APPENDIX 26

Interim Report of Metallurgical Test Work, November 2010

Victoria GOLD CORP

Stantec

Eagle Gold Project
Interim Report of Metallurgical Test Work
November 2010

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10 November 2010

Eagle Gold Project
Interim Report of Metallurgical Test Work
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1.0 Introduction to Interim Report

This interim report discusses the metallurgical test work completed to date on a Master Composite sample developed from core initially worked on by Kappes, Cassiday & Associates (KCA) in 1996.

The test work completed to date included the preparation of the Master Composite sample by SGS Lakefield. Lakefield utilized a laboratory scale High Pressure Grinding Roll (HPGR) unit to crush a portion of the Master Composite to a particle size of 80% passing 3.641 millimeters.

The crushed material was returned to KCA and a sodium cyanide column leach test was conducted over a 33 day leach period. Following the leach phase the leach solution was treated with hydrogen peroxide to neutralize the Weak Acid Dissociable (WAD) Cyanide and the solution recycled to the column of leached tailings. The detox/rinse test work was continued until a WAD cyanide value of less than 0.2 mg/L was obtained in the column effluent.

After completion of the detox test work the column of leached and detoxified material underwent a modified humidity cell test program.

The humidity cell test is continuing at this point and final column tailings have not been assay for gold or silver. For the purpose of this report the weighted average grade of the Master Composite material based upon the head screen analysis with assays by size fraction was utilized as an estimate for the grade of the material leached in the column.

2.0 Sample Receipt and Preparation

In July 1995, the laboratory facility of Kappes, Cassiday & Associates (KCA) in Reno, Nevada received core material from the Dublin Gulch Project located in the Central Yukon Territory of Canada. Portions of this material were stored at KCA in sealed steel drums.

In June 2009, Victoria Gold acquired its interest in the Dublin Gulch Property (which contains the Eagle Gold Project) as a result of its takeover of of the previous owner.

In September 2009, selected stored crushed reject samples received in July 1995 were utilized to generate the Eagle Gold Master Composite (KCA Sample No. 42979).

Sample preparation was conducted utilizing each of the three (3) separate core intervals, used to generate the Master Composite, to provide material for head analyses.

Portions of the reject core intervals (crushed to minus 50 millimeters) were then combined to generate the Eagle Gold Master Composite (KCA Sample No. 42979).

A portion of the Master Composite was then sent to SGS for High Pressure Grinding Roll (HPGR) test work.

The HPGR product was returned to KCA for additional metallurgical test work including head screen analyses, agglomeration test work, cyanide column leach test work, detoxification and Humidity Cell Testing (HCT).

A description of the selected stored reject core intervals utilized to generate the Master Composite is presented in Table 2-1.

Table 2-1.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
Description and Weights of Reject Core Material

KCA Sample No.	Core Hole	Interval From, meters	Interval To, meters	Unit Type	Description	Crush Size, millimeters	Weight, kg	Weight to Composite, kg
22602	74 C	47.3	99.1	C1	Sericite altered granodiorite	50	594	41.25
22603	74 C	99.1	177.2	B	Fresh to weakly altered granodiorite	50	938	41.25
22616	76 C	22.9	190.0	A	Weathered granodiorite	50	1955	67.50
42979					**Master Composite**			**150.00**

Note: Core Hole, Interval, Unit Type and Description provided by First Dynasty Mine/ Ivanhoe Goldfields, LTD (1995).

2.1 Sample Preparation of the Master Composite (KCA Sample No. 42979)

Sample preparation of the reject core intervals (crushed to minus 50 millimeters) was conducted individually but identically as follows:

1. The minus 50 millimeter crushed material was coned three (3) times and quartered.

2. One quarter was selected and stage crushed to minus 6.3 millimeters.

3. From the minus 6.3 millimeter crushed material a 10 kilogram portion was split out and crushed to nominal 1.70 millimeters.

4. From the nominal 1.70 millimeter crushed material two (2) 500 gram portions were split out and pulverized individually to 80% passing 0.075 millimeters.

5. The pulverized portions were assayed for gold and silver by standard fire assay and wet chemistry methods. A portion of one pulverized portion was also utilized for multi-element, whole rock, total carbon, total sulfur (sulfur speciation) and mercury analyses. In addition to these analyses, a cold cyanide soluble copper shake test was conducted.

6. In addition to the head analyses, a portion of one pulverized portion was utilized for Acid Base Accounting (ABA) test work.

