18	NTW	9	R5	6	2	5
K-10-0299	272.80	274.32	1.52	1.31	86.18	0.80	52.63	NTW	12	R4	6	2	7
K-10-0299	274.32	275.84	1.52	1.40	92.11	0.46	30.26	NTW	9	R4	5	1	5
K-10-0299	275.84	277.37	1.53	1.28	83.66	1.12	73.20	NTW	20	R4	5	1	2
K-10-0299	277.37	278.89	1.52	1.42	93.42	0.26	17.11	NTW	16	R3	10	2	10
K-10-0299	278.89	280.42	1.53	1.47	96.08	0.69	45.10	NTW	12	R4	11	1	20
K-10-0299	280.42	281.94	1.52	1.50	98.68	0.58	38.16	NTW	16	R3	5	2	5
K-10-0299	281.94	283.46	1.52	1.30	85.53	0.41	26.97	NTW	31	R3	8	2	15
K-10-0299	283.46	284.99	1.53	1.44	94.12	0.42	27.45	NTW	22	R3	16	1	15
K-10-0299	284.99	286.31	1.32	1.32	100.00	0.51	38.64	NTW	21	R3	8	1	5
K-10-0299	286.31	288.04	1.73	1.43	82.66	0.11	6.36	NTW	32	R2	12	2	20
K-10-0299	288.04	289.56	1.52	1.15	75.66	0.00	0.00	NTW	44	R2	5	2	5
K-10-0299	289.56	291.08	1.52	1.52	100.00	0.68	44.74	NTW	34	R3	10	2	10
K-10-0299	291.08	292.61	1.53	1.39	90.85	0.65	42.48	NTW	12	R4	19	2	40
K-10-0299	292.61	294.13	1.52	1.50	98.68	0.98	64.47	NTW	9	R5	11	1	15
K-10-0299	294.13	295.66	1.53	1.45	94.77	0.52	33.99	NTW	18	R4	15	2	20
K-10-0299	295.66	297.18	1.52	1.41	92.76	0.82	53.95	NTW	11	R4	10	1	20

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0299	297.18	298.70	1.52	1.50	98.68	0.56	36.84	NTW	17	R4	9	1	10
K-10-0299	298.70	300.23	1.53	1.41	92.16	0.44	28.76	NTW	20	R3	13	1	5
K-10-0299	300.23	301.75	1.52	1.43	94.08	1.16	76.32	NTW	5	R5	4	2	2
K-10-0299	301.75	303.28	1.53	1.52	99.35	1.11	72.55	NTW	4	R6	5	2	10
K-10-0299	303.28	304.80	1.52	1.40	92.11	0.85	55.92	NTW	10	R5	5	1	5
K-10-0299	304.80	306.32	1.52	1.34	88.16	0.86	56.58	NTW	14	R5	9	1	5

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0303	0.00	4.70	OVB
K-10-0303	4.70	11.52	ICQS
K-10-0303	11.52	14.32	GSCH
K-10-0303	14.32	15.29	SSCH
K-10-0303	15.29	17.58	ICQS
K-10-0303	17.58	19.43	SSCH
K-10-0303	19.43	28.37	TQTZT
K-10-0303	28.37	35.43	QTZT
K-10-0303	35.43	39.47	TQTZT
K-10-0303	39.47	43.77	ICQS
K-10-0303	43.77	48.99	TQTZT
K-10-0303	48.99	52.85	QTZT
K-10-0303	52.85	61.47	TQTZT
K-10-0303	61.47	69.05	ICQS
K-10-0303	69.05	74.56	TQTZT
K-10-0303	74.56	76.21	ICQS
K-10-0303	76.21	85.62	QTZT
K-10-0303	85.62	90.00	TQTZT
K-10-0303	90.00	94.32	ICQS
K-10-0303	94.32	96.66	SSCH
K-10-0303	96.66	97.43	ICQS
K-10-0303	97.43	99.05	SSCH
K-10-0303	99.05	100.77	ICQS
K-10-0303	100.77	123.90	TQTZT
K-10-0303	123.90	130.33	QTZT
K-10-0303	130.33	133.59	TQTZT
K-10-0303	133.59	134.58	GSCH
K-10-0303	134.58	136.35	SSCH
K-10-0303	136.35	138.30	TQTZT
K-10-0303	138.30	141.72	QTZT
K-10-0303	141.72	143.50	ICQS
K-10-0303	143.50	154.90	TQTZT
K-10-0303	154.90	157.18	FLT
K-10-0303	157.18	161.48	TQTZT
K-10-0303	161.48	166.60	QTZT
K-10-0303	166.60	170.21	TQTZT
K-10-0303	170.21	171.20	TQTZT
K-10-0303	171.20	173.09	FLT
K-10-0303	173.09	175.64	QTZT
K-10-0303	175.64	176.21	FLT
K-10-0303	176.21	177.31	QTZT
K-10-0303	177.31	184.81	GNST
K-10-0303	184.81	188.85	QTZT
K-10-0303	188.85	190.74	ICQS
K-10-0303	190.74	196.62	QTZT
K-10-0303	196.62	204.33	TQTZT
K-10-0303	204.33	209.09	MCQ
K-10-0303	209.09	212.65	TQTZT
K-10-0303	212.65	213.81	ICQS
K-10-0303	213.81	217.76	TQTZT
K-10-0303	217.76	221.78	ICQS
K-10-0303	221.78	224.97	QTZT
K-10-0303	224.97	227.06	ICQS
K-10-0303	227.06	230.09	TQTZT
K-10-0303	230.09	236.58	QTZT
K-10-0303	236.58	239.77	TQTZT
K-10-0303	239.77	280.30	GNST
K-10-0303	280.30	287.15	SM
K-10-0303	287.15	288.43	VM
K-10-0303	288.43	295.60	SM
K-10-0303	295.60	301.37	SM
K-10-0303	301.37	302.15	SM
K-10-0303	302.15	303.66	VM
K-10-0303	303.66	306.15	FLT
K-10-0303	306.15	307.60	QTZT
K-10-0303	307.60	310.56	ICQS
K-10-0303	310.56	312.63	QTZT
K-10-0303	312.63	315.39	ICQS
K-10-0303	315.39	317.25	QTZT
K-10-0303	317.25	318.41	ICQS
K-10-0303	318.41	327.06	QTZT
K-10-0303	327.06	329.58	QTZT
K-10-0303	329.58	330.84	ICQS
K-10-0303	330.84	332.47	QTZT
K-10-0303	332.47	334.39	TQTZT
K-10-0303	334.39	335.71	GSCH
K-10-0303	335.71	338.60	QTZT
K-10-0303	338.60	339.06	ICQS
K-10-0303	339.06	340.84	QTZT
K-10-0303	340.84	342.30	TQTZT

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0303	342.30	343.30	ICQS
K-10-0303	343.30	345.48	ICQS
K-10-0303	345.48	346.72	QTZT
K-10-0303	346.72	348.08	ICQS

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0303	0.00	4.57	4.57	1.65	36.11	0.32	7.00	HTW					
K-10-0303	4.57	6.10	1.53	1.74	113.73	0.91	59.48	HTW					
K-10-0303	6.10	7.62	1.52	1.58	103.95	0.94	61.84	HTW					
K-10-0303	7.62	9.14	1.52	1.66	109.21	0.86	56.58	HTW					
K-10-0303	9.14	10.67	1.53	1.23	80.39	0.35	22.88	HTW					
K-10-0303	10.67	12.19	1.52	1.34	88.16	0.00	0.00	HTW					
K-10-0303	12.19	13.72	1.53	1.23	80.39	0.00	0.00	HTW					
K-10-0303	13.72	15.24	1.52	1.50	98.68	0.20	13.16	HTW					
K-10-0303	15.24	16.76	1.52	1.44	94.74	0.44	28.95	HTW					
K-10-0303	16.76	18.29	1.53	1.38	90.20	0.59	38.56	HTW					
K-10-0303	18.29	19.81	1.52	1.26	82.89	0.51	33.55	HTW					
K-10-0303	19.81	21.34	1.53	1.19	77.78	0.29	18.95	NTW					
K-10-0303	21.34	22.86	1.52	1.22	80.26	0.24	15.79	NTW					
K-10-0303	22.86	24.38	1.52	1.38	90.79	0.91	59.87	NTW					
K-10-0303	24.38	25.91	1.53	1.37	89.54	1.19	77.78	NTW					
K-10-0303	25.91	27.43	1.52	1.43	94.08	1.41	92.76	NTW					
K-10-0303	27.43	28.96	1.53	1.40	91.50	0.39	25.49	NTW					
K-10-0303	28.96	30.48	1.52	1.46	96.05	0.89	58.55	NTW					
K-10-0303	30.48	33.53	3.05	2.87	94.10	1.65	54.10	NTW					
K-10-0303	33.53	36.58	3.05	2.54	83.28	1.08	35.41	NTW					
K-10-0303	36.58	39.62	3.04	2.86	94.08	1.38	45.39	NTW					
K-10-0303	39.62	42.67	3.05	2.47	80.98	1.53	50.16	NTW					
K-10-0303	42.67	45.72	3.05	2.35	77.05	0.57	18.69	NTW					
K-10-0303	45.72	48.77	3.05	1.93	63.28	0.00	0.00	NTW					
K-10-0303	48.77	51.82	3.05	2.56	83.93	1.48	48.52	NTW					
K-10-0303	51.82	54.86	3.04	2.52	82.89	0.81	26.64	NTW					
K-10-0303	54.86	57.91	3.05	2.57	84.26	0.74	24.26	NTW					
K-10-0303	57.91	60.96	3.05	2.44	80.00	0.57	18.69	NTW					
K-10-0303	60.96	62.48	1.52	1.34	88.16	0.51	33.55	NTW					
K-10-0303	62.48	65.53	3.05	2.86	93.77	0.64	20.98	NTW					
K-10-0303	65.53	68.58	3.05	2.79	91.48	0.82	26.89	NTW					
K-10-0303	68.58	71.63	3.05	2.93	96.07	0.19	6.23	NTW					
K-10-0303	71.63	74.68	3.05	2.89	94.75	0.80	26.23	NTW					
K-10-0303	74.68	77.72	3.04	2.88	94.74	0.97	31.91	NTW					
K-10-0303	77.72	80.77	3.05	3.05	100.00	2.79	91.48	NTW					
K-10-0303	80.77	83.82	3.05	2.88	94.43	2.01	65.90	NTW					
K-10-0303	83.82	85.34	1.52	1.46	96.05	1.18	77.63	NTW					
K-10-0303	85.34	88.39	3.05	2.42	79.34	1.52	49.84	NTW					
K-10-0303	88.39	91.44	3.05	2.21	72.46	0.54	17.70	NTW					
K-10-0303	91.44	94.49	3.05	2.41	79.02	0.59	19.34	NTW					
K-10-0303	94.49	97.54	3.05	2.63	86.23	0.88	28.85	NTW					
K-10-0303	97.54	100.58	3.04	2.81	92.43	1.21	39.80	NTW					
K-10-0303	100.58	103.63	3.05	2.64	86.56	1.23	40.33	NTW					
K-10-0303	103.63	106.68	3.05	2.98	97.70	2.31	75.74	NTW					
K-10-0303	106.68	109.73	3.05	2.86	93.77	2.14	70.16	NTW					
K-10-0303	109.73	112.78	3.05	2.75	90.16	2.17	71.15	NTW					
K-10-0303	112.78	115.82	3.04	2.80	92.11	1.49	49.01	NTW					
K-10-0303	115.82	118.87	3.05	3.04	99.67	1.87	61.31	NTW					
K-10-0303	118.87	120.40	1.53	1.28	83.66	1.13	73.86	NTW					
K-10-0303	120.40	121.92	1.52	1.47	96.71	0.96	63.16	NTW					
K-10-0303	121.92	124.97	3.05	2.71	88.85	1.83	60.00	NTW					
K-10-0303	124.97	126.49	1.52	1.36	89.47	1.29	84.87	NTW					
K-10-0303	126.49	128.02	1.53	1.47	96.08	1.08	70.59	NTW					
K-10-0303	128.02	129.54	1.52	1.32	86.84	0.81	53.29	NTW					
K-10-0303	129.54	132.59	3.05	2.47	80.98	1.23	40.33	NTW					
K-10-0303	132.59	134.11	1.52	1.32	86.84	0.57	37.50	NTW					
K-10-0303	134.11	137.16	3.05	2.84	93.11	1.94	63.61	NTW					
K-10-0303	137.16	140.21	3.05	2.96	97.05	1.80	59.02	NTW					
K-10-0303	140.21	143.26	3.05	2.99	98.03	2.27	74.43	NTW					
K-10-0303	143.26	146.30	3.04	2.95	97.04	2.58	84.87	NTW					
K-10-0303	146.30	149.35	3.05	2.68	87.87	1.84	60.33	NTW					
K-10-0303	149.35	150.88	1.53	1.36	88.89	0.91	59.48	NTW					
K-10-0303	150.88	153.92	3.04	2.47	81.25	1.63	53.62	NTW					
K-10-0303	153.92	155.45	1.53	0.68	44.44	0.00	0.00	NTW					
K-10-0303	155.45	156.97	1.52	0.79	51.97	0.13	8.55	NTW					
K-10-0303	156.97	160.02	3.05	2.85	93.44	2.24	73.44	NTW					
K-10-0303	160.02	163.07	3.05	3.05	100.00	2.67	87.54	NTW					
K-10-0303	163.07	164.59	1.52	1.39	91.45	1.07	70.39	NTW					
K-10-0303	164.59	167.64	3.05	2.78	91.15	1.86	60.98	NTW					
K-10-0303	167.64	170.69	3.05	2.67	87.54	1.38	45.25	NTW					
K-10-0303	170.69	173.74	3.05	2.62	85.90	1.04	34.10	NTW					
K-10-0303	173.74	176.78	3.04	2.70	88.82	1.12	36.84	NTW					
K-10-0303	176.78	179.83	3.05	3.00	98.36	2.43	79.67	NTW					
K-10-0303	179.83	182.88	3.05	3.00	98.36	2.50	81.97	NTW					
K-10-0303	182.88	185.93	3.05	3.05	100.00	2.32	76.07	NTW					
K-10-0303	185.93	188.98	3.05	3.00	98.36	2.31	75.74	NTW					
K-10-0303	188.98	192.02	3.04	3.00	98.68	1.14	37.50	NTW					
K-10-0303	192.02	195.07	3.05	2.95	96.72	2.63	86.23	NTW					
K-10-0303	195.07	198.12	3.05	3.03	99.34	1.87	61.31	NTW					
K-10-0303	198.12	201.17	3.05	3.05	100.00	2.01	65.90	NTW					
K-10-0303	201.17	204.22	3.05	2.89	94.75	1.60	52.46	NTW					
K-10-0303	204.22	207.26	3.04	2.87	94.41	0.22	7.24	NTW					
K-10-0303	207.26	210.31	3.05	2.81	92.13	0.89	29.18	NTW					
K-10-0303	210.31	213.36	3.05	2.77	90.82	1.21	39.67	NTW					
K-10-0303	213.36	214.88	1.52	1.52	100.00	0.34	22.37	NTW					
K-10-0303	214.88	216.41	1.53	1.54	100.65	0.95	62.09	NTW					
K-10-0303	216.41	219.46	3.05	2.82	92.46	0.91	29.84	NTW					
K-10-0303	219.46	222.50	3.04	2.65	87.17	1.34	44.08	NTW					
K-10-0303	222.50	224.03	1.53	1.30	84.97	0.85	55.56	NTW					
K-10-0303	224.03	225.55	1.52	1.64	107.89	1.26	82.89	NTW					
K-10-0303	225.55	228.60	3.05	3.05	100.00	1.19	39.02	NTW					
K-10-0303	228.60	231.65	3.05	2.98	97.70	1.52	49.84	NTW					
K-10-0303	231.65	234.70	3.05	3.00	98.36	3.00	98.36	NTW					
K-10-0303	234.70	237.74	3.04	3.04	100.00	1.80	59.21	NTW					
K-10-0303	237.74	240.79	3.05	2.71	88.85	1.28	41.97	NTW					
K-10-0303	240.79	243.84	3.05	3.01	98.69	2.55	83.61	NTW					
K-10-0303	243.84	246.89	3.05	2.99	98.03	2.67	87.54	NTW					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0303	246.89	249.94	3.05	3.02	99.02	2.21	72.46	NTW					
K-10-0303	249.94	251.46	1.52	1.41	92.76	0.73	48.03	NTW					
K-10-0303	251.46	252.98	1.52	1.49	98.03	1.31	86.18	NTW					
K-10-0303	252.98	256.03	3.05	3.05	100.00	2.30	75.41	NTW					
K-10-0303	256.03	259.08	3.05	2.93	96.07	2.45	80.33	NTW					
K-10-0303	259.08	262.13	3.05	2.88	94.43	2.58	84.59	NTW					
K-10-0303	262.13	265.18	3.05	2.90	95.08	2.29	75.08	NTW					
K-10-0303	265.18	268.22	3.04	2.85	93.75	1.89	62.17	NTW					
K-10-0303	268.22	271.27	3.05	2.55	83.61	1.96	64.26	NTW					
K-10-0303	271.27	274.32	3.05	2.86	93.77	1.41	46.23	NTW					
K-10-0303	274.32	277.37	3.05	2.94	96.39	1.77	58.03	NTW					
K-10-0303	277.37	280.42	3.05	2.87	94.10	0.14	4.59	NTW					
K-10-0303	280.42	283.46	3.04	2.97	97.70	2.53	83.22	NTW					
K-10-0303	283.46	286.51	3.05	2.68	87.87	1.81	59.34	NTW					
K-10-0303	286.51	289.56	3.05	3.00	98.36	2.23	73.11	NTW					
K-10-0303	289.56	292.61	3.05	2.87	94.10	1.91	62.62	NTW					
K-10-0303	292.61	295.66	3.05	2.98	97.70	2.57	84.26	NTW					
K-10-0303	295.66	298.70	3.04	2.81	92.43	2.03	66.78	NTW					
K-10-0303	298.70	301.75	3.05	2.80	91.80	1.55	50.82	NTW					
K-10-0303	301.75	303.28	1.53	1.52	99.35	0.93	60.78	NTW					
K-10-0303	303.28	304.80	1.52	1.14	75.00	0.53	34.87	NTW					
K-10-0303	304.80	306.32	1.52	1.50	98.68	0.17	11.18	NTW					
K-10-0303	306.32	309.37	3.05	2.76	90.49	0.47	15.41	NTW					
K-10-0303	309.37	310.90	1.53	1.27	83.01	0.00	0.00	NTW					
K-10-0303	310.90	313.94	3.04	3.02	99.34	0.68	22.37	NTW					
K-10-0303	313.94	315.47	1.53	1.32	86.27	0.13	8.50	NTW					
K-10-0303	315.47	316.99	1.52	1.56	102.63	0.26	17.11	NTW					
K-10-0303	316.99	320.04	3.05	2.90	95.08	0.51	16.72	NTW					
K-10-0303	320.04	321.56	1.52	1.51	99.34	0.00	0.00	NTW					
K-10-0303	321.56	323.09	1.53	1.41	92.16	0.51	33.33	NTW					
K-10-0303	323.09	324.61	1.52	1.67	109.87	0.94	61.84	NTW					
K-10-0303	324.61	327.66	3.05	2.88	94.43	1.38	45.25	NTW					
K-10-0303	327.66	329.18	1.52	1.52	100.00	0.34	22.37	NTW					
K-10-0303	329.18	330.71	1.53	1.18	77.12	0.44	28.76	NTW					
K-10-0303	330.71	333.76	3.05	3.05	100.00	1.10	36.07	NTW					
K-10-0303	333.76	336.80	3.04	2.90	95.39	1.40	46.05	NTW					
K-10-0303	336.80	338.33	1.53	1.53	100.00	0.84	54.90	NTW					
K-10-0303	338.33	339.85	1.52	1.52	100.00	1.21	79.61	NTW					
K-10-0303	339.85	342.90	3.05	3.02	99.02	1.19	39.02	NTW					
K-10-0303	342.90	345.95	3.05	2.30	75.41	0.51	16.72	NTW					
K-10-0303	345.95	347.47	1.52	1.42	93.42	0.13	8.55	NTW					
K-10-0303	347.47	348.07	0.60	0.61	101.67	0.00	0.00	NTW					

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0304	0.00	22.46	QTZT
K-10-0304	22.46	25.60	ICQS
K-10-0304	25.60	30.20	QTZT
K-10-0304	30.20	31.24	ICQS
K-10-0304	31.24	31.90	TQTZT
K-10-0304	31.90	38.28	QTZT
K-10-0304	38.28	42.34	ICQS
K-10-0304	42.34	47.24	TQTZT
K-10-0304	47.24	52.25	QTZT
K-10-0304	52.25	52.90	TQTZT
K-10-0304	52.90	58.99	SSCH
K-10-0304	58.99	66.14	QTZT
K-10-0304	66.14	66.90	TQTZT
K-10-0304	66.90	69.74	QTZT
K-10-0304	69.74	73.30	ICQS
K-10-0304	73.30	78.28	QTZT
K-10-0304	78.28	79.15	TQTZT
K-10-0304	79.15	80.70	CHSCH
K-10-0304	80.70	86.21	TQTZT
K-10-0304	86.21	87.90	QTZT
K-10-0304	87.90	90.74	TQTZT
K-10-0304	90.74	92.15	ICQS
K-10-0304	92.15	96.32	QTZT
K-10-0304	96.32	99.47	ICQS
K-10-0304	99.47	103.09	QTZT
K-10-0304	103.09	105.50	TQTZT
K-10-0304	105.50	110.21	ICQS
K-10-0304	110.21	118.14	QTZT
K-10-0304	118.14	127.10	TQTZT
K-10-0304	127.10	137.00	TQTZT
K-10-0304	137.00	138.94	ICQS
K-10-0304	138.94	146.50	GNST
K-10-0304	146.50	147.14	VL
K-10-0304	147.14	154.53	GNST
K-10-0304	154.53	155.12	VL
K-10-0304	155.12	169.52	GNST
K-10-0304	169.52	173.70	CHSCH
K-10-0304	173.70	174.41	GNST
K-10-0304	174.41	185.06	GNST
K-10-0304	185.06	185.39	GSCH
K-10-0304	185.39	188.13	QTZT
K-10-0304	188.13	198.07	TQTZT
K-10-0304	198.07	200.44	ICQS
K-10-0304	200.44	201.19	SM
K-10-0304	201.19	201.77	TQTZT
K-10-0304	201.77	202.85	SM
K-10-0304	202.85	203.35	ICQS
K-10-0304	203.35	203.61	VM
K-10-0304	203.61	203.93	QTZT
K-10-0304	203.93	205.21	NR
K-10-0304	205.21	207.45	SM
K-10-0304	207.45	207.80	VM
K-10-0304	207.80	212.58	GSCH
K-10-0304	212.58	214.97	SM
K-10-0304	214.97	217.01	FLT
K-10-0304	217.01	217.38	FLT
K-10-0304	217.38	219.60	FLT
K-10-0304	219.60	220.71	FLT
K-10-0304	220.71	221.60	FLT
K-10-0304	221.60	222.36	TQTZT
K-10-0304	222.36	225.05	GNST
K-10-0304	225.05	226.27	TQTZT
K-10-0304	226.27	230.45	GNST
K-10-0304	230.45	231.59	SM
K-10-0304	231.59	233.66	TQTZT
K-10-0304	233.66	234.23	GSCH
K-10-0304	234.23	237.38	TQTZT
K-10-0304	237.38	241.80	QTZT
K-10-0304	241.80	247.11	TQTZT
K-10-0304	247.11	248.12	ICQS
K-10-0304	248.12	252.07	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0304	0.00	5.18	5.18	1.79	34.56	0.94	18.15	HQ	14	R4	1	1	1
K-10-0304	5.18	8.23	3.05	2.76	90.49	2.05	67.21	HQ	11	R4	0		0
K-10-0304	8.23	9.60	1.37	1.24	90.51	0.88	64.23	HQ	10	R4	0		0
K-10-0304	9.60	11.28	1.68	1.50	89.29	1.16	69.05	HQ	6	R4	1	1	1
K-10-0304	11.28	14.33	3.05	2.94	96.39	1.88	61.64	HQ	14	R4	1	1	1
K-10-0304	14.33	14.94	0.61	0.60	98.36	0.37	60.66	HQ	7	R4	0		0
K-10-0304	14.94	17.37	2.43	2.18	89.71	1.06	43.62	HQ	11	R4	2	1	1
K-10-0304	17.37	18.75	1.38	0.95	68.84	0.52	37.68	HQ	10	R4	1	1	1
K-10-0304	18.75	19.20	0.45	0.23	51.11	0.00	0.00	HQ	8	R3	1	1	2
K-10-0304	19.20	20.42	1.22	1.03	84.43	0.88	72.13	HQ	9	R5	3	1	45
K-10-0304	20.42	22.56	2.14	2.15	100.47	1.72	80.37	HQ	12	R6	17	2	60
K-10-0304	22.56	23.47	0.91	0.67	73.63	0.00	0.00	HQ	12	R3	1	1	1
K-10-0304	23.47	26.52	3.05	2.95	96.72	1.15	37.70	HQ	33	R3	9	2	10
K-10-0304	26.52	28.65	2.13	2.02	94.84	1.71	80.28	HQ	8	R5	12	2	5
K-10-0304	28.65	29.57	0.92	0.79	85.87	0.59	64.13	HQ	3	R5	5	1	30
K-10-0304	29.57	32.31	2.74	2.64	96.35	1.54	56.20	HQ	24	R4	14	1	25
K-10-0304	32.31	32.61	0.30	0.30	100.00	0.18	60.00	HQ	2	R5	0		0
K-10-0304	32.61	35.20	2.59	2.39	92.28	2.15	83.01	HQ	7	R6	3	1	2
K-10-0304	35.20	35.66	0.46	0.46	100.00	0.46	100.00	HQ	2	R6	2	1	25
K-10-0304	35.66	37.49	1.83	1.57	85.79	1.08	59.02	HQ	9	R5	2	1	5
K-10-0304	37.49	38.40	0.91	0.91	100.00	0.36	39.56	HQ	12	R4	13	1	10
K-10-0304	38.40	38.71	0.31	0.36	116.13	0.27	87.10	HQ					
K-10-0304	38.71	39.62	0.91	0.76	83.52	0.52	57.14	HQ	4	R4	5	1	5
K-10-0304	39.62	41.76	2.14	2.00	93.46	0.90	42.06	HQ	23	R3	3	1	2
K-10-0304	41.76	44.81	3.05	2.92	95.74	1.60	52.46	HQ	38	R3	6	1	5
K-10-0304	44.81	47.24	2.43	2.40	98.77	0.83	34.16	HQ	33	R3	7	1	10
K-10-0304	47.24	47.85	0.61	0.61	100.00	0.23	37.70	HQ	7	R4	3	1	5
K-10-0304	47.85	50.29	2.44	2.27	93.03	1.40	57.38	HQ	23	R4	3	1	2
K-10-0304	50.29	50.90	0.61	0.60	98.36	0.30	49.18	HQ	5	R4	0		0
K-10-0304	50.90	52.73	1.83	1.72	93.99	0.92	50.27	HQ	25	R3	0		0
K-10-0304	52.73	53.95	1.22	0.90	73.77	0.40	32.79	HQ	16	R3	4	1	25
K-10-0304	53.95	57.00	3.05	2.86	93.77	1.21	39.67	HQ	34	R4	9	1	15
K-10-0304	57.00	59.13	2.13	2.04	95.77	1.38	64.79	HQ	15	R3	6	1	10
K-10-0304	59.13	59.59	0.46	0.42	91.30	0.13	28.26	HQ	6	R4	1	1	10
K-10-0304	59.59	60.05	0.46	0.37	80.43	0.18	39.13	HQ	8	R4	1	1	5
K-10-0304	60.05	62.79	2.74	2.79	101.82	2.35	85.77	HQ	8	R5	15	1	15
K-10-0304	62.79	63.09	0.30	0.26	86.67	0.26	86.67	HQ	0	R5	0		0
K-10-0304	63.09	63.70	0.61	0.59	96.72	0.53	86.89	HQ	1	R5	1	1	5
K-10-0304	63.70	65.53	1.83	1.53	83.61	1.06	57.92	HQ	11	R4	12	1	5
K-10-0304	65.53	66.14	0.61	0.52	85.25	0.42	68.85	HQ	2	R5	1	1	20
K-10-0304	66.14	66.90	0.76	0.66	86.84	0.18	23.68	HQ	10	R4	4	2	15
K-10-0304	66.90	69.19	2.29	2.15	93.89	1.30	56.77	HQ	19	R4	5	2	30
K-10-0304	69.19	71.17	1.98	1.98	100.00	0.93	46.97	HQ	28	R2	6	2	5
K-10-0304	71.17	72.24	1.07	1.07	100.00	0.46	42.99	HQ	9	R3	2	1	1
K-10-0304	72.24	74.52	2.28	2.19	96.05	1.33	58.33	HQ	13	R3	4	1	3
K-10-0304	74.52	75.29	0.77	0.78	101.30	0.41	53.25	HQ	5	R5	1	1	5
K-10-0304	75.29	75.90	0.61	0.55	90.16	0.36	59.02	HQ	6	R5	1	1	5
K-10-0304	75.90	76.20	0.30	0.17	56.67	0.00	0.00	HQ	8	R3	0		0
K-10-0304	76.20	78.33	2.13	1.91	89.67	0.92	43.19	HQ	14	R5	9	1	35
K-10-0304	78.33	80.01	1.68	1.70	101.19	0.80	47.62	HQ	17	R4	8	1	25
K-10-0304	80.01	81.38	1.37	1.26	91.97	0.14	10.22	HQ	37	R4	4	1	10
K-10-0304	81.38	83.21	1.83	1.83	100.00	0.71	38.80	HQ	36	R4	16	1	50
K-10-0304	83.21	84.43	1.22	1.06	86.89	0.47	38.52	HQ	16	R4	4	1	25
K-10-0304	84.43	84.73	0.30	0.30	100.00	0.14	46.67	HQ	8	R3	1	1	5
K-10-0304	84.73	85.34	0.61	0.60	98.36	0.00	0.00	HQ	13	R3	3	1	10
K-10-0304	85.34	87.17	1.83	1.83	100.00	1.15	62.84	HQ	21	R4	8	1	15
K-10-0304	87.17	87.48	0.31	0.18	58.06	0.00	0.00	HQ	5	R4	1	1	1
K-10-0304	87.48	88.24	0.76	0.76	100.00	0.34	44.74	HQ	6	R4	2	2	5
K-10-0304	88.24	90.22	1.98	1.98	100.00	0.96	48.48	HQ	19	R3	7	1	5
K-10-0304	90.22	90.53	0.31	0.15	48.39	0.00	0.00	HQ	5	R3	1	1	1
K-10-0304	90.53	91.14	0.61	0.65	106.56	0.10	16.39	HQ	17	R3	1	1	1
K-10-0304	91.14	92.35	1.21	1.21	100.00	0.28	23.14	HQ	18	R3	5	1	10
K-10-0304	92.35	93.57	1.22	0.61	50.00	0.14	11.48	HQ	11	R3	0		0
K-10-0304	93.57	93.88	0.31	0.25	80.65	0.00	0.00	HQ	12	R3	0		0
K-10-0304	93.88	94.49	0.61	0.20	32.79	0.00	0.00	HQ	12	R3	0		0
K-10-0304	94.49	96.32	1.83	1.26	68.85	0.48	26.23	HQ	21	R4	0		0
K-10-0304	96.32	96.62	0.30	0.22	73.33	0.00	0.00	HQ	5	R3	1	1	5
K-10-0304	96.62	97.08	0.46	0.46	100.00	0.18	39.13	HQ	9	R4	4	1	5
K-10-0304	97.08	99.67	2.59	2.45	94.59	1.39	53.67	HQ	19	R3	7	1	5
K-10-0304	99.67	102.72	3.05	2.92	95.74	1.76	57.70	HQ	20	R5	2	1	1
K-10-0304	102.72	105.46	2.74	2.61	95.26	1.17	42.70	HQ	24	R4	3	1	5
K-10-0304	105.46	105.77	0.31	0.30	96.77	0.16	51.61	HQ	1	R3	0		0
K-10-0304	105.77	108.51	2.74	2.67	97.45	1.72	62.77	HQ	12	R4	7	1	5
K-10-0304	108.51	108.81	0.30	0.24	80.00	0.24	80.00	HQ	1	R4	3	1	5
K-10-0304	108.81	111.60	2.79	2.69	96.42	1.57	56.27	HQ	17	R4	12	1	10
K-10-0304	111.60	111.86	0.26	0.20	76.92	0.20	76.92	HQ	1	R5	1	1	1
K-10-0304	111.86	114.60	2.74	2.58	94.16	1.65	60.22	HQ	19	R4	7	1	5
K-10-0304	114.60	114.91	0.31	0.31	100.00	0.22	70.97	HQ	1	R5	1		0
K-10-0304	114.91	117.96	3.05	2.70	88.52	1.78	58.36	HQ	21	R5	7	1	35
K-10-0304	117.96	121.01	3.05	2.92	95.74	1.76	57.70	HQ	15	R6	1	1	1
K-10-0304	121.01	124.05	3.04	2.78	91.45	1.34	44.08	HQ	26	R4	4	1	3
K-10-0304	124.05	126.49	2.44	2.44	100.00	1.77	72.54	HQ	16	R4	2	1	1
K-10-0304	126.49	127.10	0.61	0.51	83.61	0.40	65.57	HQ	1	R4	0		0
K-10-0304	127.10	130.15	3.05	2.92	95.74	1.78	58.36	HQ	26	R4	8	1	5
K-10-0304	130.15	131.67	1.52	1.22	80.26	0.31	20.39	HQ	34	R3	2	1	1
K-10-0304	131.67	133.20	1.53	1.53	100.00	1.07	69.93	HQ	19	R4	2	1	2
K-10-0304	133.20	136.25	3.05	2.89	94.75	1.91	62.62	HQ	19	R4	1	1	1
K-10-0304	136.25	139.29	3.04	3.04	100.00	2.10	69.08	HQ	28	R5	4	2	10
K-10-0304	139.29	142.34	3.05	2.94	96.39	2.53	82.95	HQ	4	R6	10	1	15
K-10-0304	142.34	145.39	3.05	2.86	93.77	2.13	69.84	HQ	14	R4	6	1	10
K-10-0304	145.39	148.44	3.05	3.05	100.00	2.37	77.70	HQ	7	R5	5	1	30
K-10-0304	148.44	151.49	3.05	2.95	96.72	2.54	83.28	HQ	4	R6	10	1	10
K-10-0304	151.49	154.53	3.04	3.04	100.00	2.77	91.12	HQ	6	R6	8	2	10
K-10-0304	154.53	157.58	3.05	2.86	93.77	2.25	73.77	HQ	5	R5	8	1	25
K-10-0304	157.58	160.63	3.05	2.88	94.43	1.80	59.02	HQ	17	R5	5	2	10
K-10-0304	160.63	162.95	2.32	2.02	87.07	1.12	48.28	HQ	16	R5	9	1	12
K-10-0304	162.95	163.68	0.73	0.73	100.00	0.73	100.00	HQ	0	R6	13	1	90