7. From the remaining quarter splits (minus 50 millimeter crushed material) the follow portions were split out and combined to generate the Eagle Gold Master Composite (KCA Sample No. 42979); 41.25 kilograms (KCA Sample No. 22602), 41.25 kilograms (KCA Sample No 22603) and 67.50 kilograms (KCA Sample No. 22616). The reject material for each separate core interval was stored individually.

8. The Eagle Gold Master Composite (150 kilograms) was sent to SGS for High Pressure Grinding Roll (HPGR) test work. The crushed product was then returned to KCA for additional metallurgical test work.

9. The HPGR product was thoroughly blended. An 80-kilogram portion was split out and utilized for a cyanide column leach test work, a 10-kilogram portion was split out and utilized for a head screen analysis and four (4) 2-kilogram portions were split out and utilized for agglomeration test work. The reject material was stored.

3.0 Head Analyses

Head analyses were completed on each of the three (3) separate reject core intervals, received in July 1995 and crushed to minus 50 millimeters, utilized to generate the Eagle Gold Master Composite (KCA Sample No. 42979).

The reject core material (crushed to minus 50 millimeters) from each separate interval was coned three (3) times and quartered. One quarter was selected and stage crushed to minus 6.3 millimeters. A 10-kilogram portion was then split out and crushed to nominal 1.70 millimeters. From the nominal 1.70 millimeter crushed material two (2) 500 gram portions were split out and pulverized individually to 80% passing 0.075 millimeters.

Each pulverized portion was analyzed for gold and silver by standard fire assay and wet chemistry methods.

A portion of one pulverized portion was assayed semi-quantitatively by means of inductively coupled argon plasma – optical emission spectrophotometer (ICAP-OES) for an additional series of elements and for a whole rock analyses. In addition to these semi-quantitative analyses, the sample was assayed by quantitative methods for total carbon, total sulfur (sulfur speciation) and mercury. A cyanide soluble copper shake test was conducted on a portion of the pulverized head material.

3.1 Head Analyses for Gold and Silver

Head analyses for gold and silver were completed by standard fire assay and wet chemistry methods.

The results of the head analyses for gold and silver are presented in Table 3-1.

Table 3-1.
Eagle Gold Project
Reject Core Intervals
Head Analyses – Gold and Silver

KCA Sample No.	Unit Type	Assays 2009		
		Assay 1, gms Au/MT	Assay 2, gms Au/MT	Average Assay, gms Au/MT
22602	C1	0.47	0.28	0.37
22603	B	0.44	0.37	0.41
22616	A	0.98	0.92	0.95

KCA Sample No.	Unit Type	Assays 2009		
		Assay 1, gms Ag/MT	Assay 2, gms Ag/MT	Average Assay, gms Ag/MT
22602	C1	5.3	1.6	3.4
22603	B	2.0	6.5	4.2
22616	A	1.5	1.3	1.4

3.2 Head Analyses for Multi-elements

A portion of the pulverized material for each core interval was assayed semi-quantitatively by means of inductively coupled argon plasma – optical emission spectrophotometer (ICAP-OES) as well as by flame atomic absorption spectrophotometer (FAAS) methods for an additional series of elements and for a whole rock analyses. In addition to these semi-quantitative analyses, the samples were assayed by quantitative methods for total carbon, total sulfur (sulfur speciation) utilizing a LECO CS 400 unit.

The results of the multi-element analyses are presented in Table 3-2. The results of the whole rock analyses are presented in Table 3-3.

Table 3-2.
Eagle Gold Project
Reject Core Intervals
Head Analyses – Multi-element Analyses

Constituent	Unit	Apr-96			Oct-09		
		KCA Sample No. 22602	KCA Sample No. 22603	KCA Sample No. 22616	KCA Sample No. 22602	KCA Sample No. 22603	KCA Sample No. 22616
Al	%				7.63	7.74	8.19
As	mg/kg	150	670	40	223	416	158
Ba	mg/kg	227	258	208	1531	1524	1555
Bi	mg/kg	14.0	5.4	7.03	24	24	26
C_{total}	%	0.50	0.46	0.19	0.54	0.49	0.14
Ca	%				2.51	2.41	2.34
Cd	mg/kg	6.03	6.14	2.14	7	6	6
Co	mg/kg				13	12	12
Cr	mg/kg	52.5	46.1	24.9	93	90	116
Cu	mg/kg	27.7	15.9	8.11	38	33	20
$Cu_{(cyanide\ soluble)}$	mg/kg				8	6	6
Fe	%	2.00	1.85	0.71	2.54	2.39	2.39
Hg	mg/kg	<2.00	<2.00	<2.00	<0.05	<0.05	<0.05
K	%				3.69	3.85	3.80
Mg	%				1.07	0.88	0.93
Mn	mg/kg	217	212	66.5	271	231	182
Mo	mg/kg	58.8	49.2	23.9	3	2	1
Na	%				1.59	1.60	1.76
Ni	mg/kg	16.3	15.4	7.94	28	30	32
Pb	mg/kg	25.6	191	1.10	42	38	24
S_{total}	%	0.34	0.44	0.08	0.21	0.22	0.05
$S_{sulfide}$	%	0.26	0.31	<0.01	0.11	0.07	<0.01
$S_{sulfate}$	%	<0.01	0.13	<0.03	0.10	0.15	0.05
Sb	mg/kg	<0.05	16.4	<0.05	9	10	5
Sr	mg/kg				417	431	466
Ti	%				0.30	0.28	0.33
V	mg/kg				44	34	38
W	mg/kg				35	25	11
Zn	mg/kg	45.2	297	9.08	95	52	33

Table 3-3.
Eagle Gold Project
Reject Core Intervals
Head Analyses - Lithium Metaborate Fusion - Whole Rock Analyses

Constuituent	Units	KCA Sample No. 22602		KCA Sample No. 22603		KCA Sample No. 22616	
SiO_2	%	64.53		64.99		66.66	
Si	%		30.17		30.38		31.16
Al_2O_3	%	14.17		14.80		15.00	
Al	%		7.50		7.83		7.94
Fe_2O_3	%	3.68		3.39		3.36	
Fe	%		2.57		2.37		2.35
CaO	%	3.60		3.59		3.10	
Ca	%		2.57		2.57		2.22
MgO	%	1.68		1.42		1.51	
Mg	%		1.01		0.86		0.91
Na_2O	%	2.14		2.21		2.38	
Na	%		1.59		1.64		1.77
K_2O	%	4.52		4.78		4.49	
K	%		3.75		3.97		3.73
TiO_2	%	0.51		0.49		0.53	
Ti	%		0.31		0.29		0.32
MnO	%	0.03		0.03		0.02	
Mn	%		0.02		0.02		0.02
SrO	%	0.05		0.05		0.06	
Sr	%		0.04		0.04		0.05
BaO	%	0.17		0.17		0.18	
Ba	%		0.15		0.15		0.16
Cr_2O_3	%	0.02		0.02		0.02	
Cr	%		0.01		0.01		0.01
P_2O_5	%	0.12		0.12		0.14	
P	%		0.05		0.05		0.06
LOI (1,093^oC)	%	4.21		3.52		1.73	
SUM	%	99.43		99.58		99.18	

Note: For the purpose of calculation, for values less than the detection limit a value of ½ the detection limit is utilized.
Note: The SUM is the total of the oxide constituents and the loss on ignition.

3.3 Head Screen Analyses with Assays by Size Fraction

Portions of the reject core intervals (crushed to minus 50 millimeters) were then combined to generate the Eagle Gold Master Composite (KCA Sample No. 42979).

A portion of the Master Composite was then sent to SGS for High Pressure Grinding Roll (HPGR) test work. The HPGR product was returned to KCA for additional metallurgical test work. From the HPGR product a 10-kilogram portion was split out and utilized for a head screen analysis.

The head screen analysis is summarized in Table 3-4.

The complete head screen analysis is presented in Table 3-5.

The head screen analysis is presented, graphically, in Figure 3-1.

Table 3-4.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
Summary of Head Screen Analyses – Gold and Silver