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0304	163.68	166.73	3.05	2.91	95.41	2.26	74.10	HQ	8	R6	19	1	50
K-10-0304	166.73	169.77	3.04	3.05	100.33	1.96	64.47	HQ	16	R5	4	1	20
K-10-0304	169.77	172.82	3.05	2.79	91.48	1.47	48.20	HQ	17	R5	5	1	10
K-10-0304	172.82	174.35	1.53	1.53	100.00	0.91	59.48	HQ	14	R5	1	1	1
K-10-0304	174.35	175.87	1.52	1.22	80.26	1.00	65.79	HQ	6	R5	3	1	20
K-10-0304	175.87	178.16	2.29	2.29	100.00	2.24	97.82	HQ	13	R5	1	1	1
K-10-0304	178.16	178.92	0.76	0.66	86.84	0.34	44.74	HQ	7	R5	3	1	15
K-10-0304	178.92	181.20	2.28	2.01	88.16	1.15	50.44	HQ	10	R5	4	1	5
K-10-0304	181.20	181.97	0.77	0.77	100.00	0.60	77.92	HQ	4	R6	1	1	1
K-10-0304	181.97	185.01	3.04	2.74	90.13	1.61	52.96	HQ	20	R5	12	1	20
K-10-0304	185.01	187.15	2.14	2.03	94.86	1.28	59.81	HQ	6	R6	9	1	10
K-10-0304	187.15	188.06	0.91	0.91	100.00	0.49	53.85	HQ	7	R4	9	1	10
K-10-0304	188.06	189.28	1.22	1.15	94.26	0.68	55.74	HQ	10	R4	8	1	30
K-10-0304	189.28	191.11	1.83	1.57	85.79	0.87	47.54	HQ	15	R4	5	1	15
K-10-0304	191.11	193.24	2.13	1.81	84.98	0.66	30.99	HQ	32	R4	3	1	5
K-10-0304	193.24	194.16	0.92	0.92	100.00	0.34	36.96	HQ	11	R4	4	1	5
K-10-0304	194.16	197.21	3.05	2.82	92.46	1.39	45.57	HQ	31	R4	7	1	5
K-10-0304	197.21	198.73	1.52	0.97	63.82	0.51	33.55	HQ	25	R3	5	1	5
K-10-0304	198.73	200.25	1.52	1.22	80.26	0.00	0.00	HQ	23	R3	4	2	15
K-10-0304	200.25	202.08	1.83	1.77	96.72	0.85	46.45	HQ	26	R3	9	1	10
K-10-0304	202.08	203.30	1.22	1.20	98.36	0.00	0.00	HQ	31	R3	5	1	5
K-10-0304	203.30	205.44	2.14	0.86	40.19	0.29	13.55	HQ	20	R2	3	2	40
K-10-0304	205.44	206.35	0.91	0.67	73.63	0.20	21.98	HQ	23	R3	1	1	1
K-10-0304	206.35	207.87	1.52	1.30	85.53	0.40	26.32	HQ	30	R3	4	1	5
K-10-0304	207.87	209.40	1.53	1.53	100.00	0.78	50.98	HQ	18	R2	4	1	2
K-10-0304	209.40	211.23	1.83	1.60	87.43	0.13	7.10	HQ	33	R2	1	2	1
K-10-0304	211.23	212.45	1.22	1.24	101.64	0.12	9.84	HQ	15	R2	2	3	1
K-10-0304	212.45	215.49	3.04	3.05	100.33	1.24	40.79	HQ	24	R2	3	2	1
K-10-0304	215.49	216.71	1.22	1.16	95.08	0.00	0.00	HQ	0	R0	0	3	0
K-10-0304	216.71	218.54	1.83	1.78	97.27	0.00	0.00	HQ	9	R2	2	2	20
K-10-0304	218.54	220.37	1.83	1.63	89.07	0.00	0.00	HQ	6	R6	1	2	1
K-10-0304	220.37	221.59	1.22	1.32	108.20	0.00	0.00	HQ	9	R2	1	2	1
K-10-0304	221.59	223.11	1.52	1.55	101.97	0.57	37.50	HQ	11	R4	2	2	5
K-10-0304	223.11	224.64	1.53	1.40	91.50	0.90	58.82	HQ	10	R6	1	1	0.5
K-10-0304	224.64	227.69	3.05	3.04	99.67	1.72	56.39	HQ	9	R5	1	1	0.5
K-10-0304	227.69	230.73	3.04	3.07	100.99	2.30	75.66	HQ	6	R5	4	2	10
K-10-0304	230.73	233.78	3.05	2.88	94.43	1.02	33.44	HQ	12	R3	5	2	3
K-10-0304	233.78	236.83	3.05	3.01	98.69	1.40	45.90	HQ	8	R4	1	2	0.5
K-10-0304	236.83	239.88	3.05	2.94	96.39	1.28	41.97	HQ	5	R4	1	1	2
K-10-0304	239.88	242.93	3.05	2.83	92.79	0.56	18.36	HQ	15	R3	4	3	10
K-10-0304	242.93	245.06	2.13	2.18	102.35	0.78	36.62	HQ	17	R4	3	1	3
K-10-0304	245.06	245.97	0.91	0.75	82.42	0.00	0.00	HQ	4	R4	4	2	8
K-10-0304	245.97	249.02	3.05	2.87	94.10	1.13	37.05	HQ	23	R3	5	2	5
K-10-0304	249.02	250.55	1.53	1.27	83.01	0.00	0.00	HQ	5	R3	2	2	2
K-10-0304	250.55	252.07	1.52	1.43	94.08	0.89	58.55	HQ					

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0305	0.00	11.10	OVB
K-10-0305	11.10	17.66	ICQS
K-10-0305	17.66	18.10	SSCH
K-10-0305	18.10	28.43	TQTZT
K-10-0305	28.43	33.02	QTZT
K-10-0305	33.02	35.36	ICQS
K-10-0305	35.36	37.93	TQTZT
K-10-0305	37.93	40.57	ICQS
K-10-0305	40.57	61.05	TQTZT
K-10-0305	61.05	65.46	ICQS
K-10-0305	65.46	69.93	TQTZT
K-10-0305	69.93	73.85	ICQS
K-10-0305	73.85	84.06	TQTZT
K-10-0305	84.06	86.18	ICQS
K-10-0305	86.18	87.63	SSCH
K-10-0305	87.63	88.30	ICQS
K-10-0305	88.30	88.86	SSCH
K-10-0305	88.86	89.72	ICQS
K-10-0305	89.72	91.82	QTZT
K-10-0305	91.82	112.02	TQTZT
K-10-0305	112.02	112.66	VN
K-10-0305	112.66	117.61	QTZT
K-10-0305	117.61	119.47	SSCH
K-10-0305	119.47	120.38	FLT
K-10-0305	120.38	121.28	QTZT
K-10-0305	121.28	122.83	FLT
K-10-0305	122.83	124.77	QTZT
K-10-0305	124.77	125.58	FLT
K-10-0305	125.58	127.78	QTZT
K-10-0305	127.78	128.57	FLT
K-10-0305	128.57	130.38	FLT
K-10-0305	130.38	131.45	QTZT
K-10-0305	131.45	132.08	VN
K-10-0305	132.08	134.54	CQTZT
K-10-0305	134.54	135.94	ICQS
K-10-0305	135.94	141.33	QTZT
K-10-0305	141.33	147.56	TQTZT
K-10-0305	147.56	153.36	QTZT
K-10-0305	153.36	155.54	ICQS
K-10-0305	155.54	157.96	GSCH
K-10-0305	157.96	159.89	ICQS
K-10-0305	159.89	162.39	QTZT
K-10-0305	162.39	162.81	VN
K-10-0305	162.81	164.29	TQTZT
K-10-0305	164.29	171.64	GNST
K-10-0305	171.64	175.32	TQTZT
K-10-0305	175.32	185.23	QTZT
K-10-0305	185.23	188.83	ICQS
K-10-0305	188.83	194.30	QTZT
K-10-0305	194.30	200.79	ICQS
K-10-0305	200.79	209.78	TQTZT
K-10-0305	209.78	215.41	QTZT
K-10-0305	215.41	220.10	TQTZT
K-10-0305	220.10	268.23	GNST
K-10-0305	268.23	272.22	CHSCH
K-10-0305	272.22	279.26	QTZT
K-10-0305	279.26	286.13	TQTZT
K-10-0305	286.13	290.52	QTZT
K-10-0305	290.52	290.95	GSCH
K-10-0305	290.95	297.21	GNST
K-10-0305	297.21	299.45	ICQS
K-10-0305	299.45	304.88	TQTZT
K-10-0305	304.88	308.66	ICQS
K-10-0305	308.66	315.91	GSCH
K-10-0305	315.91	317.63	SM
K-10-0305	317.63	318.64	VM
K-10-0305	318.64	319.01	VM
K-10-0305	319.01	320.65	SM
K-10-0305	320.65	321.51	VM
K-10-0305	321.51	323.17	SM
K-10-0305	323.17	324.82	SM
K-10-0305	324.82	326.21	VN
K-10-0305	326.21	327.36	VM
K-10-0305	327.36	328.15	SM
K-10-0305	328.15	329.20	VM
K-10-0305	329.20	330.03	FLT
K-10-0305	330.03	334.58	FLT
K-10-0305	334.58	335.69	FLT
K-10-0305	335.69	336.62	GSCH
K-10-0305	336.62	340.24	QTZT

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0305	340.24	349.75	GNST
K-10-0305	349.75	350.85	QTZT
K-10-0305	350.85	351.18	QTZT
K-10-0305	351.18	352.35	QTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0305	0.00	6.10	6.10	0.00	0.00	0.00	0.00	HQ					
K-10-0305	6.10	9.75	3.65	1.07	29.32	0.10	2.74	HQ					
K-10-0305	9.75	10.97	1.22	0.45	36.89	0.30	24.59	HQ					
K-10-0305	10.97	14.21	3.24	2.93	90.43	0.81	25.00	HQ					
K-10-0305	14.21	17.07	2.86	2.86	100.00	1.62	56.64	HQ					
K-10-0305	17.07	20.12	3.05	2.95	96.72	1.30	42.62	HQ					
K-10-0305	20.12	21.34	1.22	0.53	43.44	0.00	0.00	HQ					
K-10-0305	21.34	23.17	1.83	1.83	100.00	0.49	26.78	HQ					
K-10-0305	23.17	26.21	3.04	2.43	79.93	0.96	31.58	HQ					
K-10-0305	26.21	27.13	0.92	0.70	76.09	0.46	50.00	HQ					
K-10-0305	27.13	27.74	0.61	0.61	100.00	0.00	0.00	HQ					
K-10-0305	27.74	29.26	1.52	1.52	100.00	0.27	17.76	HQ					
K-10-0305	29.26	29.56	0.30	0.30	100.00	0.17	56.67	HQ					
K-10-0305	29.56	32.31	2.75	2.56	93.09	0.85	30.91	HQ					
K-10-0305	32.31	35.36	3.05	2.58	84.59	0.15	4.92	HQ					
K-10-0305	35.36	36.58	1.22	1.00	81.97	0.42	34.43	HQ					
K-10-0305	36.58	37.34	0.76	0.76	100.00	0.66	86.84	HQ					
K-10-0305	37.34	38.41	1.07	0.85	79.44	0.21	19.63	HQ					
K-10-0305	38.41	41.45	3.04	2.82	92.76	2.03	66.78	HQ					
K-10-0305	41.45	44.50	3.05	3.05	100.00	2.13	69.84	HQ					
K-10-0305	44.50	46.63	2.13	2.13	100.00	0.92	43.19	HQ					
K-10-0305	46.63	47.55	0.92	0.92	100.00	0.36	39.13	HQ					
K-10-0305	47.55	49.53	1.98	1.97	99.49	0.80	40.40	HQ					
K-10-0305	49.53	50.60	1.07	0.98	91.59	0.47	43.93	HQ					
K-10-0305	50.60	53.64	3.04	3.04	100.00	0.70	23.03	HQ					
K-10-0305	53.64	56.08	2.44	2.48	101.64	1.34	54.92	HQ					
K-10-0305	56.08	56.69	0.61	0.56	91.80	0.22	36.07	HQ					
K-10-0305	56.69	56.99	0.30	0.17	56.67	0.00	0.00	HQ					
K-10-0305	56.99	58.52	1.53	1.52	99.35	0.51	33.33	HQ					
K-10-0305	58.52	58.83	0.31	0.30	96.77	0.00	0.00	HQ					
K-10-0305	58.83	59.74	0.91	0.89	97.80	0.53	58.24	HQ					
K-10-0305	59.74	62.78	3.04	3.04	100.00	1.76	57.89	HQ					
K-10-0305	62.78	65.84	3.06	2.98	97.39	1.28	41.83	HQ					
K-10-0305	65.84	68.88	3.04	2.89	95.07	1.00	32.89	HQ					
K-10-0305	68.88	71.02	2.14	1.95	91.12	0.86	40.19	HQ					
K-10-0305	71.02	71.93	0.91	0.91	100.00	0.33	36.26	HQ					
K-10-0305	71.93	74.98	3.05	2.68	87.87	1.39	45.57	HQ					
K-10-0305	74.98	76.81	1.83	1.83	100.00	1.83	100.00	HQ					
K-10-0305	76.81	78.03	1.22	1.21	99.18	0.38	31.15	HQ					
K-10-0305	78.03	81.08	3.05	3.05	100.00	1.76	57.70	HQ					
K-10-0305	81.08	84.12	3.04	2.72	89.47	1.67	54.93	HQ					
K-10-0305	84.12	87.17	3.05	2.87	94.10	0.74	24.26	HQ					
K-10-0305	87.17	90.22	3.05	2.91	95.41	1.29	42.30	HQ					
K-10-0305	90.22	93.27	3.05	2.96	97.05	1.89	61.97	HQ					
K-10-0305	93.27	94.49	1.22	1.12	91.80	0.58	47.54	HQ					
K-10-0305	94.49	96.32	1.83	1.83	100.00	1.20	65.57	HQ					
K-10-0305	96.32	99.37	3.05	3.05	100.00	1.90	62.30	HQ					
K-10-0305	99.37	102.41	3.04	2.82	92.76	1.65	54.28	HQ					
K-10-0305	102.41	105.46	3.05	3.05	100.00	1.79	58.69	HQ					
K-10-0305	105.46	108.05	2.59	2.68	103.47	2.00	77.22	HQ					
K-10-0305	108.05	108.51	0.46	0.45	97.83	0.28	60.87	HQ					
K-10-0305	108.51	111.56	3.05	3.05	100.00	2.28	74.75	HQ					
K-10-0305	111.56	114.61	3.05	3.05	100.00	2.16	70.82	HQ					
K-10-0305	114.61	115.52	0.91	0.86	94.51	0.32	35.16	HQ					
K-10-0305	115.52	117.65	2.13	1.38	64.79	0.48	22.54	HQ					
K-10-0305	117.65	118.57	0.92	1.06	115.22	0.80	86.96	HQ					
K-10-0305	118.57	120.70	2.13	1.52	71.36	0.34	15.96	HQ					
K-10-0305	120.70	121.92	1.22	0.90	73.77	0.36	29.51	HQ					
K-10-0305	121.92	122.83	0.91	0.83	91.21	0.00	0.00	HQ					
K-10-0305	122.83	123.75	0.92	0.87	94.57	0.22	23.91	HQ					
K-10-0305	123.75	125.58	1.83	1.81	98.91	0.51	27.87	HQ					
K-10-0305	125.58	126.80	1.22	1.10	90.16	0.34	27.87	HQ					
K-10-0305	126.80	129.85	3.05	2.37	77.70	0.64	20.98	HQ					
K-10-0305	129.85	132.89	3.04	3.05	100.33	0.79	25.99	HQ					
K-10-0305	132.89	135.94	3.05	3.05	100.00	0.37	12.13	HQ					
K-10-0305	135.94	138.99	3.05	3.05	100.00	1.79	58.69	HQ					
K-10-0305	138.99	142.04	3.05	2.91	95.41	2.07	67.87	HQ					
K-10-0305	142.04	145.09	3.05	2.76	90.49	1.14	37.38	HQ					
K-10-0305	145.09	146.30	1.21	0.71	58.68	0.32	26.45	HQ					
K-10-0305	146.30	147.22	0.92	0.86	93.48	0.30	32.61	HQ					
K-10-0305	147.22	148.13	0.91	0.84	92.31	0.45	49.45	HQ					
K-10-0305	148.13	149.35	1.22	1.32	108.20	0.81	66.39	HQ					
K-10-0305	149.35	151.18	1.83	1.71	93.44	1.39	75.96	HQ					
K-10-0305	151.18	154.23	3.05	3.00	98.36	2.10	68.85	HQ					
K-10-0305	154.23	157.28	3.05	3.05	100.00	1.90	62.30	HQ					
K-10-0305	157.28	160.32	3.04	3.05	100.33	1.77	58.22	HQ					
K-10-0305	160.32	163.37	3.05	2.96	97.05	2.10	68.85	HQ					
K-10-0305	163.37	166.42	3.05	3.05	100.00	2.35	77.05	HQ					
K-10-0305	166.42	169.47	3.05	2.94	96.39	2.85	93.44	HQ					
K-10-0305	169.47	172.52	3.05	3.05	100.00	2.40	78.69	HQ					
K-10-0305	172.52	173.74	1.22	1.22	100.00	0.71	58.20	HQ					
K-10-0305	173.74	174.35	0.61	0.61	100.00	0.38	62.30	HQ					
K-10-0305	174.35	175.56	1.21	1.16	95.87	0.84	69.42	HQ					
K-10-0305	175.56	176.17	0.61	0.86	140.98	0.41	67.21	HQ					
K-10-0305	176.17	177.09	0.92	0.85	92.39	0.31	33.70	HQ					
K-10-0305	177.09	178.61	1.52	1.70	111.84	0.90	59.21	HQ					
K-10-0305	178.61	181.66	3.05	3.00	98.36	2.25	73.77	HQ					
K-10-0305	181.66	184.71	3.05	3.03	99.34	2.20	72.13	HQ					
K-10-0305	184.71	187.76	3.05	2.99	98.03	0.89	29.18	HQ					
K-10-0305	187.76	188.06	0.30	0.30	100.00	0.00	0.00	HQ					
K-10-0305	188.06	190.20	2.14	2.14	100.00	1.16	54.21	HQ					
K-10-0305	190.20	190.80	0.60	0.65	108.33	0.40	66.67	HQ					
K-10-0305	190.80	193.85	3.05	2.85	93.44	1.83	60.00	HQ					
K-10-0305	193.85	196.90	3.05	2.78	91.15	0.78	25.57	HQ					
K-10-0305	196.90	199.95	3.05	2.90	95.08	0.48	15.74	HQ					
K-10-0305	199.95	203.00	3.05	2.83	92.79	1.22	40.00	HQ					
K-10-0305	203.00	206.04	3.04	3.01	99.01	1.30	42.76	HQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0305	206.04	209.09	3.05	2.98	97.70	1.23	40.33	HQ					
K-10-0305	209.09	212.14	3.05	3.05	100.00	2.35	77.05	HQ					
K-10-0305	212.14	215.19	3.05	2.88	94.43	1.55	50.82	HQ					
K-10-0305	215.19	218.24	3.05	2.92	95.74	1.42	46.56	HQ					
K-10-0305	218.24	221.28	3.04	3.05	100.33	1.96	64.47	HQ					
K-10-0305	221.28	224.33	3.05	3.05	100.00	3.05	100.00	HQ					
K-10-0305	224.33	227.38	3.05	3.05	100.00	2.34	76.72	HQ					
K-10-0305	227.38	230.43	3.05	2.95	96.72	2.68	87.87	HQ					
K-10-0305	230.43	233.48	3.05	2.96	97.05	2.38	78.03	HQ					
K-10-0305	233.48	236.52	3.04	2.81	92.43	2.42	79.61	HQ					
K-10-0305	236.52	239.57	3.05	3.01	98.69	2.36	77.38	HQ					
K-10-0305	239.57	242.62	3.05	2.89	94.75	2.60	85.25	HQ					
K-10-0305	242.62	245.67	3.05	3.05	100.00	2.21	72.46	HQ					
K-10-0305	245.67	248.72	3.05	3.05	100.00	2.85	93.44	HQ					
K-10-0305	248.72	251.76	3.04	3.04	100.00	2.94	96.71	HQ					
K-10-0305	251.76	254.81	3.05	2.98	97.70	2.87	94.10	HQ					
K-10-0305	254.81	257.86	3.05	2.98	97.70	2.88	94.43	HQ					
K-10-0305	257.86	260.91	3.05	2.95	96.72	2.62	85.90	HQ					
K-10-0305	260.91	263.96	3.05	2.96	97.05	1.44	47.21	HQ					
K-10-0305	263.96	267.01	3.05	2.98	97.70	2.34	76.72	HQ					
K-10-0305	267.01	270.05	3.04	2.94	96.71	1.41	46.38	HQ					
K-10-0305	270.05	273.10	3.05	2.95	96.72	1.40	45.90	HQ					
K-10-0305	273.10	276.15	3.05	2.90	95.08	1.00	32.79	HQ					
K-10-0305	276.15	279.20	3.05	2.92	95.74	1.59	52.13	HQ					
K-10-0305	279.20	279.81	0.61	0.61	100.00	0.12	19.67	HQ					
K-10-0305	279.81	282.25	2.44	1.52	62.30	0.61	25.00	HQ					
K-10-0305	282.25	285.29	3.04	2.60	85.53	0.54	17.76	HQ					
K-10-0305	285.29	286.82	1.53	1.09	71.24	0.17	11.11	HQ					
K-10-0305	286.82	288.34	1.52	1.60	105.26	0.49	32.24	HQ					
K-10-0305	288.34	291.39	3.05	2.87	94.10	1.35	44.26	HQ					
K-10-0305	291.39	294.44	3.05	2.91	95.41	1.67	54.75	HQ					
K-10-0305	294.44	297.49	3.05	2.82	92.46	0.00	0.00	HQ					
K-10-0305	297.49	300.53	3.04	2.93	96.38	0.43	14.14	HQ					
K-10-0305	300.53	301.45	0.92	0.66	71.74	0.00	0.00	HQ					
K-10-0305	301.45	302.36	0.91	0.75	82.42	0.00	0.00	HQ					
K-10-0305	302.36	303.58	1.22	1.30	106.56	0.15	12.30	HQ					
K-10-0305	303.58	306.63	3.05	2.78	91.15	0.40	13.11	HQ					
K-10-0305	306.63	308.76	2.13	2.05	96.24	0.27	12.68	HQ					
K-10-0305	308.76	309.68	0.92	0.90	97.83	0.11	11.96	HQ					
K-10-0305	309.68	311.81	2.13	1.81	84.98	0.00	0.00	HQ					
K-10-0305	311.81	312.73	0.92	0.56	60.87	0.00	0.00	HQ					
K-10-0305	312.73	313.94	1.21	1.12	92.56	0.23	19.01	HQ					
K-10-0305	313.94	314.86	0.92	0.84	91.30	0.14	15.22	HQ					
K-10-0305	314.86	315.77	0.91	0.68	74.73	0.33	36.26	HQ					
K-10-0305	315.77	318.82	3.05	2.82	92.46	1.68	55.08	HQ					
K-10-0305	318.82	320.65	1.83	1.70	92.90	0.32	17.49	HQ					
K-10-0305	320.65	321.87	1.22	0.99	81.15	0.00	0.00	HQ					
K-10-0305	321.87	324.31	2.44	2.21	90.57	0.35	14.34	HQ					
K-10-0305	324.31	324.92	0.61	0.61	100.00	0.51	83.61	HQ					
K-10-0305	324.92	327.97	3.05	2.85	93.44	1.53	50.16	HQ					
K-10-0305	327.97	331.01	3.04	2.73	89.80	1.36	44.74	HQ					
K-10-0305	331.01	332.84	1.83	1.50	81.97	0.22	12.02	HQ					
K-10-0305	332.84	334.06	1.22	1.36	111.48	0.28	22.95	HQ					
K-10-0305	334.06	335.59	1.53	1.13	73.86	0.12	7.84	HQ					
K-10-0305	335.59	337.11	1.52	1.28	84.21	0.36	23.68	HQ					
K-10-0305	337.11	340.16	3.05	2.90	95.08	2.02	66.23	HQ					
K-10-0305	340.16	343.21	3.05	2.91	95.41	1.28	41.97	HQ					
K-10-0305	343.21	346.25	3.04	3.00	98.68	1.15	37.83	HQ					
K-10-0305	346.25	349.30	3.05	3.04	99.67	2.08	68.20	HQ					
K-10-0305	349.30	352.35	3.05	2.83	92.79	1.83	60.00	HQ					