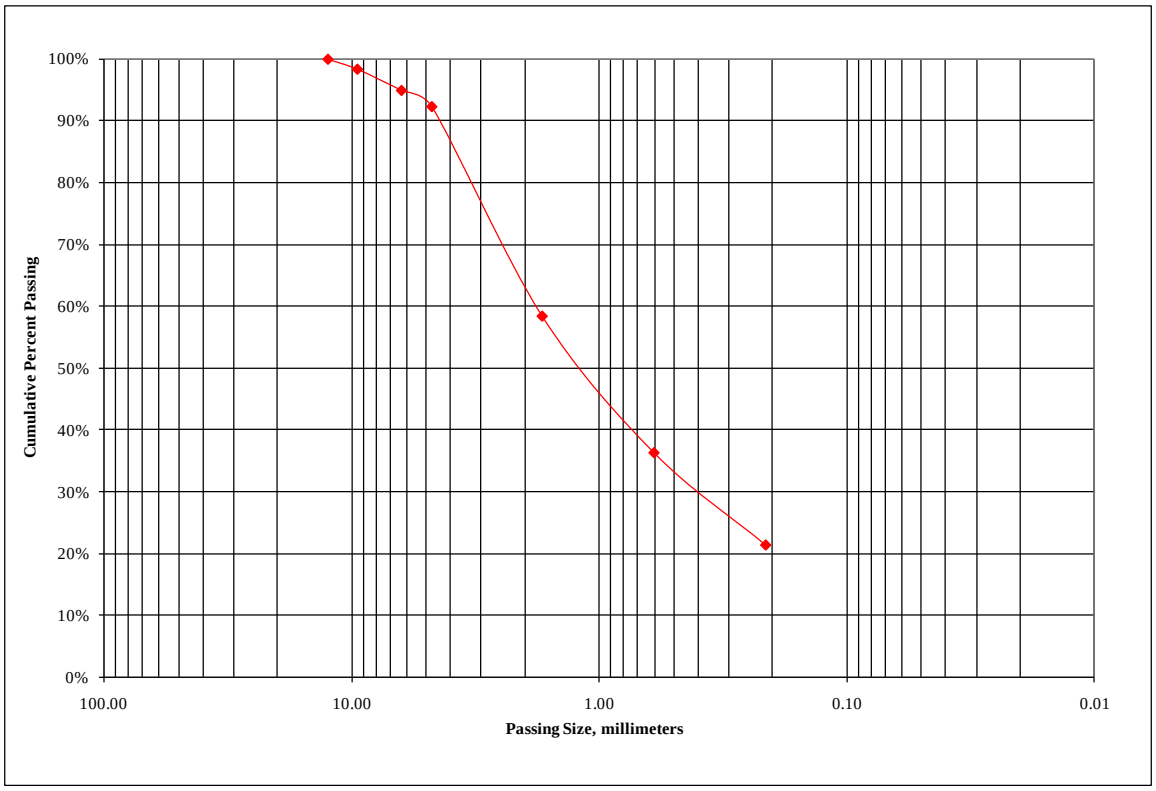
KCA Sample No.	Description	Calc. P_{80} Size, mm	Weighted Avg. Head Assay, gms Au/MT	Weighted Avg. Head Assay, gms Ag/MT
42979	Master Composite	3.641	0.51	1.79

Table 3-5.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
HPGR Crushed Product (Calculated P80 = 3.641 millimeters)
Head Screen Analysis with Assays by Size Fraction

			Dry Screen Analysis				Analysis of Gold Content			
KCA Sample No.	Passing, mm	Retained, mm	Sample Weight, kg	Weight Distribution, %	Cumulative Weight Retained, %	Cumulative Weight Passing, %	Assay 1, gms Au/MT	Assay 2, gms Au/MT	Average Assay, gms Au/MT	Weight Au, %
42979		12.50	0.00				---	---	---	---
	12.50	9.50	0.16	1.61%	1.61%	100.00%	0.14	0.14	0.14	0.45%
	9.50	6.30	0.34	3.43%	5.05%	98.39%	0.30	0.55	0.43	2.91%
	6.30	4.75	0.26	2.62%	7.67%	94.95%	0.17	0.23	0.20	1.03%
	4.75	1.70	3.36	33.91%	41.57%	92.33%	0.73	0.36	0.55	36.70%
	1.70	0.600	2.19	22.10%	63.67%	58.43%	0.37	0.39	0.38	16.55%
	0.600	0.212	1.48	14.93%	78.61%	36.33%	0.41	0.34	0.37	10.98%
	0.212	Pan	2.12	21.39%	100.00%	21.39%	0.74	0.75	0.74	31.38%
Total -			9.91	100.00%			0.57	0.45	0.51	100.00%
Detection -							0.10	0.10		

			Dry Screen Analysis				Analysis of Silver Content			
KCA Sample No.	Passing, mm	Retained, mm	Sample Weight, kg	Weight Distribution, %	Cumulative Weight Retained, %	Cumulative Weight Passing, %	Assay 1, gms Ag/MT	Assay 2, gms Ag/MT	Average Assay, gms Ag/MT	Weight Ag, %
42979		12.50	0.00				---	---	---	---
	12.50	9.50	0.16	1.61%	1.61%	100.00%	2.06	2.06	2.06	1.85%
	9.50	6.30	0.34	3.43%	5.05%	98.39%	1.71	1.71	1.71	3.28%
	6.30	4.75	0.26	2.62%	7.67%	94.95%	1.37	1.71	1.54	2.26%
	4.75	1.70	3.36	33.91%	41.57%	92.33%	1.71	1.37	1.54	29.16%
	1.70	0.600	2.19	22.10%	63.67%	58.43%	1.37	1.37	1.37	16.89%
	0.600	0.212	1.48	14.93%	78.61%	36.33%	1.37	3.43	2.40	19.98%
	0.212	Pan	2.12	21.39%	100.00%	21.39%	2.06	2.40	2.23	26.58%
Total -			9.91	100.00%			1.66	1.93	1.79	100.00%
Detection -							1.70	1.70		

Figure 3-1.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
Head Screen Analyses



4.0 Acid Base Accounting

A pulverized portion from each of the three (3) separate core intervals was utilized for Acid Base Accounting (ABA) test work.

The ABA analysis is a static test used to determine the acid producing or acid consuming potential of a mined material.

The ABA analysis is comprised of three distinct determinations. To facilitate the comparison of values, the neutralizing potential, (NP), acid potential (AP) and net neutralization potential (NNP) are expressed in units of metric tonnes $CaCO_3$ equivalent per 1000 metric tonnes of material

1. In the procedure utilized to determine the neutralization potential (NP) of a mined material the sample is treated with an excess of standardized hydrochloric acid (HCl) at ambient temperature for a 24 hour period. During this period, the pH of the sample is checked, to insure that sufficient acid is available for consumption reaction. After the test period, the un-reacted acid is titrated with a standardized base to a neutral pH to calculate the calcium carbonate equivalent of the acid consumed.

2. In calculating the acid potential (AP) of a mined material determinations are made for the percentage of total sulfur, sulfate sulfur, and sulfide sulfur by difference in the test sample. Standards and blanks are used in the sample set to insure accuracy. The acid potential of the sample in tonnes $CaCO_3$ equivalent per 1000 tonnes is given by,

   AP = Percent "Sulfur" x 31.25

   That is assuming that 31.25 tonnes of $CaCO_3$ is needed to neutralize the acid, potentially generated, from 1 tonne of material containing 1 % sulfur.

3. The net neutralization potential (NNP) in tonnes $CaCO_3$, equivalent per 1000 tonnes of material is given by the difference of the neutralization potential and the acid potential.

   NNP = NP – AP

If a negative NNP value is determined, the material may be classified as a potentially acid producing material. Conversely, if the NNP value is positive, then the material may be classified as a potentially acid consuming material. This test does not reflect the long-term acid producing potential of a material due to geological or bacterial degradation.

Data in the table allows for the calculation of two values: acid potential (AP) and net neutralization potential (NNP).

The total sulfur (as %S) provides for the maximum potential acid generating or neutralizing potential of a mined material. The most common way to calculate the overall AP value in the mining industry today is to use the sulfide sulfur content. However, since the calculated sulfide sulfur content is below the analytical detection limit for the core interval identified as Unit Type A (KCA Sample No. 26616) the total sulfur content was utilized to calculate the overall AP value.

The net neutralization potential (NNP - based upon total sulfur content) for the core intervals indicated that the material has a net ability to neutralize or consume acid.

The results of the ABA analyses utilizing pulverized material from each of the three (3) separate core intervals are presented in Table 4-1.

Table 4-1.
Eagle Gold Project
Reject Core Intervals
Acid Base Accounting

		Apr-96							Oct-09						
KCA Sample No.	Unit Type	Total Sulfur, %	Sulfide Sulfur, %	Sulfate Sulfur, %	Paste pH	NP	AP	NNP	Total Sulfur, %	Sulfide Sulfur, %	Sulfate Sulfur, %	Paste pH	NP	AP	NNP
22602	C1	0.34	0.26	<0.01	8.22	47	10.6	36	0.21	0.11	0.10	7.6	51	7	44
22603	B	0.44	0.31	0.13	8.48	40	13.8	26	0.22	0.07	0.15	8.2	50	7	43
22616	A	0.08	<0.01	<0.03	8.47	18	2.5	16	0.05	<0.01	0.05	8.2	17	2	15

Notes: In tonnes CaCO3 equivalent per 1,000 tonnes of material.

Note: Net Neutralization Potential (NNP) = Neutralization Potential (NP) - Acidification Potential (AP).

5.0 Preliminary Agglomeration Test Work

Agglomeration tests were completed on four (4) 2 kilogram portions of the Eagle Gold Master Composite HPGR crushed product (calculated P_{80} 3.641 millimeters).