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0312	0.00	11.57	OVB
K-10-0312	11.57	28.53	ICQS
K-10-0312	28.53	30.74	SSCH
K-10-0312	30.74	38.69	TQTZT
K-10-0312	38.69	42.35	TQTZT
K-10-0312	42.35	53.43	TQTZT
K-10-0312	53.43	56.79	FLT
K-10-0312	56.79	61.92	TQTZT
K-10-0312	61.92	64.32	ICQS
K-10-0312	64.32	68.70	TQTZT
K-10-0312	68.70	69.90	ICQS
K-10-0312	69.90	81.73	QTZT
K-10-0312	81.73	87.17	TQTZT
K-10-0312	87.17	96.77	QTZT
K-10-0312	96.77	98.40	TQTZT
K-10-0312	98.40	104.27	GSCH
K-10-0312	104.27	105.46	FLT
K-10-0312	105.46	108.51	GSCH
K-10-0312	108.51	108.87	FLT
K-10-0312	108.87	110.70	TQTZT
K-10-0312	110.70	112.23	GSCH
K-10-0312	112.23	126.62	CQTZT
K-10-0312	126.62	136.36	TQTZT
K-10-0312	136.36	147.87	SSCH
K-10-0312	147.87	149.50	GSCH
K-10-0312	149.50	152.71	QTZT
K-10-0312	152.71	155.35	GSCH
K-10-0312	155.35	160.10	TQTZT
K-10-0312	160.10	165.51	QTZT
K-10-0312	165.51	169.18	TQTZT
K-10-0312	169.18	177.73	QTZT
K-10-0312	177.73	179.41	ICQS
K-10-0312	179.41	186.48	QTZT
K-10-0312	186.48	191.26	TQTZT
K-10-0312	191.26	197.10	QTZT
K-10-0312	197.10	199.25	GSCH
K-10-0312	199.25	201.32	QTZT
K-10-0312	201.32	203.86	GSCH
K-10-0312	203.86	207.50	QTZT
K-10-0312	207.50	208.34	GSCH
K-10-0312	208.34	209.78	SSCH
K-10-0312	209.78	210.80	GSCH
K-10-0312	210.80	211.20	SSCH
K-10-0312	211.20	222.60	GSCH
K-10-0312	222.60	227.99	QTZT
K-10-0312	227.99	229.06	ICQS
K-10-0312	229.06	233.25	TQTZT
K-10-0312	233.25	233.75	FLT
K-10-0312	233.75	239.45	QTZT
K-10-0312	239.45	240.10	FLT
K-10-0312	240.10	241.68	QTZT
K-10-0312	241.68	243.73	FLT
K-10-0312	243.73	245.14	QTZT
K-10-0312	245.14	245.40	FLT
K-10-0312	245.40	248.00	TQTZT
K-10-0312	248.00	252.47	QTZT
K-10-0312	252.47	259.55	TQTZT
K-10-0312	259.55	261.28	ICQS
K-10-0312	261.28	266.86	QTZT
K-10-0312	266.86	267.70	GSCH
K-10-0312	267.70	275.77	TQTZT
K-10-0312	275.77	282.02	QTZT
K-10-0312	282.02	282.77	FLT
K-10-0312	282.77	291.18	QTZT
K-10-0312	291.18	300.26	TQTZT
K-10-0312	300.26	303.40	GSCH
K-10-0312	303.40	304.84	SSCH
K-10-0312	304.84	307.24	QTZT
K-10-0312	307.24	320.48	GNST
K-10-0312	320.48	321.87	QTZT
K-10-0312	321.87	323.40	GSCH
K-10-0312	323.40	327.97	TQTZT
K-10-0312	327.97	337.90	GSCH
K-10-0312	337.90	338.95	QTZT
K-10-0312	338.95	342.64	GSCH
K-10-0312	342.64	344.30	QTZT
K-10-0312	344.30	345.50	ICQS
K-10-0312	345.50	346.75	SM
K-10-0312	346.75	348.86	GSCH
K-10-0312	348.86	350.11	QTZT

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0312	350.11	351.30	GSCH
K-10-0312	351.30	353.85	QTZT
K-10-0312	353.85	359.85	SM
K-10-0312	359.85	362.20	SM
K-10-0312	362.20	362.79	VM
K-10-0312	362.79	365.16	SM
K-10-0312	365.16	365.36	VM
K-10-0312	365.36	367.08	SM
K-10-0312	367.08	368.33	GNST
K-10-0312	368.33	369.57	SM
K-10-0312	369.57	370.64	VM
K-10-0312	370.64	371.97	SM
K-10-0312	371.97	372.47	VM
K-10-0312	372.47	373.78	SM
K-10-0312	373.78	376.80	VM
K-10-0312	376.80	377.95	SM
K-10-0312	377.95	379.20	FLT
K-10-0312	379.20	380.18	QTZT
K-10-0312	380.18	388.93	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0312	0.00	4.88	4.88	0.75	15.37	0.00	0.00	HQ					
K-10-0312	4.88	7.01	2.13	0.42	19.72	0.00	0.00	HQ					
K-10-0312	7.01	7.93	0.92	0.25	27.17	0.00	0.00	HQ					
K-10-0312	7.93	9.75	1.82	0.24	13.19	0.00	0.00	HQ					
K-10-0312	9.75	10.67	0.92	0.41	44.57	0.12	13.04	HQ					
K-10-0312	10.67	11.89	1.22	0.62	50.82	0.10	8.20	HQ					
K-10-0312	11.89	14.02	2.13	1.93	90.61	1.40	65.73	HQ					
K-10-0312	14.02	17.07	3.05	2.81	92.13	0.58	19.02	HQ					
K-10-0312	17.07	20.12	3.05	2.77	90.82	0.25	8.20	HQ					
K-10-0312	20.12	23.17	3.05	2.96	97.05	1.33	43.61	HQ					
K-10-0312	23.17	26.21	3.04	2.87	94.41	1.12	36.84	HQ					
K-10-0312	26.21	29.26	3.05	2.85	93.44	0.94	30.82	HQ					
K-10-0312	29.26	32.31	3.05	2.80	91.80	1.77	58.03	HQ					
K-10-0312	32.31	32.92	0.61	0.65	106.56	0.18	29.51	HQ					
K-10-0312	32.92	35.36	2.44	1.88	77.05	1.04	42.62	HQ					
K-10-0312	35.36	36.58	1.22	1.21	99.18	0.51	41.80	HQ					
K-10-0312	36.58	37.64	1.06	0.23	21.70	0.00	0.00	HQ					
K-10-0312	37.64	38.41	0.77	0.54	70.13	0.00	0.00	HQ					
K-10-0312	38.41	39.47	1.06	0.87	82.08	0.00	0.00	HQ					
K-10-0312	39.47	41.45	1.98	1.75	88.38	0.21	10.61	HQ					
K-10-0312	41.45	44.50	3.05	2.56	83.93	0.61	20.00	HQ					
K-10-0312	44.50	47.55	3.05	2.89	94.75	1.04	34.10	HQ					
K-10-0312	47.55	50.60	3.05	3.05	100.00	0.59	19.34	HQ					
K-10-0312	50.60	53.65	3.05	2.02	66.23	0.48	15.74	HQ					
K-10-0312	53.65	56.69	3.04	1.76	57.89	0.44	14.47	HQ					
K-10-0312	56.69	59.74	3.05	1.22	40.00	0.00	0.00	HQ					
K-10-0312	59.74	62.79	3.05	2.67	87.54	0.49	16.07	HQ					
K-10-0312	62.79	65.84	3.05	3.01	98.69	1.89	61.97	HQ					
K-10-0312	65.84	67.82	1.98	1.74	87.88	1.00	50.51	HQ					
K-10-0312	67.82	68.89	1.07	1.11	103.74	0.73	68.22	HQ					
K-10-0312	68.89	70.10	1.21	1.07	88.43	0.32	26.45	HQ					
K-10-0312	70.10	71.93	1.83	1.65	90.16	1.01	55.19	HQ					
K-10-0312	71.93	73.30	1.37	1.37	100.00	0.30	21.90	HQ					
K-10-0312	73.30	74.98	1.68	1.52	90.48	1.01	60.12	HQ					
K-10-0312	74.98	77.11	2.13	2.04	95.77	1.42	66.67	HQ					
K-10-0312	77.11	78.03	0.92	0.60	65.22	0.00	0.00	HQ					
K-10-0312	78.03	78.94	0.91	0.69	75.82	0.33	36.26	HQ					
K-10-0312	78.94	79.71	0.77	0.76	98.70	0.00	0.00	HQ					
K-10-0312	79.71	81.08	1.37	1.44	105.11	0.53	38.69	HQ					
K-10-0312	81.08	83.67	2.59	2.63	101.54	1.20	46.33	HQ					
K-10-0312	83.67	84.13	0.46	0.45	97.83	0.13	28.26	HQ					
K-10-0312	84.13	85.65	1.52	1.01	66.45	0.54	35.53	HQ					
K-10-0312	85.65	87.17	1.52	1.50	98.68	0.72	47.37	HQ					
K-10-0312	87.17	90.22	3.05	2.76	90.49	0.56	18.36	HQ					
K-10-0312	90.22	93.27	3.05	2.71	88.85	0.69	22.62	HQ					
K-10-0312	93.27	96.32	3.05	2.83	92.79	1.77	58.03	HQ					
K-10-0312	96.32	99.37	3.05	2.79	91.48	0.48	15.74	HQ					
K-10-0312	99.37	102.41	3.04	2.93	96.38	0.78	25.66	HQ					
K-10-0312	102.41	105.46	3.05	2.46	80.66	0.66	21.64	HQ					
K-10-0312	105.46	108.51	3.05	1.31	42.95	0.00	0.00	HQ					
K-10-0312	108.51	111.56	3.05	2.87	94.10	0.67	21.97	HQ					
K-10-0312	111.56	113.08	1.52	1.44	94.74	0.63	41.45	HQ					
K-10-0312	113.08	114.61	1.53	1.45	94.77	0.88	57.52	HQ					
K-10-0312	114.61	117.65	3.04	2.83	93.09	1.94	63.82	HQ					
K-10-0312	117.65	120.70	3.05	2.97	97.38	2.17	71.15	HQ					
K-10-0312	120.70	123.75	3.05	2.81	92.13	2.18	71.48	HQ					
K-10-0312	123.75	126.80	3.05	3.05	100.00	2.15	70.49	HQ					
K-10-0312	126.80	129.84	3.04	2.78	91.45	2.29	75.33	HQ					
K-10-0312	129.84	130.76	0.92	0.87	94.57	0.61	66.30	HQ					
K-10-0312	130.76	132.89	2.13	2.07	97.18	1.42	66.67	HQ					
K-10-0312	132.89	135.94	3.05	2.94	96.39	1.20	39.34	HQ					
K-10-0312	135.94	138.07	2.13	2.12	99.53	0.70	32.86	HQ					
K-10-0312	138.07	138.99	0.92	0.91	98.91	0.80	86.96	HQ					
K-10-0312	138.99	140.36	1.37	1.38	100.73	0.46	33.58	HQ					
K-10-0312	140.36	142.04	1.68	1.52	90.48	0.62	36.90	HQ					
K-10-0312	142.04	144.32	2.28	2.39	104.82	0.80	35.09	HQ					
K-10-0312	144.32	145.09	0.77	0.57	74.03	0.00	0.00	HQ					
K-10-0312	145.09	145.69	0.60	0.50	83.33	0.00	0.00	HQ					
K-10-0312	145.69	147.22	1.53	1.52	99.35	0.51	33.33	HQ					
K-10-0312	147.22	148.13	0.91	0.90	98.90	0.29	31.87	HQ					
K-10-0312	148.13	149.50	1.37	1.27	92.70	0.68	49.64	HQ					
K-10-0312	149.50	151.18	1.68	1.52	90.48	0.88	52.38	HQ					
K-10-0312	151.18	152.71	1.53	1.52	99.35	0.43	28.10	HQ					
K-10-0312	152.71	154.23	1.52	1.31	86.18	0.78	51.32	HQ					
K-10-0312	154.23	157.28	3.05	2.83	92.79	1.57	51.48	HQ					
K-10-0312	157.28	160.33	3.05	3.05	100.00	1.87	61.31	HQ					
K-10-0312	160.33	163.37	3.04	2.89	95.07	2.19	72.04	HQ					
K-10-0312	163.37	165.51	2.14	2.13	99.53	1.39	64.95	HQ					
K-10-0312	165.51	166.42	0.91	0.88	96.70	0.38	41.76	HQ					
K-10-0312	166.42	167.64	1.22	0.95	77.87	0.57	46.72	HQ					
K-10-0312	167.64	169.47	1.83	2.00	109.29	1.32	72.13	HQ					
K-10-0312	169.47	172.52	3.05	3.03	99.34	2.49	81.64	HQ					
K-10-0312	172.52	175.57	3.05	2.88	94.43	1.98	64.92	HQ					
K-10-0312	175.57	178.61	3.04	2.99	98.36	2.07	68.09	HQ					
K-10-0312	178.61	181.66	3.05	3.04	99.67	1.96	64.26	HQ					
K-10-0312	181.66	184.71	3.05	2.96	97.05	2.19	71.80	HQ					
K-10-0312	184.71	187.15	2.44	2.30	94.26	1.63	66.80	HQ					
K-10-0312	187.15	187.76	0.61	0.61	100.00	0.41	67.21	HQ					
K-10-0312	187.76	188.67	0.91	0.89	97.80	0.64	70.33	HQ					
K-10-0312	188.67	190.81	2.14	2.10	98.13	1.38	64.49	HQ					
K-10-0312	190.81	193.83	3.02	2.81	93.05	1.55	51.32	HQ					
K-10-0312	193.83	195.38	1.55	1.41	90.97	0.91	58.71	HQ					
K-10-0312	195.38	196.90	1.52	1.52	100.00	0.82	53.95	HQ					
K-10-0312	196.90	197.66	0.76	0.65	85.53	0.52	68.42	HQ					
K-10-0312	197.66	199.95	2.29	2.03	88.65	1.56	68.12	HQ					
K-10-0312	199.95	201.32	1.37	1.26	91.97	0.53	38.69	HQ					
K-10-0312	201.32	203.00	1.68	1.52	90.48	0.14	8.33	HQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0312	203.00	203.30	0.30	0.30	100.00	0.30	100.00	HQ					
K-10-0312	203.30	206.05	2.75	2.62	95.27	1.90	69.09	HQ					
K-10-0312	206.05	209.09	3.04	2.93	96.38	1.79	58.88	HQ					
K-10-0312	209.09	212.14	3.05	2.92	95.74	2.06	67.54	HQ					
K-10-0312	212.14	215.19	3.05	3.05	100.00	1.85	60.66	HQ					
K-10-0312	215.19	218.24	3.05	3.00	98.36	1.85	60.66	HQ					
K-10-0312	218.24	221.29	3.05	2.86	93.77	1.01	33.11	HQ					
K-10-0312	221.29	222.81	1.52	1.34	88.16	0.49	32.24	HQ					
K-10-0312	222.81	224.33	1.52	1.30	85.53	0.55	36.18	HQ					
K-10-0312	224.33	226.31	1.98	1.73	87.37	0.73	36.87	HQ					
K-10-0312	226.31	227.38	1.07	0.99	92.52	0.50	46.73	HQ					
K-10-0312	227.38	227.99	0.61	0.51	83.61	0.18	29.51	HQ					
K-10-0312	227.99	229.06	1.07	1.04	97.20	0.40	37.38	HQ					
K-10-0312	229.06	230.43	1.37	1.13	82.48	0.16	11.68	HQ					
K-10-0312	230.43	231.95	1.52	1.35	88.82	0.54	35.53	HQ					
K-10-0312	231.95	233.48	1.53	1.52	99.35	0.61	39.87	HQ					
K-10-0312	233.48	235.00	1.52	1.36	89.47	0.44	28.95	HQ					
K-10-0312	235.00	236.22	1.22	1.07	87.70	0.32	26.23	HQ					
K-10-0312	236.22	236.53	0.31	0.31	100.00	0.25	80.65	HQ					
K-10-0312	236.53	238.05	1.52	1.42	93.42	0.63	41.45	HQ					
K-10-0312	238.05	239.57	1.52	1.41	92.76	0.41	26.97	HQ					
K-10-0312	239.57	242.62	3.05	2.55	83.61	0.36	11.80	HQ					
K-10-0312	242.62	245.67	3.05	3.05	100.00	1.05	34.43	HQ					
K-10-0312	245.67	248.72	3.05	2.83	92.79	0.69	22.62	HQ					
K-10-0312	248.72	251.77	3.05	3.05	100.00	2.04	66.89	HQ					
K-10-0312	251.77	252.98	1.21	1.05	86.78	0.86	71.07	HQ					
K-10-0312	252.98	254.81	1.83	1.52	83.06	0.88	48.09	HQ					
K-10-0312	254.81	255.21	0.40	0.31	77.50	0.14	35.00	HQ					
K-10-0312	255.21	256.49	1.28	1.33	103.91	0.33	25.78	HQ					
K-10-0312	256.49	257.56	1.07	1.24	115.89	0.57	53.27	HQ					
K-10-0312	257.56	258.47	0.91	0.52	57.14	0.45	49.45	HQ					
K-10-0312	258.47	259.99	1.52	1.33	87.50	0.23	15.13	HQ					
K-10-0312	259.99	260.91	0.92	0.77	83.70	0.12	13.04	HQ					
K-10-0312	260.91	261.52	0.61	0.60	98.36	0.00	0.00	HQ					
K-10-0312	261.52	263.35	1.83	1.37	74.86	0.44	24.04	HQ					
K-10-0312	263.35	263.96	0.61	0.65	106.56	0.51	83.61	HQ					
K-10-0312	263.96	266.40	2.44	2.41	98.77	1.25	51.23	HQ					
K-10-0312	266.40	267.01	0.61	0.59	96.72	0.26	42.62	HQ					
K-10-0312	267.01	267.92	0.91	0.62	68.13	0.28	30.77	HQ					
K-10-0312	267.92	270.05	2.13	2.11	99.06	0.96	45.07	HQ					
K-10-0312	270.05	273.10	3.05	2.96	97.05	1.92	62.95	HQ					
K-10-0312	273.10	276.15	3.05	2.93	96.07	0.65	21.31	HQ					
K-10-0312	276.15	279.20	3.05	2.95	96.72	2.04	66.89	HQ					
K-10-0312	279.20	282.25	3.05	2.71	88.85	1.48	48.52	HQ					
K-10-0312	282.25	285.29	3.04	2.95	97.04	1.44	47.37	HQ					
K-10-0312	285.29	288.34	3.05	3.00	98.36	1.99	65.25	HQ					
K-10-0312	288.34	291.39	3.05	2.88	94.43	1.59	52.13	HQ					
K-10-0312	291.39	294.44	3.05	2.51	82.30	0.65	21.31	HQ					
K-10-0312	294.44	295.96	1.52	1.45	95.39	0.37	24.34	HQ					
K-10-0312	295.96	297.49	1.53	1.41	92.16	0.72	47.06	HQ					
K-10-0312	297.49	298.40	0.91	0.86	94.51	0.00	0.00	HQ					
K-10-0312	298.40	299.62	1.22	1.04	85.25	0.10	8.20	HQ					
K-10-0312	299.62	300.53	0.91	0.88	96.70	0.54	59.34	HQ					
K-10-0312	300.53	302.82	2.29	2.17	94.76	0.40	17.47	HQ					
K-10-0312	302.82	303.58	0.76	0.95	125.00	0.00	0.00	HQ					
K-10-0312	303.58	304.50	0.92	0.85	92.39	0.00	0.00	HQ					
K-10-0312	304.50	306.02	1.52	1.34	88.16	0.15	9.87	HQ					
K-10-0312	306.02	306.63	0.61	0.30	49.18	0.00	0.00	HQ					
K-10-0312	306.63	307.24	0.61	0.49	80.33	0.14	22.95	HQ					
K-10-0312	307.24	309.37	2.13	2.20	103.29	1.59	74.65	HQ					
K-10-0312	309.37	309.68	0.31	0.30	96.77	0.11	35.48	HQ					
K-10-0312	309.68	311.66	1.98	1.83	92.42	0.58	29.29	HQ					
K-10-0312	311.66	312.73	1.07	1.14	106.54	0.74	69.16	HQ					
K-10-0312	312.73	315.77	3.04	3.05	100.33	1.40	46.05	HQ					
K-10-0312	315.77	318.82	3.05	2.85	93.44	1.54	50.49	HQ					
K-10-0312	318.82	320.19	1.37	1.21	88.32	0.68	49.64	HQ					
K-10-0312	320.19	321.87	1.68	1.10	65.48	0.40	23.81	HQ					
K-10-0312	321.87	322.48	0.61	0.35	57.38	0.18	29.51	HQ					
K-10-0312	322.48	323.39	0.91	0.73	80.22	0.00	0.00	HQ					
K-10-0312	323.39	324.46	1.07	1.05	98.13	0.34	31.78	HQ					
K-10-0312	324.46	324.92	0.46	0.37	80.43	0.10	21.74	HQ					
K-10-0312	324.92	325.83	0.91	0.72	79.12	0.12	13.19	HQ					
K-10-0312	325.83	327.66	1.83	0.95	51.91	0.47	25.68	HQ					
K-10-0312	327.66	327.97	0.31	0.26	83.87	0.00	0.00	HQ					
K-10-0312	327.97	328.73	0.76	0.71	93.42	0.00	0.00	HQ					
K-10-0312	328.73	329.49	0.76	0.74	97.37	0.15	19.74	HQ					
K-10-0312	329.49	330.71	1.22	1.01	82.79	0.00	0.00	HQ					
K-10-0312	330.71	331.01	0.30	0.25	83.33	0.11	36.67	HQ					
K-10-0312	331.01	331.62	0.61	0.26	42.62	0.00	0.00	HQ					
K-10-0312	331.62	334.06	2.44	0.64	26.23	0.29	11.89	HQ					
K-10-0312	334.06	337.11	3.05	2.75	90.16	0.15	4.92	HQ					
K-10-0312	337.11	340.16	3.05	2.98	97.70	0.32	10.49	HQ					
K-10-0312	340.16	343.21	3.05	2.83	92.79	1.03	33.77	HQ					
K-10-0312	343.21	346.25	3.04	2.71	89.14	0.56	18.42	HQ					
K-10-0312	346.25	347.02	0.77	0.75	97.40	0.23	29.87	HQ					
K-10-0312	347.02	349.00	1.98	1.86	93.94	0.93	46.97	HQ					
K-10-0312	349.00	349.30	0.30	0.28	93.33	0.19	63.33	HQ					
K-10-0312	349.30	350.98	1.68	1.52	90.48	0.57	33.93	HQ					
K-10-0312	350.98	352.35	1.37	1.10	80.29	0.00	0.00	HQ					
K-10-0312	352.35	353.42	1.07	0.64	59.81	0.00	0.00	HQ					
K-10-0312	353.42	355.40	1.98	2.06	104.04	0.90	45.45	HQ					
K-10-0312	355.40	358.45	3.05	2.82	92.46	2.02	66.23	HQ					
K-10-0312	358.45	361.49	3.04	2.96	97.37	2.30	75.66	HQ					
K-10-0312	361.49	364.54	3.05	3.02	99.02	2.33	76.39	HQ					
K-10-0312	364.54	365.76	1.22	1.17	95.90	0.62	50.82	HQ					
K-10-0312	365.76	367.59	1.83	1.90	103.83	1.34	73.22	HQ					
K-10-0312	367.59	370.64	3.05	3.03	99.34	1.95	63.93	HQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0312	370.64	373.69	3.05	2.88	94.43	2.44	80.00	HQ					
K-10-0312	373.69	376.73	3.04	3.05	100.33	2.72	89.47	HQ					
K-10-0312	376.73	377.95	1.22	0.92	75.41	0.40	32.79	HQ					
K-10-0312	377.95	379.78	1.83	0.97	53.01	0.00	0.00	HQ					
K-10-0312	379.78	381.31	1.53	1.41	92.16	0.00	0.00	HQ					
K-10-0312	381.31	382.83	1.52	1.39	91.45	0.11	7.24	HQ					
K-10-0312	382.83	383.74	0.91	0.98	107.69	0.00	0.00	HQ					
K-10-0312	383.74	385.72	1.98	1.86	93.94	0.18	9.09	HQ					
K-10-0312	385.72	385.77	0.05	0.05	100.00	0.00	0.00	HQ					
K-10-0312	385.77	387.40	1.63	1.39	85.28	0.00	0.00	HQ					
K-10-0312	387.40	388.93	1.53	1.45	94.77	0.63	41.18	HQ					

Hole_ID	mFrom	mTo	Dominant Lithology
K-10-0320	0.00	13.62	OVB
K-10-0320	13.62	21.90	GSCH
K-10-0320	21.90	22.70	SSCH
K-10-0320	22.70	27.23	TQTZT
K-10-0320	27.23	50.22	QTZT
K-10-0320	50.22	52.13	GSCH
K-10-0320	52.13	54.63	QTZT
K-10-0320	54.63	55.57	ICQS
K-10-0320	55.57	56.69	FLT
K-10-0320	56.69	63.35	QTZT
K-10-0320	63.35	70.32	TQTZT
K-10-0320	70.32	75.20	ICQS
K-10-0320	75.20	81.08	QTZT
K-10-0320	81.08	81.90	ICQS
K-10-0320	81.90	87.60	QTZT
K-10-0320	87.60	92.10	ICQS
K-10-0320	92.10	95.44	QTZT
K-10-0320	95.44	98.18	TQTZT
K-10-0320	98.18	101.94	QTZT
K-10-0320	101.94	103.13	TQTZT
K-10-0320	103.13	105.72	QTZT
K-10-0320	105.72	109.03	GSCH
K-10-0320	109.03	110.71	SSCH
K-10-0320	110.71	111.33	GSCH
K-10-0320	111.33	113.40	SSCH
K-10-0320	113.40	114.65	GSCH
K-10-0320	114.65	117.56	QTZT
K-10-0320	117.56	118.35	GSCH
K-10-0320	118.35	123.60	TQTZT
K-10-0320	123.60	133.20	QTZT
K-10-0320	133.20	135.00	ICQS
K-10-0320	135.00	140.65	TQTZT
K-10-0320	140.65	149.20	QTZT
K-10-0320	149.20	152.58	TQTZT
K-10-0320	152.58	157.98	SSCH
K-10-0320	157.98	169.95	GSCH
K-10-0320	169.95	188.98	TQTZT
K-10-0320	188.98	189.45	FLT
K-10-0320	189.45	195.38	QTZT
K-10-0320	195.38	202.26	TQTZT
K-10-0320	202.26	207.47	TQTZT
K-10-0320	207.47	209.56	GSCH
K-10-0320	209.56	216.52	QTZT
K-10-0320	216.52	219.76	FLT
K-10-0320	219.76	221.00	VM
K-10-0320	221.00	224.02	VM
K-10-0320	224.02	227.00	GSCH
K-10-0320	227.00	229.25	QTZT
K-10-0320	229.25	241.50	ICQS
K-10-0320	241.50	242.83	FLT
K-10-0320	242.83	243.26	GNST
K-10-0320	243.26	243.84	TQTZT

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0320	7.01	7.93	0.92	0.92	100.00	0.24	26.09	HQ					
K-10-0320	7.93	10.06	2.13	0.75	35.21	0.20	9.39	HQ					
K-10-0320	10.06	10.97	0.91	0.41	45.05	0.13	14.29	HQ					
K-10-0320	10.97	13.11	2.14	0.50	23.36	0.00	0.00	HQ					
K-10-0320	13.11	14.02	0.91	0.91	100.00	0.00	0.00	HQ					
K-10-0320	14.02	15.85	1.83	1.75	95.63	0.32	17.49	HQ					
K-10-0320	15.85	17.07	1.22	1.14	93.44	0.00	0.00	HQ					
K-10-0320	17.07	18.90	1.83	1.80	98.36	1.16	63.39	HQ					
K-10-0320	18.90	20.12	1.22	1.21	99.18	0.61	50.00	HQ					
K-10-0320	20.12	23.17	3.05	3.00	98.36	2.00	65.57	HQ					
K-10-0320	23.17	26.21	3.04	2.95	97.04	1.95	64.14	HQ					
K-10-0320	26.21	29.26	3.05	3.01	98.69	1.85	60.66	HQ					
K-10-0320	29.26	32.31	3.05	2.97	97.38	1.54	50.49	HQ					
K-10-0320	32.31	35.36	3.05	3.05	100.00	2.05	67.21	HQ					
K-10-0320	35.36	36.73	1.37	1.40	102.19	0.86	62.77	HQ					
K-10-0320	36.73	38.41	1.68	1.68	100.00	1.11	66.07	HQ					
K-10-0320	38.41	41.45	3.04	2.92	96.05	1.57	51.64	HQ					
K-10-0320	41.45	43.89	2.44	2.10	86.07	1.22	50.00	HQ					
K-10-0320	43.89	44.50	0.61	0.55	90.16	0.36	59.02	HQ					
K-10-0320	44.50	47.55	3.05	2.98	97.70	1.93	63.28	HQ					
K-10-0320	47.55	50.60	3.05	2.70	88.52	1.20	39.34	HQ					
K-10-0320	50.60	53.65	3.05	2.90	95.08	0.35	11.48	HQ					
K-10-0320	53.65	56.69	3.04	2.65	87.17	1.16	38.16	HQ					
K-10-0320	56.69	57.46	0.77	0.49	63.64	0.00	0.00	HQ					
K-10-0320	57.46	59.74	2.28	1.52	66.67	0.46	20.18	HQ					
K-10-0320	59.74	62.79	3.05	2.88	94.43	1.27	41.64	HQ					
K-10-0320	62.79	65.84	3.05	2.82	92.46	1.68	55.08	HQ					
K-10-0320	65.84	68.89	3.05	2.50	81.97	0.41	13.44	HQ					
K-10-0320	68.89	71.93	3.04	2.83	93.09	1.27	41.78	HQ					
K-10-0320	71.93	74.98	3.05	2.94	96.39	0.59	19.34	HQ					
K-10-0320	74.98	78.03	3.05	2.74	89.84	0.75	24.59	HQ					
K-10-0320	78.03	80.47	2.44	2.07	84.84	0.94	38.52	HQ					
K-10-0320	80.47	81.08	0.61	0.60	98.36	0.00	0.00	HQ					
K-10-0320	81.08	84.13	3.05	3.05	100.00	1.05	34.43	HQ					
K-10-0320	84.13	87.17	3.04	3.04	100.00	0.96	31.58	HQ					
K-10-0320	87.17	88.54	1.37	1.29	94.16	0.51	37.23	HQ					
K-10-0320	88.54	90.22	1.68	1.63	97.02	0.90	53.57	HQ					
K-10-0320	90.22	90.83	0.61	0.61	100.00	0.34	55.74	HQ					
K-10-0320	90.83	92.81	1.98	1.44	72.73	0.43	21.72	HQ					
K-10-0320	92.81	93.27	0.46	0.34	73.91	0.00	0.00	HQ					
K-10-0320	93.27	96.32	3.05	2.80	91.80	2.12	69.51	HQ					
K-10-0320	96.32	99.37	3.05	2.89	94.75	2.06	67.54	HQ					
K-10-0320	99.37	100.13	0.76	0.69	90.79	0.42	55.26	HQ					
K-10-0320	100.13	102.41	2.28	2.07	90.79	1.15	50.44	HQ					
K-10-0320	102.41	105.46	3.05	3.05	100.00	1.80	59.02	HQ					
K-10-0320	105.46	106.22	0.76	0.65	85.53	0.25	32.89	HQ					
K-10-0320	106.22	108.51	2.29	2.22	96.94	1.44	62.88	HQ					
K-10-0320	108.51	111.56	3.05	2.92	95.74	1.25	40.98	HQ					
K-10-0320	111.56	113.08	1.52	1.52	100.00	0.54	35.53	HQ					
K-10-0320	113.08	114.61	1.53	1.45	94.77	0.95	62.09	HQ					
K-10-0320	114.61	117.65	3.04	2.85	93.75	2.03	66.78	HQ					
K-10-0320	117.65	120.70	3.05	2.83	92.79	0.94	30.82	HQ					
K-10-0320	120.70	123.75	3.05	2.79	91.48	2.00	65.57	HQ					
K-10-0320	123.75	126.80	3.05	2.75	90.16	1.29	42.30	HQ					
K-10-0320	126.80	129.84	3.04	3.02	99.34	2.52	82.89	HQ					
K-10-0320	129.84	132.89	3.05	2.65	86.89	1.10	36.07	HQ					
K-10-0320	132.89	135.94	3.05	2.83	92.79	1.35	44.26	HQ					
K-10-0320	135.94	138.99	3.05	2.97	97.38	2.51	82.30	HQ					
K-10-0320	138.99	142.04	3.05	2.98	97.70	2.34	76.72	HQ					
K-10-0320	142.04	145.08	3.04	3.01	99.01	2.67	87.83	HQ					
K-10-0320	145.08	148.13	3.05	2.95	96.72	2.56	83.93	HQ					
K-10-0320	148.13	151.18	3.05	2.86	93.77	2.03	66.56	HQ					
K-10-0320	151.18	154.23	3.05	2.97	97.38	2.09	68.52	HQ					
K-10-0320	154.23	157.28	3.05	3.02	99.02	1.98	64.92	HQ					
K-10-0320	157.28	160.32	3.04	2.98	98.03	2.31	75.99	HQ					
K-10-0320	160.32	163.37	3.05	3.04	99.67	2.01	65.90	HQ					
K-10-0320	163.37	166.42	3.05	2.97	97.38	2.32	76.07	HQ					
K-10-0320	166.42	169.47	3.05	3.00	98.36	1.58	51.80	HQ					
K-10-0320	169.47	172.52	3.05	3.03	99.34	1.40	45.90	HQ					
K-10-0320	172.52	175.56	3.04	2.96	97.37	1.61	52.96	HQ					
K-10-0320	175.56	178.61	3.05	3.02	99.02	1.82	59.67	HQ					
K-10-0320	178.61	181.05	2.44	2.41	98.77	1.32	54.10	HQ					
K-10-0320	181.05	181.66	0.61	0.56	91.80	0.29	47.54	HQ					
K-10-0320	181.66	182.88	1.22	0.62	50.82	0.35	28.69	HQ					
K-10-0320	182.88	184.40	1.52	1.22	80.26	0.00	0.00	HQ					
K-10-0320	184.40	184.71	0.31	0.31	100.00	0.00	0.00	HQ					
K-10-0320	184.71	186.84	2.13	1.85	86.85	0.27	12.68	HQ					
K-10-0320	186.84	187.76	0.92	0.88	95.65	0.00	0.00	HQ					
K-10-0320	187.76	189.43	1.67	1.31	78.44	0.11	6.59	HQ					
K-10-0320	189.43	190.81	1.38	1.32	95.65	0.63	45.65	HQ					
K-10-0320	190.81	192.48	1.67	1.53	91.62	0.64	38.32	HQ					
K-10-0320	192.48	193.85	1.37	1.19	86.86	0.42	30.66	HQ					
K-10-0320	193.85	195.38	1.53	1.35	88.24	0.48	31.37	HQ					
K-10-0320	195.38	196.90	1.52	1.47	96.71	0.34	22.37	HQ					
K-10-0320	196.90	197.21	0.31	0.31	100.00	0.00	0.00	HQ					
K-10-0320	197.21	199.95	2.74	2.51	91.61	0.57	20.80	HQ					
K-10-0320	199.95	203.00	3.05	2.79	91.48	0.83	27.21	HQ					
K-10-0320	203.00	206.05	3.05	2.91	95.41	0.72	23.61	HQ					
K-10-0320	206.05	207.57	1.52	1.52	100.00	0.50	32.89	HQ					
K-10-0320	207.57	209.09	1.52	1.52	100.00	0.38	25.00	HQ					
K-10-0320	209.09	212.14	3.05	2.91	95.41	1.68	55.08	HQ					
K-10-0320	212.14	215.19	3.05	2.92	95.74	2.28	74.75	HQ					
K-10-0320	215.19	216.87	1.68	1.58	94.05	0.78	46.43	HQ					
K-10-0320	216.87	218.24	1.37	1.08	78.83	0.43	31.39	HQ					
K-10-0320	218.24	221.29	3.05	3.05	100.00	2.03	66.56	HQ					
K-10-0320	221.29	224.33	3.04	2.78	91.45	1.83	60.20	HQ					
K-10-0320	224.33	226.47	2.14	2.10	98.13	0.66	30.84	HQ					

Hole_ID	mFrom	mTo	Interval m	Recovery m	Recovery %	RQD m	RQD %	Core_Size	No. Fractures	Rock Strength	No. Cemented Joint/Vein	Cemented Joint/Vein Strength	Vein %
K-10-0320	226.47	227.38	0.91	0.79	86.81	0.31	34.07	HQ					
K-10-0320	227.38	230.43	3.05	3.05	100.00	1.54	50.49	HQ					
K-10-0320	230.43	232.41	1.98	0.66	33.33	0.00	0.00	HQ					
K-10-0320	232.41	233.48	1.07	1.07	100.00	0.00	0.00	HQ					
K-10-0320	233.48	233.78	0.30	0.29	96.67	0.10	33.33	HQ					
K-10-0320	233.78	236.52	2.74	2.63	95.99	0.11	4.01	HQ					
K-10-0320	236.52	238.35	1.83	1.04	56.83	0.00	0.00	HQ					
K-10-0320	238.35	239.57	1.22	0.66	54.10	0.00	0.00	HQ					
K-10-0320	239.57	239.87	0.30	0.21	70.00	0.00	0.00	HQ					
K-10-0320	239.87	241.25	1.38	1.12	81.16	0.00	0.00	HQ					
K-10-0320	241.25	242.32	1.07	0.59	55.14	0.00	0.00	HQ					
K-10-0320	242.32	242.62	0.30	0.28	93.33	0.00	0.00	HQ					
K-10-0320	242.62	243.84	1.22	0.88	72.13	0.00	0.00	HQ					

Alexco Keno Hill Mining Corp.

Groundwater Monitoring Plan

Water Use Licence QZ09-092

Appendix C

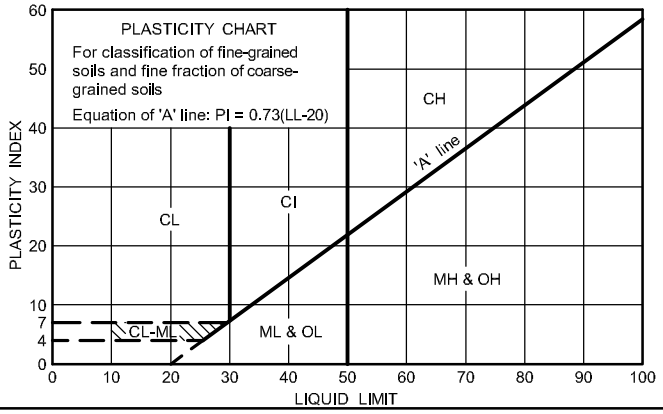
Flame and Moth Site Geotechnical Borehole Logs

APPENDIX A

APPENDIX A TESTHOLE LOGS

MODIFIED UNIFIED SOIL CLASSIFICATION

MAJOR DIVISIONS			GROUP SYMBOLS	TYPICAL NAMES	CLASSIFICATION CRITERIA
COARSE - GRAINED SOILS More than 50% retained on No. 200 sieve*	GRAVELS 50% or more of coarse fraction retained on No. 4 sieve	CLEAN GRAVELS	GW	Well-graded gravels and gravel-sand mixtures, little or no fines	Classification on basis of percentage of fines Less than 5% pass No. 200 sieve GW, GP, SW, SP More than 12% pass No. 200 sieve GM, GC, SM, SC 5% to 12% pass No. 200 sieve Borderline classification requiring use of dual symbols $C_u = D_{60}/D_{10}$ Greater than 4 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3
			GP	Poorly-graded gravels and gravel-sand mixtures, little or no fines	Not meeting both criteria for GW
		GRAVELS WITH FINES	GM	Silty gravels, gravel-sand-silt mixtures	Atterberg limits plot below 'A' line or plasticity index less than 4 / Atterberg limits plot above 'A' line and plasticity index greater than 7 — Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols
			GC	Clayey gravels, gravel-sand-clay mixtures	
	SANDS More than 50% of coarse fraction passes No. 4 sieve	CLEAN SANDS	SW	Well-graded sands and gravelly sands, little or no fines	$C_u = D_{60}/D_{10}$ Greater than 6 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3
			SP	Poorly-graded sands and gravelly sands, little or no fines	Not meeting both criteria for SW
		SANDS WITH FINES	SM	Silty sands, sand-silt mixtures	Atterberg limits plot below 'A' line or plasticity index less than 4 / Atterberg limits plot above 'A' line and plasticity index greater than 7 — Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols
			SC	Clayey sands, sand-clay mixtures	
FINE - GRAINED SOILS 50% or more passes No. 200 sieve*	SILTS AND CLAYS Liquid Limit 50% or less		ML	Inorganic silts, very fine sands, rock flour, silty or clayey fine sands	
			CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays silty clays, lean clays	
			OL	Organic silts and organic silty clays of low plasticity	
	SILTS AND CLAYS Liquid Limit greater than 50%		MH	Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts	
			CH	Inorganic clay of high plasticity, fat clays	
			OH	Organic clays of medium to high plasticity	
HIGHLY ORGANIC SOILS			PT	Peat, muck and other highly organic soils	



* Based on the material passing the 3 in. (75 mm) sieve
† ASTM Designation D 2487, for identification procedure see D 2488

GROUND ICE DESCRIPTION

ICE NOT VISIBLE

GROUP SYMBOLS	SYMBOLS	SUBGROUP DESCRIPTION	
N	Nf	Poorly-bonded or friable	
	Nbn	No excess ice, well- bonded	
	Nbe	Excess ice, well- bonded	

VISIBLE ICE LESS THAN 50% BY VOLUME

GROUP SYMBOLS	SYMBOLS	SUBGROUP DESCRIPTION	
V	Vx	Individual ice crystals or inclusions	
	Vc	Ice coatings on particles	
	Vr	Random or irregularly oriented ice formations	
	Vs	Stratified or distinctly oriented ice formations	

VISIBLE ICE GREATER THAN 50% BY VOLUME

ICE	ICE + Soil Type	Ice with soil inclusions	
	ICE	Ice without soil inclusions (greater than 25 mm (1 in.) thick	

NOTES:

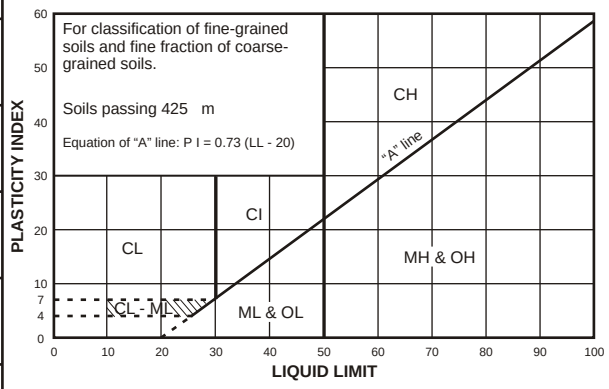
1. Dual symbols are used to indicate borderline or mixed ice classifications.
2. Visual estimates of ice contents indicated on borehole logs ± 5%
3. This system of ground ice description has been modified from NRC Technical Memo 79, Guide to the Field Description of Permafrost for Engineering Purposes.

LEGEND:

Soil ☐ Ice ■

MODIFIED UNIFIED SOIL CLASSIFICATION †

MAJOR DIVISIONS			GROUP SYMBOLS	TYPICAL NAMES	CLASSIFICATION CRITERIA		
COARSE-GRAINED SOILS More than 50% retained on No. 200 sieve*	GRAVELS 50% or more of coarse fraction retained on No. 4 sieve	CLEAN GRAVELS	GW	Well-graded gravels and gravel-sand mixtures, little or no fines	Classification on basis of percentage of fines GW, GP, SW, SP GM, GC, SM, SC Bordering Classification requiring use of dual symbols	$C_U = D_{60}/D_{10}$ Greater than 4 $C_U = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3	
			GP	Poorly graded gravels and gravel-sand mixtures, little or no fines		Not meeting both criteria for GW	
		GRAVELS WITH FINES	GM	Silty gravels, gravel-sand-silt mixtures		Atterburg limits plot below "A" line or plasticity index less than 4	Atterburg limits plotting in hatched area are borderline classifications requiring use of dual symbols
			GC	Clayey gravels, gravel-sand-clay mixtures		Atterburg limits plot above "A" line or plasticity index greater than 7	
	SANDS More than 50% of coarse fraction passes No. 4 sieve	CLEAN SANDS	SW	Well-graded sands and gravelly sands,little or no fines	Classification on basis of percentage of fines Less than 5% Pass No. 200 sieve More than 12% Pass No. 200 sieve 5% to 12% Pass No. 200 sieve	$C_U = D_{60}/D_{10}$ Greater than 6 $C_U = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3	
			SP	Poorly graded sands and gravelly sands, little or no fines		Not meeting both criteria for SW	
		SANDS WITH FINES	SM	Silty sands, sand-silt mixtures		Atterburg limits plot below "A" line or plasticity index less than 4	Atterburg limits plotting in hatched area are borderline classifications requiring use of dual symbols
			SC	Clayey sands, sand-clay mixtures		Atterburg limits plot above "A" line or plasticity index greater than 7	
FINE-GRAINED SOILS 50% or more passes No. 200 sieve*	SILTS AND CLAYS Liquid limit 50% or less		ML	Inorganic silts, very fine sands, rock flour, silty or clayey fine sands	PLASTICITY CHART		
			CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays			
			OL	Organic silts and organic silty clays of low plasticity			
	SILTS AND CLAYS Liquid limit greater than 50%		MH	Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts			
			CH	Inorganic clays of high plasticity, fat clays			
			OH	Organic clays of medium to high plasticity			
HIGHLY ORGANIC SOILS			PT	Peat, muck and other highly organic soils	*Based on the material passing the 3 in. (75 mm) sieve †ASTM Designation D 2487, for identification procedure see D2488		



SOIL COMPONENTS

FRACTION	SIEVE SIZE		DEFINING RANGES OF PERCENTAGE BY WEIGHT OF MINOR COMPONENTS	
	PASSING	RETAINED	PERCENTAGE	DESCRIPTOR
GRAVEL				
coarse	75 mm	19 mm	>35 %	"and"
fine	19 mm	4.75 mm	21 to 35 %	"y-adjective"
SAND				
coarse	4.75 mm	2.00 mm	10 to 20 %	"some"
medium	2.00 mm	425 m		
fine	425 m	75 m	>0 to 10 %	"trace"
SILT (non plastic) or CLAY (plastic)	75 m		as above but by behavior	

OVERSIZE MATERIAL

Rounded or subrounded

COBBLES	75 mm to 200 mm
BOULDERS	> 200 mm

Not rounded

ROCK FRAGMENTS	>75 mm
ROCKS	> 0.76 cubic metre in volume

Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Lower Diversion Stucture	DRILL: Mini-Sonic	W14101178.003-BH15
Keno City, YT		ELEVATION: 896.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	SPT (N)	GROUND ICE DESCRIPTION	Thermistor	Elevation (m)
0	PEAT - amorphous, granular, dark brown, damp					UNFROZEN		
	GRAVEL AND SAND - trace silt, compact (est.), medium grained, well graded, damp, light brown							
1			SA01	-0.5				896.0
2			SA02	0				895.0
	GRAVEL AND SILT (TILL) - sandy, non-plastic, gap graded, massive, olive grey, contains cobbles					FROZEN - no visible ice in cuttings		
3			SA03	0	94			894.0
	ICE AND SILT - some sand, some gravel, trace clay, low plastic		SA04			Vs(65%)		
4	ICE - massive ice					MASSIVE ICE - cloudy, white, stratified		893.0
			SA05	-0.1		25075		
	SILT (TILL) - gravelly, sandy, trace clay, low plastic							
5			SA06			1202		892.0
	ICE - massive ice					oriented		
6								891.0
	SILT (TILL) - sandy, gravelly, trace clay, low plastic, olive grey		SA07			Vr, Vx (15%) Nbe (25%)		
				-0.2				
7			SA08					890.0
			SA09			becomes Vx (10%) Nbe (50%)		
8			SA10			Vs (10%)		889.0
			SA11					
9			SA12					888.0
			SA13	-0.2				
			SA14					
10								887.0

STANDARD PENETRATION (N): 20 40 60 80

POCKET PEN. (kPa): 100 200 300 400

PLASTIC M.C. LIQUID: 20 40 60 80

Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Lower Diversion Stucture	DRILL: Mini-Sonic	W14101178.003-BH15
Keno City, YT		ELEVATION: 896.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	SPT (N)	STANDARD PENETRATION (N) 20 40 60 80; POCKET PEN. (kPa) 100 200 300 400; PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Thermistor	Elevation (m)
10			SA15						
11			SA16						886.0
			SA17						
12			SA18	-0.2					885.0
	ICE - massive ice						MASSIVE ICE - cloudy, stratified crystals		
			SA19						
13									884.0
	SILT AND GRAVEL - sandy, trace clay, low plastic, gap graded, massive, olive grey						(Vs, Vx 10%), ice stratification is vertical		
14			SA20	-0.2					883.0
15			SA21						882.0
				-0.2					
			SA22						
16	BOULDERS AND COBBLES - gravelly, some sand, gap graded, lens of fine gravel						- no visible ice but may be thawed by drilling, sample wet		881.0
	- slough at borehole at completion			-0.1					
	SAND - some silt, trace gravel, fine grained, well sorted, wet, grey/yellow								
17	SILT (TILL) - gravelly, sandy, trace clay, soft, non-plastic, massive, wet, brownish-grey								880.0
				-0.2					
18	SAND - some gravel, coarse grained, well graded, moist, grey								879.0
	- becomes fine grained, well sorted		SA23						
	SILT AND GRAVEL (TILL) - sandy, non-plastic, massive, firm, moist, olive grey								
			SA24						
19	GRAVEL - cobbly, sandy, trace silt, dense, well graded, damp, light grey								878.0
20	SILT AND GRAVEL - sandy, non-plastic, firm, massive,								877.0

Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Lower Diversion Stucture	DRILL: Mini-Sonic	W14101178.003-BH15
Keno City, YT		ELEVATION: 896.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	SPT (N)	STANDARD PENETRATION (N) 20 40 60 80; POCKET PEN. (kPa) 100 200 300 400; PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Thermistor	Elevation (m)
20	damp, olive grey		SA25						
21	GRAVEL - sandy, cobbles, trace silt, dense, well graded, dry to damp, light brown, subrounded to subangular		SA26						876.0
	END OF BOREHOLE 21.3 m								
22									875.0
23									874.0
24									873.0
25									872.0
26									871.0
27									870.0
28									869.0
29									868.0
30									867.0

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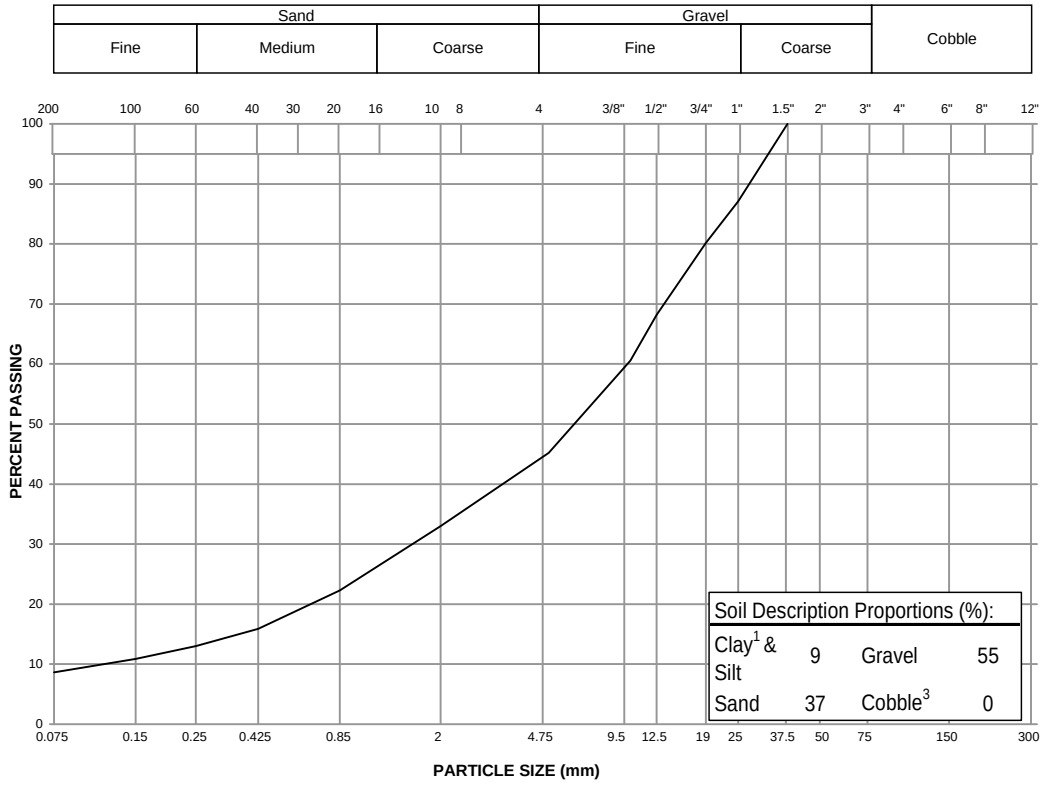
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REVIEWED BY:	COMPLETE: 8/30/2009
DRAWING NO:	Page 3 of 3

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	20-Oct-2009 By: SMS
Sample No.:	SA01	Soil Description[2]:	GRAVEL AND SAND - trace silt
Sample Loc.:	BH15		
Sample Depth:	1.0 - 1.2 m	USC Classification:	Cu: 81.0
Sampling Method:			Cc: 2.4
Date sampled:	Sep-09 By: Client	Moisture Content:	7.4

Particle Size (mm)	Percent Passing
300	
200	
150	
100	
75	
50	
38	100
25	87
19	80
12.5	68
10	61
5	45
2	33
0.85	22
0.425	16
0.25	13
0.15	11
0.075	9



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

[3] If cobbles are present, sampling procedure may not meet ASTM C702 & D75

Specification: _____

Remarks: _____

Reviewed By: C.J. Dixon

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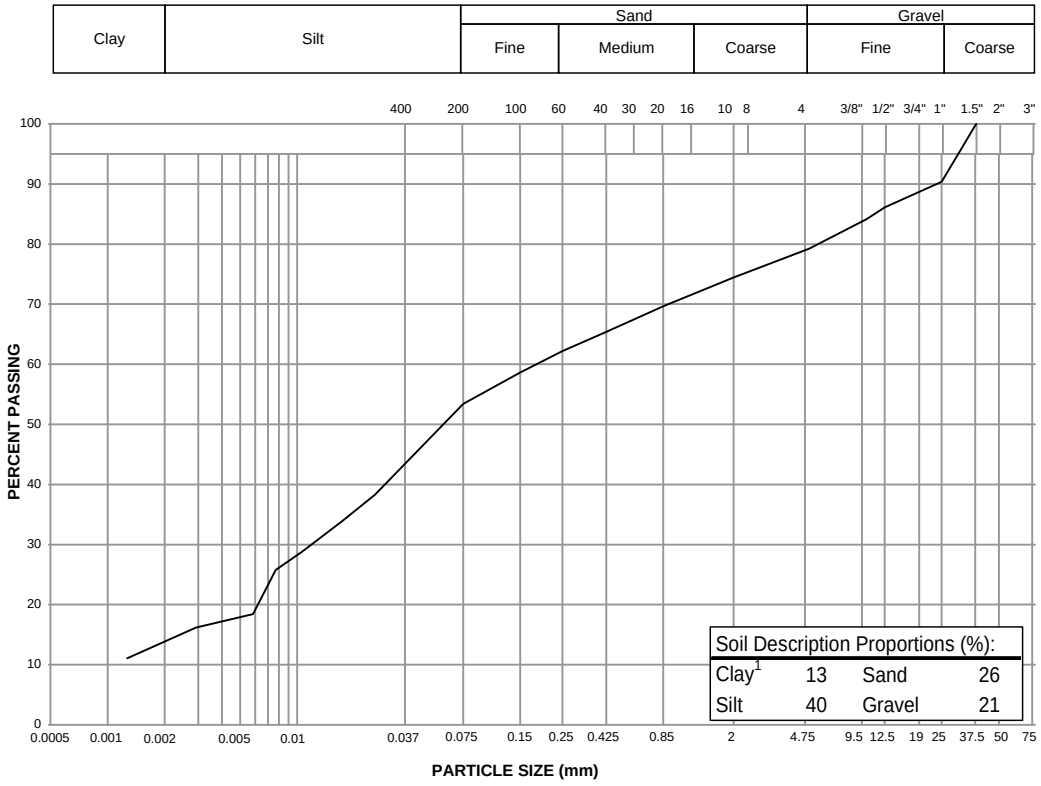
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA08	Soil Description[2]:	SILT - sandy, gravelly, trace clay
Sample Loc.:	BH15		
Sample Depth:	6.3 - 6.4 m	USC Classification:	Cu:
Sampling Method:			Cc:
Date sampled:	Sep-09 By: Client	Moisture Content:	70.2

Particle Size (mm)	Percent Passing
75	
50	
38	100
25	90
19	
12.5	86
10	84
5	79
2	74
0.85	70
0.425	65
0.25	62
0.15	59
0.075	53
0.0256	38.3
0.0172	33.9
0.0105	28.7
0.0077	25.8
0.0058	18.4
0.0029	16.2
0.0013	11.1



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification: _____

Remarks: _____

Reviewed By: C.J. Dixon

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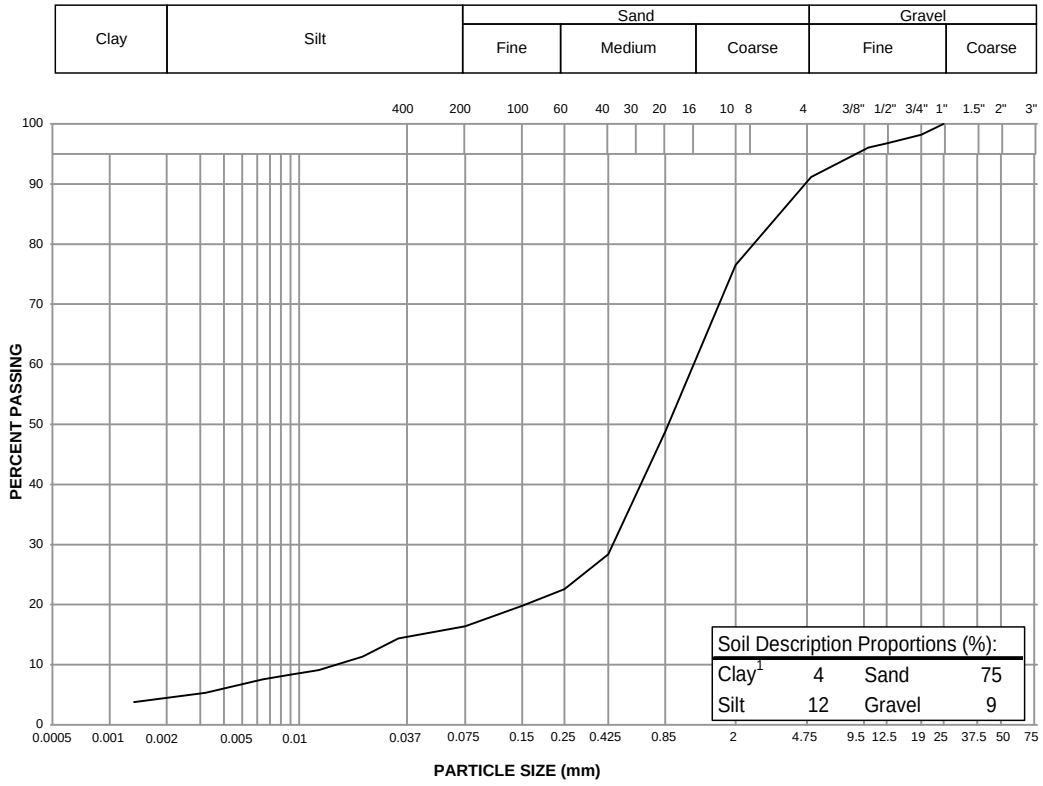
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA23	Soil Description[2]:	SAND - some silt, trace gravel, trace clay
Sample Loc.:	BH15		
Sample Depth:	18.2 - 18.3 M	USC Classification:	Cu: 81.2
Sampling Method:			Cc: 9.9
Date sampled:	Sep-09 By: Client	Moisture Content:	1.3

Particle Size (mm)	Percent Passing
75	
50	
38	
25	100
19	98
12.5	97
10	96
5	91
2	77
0.85	49
0.425	28
0.25	23
0.15	20
0.075	16
0.0333	14.4
0.0215	11.4
0.0127	9.1
0.0090	8.3
0.0064	7.6
0.0032	5.3
0.0013	3.8



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification: _____

Remarks: _____

Reviewed By: C.J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Lower Diversion Stucture	DRILL: Mini-Sonic	W14101178.003-BH16
Keno City, YT		ELEVATION: 895.8m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	MOSS COVER - peat, black				UNFROZEN	
	GRAVEL AND SAND - some silt, well graded, subrounded gravel, medium to coarse sand, compact, moist, brown		SA01			895.0
1	- colour changes to mottled grey around 1.0 m		SA02		FROZEN - visible ice inclusions <5%, poorly bonded, partial thaw during drilling	
			SA03			
	SAND (TILL) - some gravel, some silt, trace clay, medium to coarse sand, well graded, subrounded gravel, grey					894.0
2			SA04			
			SA05	H	Vs, Vr (30%)	893.0
3						
			SA06			892.0
4			SA07			
						891.0
5			SA08			
						890.0
6			SA09			
			SA10			
	ICE - massive ice				MASSIVE ICE	889.0
7						
						888.0
8						
						887.0
9						
						886.0
10						

EBA Engineering Consultants Ltd.