The crushed material was tested with the addition of 0, 2, 4 and 8 kilograms of Portland Type II cement per metric tonne of ore.

The percolation tests were conducted in small (7.5 cm inner diameter) columns at a range of cement levels with no compressive load applied. The purpose of the percolation tests was to examine the permeability of the material under various cement agglomeration levels.

The non-agglomerated (no cement added) percolation test failed. The percolation tests utilizing material agglomerated with 2, 4 and 8 kilograms of Portland Type II cement per metric tonne of ore passed.

5.1 Agglomeration and Percolation Test Procedure

Agglomeration tests were conducted on 2 kilogram portions of HPGR crushed material (calculated P_{80} 3.641 millimeters). Agglomeration tests were conducted utilizing 0, 2, 4 and 8 kilograms of Portland Type II cement per metric tonne of ore. The procedure used for these tests was as follows:

1. A 2 kilogram split of material was placed into the agglomerating drum and a specified amount of cement was added.

2. The drum was rotated for several minutes to mix the ore and cement thoroughly.

3. The material was sprayed with a solution of tap water to form the agglomerates. The amount of solution required for agglomeration was recorded.

4. The agglomerates were then placed into a 75 millimeter diameter column and the initial ore height was recorded. The agglomerates were allowed to cure for a period of 24 hours.

5. Solution was applied to the column at a rate of 10 - 12 liters per hour per square meter of column surface area for 72 hours. Changes in the height of the ore in the column, agglomerate stability and percolation problems were recorded.

6. After 72 hours of solution application, the sides of the column were tapped sharply until the ore height within the column remained stable. The final ore height was recorded.

7. The exit line from the column was clamped off and the column was flooded with solution to a level equal to 25 - 50 millimeters above the ore surface.

8. The clamp was removed and while the solution level above the ore was maintained, the solution flow rate from the bottom of the column was measured.

5.2 Discussion of Results

The complete results of this test program (including a pass/fail analysis of the information) are shown in Table 5-1.

Over the test period the pH of the effluent solution was monitored. In general a pH below 10 was an indication of a low pH and not acceptable for leaching. However, a high pH (a pH greater than 11.5) would also be noted as high.

In the non-compacted agglomeration tests, KCA generally considers a slump of over 10% as an indication of failure. One item also examined is the consistency of results with regard to slump. KCA would expect a lower slump with higher cement levels.

The slumps calculated for the agglomerated columns were negligible (0% slump was obtained).

The typical heap design solution application rate of 10 - 12 LpHr/m^2 is utilized when examining the agglomeration data. When examining results from this type of agglomeration tests KCA considers a measured flow of one hundred times (100X) the heap design rate as a "pass". A measured flow less than 100X the heap design flow is not necessarily a failure. If there are enough tests with enough consistency between tests, and all other points indicate a "pass", then KCA sometimes will "pass" a test with less than the 100X flow. However, we will never pass a test at 10X and probably not at 50X.

In examining the Pellet Breakdown, it is felt that 10% is marginally acceptable and anything higher is a failure. In general we allow more range in the allowable Pellet Breakdown as this is a subjective value based on the visual observation of the pellets after the test by the technicians performing the test.

Pellet breakdown for the agglomerated column tests for each separate crush size was not significant (less than 3%).

Solution color and clarity typically is an indicator of agglomerate failure. This information is utilized in coordination with both slump as well as Pellet Breakdown to determine if the test passes.

It is believed that these types of tests are indicative of cement requirements for a low, single lift heap height (6 meter maximum) and provide cement levels for larger scale column test work. Compacted permeability tests may be required to evaluate heap heights over 6 meters.

Table 5-1.
Eagle Gold Project
Master Composite
HPGR Crushed Product (Calculated P_{80} = 3.641 millimeters)
Summary of Agglomeration Test Work