LOGGED BY: JSB	COMPLETION DEPTH: 15.2m
REVIEWED BY:	COMPLETE: 9/7/2009
DRAWING NO:	Page 1 of 2

Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Lower Diversion Stucture	DRILL: Mini-Sonic	W14101178.003-BH16
Keno City, YT		ELEVATION: 895.8m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
10						885.0
11						
	SAND (TILL) - some gravel, some silt, trace clay, medium to coarse sand, well graded, sub rounded gravel, grey				- visible ice inclusions <5%, well bonded	884.0
12						
						883.0
13						
						882.0
14			SA11			
			SA12		UNFROZEN	881.0
15			SA13			
	END OF BOREHOLE 15.2 m					
16						880.0
17						879.0
18						878.0
19						877.0
20						876.0

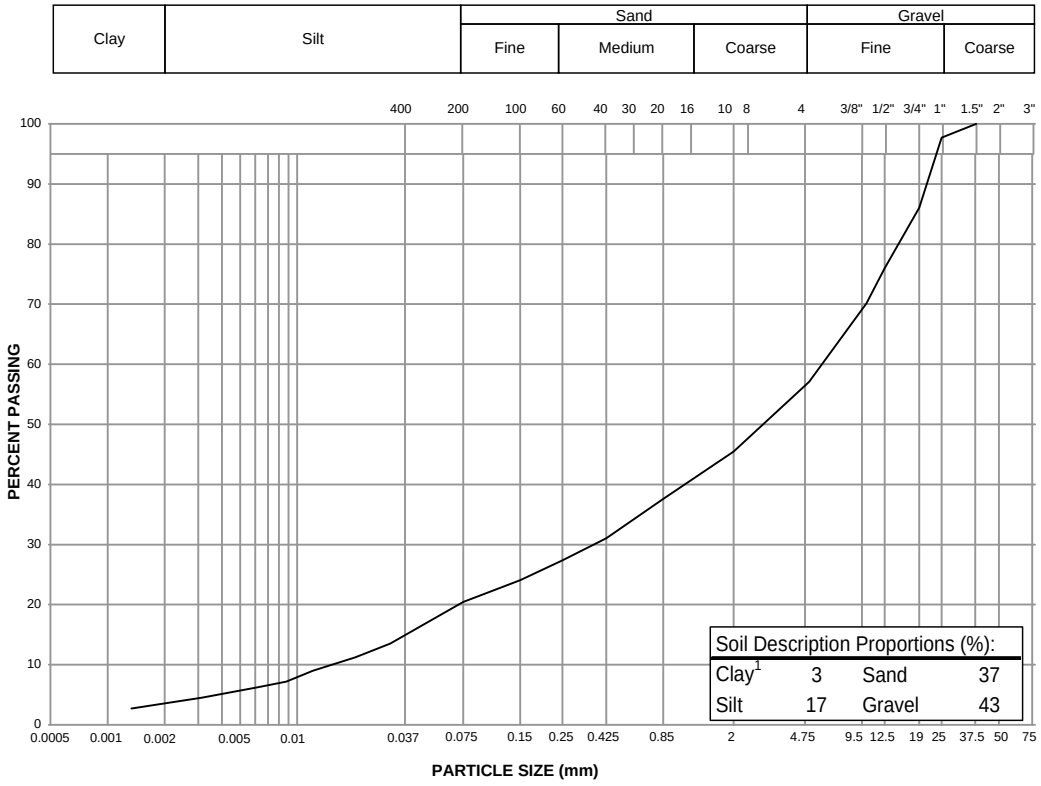
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	REVIEWED BY:	COMPLETE: 9/7/2009
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA02	Soil Description[2]:	GRAVEL AND SAND - some silt, trace clay
Sample Loc.:	BH16		
Sample Depth:	0.2 - 0.4 m	USC Classification:	Cu: 389.9
Sampling Method:			Cc: 1.5
Date sampled:	Sep-09 By: Client	Moisture Content:	10.0

Particle Size (mm)	Percent Passing
75	
50	
38	100
25	98
19	86
12.5	76
10	70
5	57
2	45
0.85	38
0.425	31
0.25	27
0.15	24
0.075	20
0.0310	13.5
0.0203	11.3
0.0121	9.0
0.0088	7.2
0.0063	6.3
0.0031	4.5
0.0013	2.7



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dicken

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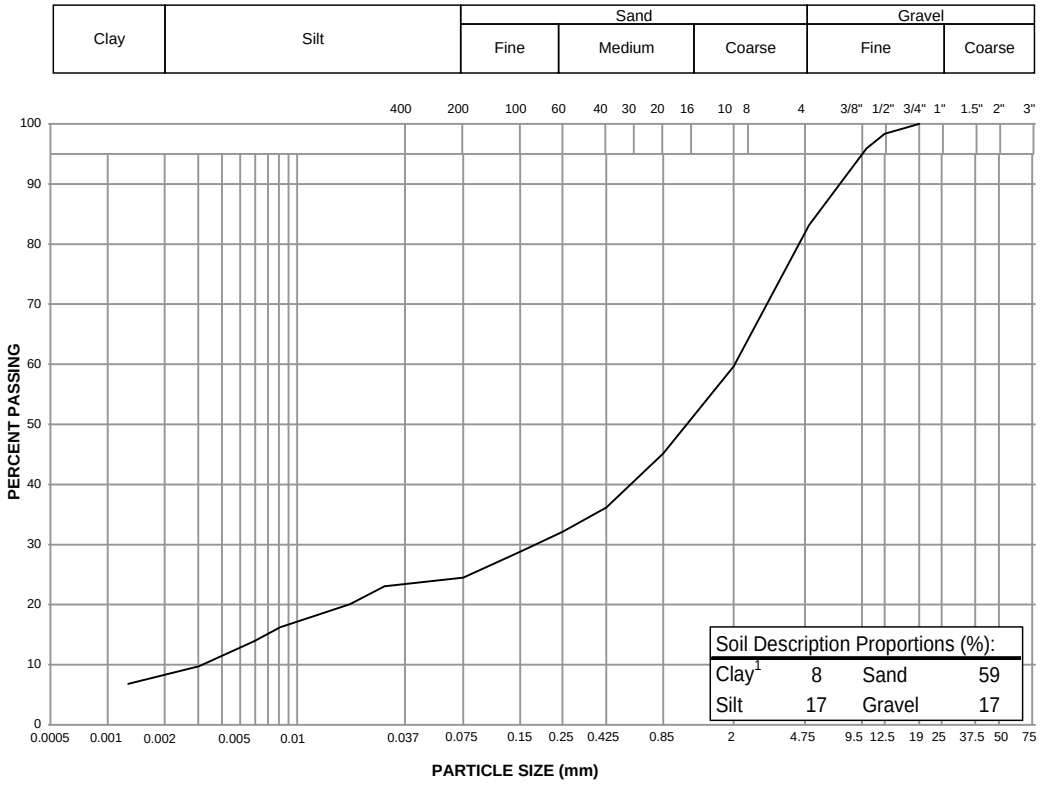
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA05	Soil Description[2]:	SAND - some gravel, some silt, trace clay
Sample Loc.:	BH16		
Sample Depth:	2.7 - 3.0 m	USC Classification:	Cu: 638.2
Sampling Method:			Cc: 5.3
Date sampled:	Sep-09 By: Client	Moisture Content:	37.6

Particle Size (mm)	Percent Passing
75	
50	
38	
25	
19	100
12.5	98
10	96
5	83
2	60
0.85	45
0.425	36
0.25	32
0.15	29
0.075	25
0.0289	23.0
0.0190	20.1
0.0113	17.7
0.0081	16.2
0.0059	13.9
0.0030	9.7
0.0013	6.8



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH17
Keno City, YT		ELEVATION: 899.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	SPT (N)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Monitoring well	Thermistor	Elevation (m)
0	GRAVEL (FILL) - sandy, trace silt, loose, coarse grained, well graded, damp, brown						UNFROZEN			
	PEAT - amorphous granular									
	GRAVEL - sandy, some cobbles, trace silt, compact, coarse grained, well graded, damp, brown, subrounded									
1			SA01	-0.1						899.0
	8/30/2009									8/30/2009
2			SA02	0						898.0
	SILT (TILL) - gravelly, some sand, trace clay, firm, non-plastic, massive, damp, olive grey		SA03							
3				0						897.0
			SA04		19					
			SA05							
4				0						896.0
	- becomes stiff, low plastic		SA06							
	ICE AND SILT - some gravel, some sand, trace clay, low plastic, grey						3318 FROZEN Vs (40%), Vr (15%)			
5			SA07	0						895.0
			SA08							
6			SA09				1643			894.0
	ICE - massive ice						MASSIVE ICE - randomly oriented crystals, trace silt (90% ICE/10% SILT)			
	- no recovery from 6.2 - 7.2 m									
7										893.0
			SA10	-0.1						
8			SA11				2379			892.0
			SA12				14391			
			SA13				19396			
9			SA14							891.0
	- no recovery from 9.2 - 10.1 m									
10										890.0

EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 15.25m
	REVIEWED BY:	COMPLETE: 8/30/2009
	DRAWING NO:	Page 1 of 2

Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH17
Keno City, YT		ELEVATION: 899.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	SPT (N)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Monitoring well	Thermistor	Elevation (m)
10	ICE AND SILT - sandy, some gravel, trace clay, low plastic, massive, grey			-0.1			Vs (25%), Vr (15%)			
	SILT (TILL) - sandy, gravelly, trace clay, non-plastic, massive, grey						Vr (5%)			
11			SA15	-0.1						889.0
			SA16							
12			SA17	-0.1						888.0
			SA18							
13				0						887.0
14				0.1						886.0
	BEDROCK (quartzite)		SA19	0.1						
15										885.0
	END OF BOREHOLE - target depth 15.25 m									
16										884.0
17										883.0
18										882.0
19										881.0
20										880.0

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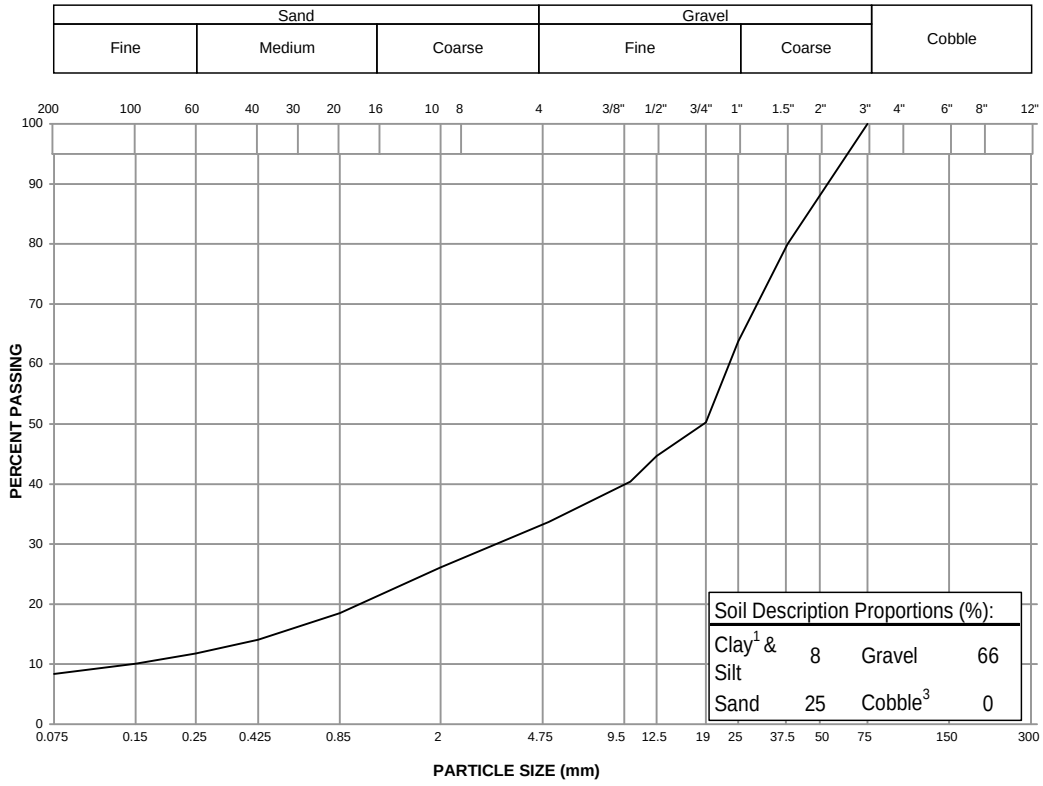
LOGGED BY: CJD	COMPLETION DEPTH: 15.25m
REVIEWED BY:	COMPLETE: 8/30/2009
DRAWING NO:	Page 2 of 2

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA01	Soil Description[2]:	GRAVEL - sandy, trace silt
Sample Loc.:	BH17		
Sample Depth:	0.9 - 1.2 m	USC Classification:	Cu: 158.7
Sampling Method:			Cc: 3.6
Date sampled:	Sep-09 By: Client	Moisture Content:	4.6

Particle Size (mm)	Percent Passing
300	
200	
150	
100	
75	100
50	
38	80
25	64
19	50
12.5	45
10	40
5	34
2	26
0.85	18
0.425	14
0.25	12
0.15	10
0.075	8



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

[3] If cobbles are present, sampling procedure may not meet ASTM C702 & D75

Specification: _____

Remarks: _____

Reviewed By: C.J. Dixon

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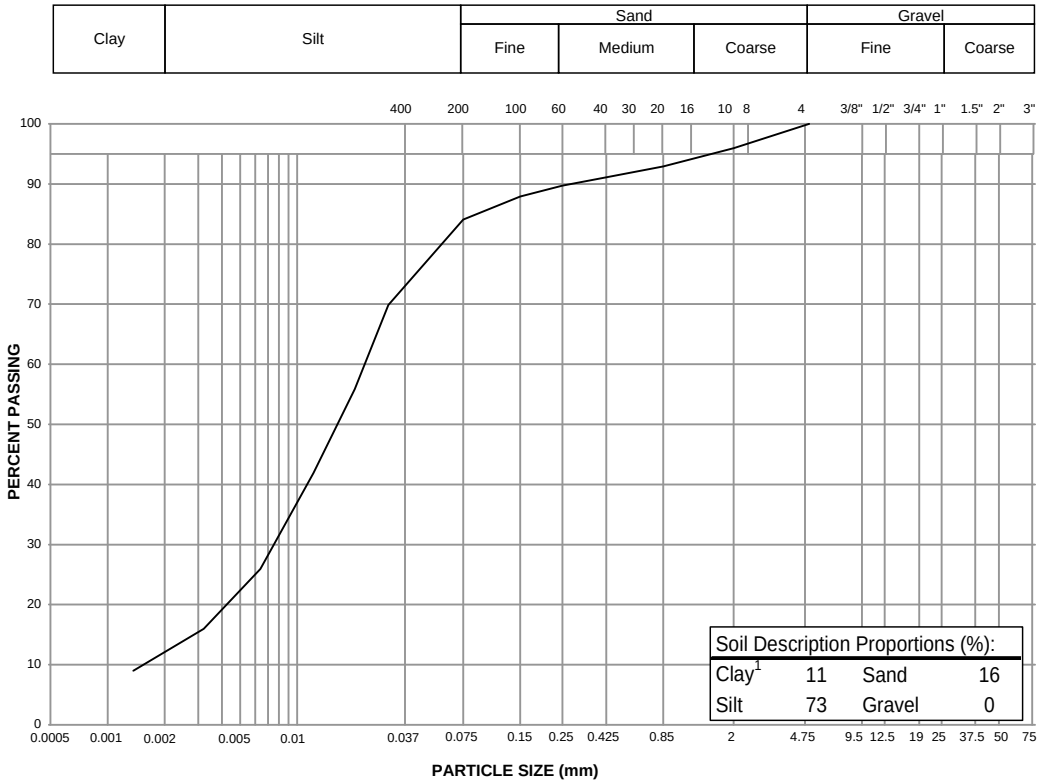
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	2-Nov-2009 By: SMS
Sample No.:	SA08	Soil Description[2]:	SILT - some sand, some clay
Sample Loc.:	BH17		
Sample Depth:	5.4 - 5.5	USC Classification:	Cu: 14.1
Sampling Method:			Cc: 1.5
Date sampled:	Sep-09 By: Client	Moisture Content:	

Particle Size (mm)	Percent Passing
75	
50	
38	
25	
19	
12.5	
10	
5	100
2	96
0.85	93
0.425	91
0.25	90
0.15	88
0.075	84
0.0302	69.8
0.0201	55.9
0.0122	41.9
0.0088	33.9
0.0064	25.9
0.0032	16.0
0.0014	9.0



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Lower Diversion Stucture	DRILL: Mini-Sonic	W14101178.003-BH18
Keno City, YT		ELEVATION: 898.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Thermistor	Elevation (m)
0	MOSS COVER					UNFROZEN		
	GRAVEL - sandy, some silt, well graded, subrounded gravel, medium to coarse sand, compact, brown, damp - cobbles, some boulders throughout gravel layer - becomes trace silt around 0.5 m							
1			SA01	-1.1				898.0
	- becomes very coarse at 1.5 m - colour changes to grey at 1.5 m - becomes silty around 1.5 m - possible boulder around 1.8m - gravel becomes coarser around 1.8 m							
2			SA02	0				897.0
3			SA03	0				896.0
			SA04					
4	SAND AND SILT (TILL) - some gravel, trace clay, well graded, subrounded gravel and sand, grey		SA05	-0.1				895.0
						FROZEN - Nbn, well bonded		
5	- less gravel, become fine to medium grained at 4.8 m		SA06	-0.2		Vs, Vx (15%)		894.0
6			SA07	-0.2				893.0
			SA08		527			
7				-0.2		Vs, 5mm thick		892.0
	ICE - massive ice		SA09		280	MASSIVE ICE		
8			SA10	-0.2	835			891.0
			SA11					
	END OF BOREHOLE 8.5 m - terminated due to schedule							
9								890.0
10								889.0

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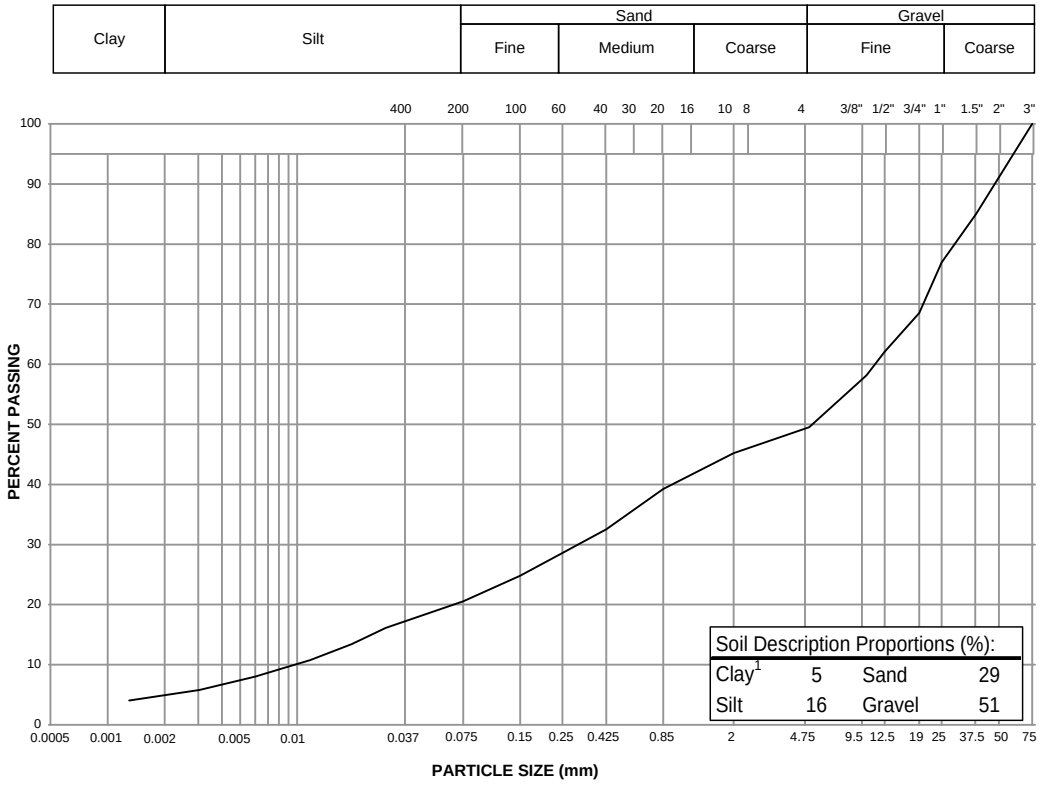
LOGGED BY: JSB	COMPLETION DEPTH: 8.5m
REVIEWED BY:	COMPLETE: 9/2/2009
DRAWING NO:	Page 1 of 1

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA02	Soil Description[2]:	GRAVEL - sandy, some silt, trace clay
Sample Loc.:	BH18		
Sample Depth:	2.2 - 2.4 m	USC Classification:	Cu: 1133.5
Sampling Method:			Cc: 0.9
Date sampled:	Sep-09 By: Client	Moisture Content:	0.0

Particle Size (mm)	Percent Passing
75	100
50	
38	85
25	77
19	69
12.5	62
10	58
5	50
2	45
0.85	39
0.425	33
0.25	29
0.15	25
0.075	21
0.0292	16.1
0.0194	13.4
0.0117	10.7
0.0084	9.4
0.0060	8.1
0.0031	5.8
0.0013	4.0



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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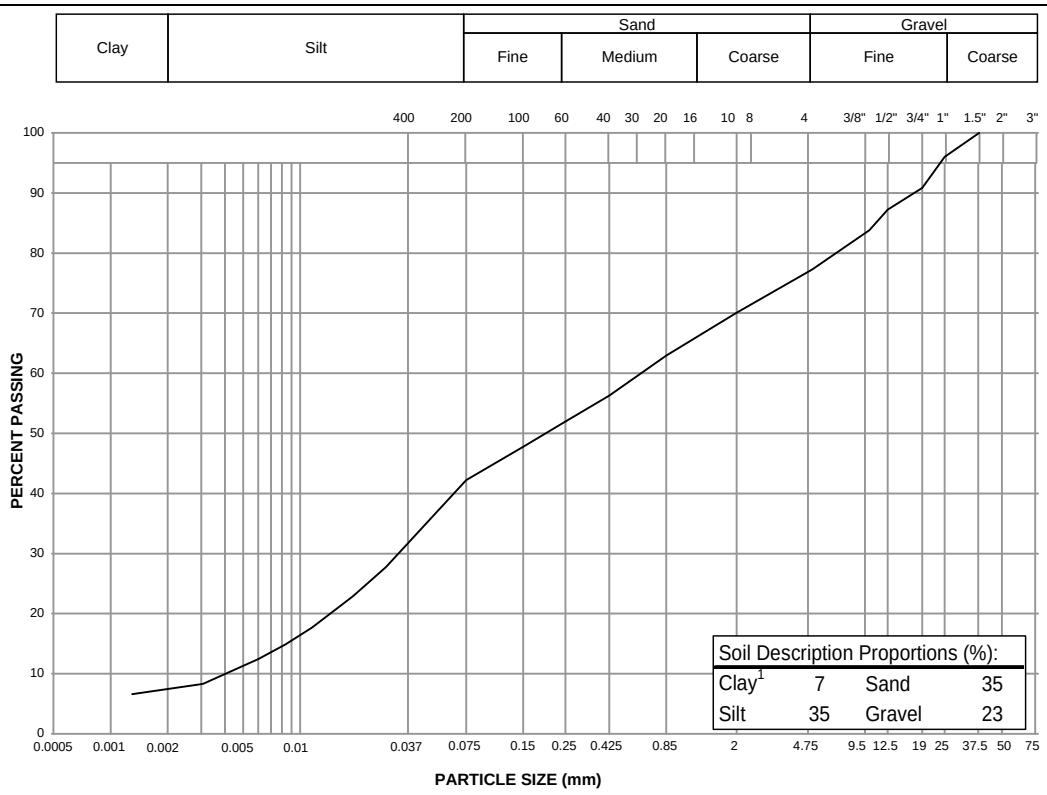
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA06	Soil Description[2]:	SAND AND SILT - some gravel, trace clay
Sample Loc.:	BH18		
Sample Depth:	5.1 - 5.4	USC Classification:	Cu: 155.7
Sampling Method:			Cc: 0.4
Date sampled:	Sep-09 By: Client	Moisture Content:	27.1

Particle Size (mm)	Percent Passing
75	
50	
38	100
25	96
19	91
12.5	87
10	84
5	77
2	70
0.85	63
0.425	56
0.25	52
0.15	48
0.075	42
0.0282	27.7
0.0189	22.9
0.0115	17.7
0.0084	14.9
0.0060	12.5
0.0031	8.3
0.0013	6.6



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH19
Keno City, YT		

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Depth (ft)
0	MOSS COVER - peat, black				UNFROZEN	0
	SILT (TILL) - sandy, some gravel, trace clay, non-plastic, massive grey		SA01		FROZEN Vr (10%)	
1			SA02		Vr (40%)	5
			SA03			
2						
	END OF BOREHOLE 2.4 m (REFUSAL)					
3						10
4						
						15
5						
6						20
7						
						25
8						
9						30
10						33

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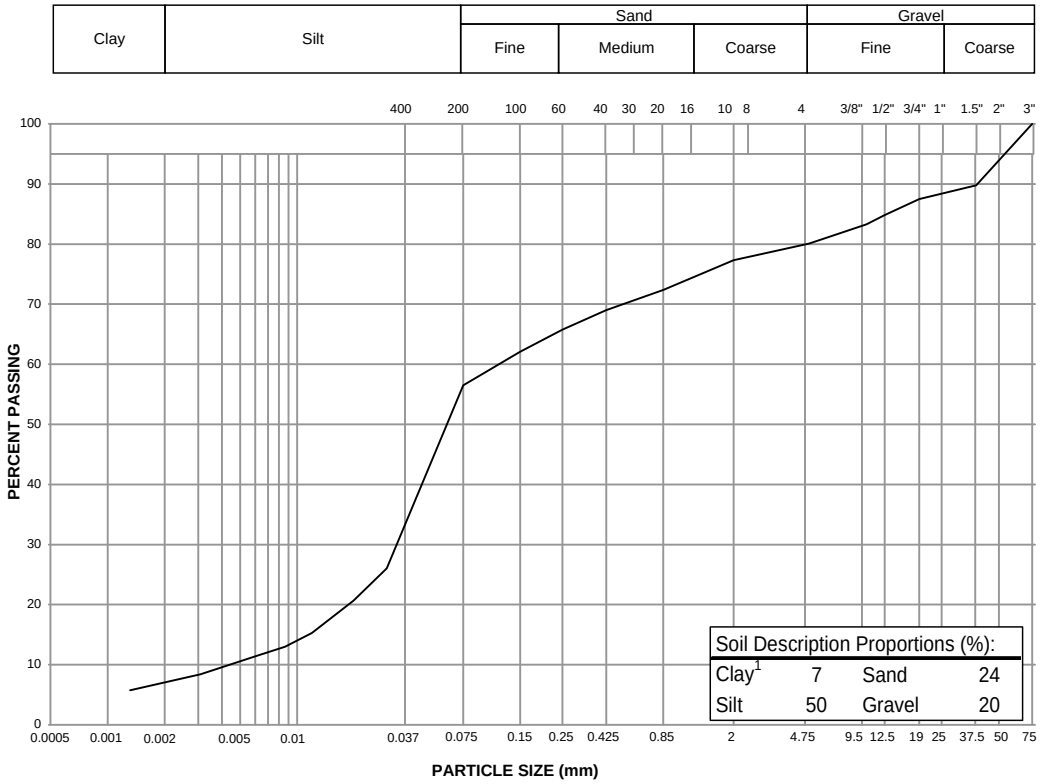
LOGGED BY: JSB	COMPLETION DEPTH: 2.4m
REVIEWED BY:	COMPLETE: 9/2/2009
DRAWING NO:	Page 1 of 1

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA02	Soil Description[2]:	SILT - sandy, some gravel, trace clay
Sample Loc.:	BH19		
Sample Depth:	1.0 - 1.2	USC Classification:	Cu: 26.2
Sampling Method:			Cc: 2.2
Date sampled:	Sep-09 By: Client	Moisture Content:	47.4

Particle Size (mm)	Percent Passing
75	100
50	
38	90
25	
19	87
12.5	85
10	83
5	80
2	77
0.85	72
0.425	69
0.25	66
0.15	62
0.075	57
0.0297	26.0
0.0198	20.7
0.0119	15.3
0.0086	13.0
0.0061	11.5
0.0031	8.4
0.0013	5.7



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH20
Keno City, YT		

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Depth (ft)
0	GRAVEL - sandy, trace silt, well graded, sand and gravel angular to subangular, compact, damp, brown		SA01		UNFROZEN	0
1	- gravel content increases from 0.5 to 1.2 m - becomes moist around 0.8 m - shale particles below 1.2 m to 1.7 m		SA02			5
2	SILT (TILL) - sandy, some gravel, trace clay, well graded sand, fine to medium grained, subrounded gravel, stiff, moist, grey		SA03 SA04			
3	END OF BOREHOLE 2.4 m - hard drilling at 2.4 m, possible boulder or bedrock					10
4						
5						15
6						20
7						
8						25
9						30
10						33

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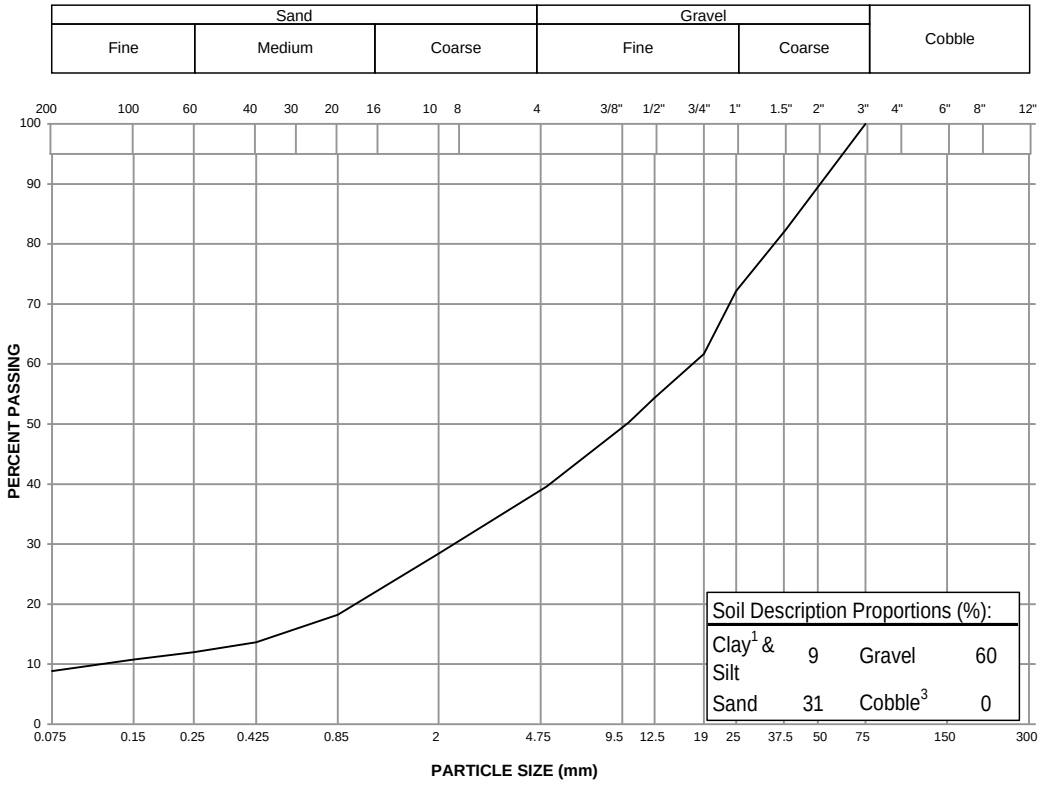
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REVIEWED BY:	COMPLETE: 9/1/2009
DRAWING NO:	Page 1 of 1

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA01	Soil Description[2]:	GRAVEL - sandy, trace silt
Sample Loc.:	BH20		
Sample Depth:	0.3 - 0.5 m	USC Classification:	Cu: 145.6
Sampling Method:			Cc: 2.8
Date sampled:	Sep-09 By: Client	Moisture Content:	5.7

Particle Size (mm)	Percent Passing
300	
200	
150	
100	
75	100
50	
38	82
25	72
19	62
12.5	54
10	50
5	40
2	28
0.85	18
0.425	14
0.25	12
0.15	11
0.075	9



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

[3] If cobbles are present, sampling procedure may not meet ASTM C702 & D75

Specification: _____

Remarks: _____

Reviewed By: C.J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH21
Keno City, YT		

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Depth (ft)
0	SILT - sandy, some gravel, trace clay, stiff, fine grained, gap graded, damp, light brown, organic inclusions, subrounded to subangular		SA01		UNFROZEN	0
	GRAVEL - sandy, trace silt, coarse grained, well graded, damp, brown, subrounded to subangular					
1			SA02			5
2	- cobbles and boulders from 2.0 to 3.0 m					
3	SAND AND GRAVEL (TILL) - silty, compact, damp, brown					10
	NOTE: Very slow drilling, bit replaced, still very slow. 1.5 hrs to retrieve bit, skid steer, also back on site					
4	END OF BOREHOLE 4.2 m - very slow drilling					15
5						
6						20
7						25
8						
9						30
10						33

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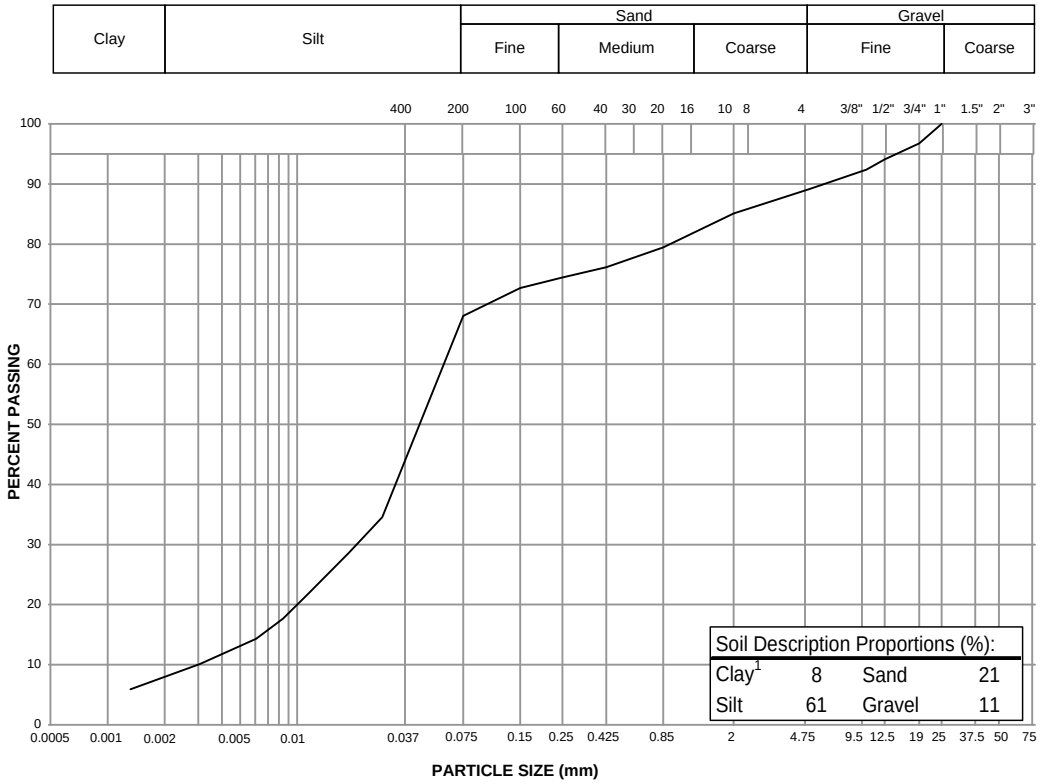
LOGGED BY: CJD	COMPLETION DEPTH: 4.2m
REVIEWED BY:	COMPLETE: 9/1/2009
DRAWING NO:	Page 1 of 1

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	22-Oct-2009 By: SMS
Sample No.:	SA01	Soil Description[2]:	SILT - sandy, some gravel, trace clay
Sample Loc.:	BH21		
Sample Depth:	0.2 - 0.4 m	USC Classification:	Cu: 21.1
Sampling Method:			Cc: 2.3
Date sampled:	Sep-09 By: Client	Moisture Content:	17.9

Particle Size (mm)	Percent Passing
75	
50	
38	
25	100
19	97
12.5	94
10	92
5	89
2	85
0.85	79
0.425	76
0.25	74
0.15	73
0.075	68
0.0281	34.5
0.0188	28.6
0.0115	21.9
0.0084	17.7
0.0061	14.3
0.0031	10.1
0.0013	5.9



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification: _____

Remarks: _____

Reviewed By: C. J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH22
Keno City, YT		

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Depth (ft)
0	MOSS COVERED - peat, black				UNFROZEN	0
	SILT -sandy, trace clay, brownish black		SA01	286	FROZEN - Nbe (25%), well bonded	
1			SA02		- visible ice inclusions, < 5 %	
	SAND (TILL) - gravelly, silty, compact (est.), well graded, brown frozen		SA03		- visible ice inclusions 50%, well bonded - visible ice inclusions 50%, poorly bonded	5
2	- very hard slow drilling 2.4 m					
	END OF BOREHOLE 2.4 m					
3						10
4						
						15
5						
6						20
7						
						25
8						
9						30
10						33

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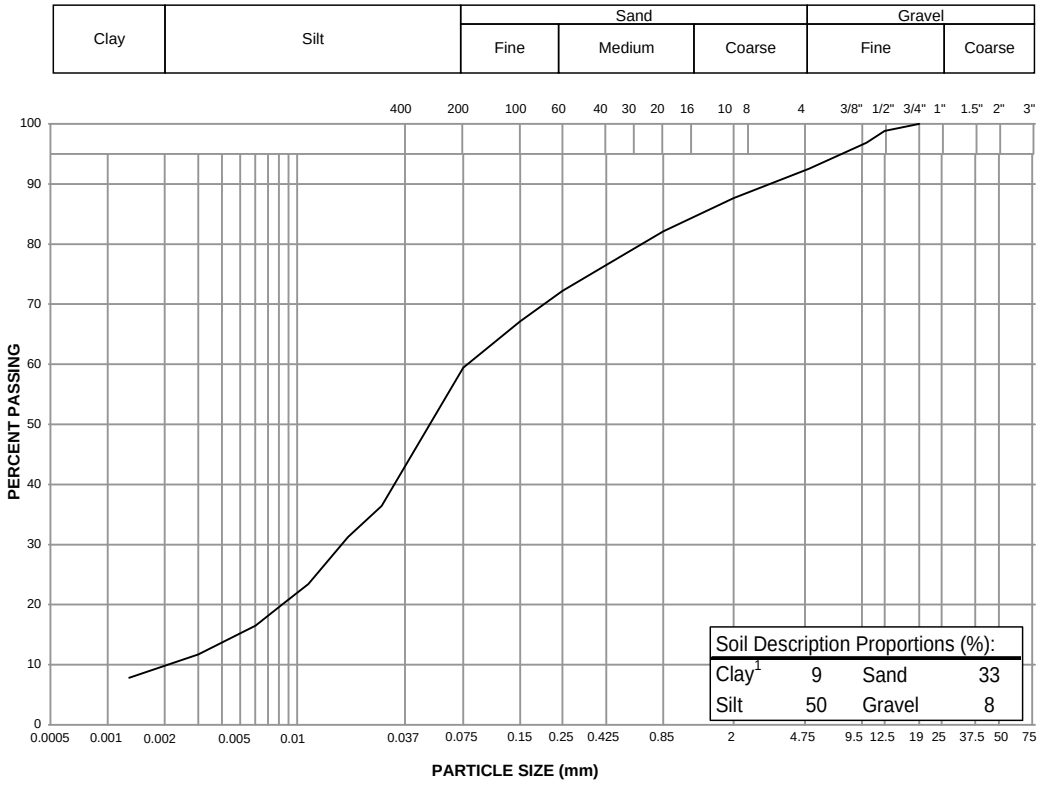
LOGGED BY: CJD	COMPLETION DEPTH: 2.4m
REVIEWED BY:	COMPLETE: 9/1/2009
DRAWING NO:	Page 1 of 1

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	23-Oct-2009 By: SMS
Sample No.:	SA03	Soil Description[2]:	SILT - sandy, trace clay, trace gravel
Sample Loc.:	BH22		
Sample Depth:	1.3 - 1.5 m	USC Classification:	Cu: 35.7
Sampling Method:			Cc: 1.7
Date sampled:	Sep-09 By: Client	Moisture Content:	71.5

Particle Size (mm)	Percent Passing
75	
50	
38	
25	
19	100
12.5	99
10	97
5	93
2	88
0.85	82
0.425	77
0.25	72
0.15	67
0.075	59
0.0278	36.4
0.0185	31.2
0.0114	23.4
0.0083	20.0
0.0060	16.5
0.0030	11.7
0.0013	7.8



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH23
Keno City, YT		ELEVATION: 908.2m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	GROUND ICE DESCRIPTION	Thermistor	Elevation (m)
0	PEAT - amorphous, granular, moist to wet		SA01	-3.4	UNFROZEN		908.0
	SILT AND SAND (TILL) - trace gravel , trace clay, low plastic, olive grey		SA02		FROZEN - Vr (20%)		
1				-0.2			907.0
			SA03		Vr (10%)		
2					Vr (15%)		906.0
			SA04	-0.4			
			SA05		Vr (35%)		
3	SAND - silty, trace gravel, trace clay, well graded, brown				Vc (10%)		905.0
					Vr (10%), becomes Vs		
			SA06	-0.4			
4			SA07				904.0
				-0.4			
			SA08				
5			SA09				903.0
	SILT AND SAND (TILL) - trace clay, low plastic, olive grey				Vs 10%		
				-0.4			
6			SA10				902.0
			SA11	-0.4			
7			SA12				901.0
			SA13	-0.4			
	GRAVEL - silty, some cobbles, some sand, well graded, greyish brown						
8	SILT (TILL) - sandy, gravelly, trace clay, non plastic, damp, olive grey (not frozen in core)		SA14				900.0
				-0.3			
9			SA15				899.0
	GRAVEL - some sand, trace silt, compact (est.), well graded, coarse grained, damp, brown		SA16	-0.3			
	SILT (TILL) - gravelly, sandy, trace clay, stiff, low to non-plastic, massive, damp, olive grey						
10							

STANDARD PENETRATION (N) 20 40 60 80

POCKET PEN. (kPa) 100 200 300 400

PLASTIC M.C. LIQUID 20 40 60 80

130

Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Dry Stack Tailings Facility	DRILL: Mini-Sonic	W14101178.003-BH23
Keno City, YT		ELEVATION: 908.2m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

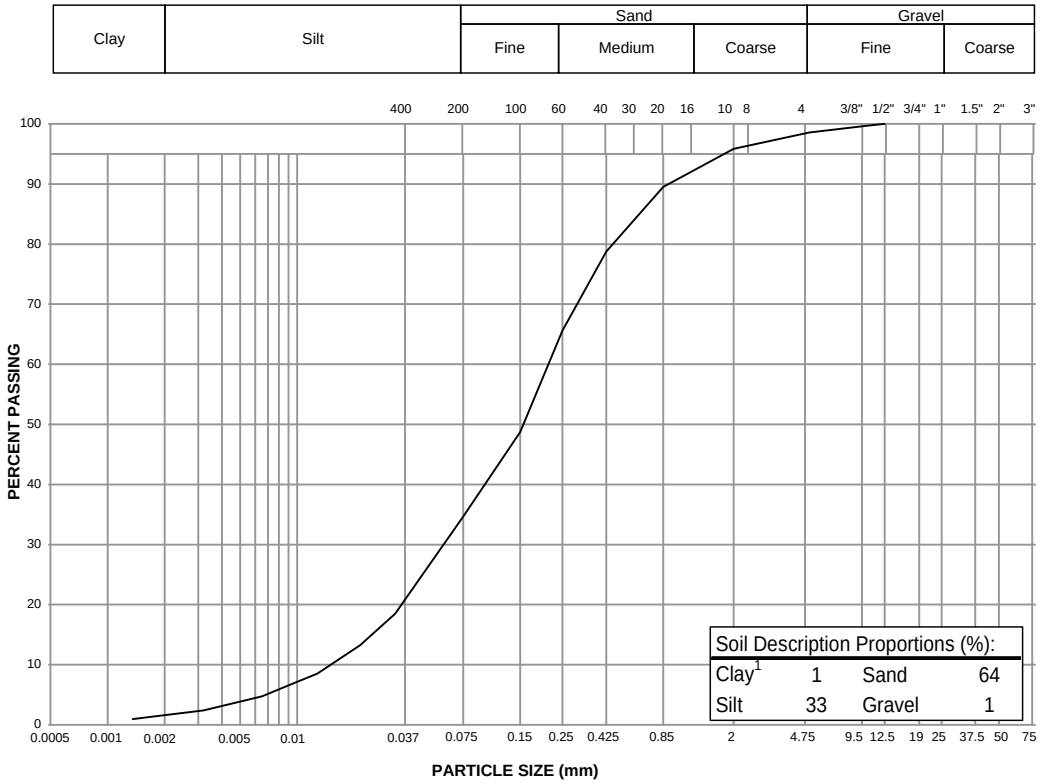
Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Thermistor	Elevation (m)
10	GRAVEL - silty, sandy, some cobbles, dense (est.), well graded, coarse grained, damp, brownish grey		SA17					898.0
	END OF BOREHOLE - refusal in cobbly soil							
11								897.0
12								896.0
13								895.0
14								894.0
15								893.0
16								892.0
17								891.0
18								890.0
19								889.0
20								

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	23-Oct-2009 By: SMS
Sample No.:	SA07	Soil Description[2]:	SAND - silty, trace clay, trace gravel
Sample Loc.:	BH23		
Sample Depth:	4.0 - 4.15 m	USC Classification:	Cu: 14.1
Sampling Method:			Cc: 1.2
Date sampled:	Sep-09 By: Client	Moisture Content:	22.6

Particle Size (mm)	Percent Passing
75	
50	
38	
25	
19	
12.5	100
10	100
5	99
2	96
0.85	90
0.425	79
0.25	66
0.15	49
0.075	35
0.0328	18.5
0.0215	13.3
0.0127	8.5
0.0091	6.6
0.0065	4.7
0.0032	2.4
0.0014	0.9



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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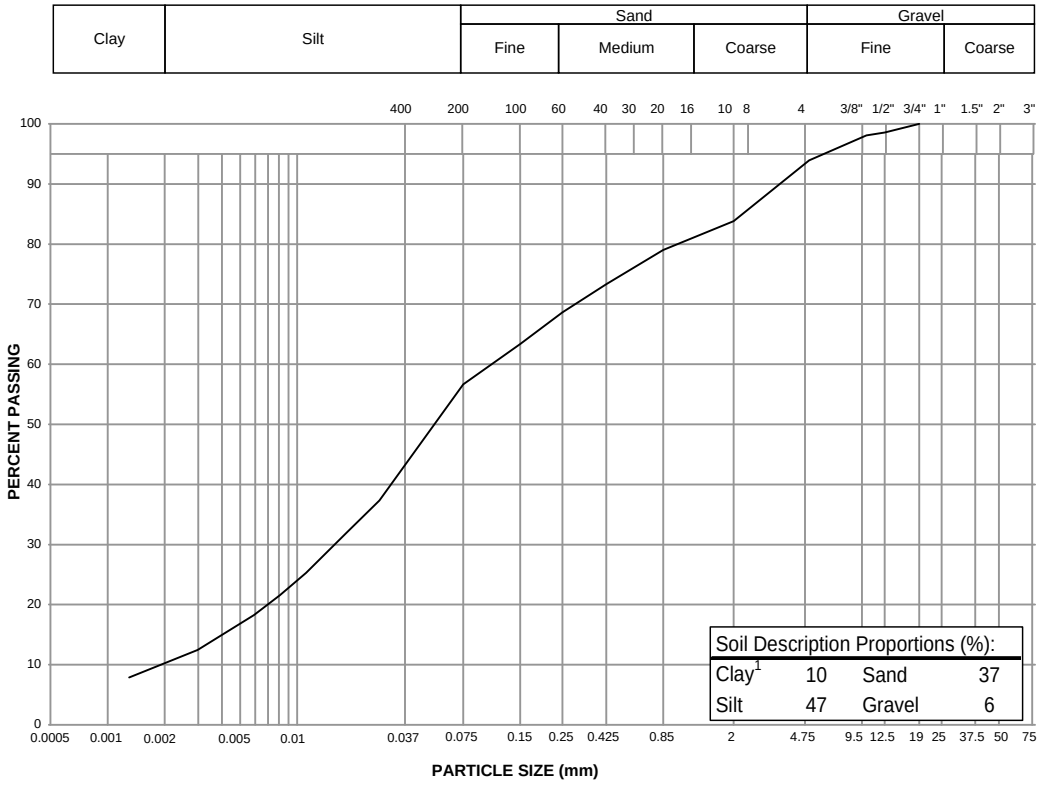
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	23-Oct-2009 By: SMS
Sample No.:	SA11	Soil Description[2]:	SILT AND SAND - trace clay, trace gravel
Sample Loc.:	BH23		
Sample Depth:	6.4 - 6.55	USC Classification:	Cu: 54.1
Sampling Method:			Cc: 1.1
Date sampled:	Sep-09 By: Client	Moisture Content:	17.1

Particle Size (mm)	Percent Passing
75	
50	
38	
25	
19	100
12.5	99
10	98
5	94
2	84
0.85	79
0.425	73
0.25	69
0.15	63
0.075	57
0.0270	37.3
0.0181	31.9
0.0111	25.3
0.0081	21.6
0.0059	18.3
0.0030	12.4
0.0013	7.9



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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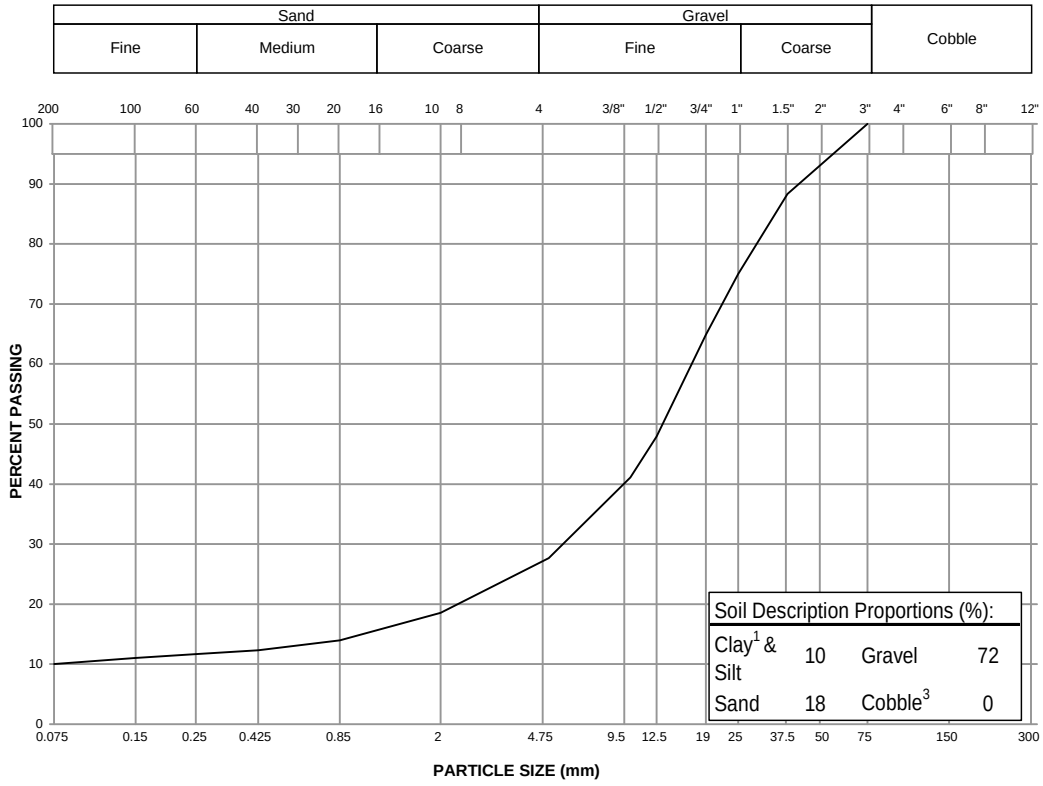
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PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	23-Oct-2009 By: SMS
Sample No.:	SA16	Soil Description[2]:	GRAVEL - some sand, trace silt
Sample Loc.:	BH23		
Sample Depth:	9.3 - 9.5 m	USC Classification:	Cu: 229.0
Sampling Method:			Cc: 26.9
Date sampled:	Sep-09 By: Client	Moisture Content:	4.0

Particle Size (mm)	Percent Passing
300	
200	
150	
100	
75	100
50	
38	88
25	75
19	65
12.5	48
10	41
5	28
2	19
0.85	14
0.425	12
0.25	12
0.15	11
0.075	10



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

[3] If cobbles are present, sampling procedure may not meet ASTM C702 & D75

Specification: _____

Remarks: _____

Reviewed By: C.J. Dicks

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Water Retention Pond	DRILL: Mini-Sonic	W14101178.003-BH24
Keno City, YT		ELEVATION: 894.1m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	STANDARD PENETRATION (N) 20 40 60 80; POCKET PEN. (kPa) 100 200 300 400; PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Monitoring well	Elevation (m)
0	SILT (FILL) - gravelly, sandy, non-plastic, damp, dark brown, organic inclusions		SA01					894.0
1	GRAVEL (FILL) - sandy, some silt, loose to compact (est.), fine grained, well graded, damp, light brown to grey, subangular		SA02					893.0
2	- no recovery from 1.7 - 2.8 m							892.0
3	SILT (TILL) - gravelly, some sandy, trace clay, very stiff, low to non-plastic, massive, damp to moist, olive grey, gravel particles, subangular			36				891.0
4								890.0
5								889.0
6			SA03					888.0
	SAND - fine sand lens		SA04	48				
7	BOULDER AND SILT TILL (as above) - no recovery from 6.6 - 6.9 m		SA05					887.0
	GRAVEL - sandy, some silt, compact, fine grained, well graded, damp to moist, greyish brown, oxide staining							
8			SA06					886.0
	SILT (TILL) - sandy, gravelly, some cobbles, trace clay, stiff (est.), non-plastic, massive, damp, olive grey							
9			SA07					885.0
	END OF BOREHOLE 9.15 m - target depth							
10								

EBA Engineering Consultants Ltd.

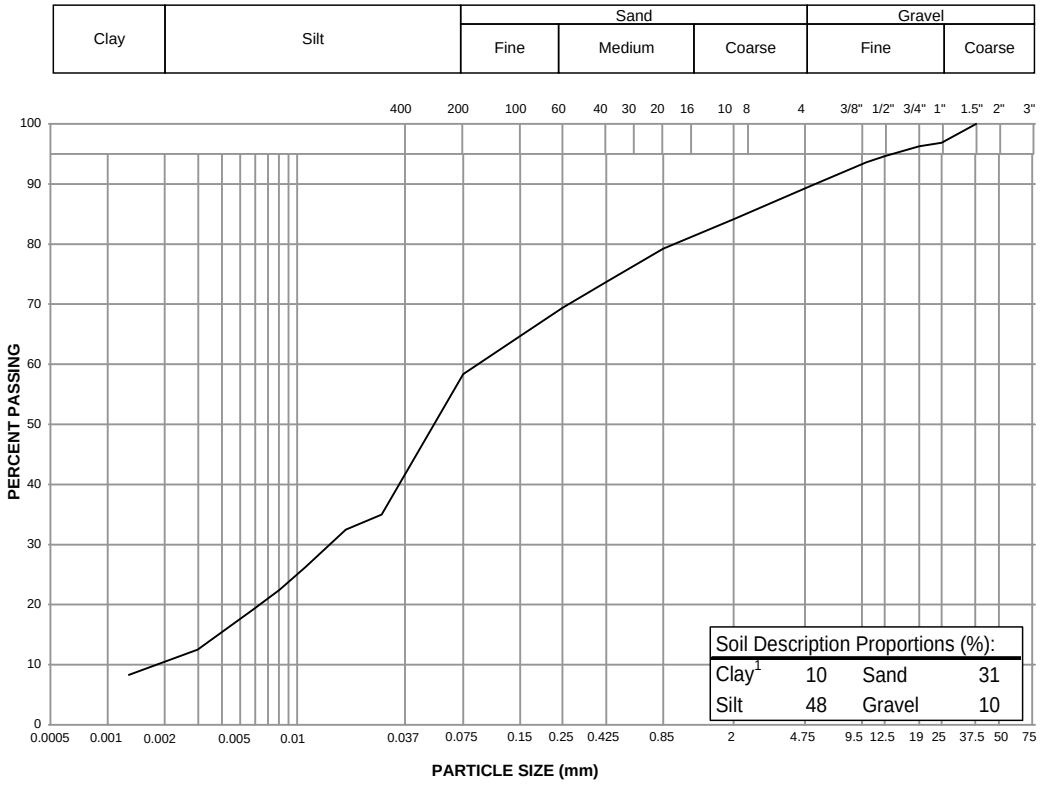
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REVIEWED BY:	COMPLETE: 8/29/2009
DRAWING NO:	Page 1 of 1

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	23-Oct-2009 By: SMS
Sample No.:	SA03	Soil Description[2]:	SILT - sandy, trace clay, trace gravel
Sample Loc.:	BH24		
Sample Depth:	5.4 - 5.6 m	USC Classification:	Cu: 47.9
Sampling Method:			Cc: 1.3
Date sampled:	Sep-09 By: Client	Moisture Content:	10.5

Particle Size (mm)	Percent Passing
75	
50	
38	100
25	97
19	96
12.5	95
10	94
5	90
2	84
0.85	79
0.425	74
0.25	69
0.15	65
0.075	58
0.0278	35.0
0.0180	32.5
0.0111	26.2
0.0081	22.5
0.0059	19.2
0.0030	12.5
0.0013	8.3



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Water Retention Pond	DRILL: Mini-Sonic	W14101178.003-BH25
Keno City, YT		ELEVATION: 894.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL (FILL) - silty, some sand, loose, gap graded, damp, brown/green, organic inclusions		SA01				
1							894.0
	GRAVEL (glaciofluvial) - sandy, some silt, compact, medium grained, well graded, damp, brown, subrounded to subangular						
2			SA02				893.0
	SAND AND GRAVEL (glaciofluvial) - trace silt, compact, medium grained, well graded, damp, brown, rounded to sub rounded						
3			SA03				892.0
				21			
			SA04				
4	- no recovery from 7.4 - 6.3 m						891.0
	GRAVEL - sandy, some cobbles, trace silt, dense, coarse grained, well graded, moist, brown, subangular to subrounded						
5							890.0
6	- SPT on boulder						889.0
7			SA05				888.0
	SILT (TILL) - gravelly, some sand, trace clay, very stiff to hard, low-non plastic, massive, moist, olive grey						
8			SA06				887.0
9			SA07				886.0
				28			
10							885.0

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 15.25m
REVIEWED BY:	COMPLETE: 8/28/2009
DRAWING NO:	Page 1 of 2

Flame & Moth DSTF Drilling	CLIENT: Alexco Resources	PROJECT NO. - BOREHOLE NO.
Water Retention Pond	DRILL: Mini-Sonic	W14101178.003-BH25
Keno City, YT		ELEVATION: 894.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
10			SA08				
	SILT (TILL) - gravelly, some sand, trace clay, stiff to hard, massive, damp grey						
11	GRAVEL - cobbly, sandy, trace silt, compact, coarse grained, gap graded, damp, rust to grey, oxidation						884.0
			SA09				
12			SA10				883.0
	- no recovery from 12.5 - 15.0 m			39			
13							882.0
14							881.0
15	- boulder of possible bedrock						880.0
	END OF BOREHOLE 15.25 m - target depth						
16							879.0
17							878.0
18							877.0
19							876.0
20							875.0

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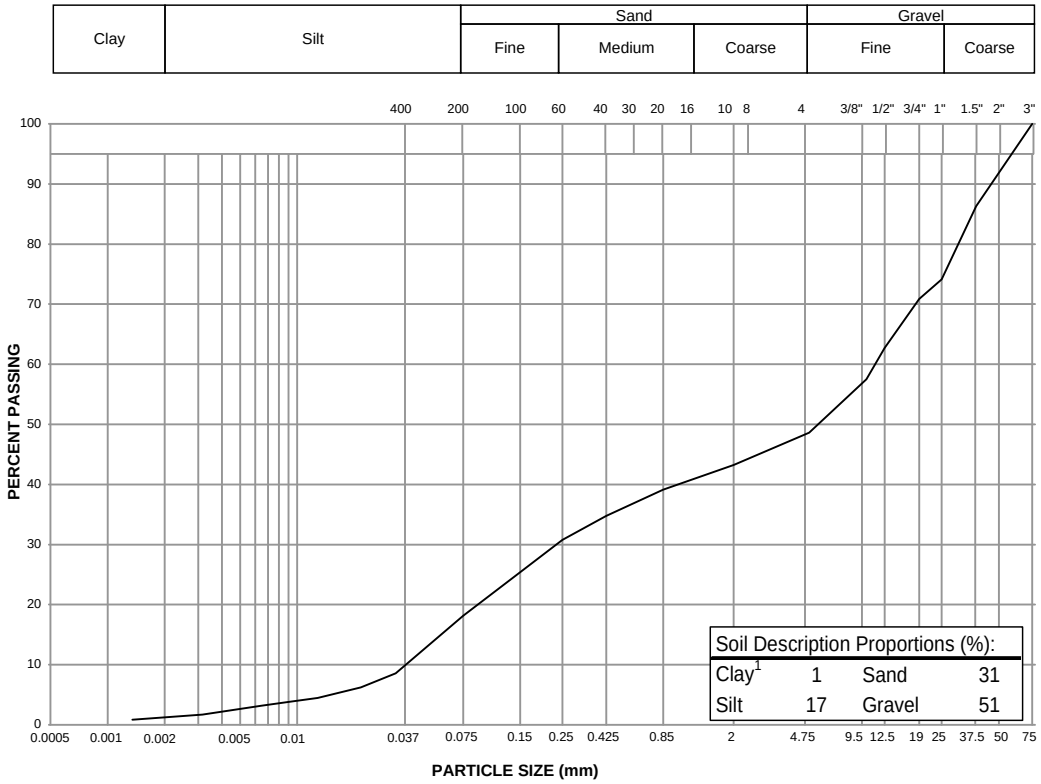
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REVIEWED BY:	COMPLETE: 8/28/2009
DRAWING NO:	Page 2 of 2