KCA Sample No.	KCA Test No.	Description	Top Size of Material, mm	Cement, $kg/MT_{dry\ ore}$	Water Added, mLs	Column Area, m^2	Dry Weight, kg	Initial Height, cm	Ht. on Day 3 of Leaching, cm	Final Height, cm	pH on Day 3	pH Comment	% Slump	Slump Result	Apparent Bulk Density, MT_{dry}/M^3	Flow Out, $LpHr/m^2$	Flow Result	Visual Estimate of % Pellet Breakdown	Pellet Result	Out Flow Solution, Color and Clarity	Solution Result	Overall Test Result
42979	43421 A	Master Composite	3.641	0	0.0	0.005	2.0	27.94	27.94	27.94	N/A	N/A	0%	Pass	1.57	-	Fail	N/A	Fail	N/A	Fail	Fail
	43421 B		3.641	2	154.9	0.005	2.0	31.12	31.12	31.12	11.5	Good	0%	Pass	1.41	10,702	Pass	<3	Pass	Colorless & Clear	Pass	Pass
	43421 C		3.641	4	176.0	0.005	2.0	32.39	32.39	32.39	11.8	High	0%	Pass	1.35	18,237	Pass	<3	Pass	Colorless & Clear	Pass	Pass
	43421 D		3.641	8	167.3	0.005	2.0	33.66	33.66	33.66	12.1	High	0%	Pass	1.30	23,601	Pass	<3	Pass	Colorless & Clear	Pass	Pass

6.0 Column Leach Test Work

A single column leach test was completed utilizing the Eagle Gold Master Composite HPGR crushed product (calculated P_{80} 3.641 millimeters).

The material utilized for the column leach test was agglomerated with 2 kilograms of Portland Type II cement per metric tonne of ore prior to loading into the column.

Following the leaching period, detoxification test work utilizing a hydrogen peroxide (copper catalyzed peroxide) detoxification method was completed. The detoxification procedure was continued until a WAD cyanide value less than 0.2 mg/L was obtained for three (3) consecutive days.

The final barren solution and the final detox solution, for each separate column leach test were analyzed for a Profile II metals analysis, total cyanide and Weak Acid Dissociable (WAD) cyanide. The column tailings after detoxification were submitted for Humidity Cell Testing (HCT). The HCT test work was on-going at the time of this report.

The column leach test is described in Table 6-1.

Table 6-1.
Eagle Gold Project
Master Composite
Column Leach Test Parameters

KCA Sample No.	KCA Test No.	Crush Size, mm	Column Diameter, meters	Initial Charge Height, meters	Charge Weight, kilograms
42979	43276	100% minus 12.5	0.203	1.702	80.00

Note: Calculated P_{80} based upon head screen analysis – 3.641 millimeters.

6.1 Column Leach Test Recoveries

Column tailings assays were not available for this report as the HCT test work was on-going at the time of this report.

Column test recoveries for this report were based upon the average head screen analysis data as shown in Table 6-1.

Table 6-2.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
Minus 12.5 millimeter Crushed Material (Calculated P_{80} = 3.641 millimeters)
Head Screen Analysis with Assays by Size Fraction

KCA Sample No.	Description	Calc. P_{80} Size, mm	Weighted Avg. Head Assay, gms Au/MT	Weighted Avg. Head Assay, gms Ag/MT
42979	Master Composite	3.641	0.506	1.79

Preliminary results for the column leach test are presented in Table 6-1.

Gold recovery for the Master Composite column test, utilizing material crushed utilizing a High Pressure Grinding Roll (HPGR) to minus 12.5 millimeters was 96% after 33 days of leaching. This recovery was based upon an estimated head grade of 0.506 gms Au/MT. Sodium cyanide consumption was 0.40 kg/MT and cement addition was 2.0 kg/MT.

Column test recovery results contained in the body of this report were based upon carbon assays vs. the estimated head as no tailings assays were available. Recovery results contained in the attached appendix (Appendix A) were based upon the daily solution assays vs. an estimated calculated head (solution assays + estimated tailings assays).

When an outside party submits samples, KCA can estimate gold recovery for an ore body based upon the assumption that the ore to be mined will be similar to the samples tested. For feasibility study purposes, KCA normally discounts laboratory gold recoveries by two to three percentage points when estimating field recoveries. This assumes a well-managed heap leach operation, and if agglomeration is required, it is assumed that this process is completed correctly.

Based upon KCA's experience with mostly clean non-reactive ores, cyanide consumption in production heaps would be only 25 to 33 percent of the laboratory column test consumptions. For ores containing high amounts of leachable copper, higher factors would be utilized.

Table 6-3.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
KCA Test No. 43276
Minus 12.5 millimeter Crushed Material (Calculated P_{80} = 3.641 millimeters)
Cyanide Column Leach Test
Metal Recoveries and Chemical Consumption

Days Leaching	Cumulative, t_s/t_o	Solution Extraction, gms Au/MT	Carbon Weight, grams	Metal on Carbon Extraction, gms Au/MT	Extraction, % Au	Cumulative Extraction, % Au	NaCN Consumed, kg/MT	Cement Added, kg/MT
0-9	1.00	0.343	185.57	0.418	83%	83%	0.17	2.00
9-20	2.32	0.030	167.98	0.043	8%	91%	0.10	0.00
21-33	3.79	0.020	182.19	0.025	5%	96%	0.13	0.00
	Total:	0.393		0.486			0.40	2.00
	Estimated Tail:	0.020		0.020				
	Estimated Head:	0.413		0.506				

t_s/t_o = Tonnes of solution effluent per tonne of dry ore leached.