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	25-Oct-2009 By: SMS
Sample No.:	SA02	Soil Description[2]:	GRAVEL - sandy, some silt, trace clay
Sample Loc.:	BH25		
Sample Depth:	1.8 - 2.1 m	USC Classification:	Cu: 284.4
Sampling Method:			Cc: 0.1
Date sampled:	Sep-09 By: Client	Moisture Content:	3.6

Particle Size (mm)	Percent Passing
75	100
50	
38	86
25	74
19	71
12.5	63
10	58
5	49
2	43
0.85	39
0.425	35
0.25	31
0.15	25
0.075	18
0.0331	8.6
0.0216	6.2
0.0128	4.5
0.0091	3.9
0.0065	3.2
0.0032	1.7
0.0014	0.9



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dicken

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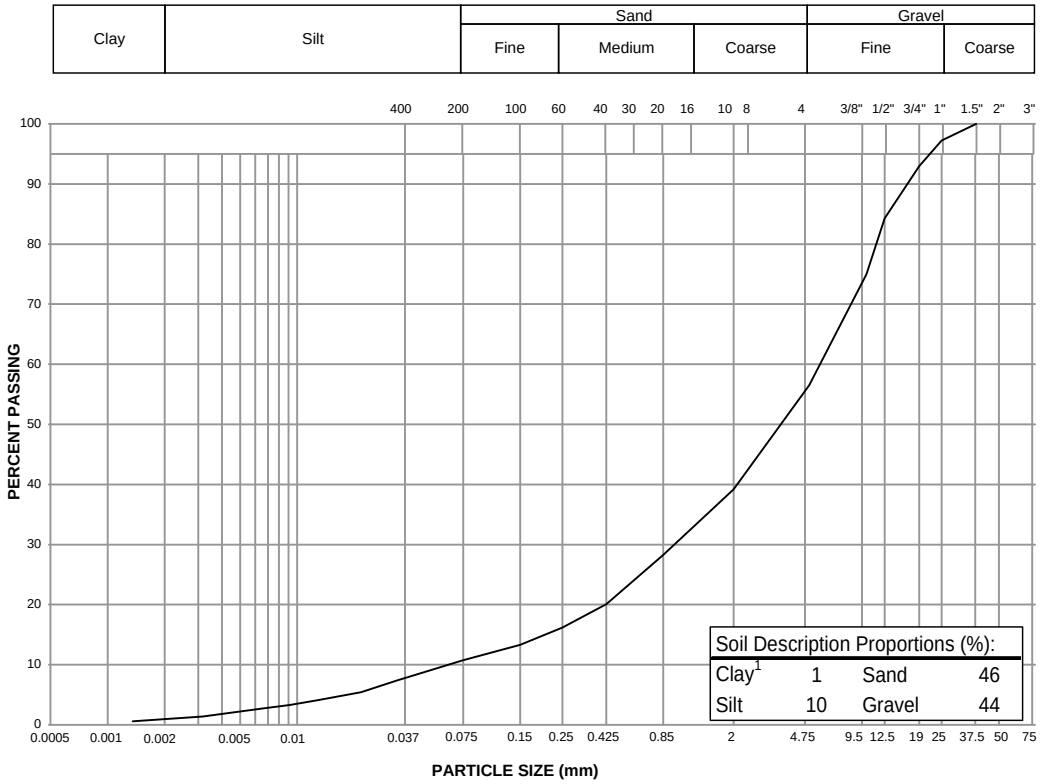
EBA Engineering Consultants Ltd. eba

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	25-Oct-2009 By: SMS
Sample No.:	SA04	Soil Description[2]:	SAND AND GRAVEL - trace silt, trace clay
Sample Loc.:	BH25		
Sample Depth:	3.3 - 3.7	USC Classification:	Cu: 90.3
Sampling Method:			Cc: 2.7
Date sampled:	Sep-09 By: Client	Moisture Content:	2.5

Particle Size (mm)	Percent Passing
75	
50	
38	100
25	97
19	93
12.5	84
10	75
5	57
2	39
0.85	28
0.425	20
0.25	16
0.15	13
0.075	11
0.0333	7.4
0.0217	5.4
0.0128	4.1
0.0091	3.3
0.0065	2.7
0.0032	1.4
0.0014	0.6



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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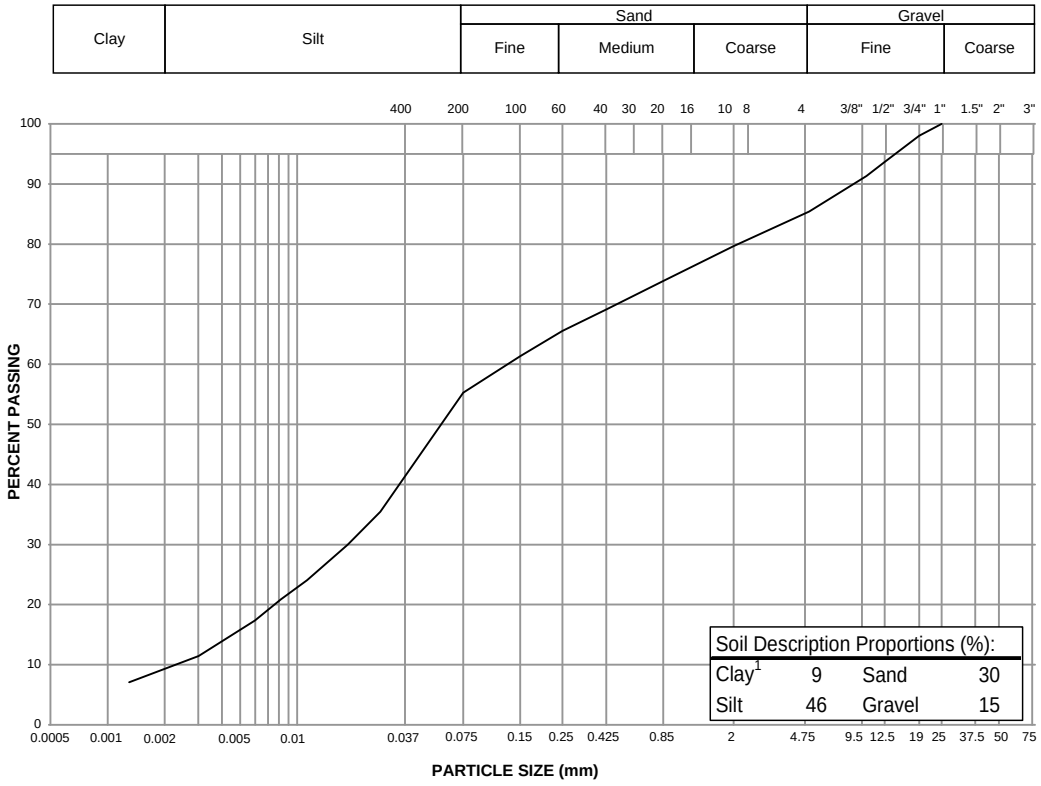
EBA Engineering Consultants Ltd.

PARTICLE SIZE ANALYSIS TEST REPORT

ASTM D422 & C136

Project:	Flame & Moth DSTF Drilling	Client:	Alexco Resource Corp
Project No.:	W14101178.003	Client Rep.:	
Site:	Keno City, YT		
Material Type:		Date Tested:	25-Oct-2009 By: SMS
Sample No.:	SA07	Soil Description[2]:	SILT - sandy, some gravel, trace clay
Sample Loc.:	BH25		
Sample Depth:	8.7 - 8.95 m	USC Classification:	Cu: 54.4
Sampling Method:			Cc: 1.0
Date sampled:	Sep-09 By: Client	Moisture Content:	9.7

Particle Size (mm)	Percent Passing
75	
50	
38	
25	100
19	98
12.5	94
10	91
5	85
2	80
0.85	74
0.425	69
0.25	66
0.15	61
0.075	55
0.0274	35.5
0.0184	30.0
0.0113	24.1
0.0082	20.9
0.0060	17.3
0.0030	11.4
0.0013	7.1



Notes:

[1] The upper clay size of 2 um, per the Canadian Foundation Engineering Manual

[2] The description is visually based & subject to EBA description protocols

Specification:

Remarks:

Reviewed By: C.J. Dixon

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Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
DSTF	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP01
near Keno City, YT	7086907N; 483901E; Zone 8	ELEVATION: 906.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - woody, some silt, roots, organics				Frozen	
	GRAVEL (FILL) - sandy - some silt, compact (est.), medium grained, well graded, frozen, sub-rounded, brown				Nbe	906.0
			SA01	●		
1					Unfrozen	
	GRAVEL - sandy, some cobbles, trace silt, compact (est.), coarse grained, well graded, damp, brown, sub-rounded					905.0
2			SA02	●		904.0
	- becomes loose					
3						903.0
	SILT - sandy, some gravel, some clay, stiff, low plastic, massive, damp, olive grey					
4			SA03	●H▲		902.0
5	EOH - refusal, possible bedrock (quartzite)					901.0
6						

EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 5m
	REVIEWED BY: JRT	COMPLETE: 5/6/2009
	DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
DSTF	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP02
near Keno City, YT	7086862N; 483957E; Zone 8	ELEVATION: 908.3m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - silty, woody, fibrous, roots, organics					Frozen	
	SAND - silty, some gravel, trace clay, loose (est.), low plastic, massive, frozen, organic inclusions					Vr, Vs (35%) ice lens up to 10cm thick	908.0
1			SA01		141		907.0
	-becomes some clay		SA02	-0.6		Vx (5%)	
2						Vx, Vs (10%)	906.0
			SA03				
3	EOH - target depth						905.0
4							904.0
5							903.0
6							

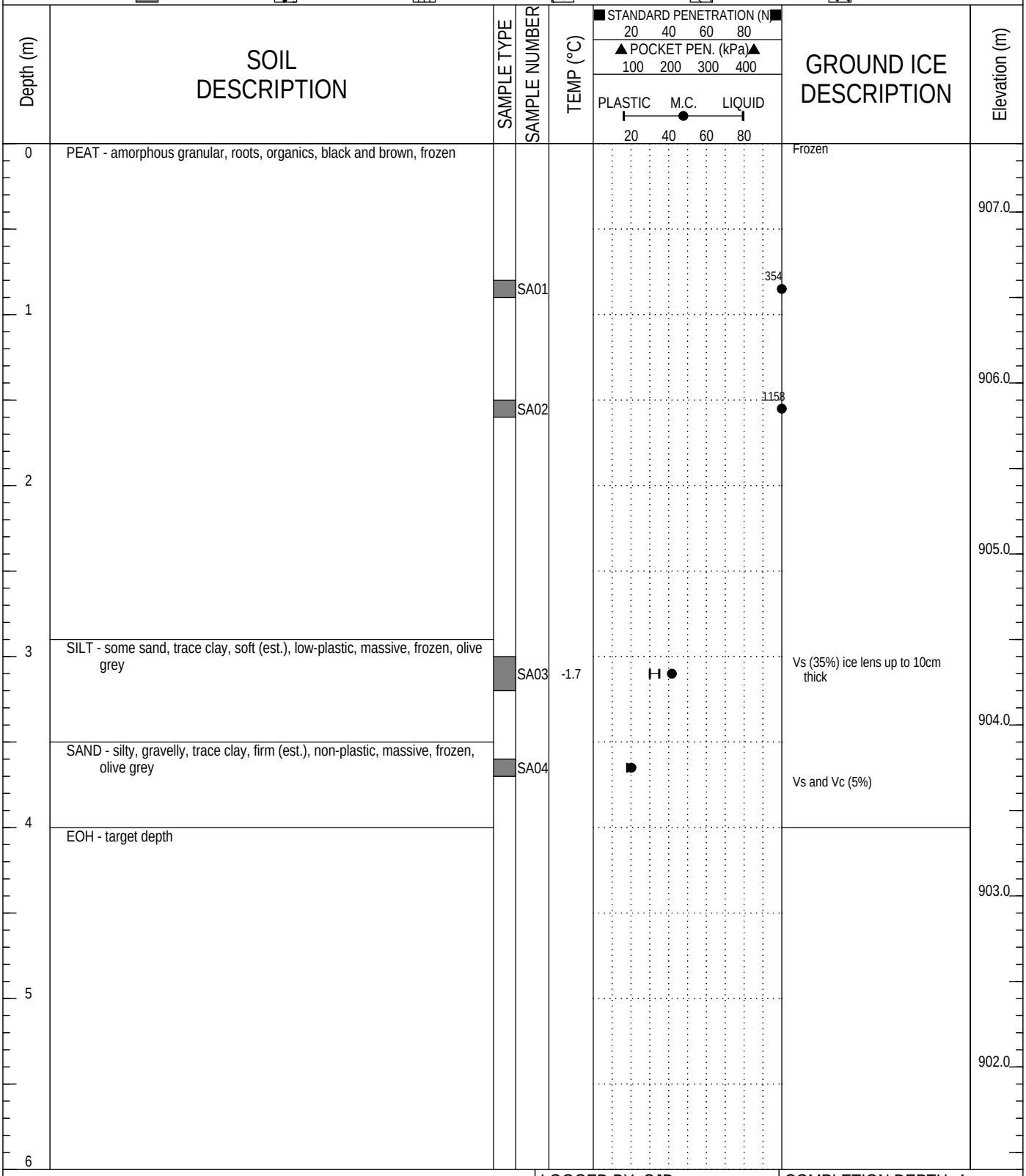
EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 3.1m
REVIEWED BY: JRT	COMPLETE: 5/6/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP03
near Keno City, YT	7086760N; 484004E; Zone 8	ELEVATION: 907.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND



EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 4m
	REVIEWED BY: JRT	COMPLETE: 5/6/2009
	DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP04
near Keno City, YT	7086712N; 483906E; Zone 8	ELEVATION: 903.8m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - roots, organic mat, woody, black					Frozen	
	SAND - silty, some gravel, compact (est.), medium grained, well graded, frozen, light brown, sub-rounded						
	GRAVEL - sandy, silty, some cobbles, compact (est.), coarse grained, well graded, moist, dark brown, pockets of silt, sub-rounded					Unfrozen	903.0
1			SA01				
			SA02				902.0
2						Frozen Nbn	
							901.0
3						Vc (10%)	
			SA03	-0.3			
	EOH - refusal in frozen gravel						900.0
4							
							899.0
5							
							898.0
6							

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 3.5m
REVIEWED BY: JRT	COMPLETE: 5/6/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP05
near Keno City, YT	7086736N; 483899E; Zone 8	ELEVATION: 903.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - roots, organics				Frozen	
	SAND AND GRAVEL - silty, trace cobbles, compact (est.), coarse grained, well graded, frozen, medium brown, sub-rounded		SA01			903.0
1						
	0.1 m thick silt lens - frozen, light brown		SA02		Unfrozen	902.0
2	SAND - some gravel, some silt, trace cobbles, loose (est.), coarse grained, well graded, damp, dark brown, sub-angular					901.0
	SAND AND GRAVEL - trace silt, trace cobbles, compact (est.), medium grained, well graded, damp, dark brown, sub-rounded					
3			SA03			900.0
4			SA04			899.0
	EOH - target depth					
5						898.0
6						

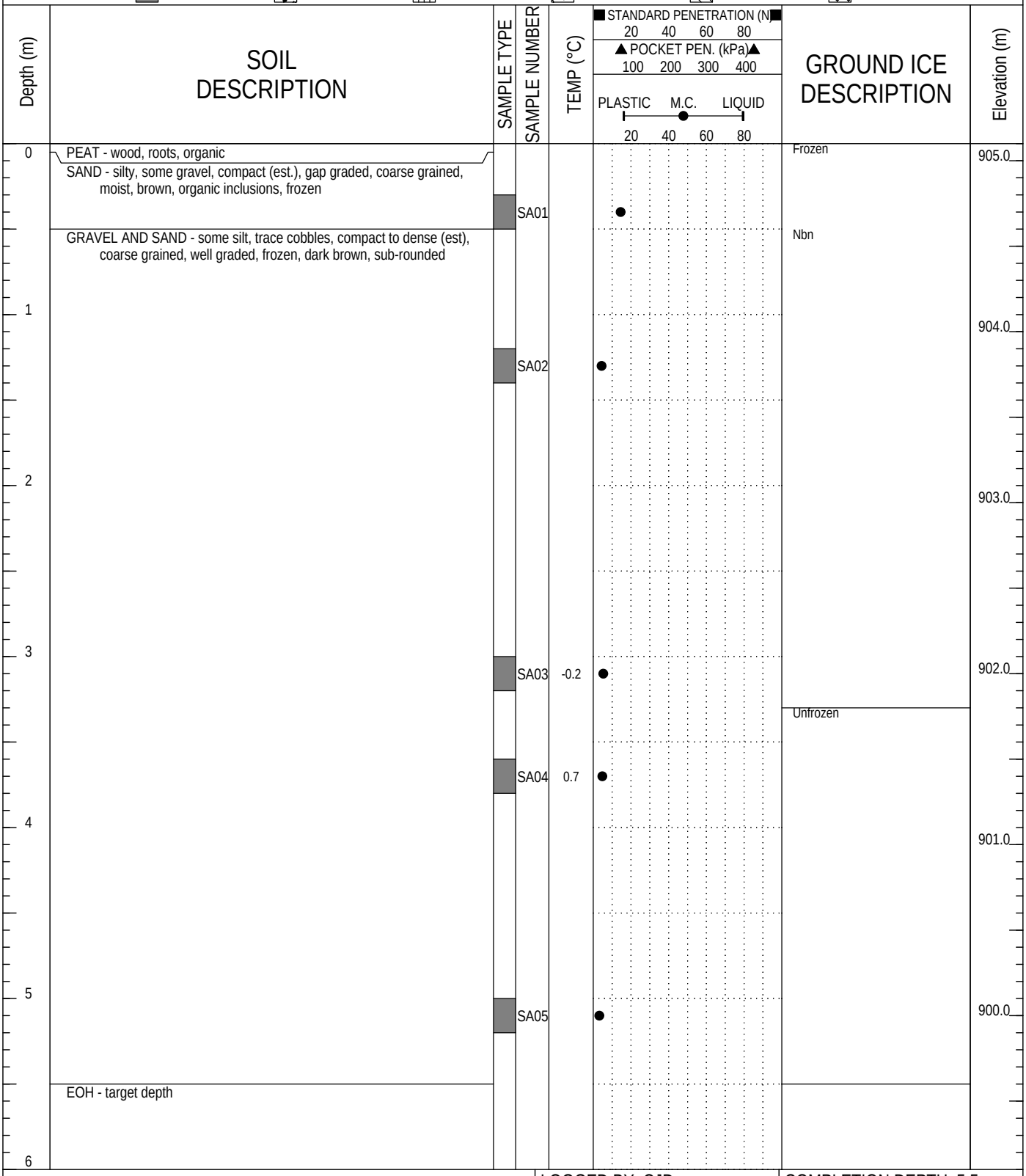
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LOGGED BY: CJD	COMPLETION DEPTH: 4.5m
REVIEWED BY: JRT	COMPLETE: 5/3/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP06
near Keno City, YT	7086719N; 483925E; Zone 8	ELEVATION: 905.1m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND



EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 5.5m
	REVIEWED BY: JRT	COMPLETE: 5/6/2009
	DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP07
near Keno City, YT	7086712N; 483955E; Zone 8	ELEVATION: 906.7m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - some silt, woody, roots, black					Frozen	
	SILT - sandy, some gravel, medium, non-plastic, frozen, brown, organics, roots		SA01				906.0
	SAND - gravelly, trace cobbles, trace silt,, compact (est.), medium grained, well graded, damp to moist, brown, sub-rounded						
1			SA02			Unfrozen	
	- seepage						905.0
2						Frozen Nbn	
	SILT - sandy, some gravel, trace clay, stiff (est.), low plastic, massive, olive grey						904.0
3			SA03	-0.1	H	Vx, Vc (<5%)	
							903.0
						Unfrozen	
4							
			SA04	1.5	▲		902.0
5							
	EOH - refusal at probable bedrock (quarzite)						901.0
6							

EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 5.4m
	REVIEWED BY: JRT	COMPLETE: 5/6/2009
	DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP08
near Keno City, YT	7086741N; 483974E; Zone 8	ELEVATION: 908.6m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - silty, woody, organics, roots, frozen					Frozen	
	SAND - gravelly, some silt, loost (est.), well graded, coarse grained, frozen						908.0
1			SA01	-0.5	●	Vc, Vr (25%)	
							907.0
	BEDROCK - laminated, moderately weathered						
2			SA02		●	Vs (10%)	
			SA03		●		
	EOH refusal, frozen bedrock						906.0
3							
							905.0
4							
							904.0
5							
							903.0
6							

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LOGGED BY: CJD	COMPLETION DEPTH: 2.2m
REVIEWED BY: JRT	COMPLETE: 5/6/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Detention Berm	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP09
near Keno City, YT	7086737N; 483797E; Zone 8	ELEVATION: 895.8m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - woody, organic, dark brown, frozen				Frozen	895.0
	GRAVEL AND SAND - some cobbles, trace silt, compact to dense (est.), coarse grained, well graded, damp, medium brown, sub-rounded					
1	- unfrozen		SA01		Unfrozen	894.0
2						
	BOULDERS - cobbley, some gravel, some silt, dense (est.), coarse grained, gap graded, damp, bluish grey, sub-rounded					893.0
	SILT (till) - gravelly, sandy, trace clay, stiff, low plastic, damp, olive grey, massive		SA02			
3						892.0
4			SA03			
						891.0
5			SA04			
	EOH - target depth					890.0
6						

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 5.2m
REVIEWED BY: JRT	COMPLETE: 5/5/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Runoff Collection Pond	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP10
near Keno City, YT	7086754N; 483834E; Zone 8	ELEVATION: 896m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - sandy, some cobbles, trace silt, dense (est.), coarse grained, well graded, damp, medium brown, frozen				Frozen	896.0
					Unfrozen	
1			SA01			895.0
2						894.0
3			SA02			893.0
4			SA03			892.0
	- water					
5			SA04			891.0
	EOH - target depth					
6						890.0

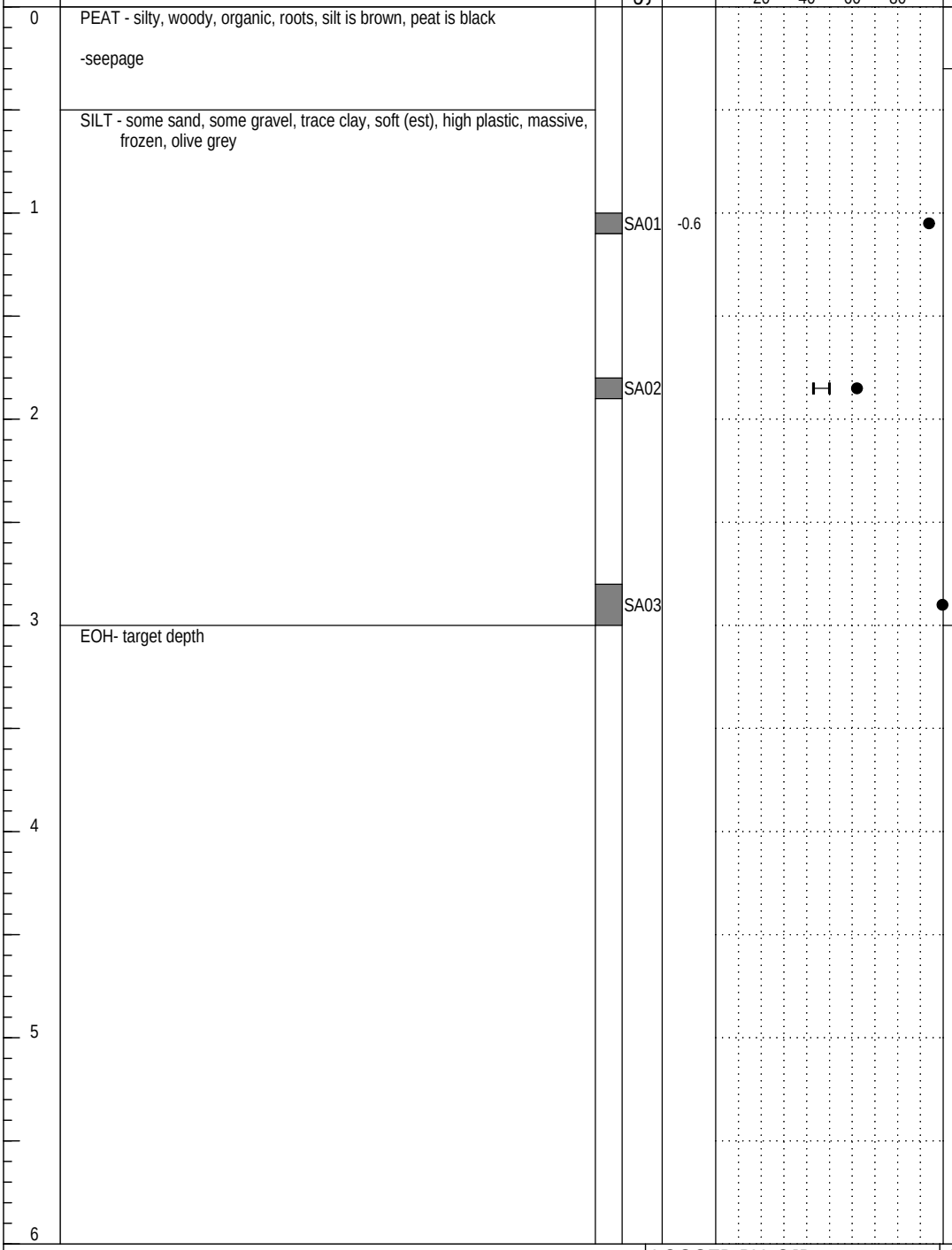
EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 5.1m
	REVIEWED BY: JRT	COMPLETE: 5/5/2009
	DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP11
near Keno City, YT	7086737N; 484046E; Zone 8	ELEVATION: 912.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - silty, woody, organic, roots, silt is brown, peat is black -seepage					Unfrozen	
						Frozen	912.0
	SILT - some sand, some gravel, trace clay, soft (est), high plastic, massive, frozen, olive grey					Vs, Vc (25%)	
1			SA01	-0.6			911.0
2			SA02			Vs, Vc (20%)	910.0
3			SA03			Vs, Vc (30%)	
	EOH- target depth						909.0
4							908.0
5							907.0
6							



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LOGGED BY: CJD	COMPLETION DEPTH: 3m
REVIEWED BY: JRT	COMPLETE: 5/6/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
DSTF	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP12
near Keno City, YT	7086942N; 483955E; Zone 8	ELEVATION: 913.8m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - woody, roots, organics					Frozen	913.8
	SILT - sandy, some gravel, trace clay, stiff (est.), non-plastic, frozen, light brown, organic, roots						
	GRAVEL AND SAND - some cobbles, trace silt, compact (est.), medium grained, well graded, brown					unfrozen	913.0
1			SA01		●		912.0
2	SILT and BOULDERS - sandy, trace clay, trace gravel, non-plastic, bedded, frozen, brown		SA02	-0.3	●	Frozen, Vs (<5%)	911.0
	EOH - refusal at possible bedrock (quartzite)						
3							910.0
4							909.0
5							908.0
6							

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 2.1m
REVIEWED BY: JRT	COMPLETE: 5/7/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP13
near Keno City, YT	7086811N; 483912E; Zone 8	ELEVATION: 905m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - (waste rock) - cobbley, some sand, trace silt, loose to compact (est.), coarse grained, well graded, damp to moist, reddish-brown, angular				Unfrozen	905.0
			SA01			
1	-hole sloughing					904.0
	BEDROCK (quartzite), moderately weathered, oxidized, blocky					
2						903.0
3	EOH - target depth and sloughing					902.0
4						901.0
5						900.0
6						899.0

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LOGGED BY: CJD	COMPLETION DEPTH: 3m
REVIEWED BY: JRT	COMPLETE: 5/7/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
DSTF	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP14
near Keno City, YT	7086986N; 483897E; Zone 8	ELEVATION: 901.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - amorphous granular, organic, roots and rootlets					Frozen	901.0
1	SILT - sandy, some gravel, non-plastic, massive, frozen, olive grey		SA01			Vs (10%)	
	SAND - gravelly, some cobbles, trace silt, dense (est.), well graded, coarse grained, sub-rounded, brown, frozen						900.0
			SA02			Vc, Vx (10%)	
2			SA03	-0.2		Vc, Vx (5%)	899.0
			SA04			Nbn	
3	EOH - target depth						898.0
4							897.0
5							896.0
6							

EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 3m
	REVIEWED BY: JRT	COMPLETE: 5/7/2009
	DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
DSTF	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP15
near Keno City, YT	7086939N; 483873E; Zone 8	ELEVATION: 900.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - organic, rootlets, black, frozen				Frozen	900.0
	GRAVEL - sandy, some cobbles, some silt, compact (est.), medium grained, well graded, frozen, brown					
1			SA01	●	Nbn	899.0
2						
	EOH - refusal at possible bedrock (quartzite)					898.0
3						897.0
4						896.0
5						895.0
6						

EBA Engineering Consultants Ltd.	LOGGED BY: CJD	COMPLETION DEPTH: 2.3m
	REVIEWED BY: JRT	COMPLETE: 5/7/2009
	DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
DSTF	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP16
near Keno City, YT	7086887N; 483836E; Zone 8	ELEVATION: 900.1m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT -amorphous granular, some silt, frozen				Frozen, visible ice wedges 10 cm wide at top	900.0
	SAND - gravelly, silty, some cobbles, dense (est.), medium grained, well graded, frozen, brown				Nbn	
1			SA01	●		899.0
	BOULDERS - some cobbles, some gravel, trace sand, trace silt, frozen				Vc (5%)	
2	EOH - refusal in frozen boulders					898.0
3						897.0
4						896.0
5						895.0
6						

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 2m
REVIEWED BY: JRT	COMPLETE: 5/7/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
DSTF	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP17
near Keno City, YT	7086807N; 483838E; Zone 8	ELEVATION: 902.5m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL AND SAND (fill) - some cobbles, some silt, coarse grained, well graded, sub-rounded, damp, brown, roots, trees, peat inclusions, frozen				Frozen	902.0
	- becomes loose to compact (est.), damp				Unfrozen	
1			SA01			901.0
2			SA02			
	PEAT - woody, roots, black					
	SILT - sandy, some gravel, firm (est.), non-plastic, massive, damp, brown					900.0
	GRAVEL AND SAND- some cobbles, trace silt, coarse grained, compact (est.), well graded, sub-rounded, damp, brown					
3			SA03			899.0
4			SA04			898.0
	EOH - target depth					
5						897.0
6						

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 4.8m
REVIEWED BY: JRT	COMPLETE: 5/7/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Pad	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP18
near Keno City, YT	7086816N; 483953E; Zone 8	ELEVATION: 908.7m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	TEMP (°C)	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - woody, fine fibrous, some silt, roots, rootlets, organics					Frozen	908.0
1	SILT AND SAND - some gravel, trace clay, non-plastic, massive, frozen, gravel angular, light brown		SA01			Vx (<5%)	
			SA02	-0.3		Vs, Vc (5%)	907.0
2	EOH - target depth						906.0
3							905.0
4							904.0
5							903.0
6							

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LOGGED BY: CJD	COMPLETION DEPTH: 1.8m
REVIEWED BY: JRT	COMPLETE: 5/7/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Case Rubber Tired Backhoe	W14101178.002-TP19
near Keno City, YT	7086795N; 483932E; Zone 8	ELEVATION: 905.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL (FILL/WASTE ROCK) - sandy, some silt, well graded sub-rounded gravel, coarse to medium grained sand, brown				905.0
	- cobbles, trace of silt below 0.3 m				
1					904.0
2					903.0
	END OF TESTPIT @ 2.5 m (REFUSAL) - hard solid ground, probable bedrock				
3					902.0
4					901.0
5					900.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: JSB	COMPLETION DEPTH: 2.5m
REVIEWED BY: JRT	COMPLETE: 6/29/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Case Rubber Tired Backhoe	W14101178.002-TP20
near Keno City, YT	7086798N; 483942E; Zone 8	ELEVATION: 905.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL (FILL/WASTE ROCK) - sandy, some silt, well graded rounded to angular particles, coarse to medium grained sand, compact, dark, damp, greyish brown				
	BEDROCK - highly fractured, some weathering, friable stratified				
1					905.0
	END OF TESTPIT @ 1.2 m (REFUSAL)				
2					904.0
3					903.0
4					902.0
5					901.0
6					900.0

EBA Engineering Consultants Ltd.

LOGGED BY: JSB	COMPLETION DEPTH: 1.2m
REVIEWED BY: JRT	COMPLETE: 6/29/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Case Rubber Tired Backhoe	W14101178.002-TP21
near Keno City, YT	7086816N; 483930E; Zone 8	ELEVATION: 905.7m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL (FILL/WASTE ROCK) - sandy, trace of silt, well graded angular gravel, coarse to medium grained sand, compact, mottled reddish brown and grey				
	BEDROCK - moderately weathered, highly fractured, friable to competent particles				
	- becomes more competent with depth				905.0
1					
					904.0
2	END OF TESTPIT @ 2.0 m (REFUSAL)				
					903.0
3					
					902.0
4					
					901.0
5					
					900.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: JSB	COMPLETION DEPTH: 2m
REVIEWED BY: JRT	COMPLETE: 6/29/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Case Rubber Tired Backhoe	W14101178.002-TP22
near Keno City, YT	7086801N; 483914E; Zone 8	ELEVATION: 904.8m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	BEDROCK - highly fractured, weathered, friable to competent particles, blocky stratigraphy				904.0
1	- becomes more competent with depth				
	END OF TESTPIT @ 1.2 m (REFUSAL)				903.0
2					
					902.0
3					
					901.0
4					
					900.0
5					
					899.0
6					

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LOGGED BY: JSB	COMPLETION DEPTH: 1.2m
REVIEWED BY: JRT	COMPLETE: 6/29/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Case Rubber Tired Backhoe	W14101178.002-TP23
near Keno City, YT	7086808N; 483906E; Zone 8	ELEVATION: 904.6m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	ORGANIC ROOT MATERIAL				
	GRAVEL (FILL) - sandy, trace of silt, well graded angular gravel, coarse to medium grained gravel, compact, damp, dark brown and grey - cobbles, some boulders below 0.3 m				904.0
1	becomes coarser with depth				903.0
2					902.0
	END OF TESTPIT @ 2.5 m NOTE: Possible bedrock, but could not confirm due to sloughing sidewalls of testpit				
3					901.0
4					900.0
5					899.0
6					

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LOGGED BY: JSB	COMPLETION DEPTH: 2.5m
REVIEWED BY: JRT	COMPLETE: 6/29/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Case Rubber Tired Backhoe	W14101178.002-TP24
near Keno City, YT	7086827N; 483902E; Zone 8	ELEVATION: 904m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	ORGANIC ROOT MATERIAL				904.0
	GRAVEL (FILL/WASTE ROCK) - sandy, trace to some silt, well graded sub-rounded and angular particles, compact, damp, dark brownish and grey				
1					903.0
2	- organic layer, rootlets, black				902.0
	GRAVEL - sandy, some silt, well graded sub-rounded gravel, medium to coarse grained sand, damp, brownish grey				
	BEDROCK - friable, weathered - becomes more competent with depth				
	END OF TESTPIT @2.8 m (REFUSAL)				
3					901.0
4					900.0
5					899.0
6					898.0

EBA Engineering Consultants Ltd.

LOGGED BY: JSB	COMPLETION DEPTH: 2.8m
REVIEWED BY: JRT	COMPLETE: 6/29/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP25
near Keno City, YT	7086790N; 483933E; Zone 8	ELEVATION: 904.5m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - sandy, some silt, compact, damp, sub-rounded to sub-angular, well graded, brown				904.0
1					903.0
2	SILT (TILL) - gravelly, sandy, trace clay, firm (est.), organic inclusions, damp, olive grey				902.0
	EOH - Target Depth				
3					901.0
4					900.0
5					899.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 2.4m
REVIEWED BY: JRT	COMPLETE: 7/16/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP26
near Keno City, YT	7086788N; 483951E; Zone 8	ELEVATION: 903.4m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	PEAT - amorphous, granular, roots, organics, black				903.0
	SILT (TILL) - gravelly, sandy, trace clay, firm, organic inclusions, damp, olive grey				
1	GRAVEL - sandy, some silt, compact, sub-rounded to sub-angular, brown				902.0
	EOH - Target Depth				
2					901.0
3					900.0
4					899.0
5					898.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 1.2m
REVIEWED BY: JRT	COMPLETE: 7/16/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP27
near Keno City, YT	7086783N; 483947E; Zone 8	ELEVATION: 902.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - sandy, some silt, compact, well graded, sub-rounded to sub-angular, damp, brown				
	- becomes silty				
					902.0
1					
	- becomes some silt				
	EOH -Refusal, probable quartzite bedrock				901.0
2					
					900.0
3					
					899.0
4					
					898.0
5					
					897.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 1.8m
REVIEWED BY: JRT	COMPLETE: 7/16/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP28
near Keno City, YT	7086795N; 483934E; Zone 8	ELEVATION: 903.8m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - sandy, some silt, compact, well graded, sub-rounded to sub-angular, damp, brown				903.0
1	EOH - Target Depth				902.0
2					901.0
3					900.0
4					899.0
5					898.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 1m
REVIEWED BY: JRT	COMPLETE: 7/16/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP29
near Keno City, YT	7086797N; 483912E; Zone 8	ELEVATION: 902.3m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - sandy, some silt, compact, well graded, sub-rounded to sub-angular, damp, brown				902.0
	Refusal, probable weathered quartzite bedrock				
1					901.0
2					900.0
3					899.0
4					898.0
5					897.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 0.5m
REVIEWED BY: JRT	COMPLETE: 7/16/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Mill Building	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP30
near Keno City, YT	N; E; Zone 8	ELEVATION: 903.2m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - sandy, some silt, compact, well graded, sub-rounded to sub-angular, damp, brown				903.0
1	SILT (TILL) - gravelly, sandy, trace clay, firm, organic inclusions, damp, olive grey				902.0
	EOH - Target Depth Note: End of bedrock knob				
2					901.0
3					900.0
4					899.0
5					898.0
6					

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 1.3m
REVIEWED BY: JRT	COMPLETE: 7/16/2009
DRAWING NO: Figure 2	Page 1 of 1

Flame and Moth Mill & DSTF	CLIENT: Alexco	PROJECT NO. - TESTPIT NO.
Borrow Pit	EXCAVATOR: Hitachi 270 LC	W14101178.002-TP31
near Keno City, YT	7086832N; 483866E; Zone 8	ELEVATION: 903.9m

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	STANDARD PENETRATION (N) 20 40 60 80 / POCKET PEN. (kPa) 100 200 300 400 / PLASTIC M.C. LIQUID 20 40 60 80	GROUND ICE DESCRIPTION	Elevation (m)
0	GRAVEL - cobbly, sandy, some to trace silt, compact, well graded, sub-rounded to sub-angular, damp, brown					903.0
1			1			902.0
2	EOH - Target Depth					901.0
3						900.0
4						899.0
5						898.0
6						

EBA Engineering Consultants Ltd.

LOGGED BY: CJD	COMPLETION DEPTH: 2m
REVIEWED BY: JRT	COMPLETE: 7/16/2009
DRAWING NO: Figure 2	Page 1 of 1

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH26
Keno City, YT	7086870N; 484037E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT
0	SAND - silty, some gravel, damp, loose, dark grey, organics near surface				
1			SA01		7.6
			SA02	12	9.7
2	GRAVEL and SAND (TILL) - some silt, damp, compact, grey				
			SA03		2.8
3					
4			SA04		4.6
	BEDROCK - weathered, grey with quartz and staining - soft rock seems 0.2 m thick, easy drilling		SA05		2.4
5	BEDROCK - hard drilling				
			SA06		0.1
6	END OF BOREHOLE @ 6.0 m (Target Depth) NOTE: Hole grouted to surface; Bentonite plug installed on surface.				
7					
8					
9					
10					

PLASTIC — M.C. — LIQUID
20 40 60 80

STANDARD PENETRATION (N)
20 40 60 80

◆ UNCONFINED (kPa) ◆
50 100 150 200

▲ POCKET PEN. (kPa) ▲
100 200 300 400

Depth (ft): 0, 5, 10, 15, 20, 25, 30, 33

EBA Engineering Consultants Ltd.

LOGGED BY: JTP	COMPLETION DEPTH: 6m
REVIEWED BY: JRT	COMPLETE: 8/18/2010
DRAWING NO:	Page 1 of 1

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH27
Keno City, YT	7086920N; 484082E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT	Depth (ft)
0	SILT - sandy, trace gravel, moist, firm, non-plastic, olive brown, organics near surface					0
1			SA07		13.3	
	- becomes sandier		SA08	18	12.6	5
2	SAND and GRAVEL - some silt, dry, light grey					
	BEDROCK - grey, hard drilling		SA09		2.1	
3	END OF BOREHOLE @ 3.0 m (Target Depth)					10
	NOTE: hole filled with bentonite chips					
4						
5						15
6						20
7						
8						25
9						30
10						33

PLASTIC M.C. LIQUID: 20 40 60 80

STANDARD PENETRATION (N): 20 40 60 80

UNCONFINED (kPa): 50 100 150 200

POCKET PEN. (kPa): 100 200 300 400

EBA Engineering Consultants Ltd.

LOGGED BY: JTP	COMPLETION DEPTH: 3m
REVIEWED BY: JRT	COMPLETE: 8/18/2010
DRAWING NO:	Page 1 of 1

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH28
Keno City, YT	7086985N; 484026E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT	Depth (ft)
0	ORGANIC MOSS COVER					0
	SILT - some sand, uniform, moist, soft, dark brown, some organics		SA10		59	
1						
						5
2	SILT (TILL) - gravelly, trace sand, frozen (Vx), firm, grey		SA11	42	45.3	
			SA12		43.2	
3	- ICE and SILT		SA13	57	25.7	10
4						
	- attempted SPT - spoon refusal		SA14		13.5	15
5	SAND and GRAVEL (TILL) - gravelly, moist, firm, grey					
6	MASSIVE ICE					20
7						
	- attempted SPT - spoon refusal		SA15		22.6	25
8	SILT (TILL) - gravelly, moist, firm, grey					
9						30
10						
	MASSIVE ICE					35
11						
12						40
13						
	GRAVEL (TILL) - some silt, frozen (Vx), compact, grey with other minerals					45
14	MASSIVE ICE - occasional gravel					
15						49

PLASTIC — M.C. — LIQUID (20 40 60 80)

STANDARD PENETRATION (N) (20 40 60 80)

UNCONFINED (kPa) (50 100 150 200)

POCKET PEN. (kPa) (100 200 300 400)

EBA Engineering Consultants Ltd.	LOGGED BY: JTP	COMPLETION DEPTH: 27.5m
	REVIEWED BY: JRT	COMPLETE: 8/20/2010
	DRAWING NO:	Page 1 of 2

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH28
Keno City, YT	7086985N; 484026E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT (PLASTIC / M.C. / LIQUID; 20 40 60 80)	STANDARD PENETRATION (N) 20 40 60 80; UNCONFINED (kPa) 50 100 150 200; POCKET PEN. (kPa) 100 200 300 400	Depth (ft)
15							50
16							
17							55
18							
19							60
20							
21	GRAVEL (TILL) - silty, some sand, dry, dense, grey						65
	SILT (TILL) - gravelly, dry, stiff, grey with staining						
22							70
23							
24	SAND and GRAVEL (TILL) - trace silt, dry, dense, grey - grey rock seem 0.3 m thick						75
25	- sand seem 0.2 m thick, tan - sand seem 0.2 m thick, tan - becomes damp - becomes some silt						80
26							85
27	BEDROCK - hard drilling, light grey						
28	END OF BOREHOLE @ 27.5 m (Target Depth) NOTES: Installed SI casing to 89' (27.13 m). Grouted hole to surface with tremie line (approx. 60 gal.)						90
29							95
30							98

EBA Engineering Consultants Ltd.	LOGGED BY: JTP	COMPLETION DEPTH: 27.5m
	REVIEWED BY: JRT	COMPLETE: 8/20/2010
	DRAWING NO:	Page 2 of 2

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH29
Keno City, YT	7087010N; 483944E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	MOISTURE CONTENT
0	MOSS COVER			
	SAND and GRAVEL - some silt, medium grained, well graded, sub-rounded, moist, compact (est.), dark brown, trace organics		SA16	12.6
1	ROCK - fractured angular cuttings returned, various colours, some staining			
	SILT - some sand, trace gravel, damp, firm (est.), non-plastic, olive grey hint of green		SA17	16.5
2	BEDROCK - hard drilling			
			SA18	1.7
3	END OF BOREHOLE @ 3.0 m (Target Depth)			
4				
5				
6				
7				
8				
9				
10				

PLASTIC — M.C. — LIQUID
20 40 60 80

STANDARD PENETRATION (N)
20 40 60 80

◆ UNCONFINED (kPa) ◆
50 100 150 200

▲ POCKET PEN. (kPa) ▲
100 200 300 400

Depth (ft): 0, 5, 10, 15, 20, 25, 30, 33

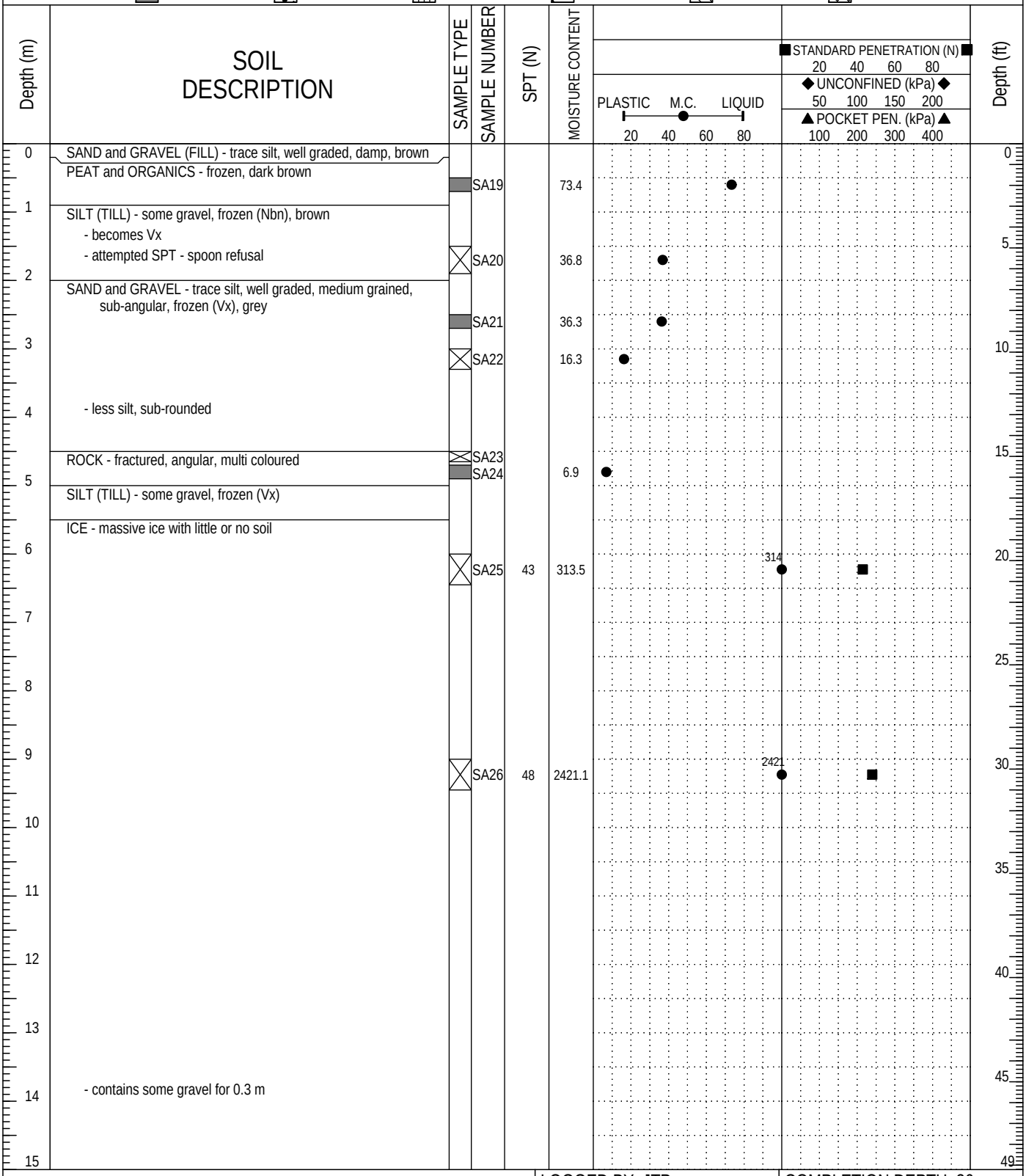
EBA Engineering Consultants Ltd.

LOGGED BY: JTP	COMPLETION DEPTH: 3m
REVIEWED BY: JRT	COMPLETE: 9/7/2010
DRAWING NO:	Page 1 of 1

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH30
Keno City, YT	7087032N; 483969E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND



EBA Engineering Consultants Ltd.	LOGGED BY: JTP	COMPLETION DEPTH: 26m
	REVIEWED BY: JRT	COMPLETE: 9/8/2010
	DRAWING NO:	Page 1 of 2

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH30
Keno City, YT	7087032N; 483969E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT	PLASTIC / M.C. / LIQUID (20 40 60 80)	STANDARD PENETRATION (N) 20 40 60 80; UNCONFINED (kPa) 50 100 150 200; POCKET PEN. (kPa) 100 200 300 400	Depth (ft)
15								50
16								
17								55
18	- contains some silt for 0.3 m							60
19								
20								65
21								
22	GRAVEL - some sand, some silt, frozen (Nbn), grey		SA27		10.4	●		70
23	- becomes Vx - becomes damp		SA28		6.9	●		75
24	- sand seem 0.2 m thick							
25	ROCK - easy drilling, dry, shiny black/grey BEDROCK - hard drilling, grey							80
26	END OF BOREHOLE @ 26.0 m (Target Depth)							85
27								
28								90
29								95
30								98

EBA Engineering Consultants Ltd.

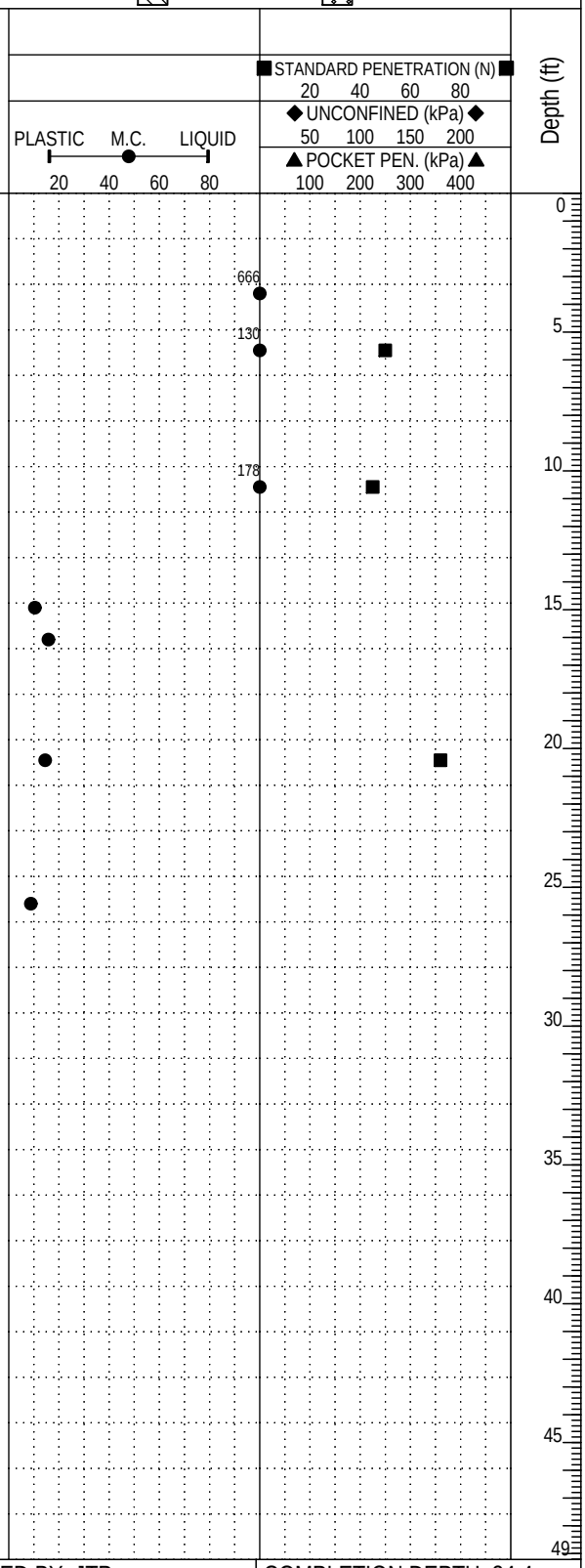
LOGGED BY: JTP	COMPLETION DEPTH: 26m
REVIEWED BY: JRT	COMPLETE: 9/8/2010
DRAWING NO:	Page 2 of 2

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH31
Keno City, YT	7078058N; 484016E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT
0	PEAT - frozen, black/dark brown				
1			SA29		666.2
2	SILT - trace gravel, frozen (Vx), brown		SA30	50	130.1
3	- organics (wood) for 1.5 m		SA31	45	177.6
4	SILT (TILL) - gravelly, trace sand, frozen (Vx), grey		SA32		10.4
5			SA33		15.8
6			SA34	72	14.5
7	- becomes some gravel				
8	SAND and GRAVEL - trace silt, well graded, medium grained, sub-angular, frozen (Vx), multi-coloured		SA35		8.8
	SILT (TILL) - some gravel, frozen, grey				
9					
10					
11	MASSIVE ICE - trace silt				
12					
13					
14	SAND and GRAVEL - some silt, frozen (Vx), grey				
15					



Depth (ft): 0, 5, 10, 15, 20, 25, 30, 35, 40, 45, 49

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH31
Keno City, YT	7078058N; 484016E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT
15	MASSIVE ICE - trace silt				
16					
17					
18			SA36		977.9
19					
20					
	SILT (TILL) - some gravel, frozen (Vx), grey		SA37		10.3
21					
22					
	ROCK - fractured, angular, damp, multi-coloured				
23	BEDROCK - hard drilling, grey				
24					
	END OF BOREHOLE @ 24.4 m (Target Depth)				
25					
26					
27					
28					
29					
30					

PLASTIC — M.C. — LIQUID
20 40 60 80

STANDARD PENETRATION (N)
20 40 60 80

UNCONFINED (kPa)
50 100 150 200

POCKET PEN. (kPa)
100 200 300 400

978

Depth (ft): 50, 55, 60, 65, 70, 75, 80, 85, 90, 95, 98

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LOGGED BY: JTP	COMPLETION DEPTH: 24.4m
REVIEWED BY: JRT	COMPLETE: 9/10/2010
DRAWING NO:	Page 2 of 2

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH32
Keno City, YT	7086999N; 484077E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	MOISTURE CONTENT	PLASTIC / M.C. / LIQUID (20 40 60 80)	STANDARD PENETRATION (N) (20 40 60 80) / UNCONFINED (kPa) (50 100 150 200) / POCKET PEN. (kPa) (100 200 300 400)	Depth (ft)
0	SAND and GRAVEL (FILL) - some silt, medium grained, well graded, sub-round, damp, loose, brown						0
1							
	PEAT - frozen, black/dark brown						5
2							
	SILT - some sand, frozen (Vx), grey						
3			SA38	109		109	10
4							
			SA39				
	- hard drilling for 0.3 m		SA40	12.8			15
	- attempted SPT - spoon refusal						
5							
6							
	- gravel content increases		SA41	8.6			20
7							
	BEDROCK - hard drilling, grey		SA42	7.8			25
8							
			SA43	1.2			
9							
	END OF BOREHOLE @ 9.0 m (Target Depth)						30
10							33

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LOGGED BY: JTP	COMPLETION DEPTH: 9m
REVIEWED BY: JRT	COMPLETE: 9/10/2010
DRAWING NO:	Page 1 of 1

GEOTECHNICAL W14101178.011.GPJ EBA.GDT 2/8/11

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH33
Keno City, YT	7086956N; 484029E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT
0	SAND and GRAVEL (FILL) - some silt, medium grained, well graded, sub-round, damp, loose, brown				
	PEAT - frozen, dark brown				
1					
	SILT (TILL) - gravelly, frozen (Vx), grey				
			SA44	73	18.5
2	- becomes trace gravel				
3			SA45	71	41.3
4					
	- becomes some gravel with visible staining - becomes damp		SA46		13.8
5	SAND and GRAVEL - silty, fine grained, dense, dry, tan		SA47		12.2
6	BEDROCK - hard drilling, grey		SA48		
			SA49		1.9
7					
	END OF BOREHOLE @ 7.5 m (Target Depth)				
8					
9					
10					

PLASTIC — M.C. — LIQUID (20 40 60 80)

STANDARD PENETRATION (N) (20 40 60 80)

UNCONFINED (kPa) (50 100 150 200)

POCKET PEN. (kPa) (100 200 300 400)

Depth (ft): 0, 5, 10, 15, 20, 25, 30, 33

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH34
Keno City, YT	7086915N; 484024E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	MOISTURE CONTENT	PLASTIC M.C. LIQUID (20 40 60 80)	STANDARD PENETRATION (N) 20 40 60 80; UNCONFINED (kPa) 50 100 150 200; POCKET PEN. (kPa) 100 200 300 400	Depth (ft)
0	SAND and GRAVEL (FILL) - trace silt, medium grained, well graded, sub-rounded, damp, loose, brown						0
	PEAT - frozen, dark brown						
1							
	SILT (TILL) - gravelly, frozen (Vx), grey						5
	- attempted SPT - spoon refusal		SA50	16.4	●		
	BEDROCK - hard drilling, light grey		SA51	4.1	●		
2							
3	END OF BOREHOLE @ 3.0 m (Target Depth)						10
4							15
5							
6							20
7							25
8							
9							30
10							33

EBA Engineering Consultants Ltd.

LOGGED BY: JTP	COMPLETION DEPTH: 3m
REVIEWED BY: JRT	COMPLETE: 9/11/2010
DRAWING NO:	Page 1 of 1

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH35
Keno City, YT	7086941N; 483996E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT
0	SAND and GRAVEL (FILL) - trace silt, medium grained, well graded, sub-rounded, damp, loose, brown				
1	PEAT - frozen, dark brown				
2			SA52	30	199.6
	SILT (TILL) - some gravel, frozen (Vx), grey				
3			SA53		37.5
4					
5			SA54	78	52.4
	- becomes gravelly		SA55		
6					
			SA56		13.4
7	- becomes some gravel				
8					
9	- becomes trace				
10					
11	- becomes SILT and GRAVEL				
12	MASSIVE ICE - trace silt				
	SILT and GRAVEL (TILL) - frozen (Vx), grey		SA57		9.3
13					
14					
	MASSIVE ICE - some gravel				
15					

PLASTIC — M.C. — LIQUID (20 40 60 80)

STANDARD PENETRATION (N) (20 40 60 80)

UNCONFINED (kPa) (50 100 150 200)

POCKET PEN. (kPa) (100 200 300 400)

200

Depth (ft): 0 5 10 15 20 25 30 35 40 45 49

EBA Engineering Consultants Ltd.	LOGGED BY: JTP	COMPLETION DEPTH: 26m
	REVIEWED BY: JRT	COMPLETE: 9/11/2010
	DRAWING NO:	Page 1 of 2

Detailed DSTF Drilling	CLIENT: Alexco Resource Corporation	PROJECT NO. - BOREHOLE NO.
Keno Hill District Mill Site	DRILL: M5 Air Rotary	W14101178.011-BH35
Keno City, YT	7086941N; 483996E; Zone 8	

SAMPLE TYPE: DISTURBED | NO RECOVERY | SPT | A-CASING | SHELBY TUBE | CORE

BACKFILL TYPE: BENTONITE | PEA GRAVEL | SLOUGH | GROUT | DRILL CUTTINGS | SAND

Depth (m)	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE NUMBER	SPT (N)	MOISTURE CONTENT	PLASTIC M.C. LIQUID (20 40 60 80)	STANDARD PENETRATION (N) 20 40 60 80 / UNCONFINED (kPa) 50 100 150 200 / POCKET PEN. (kPa) 100 200 300 400	Depth (ft)
15	- becomes trace silt							50
16								
17	GRAVEL seem - frozen (Vx), hard drilling							55
18								60
19								
20	SILT and GRAVEL (TILL) - frozen (Vx), grey		SA58		15.2	●		65
21	- hard drilling for 1.0 m, possible rock							70
22								
23	SAND - some silt, trace gravel, fine grained, compact (est.), dry, dark tan							75
24	BEDROCK - hard drilling - soft black rock seem, 0.3 m		SA59		4.5	●		80
25								
26	END OF BOREHOLE @ 26.0 m (Target Depth)							85
27								
28								90
29								95
30								98