Days Leaching	Cumulative, t_s/t_o	Solution Extraction, gms Ag/MT	Carbon Weight, grams	Metal on Carbon Extraction, gms Ag/MT	Extraction, % Ag	Cumulative Extraction, % Ag	NaCN Consumed, kg/MT	Cement Added, kg/MT
0-9	1.00	0.09	185.57	0.11	6%	6%	0.17	2.00
9-20	2.32	0.00	167.98	0.01	1%	7%	0.10	0.00
21-33	3.79	0.01	182.19	0.00	0%	7%	0.13	0.00
	Total:	0.10		0.13			0.40	2.00
	Estimated Tail:	1.66		1.66				
	Estimated Head:	1.76		1.79				

t_s/t_o = Tonnes of solution effluent per tonne of dry ore leached.

Column Parameters

KCA Sample No.	42979	KCA Test No.	43276
Dry Weight Ore, kg:	80.00	Column Area, m^2:	0.032
Initial Ore Height, m:	1.702	Column Volume (initial), m^3:	0.055
Final Ore Height, m:	1.702	Column Volume (final), m^3:	0.055
Slump, %:	0.0%	Apparent Bulk Density (final), MT_{dry}/m^3:	1.450
Cement Addition, kg/MT:	2.00	Retained Moisture, L/MT_{dry}:	n/a
Agglom. Water Added, liters (1 gpL NaCN):	4.15	Mercury on C-1 Carbon, mg/kg:	0.98
Hydrated lime added during loading, kg/MT:	0.00	Final Percolation Rate, $L/Hr/m^2$:	n/a

6.2 Cyanide Column Leach Tests, Description of Apparatus

6.2.1 Drip Leach Test Apparatus

The column tests were run as a continuously drained drip leach tests.

This type of test most accurately reflects actual heap leach conditions and is normally run when the material contains enough fines to prevent channeling of solution down individual rock faces.

The apparatus used for this test is shown schematically in Figure 6-1.

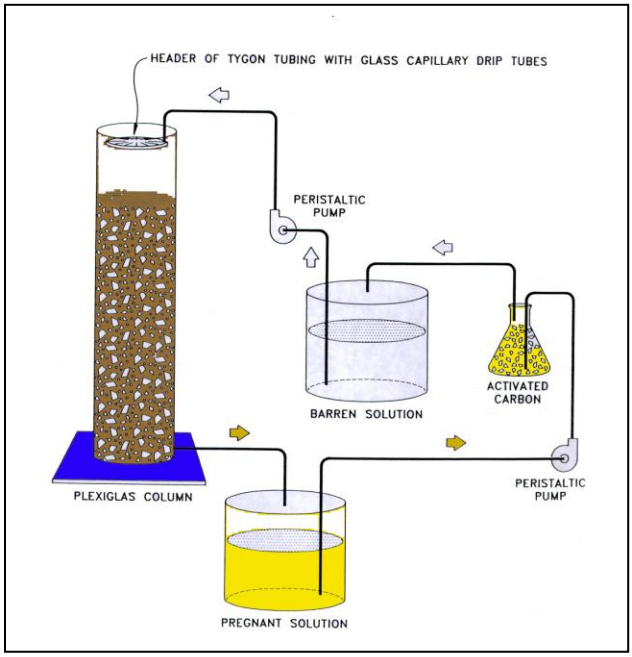
6.2.2 Column Setup

The material to be leached was placed into a Plexiglas column with an inside diameter of 203.2 millimeters (cross sectional area of 0.032 square meters).

Alkaline cyanide solution was continuously distributed onto the material through a header of Tygon tubing with glass-capillary drip tubes. Flow rate of solution dripping onto the material was controlled with a peristaltic pump to approximately 10-12 liters per hour per square meter of column surface (target flow rate of 10 liters per hour per square meter of column surface).

The solution exiting the leach column was collected in the bottom (floor – pregnant leach solution) tank. Leach solution was checked each cycle for pH, NaCN, Au and Ag. Copper was checked periodically. The solution was then passed through a bottle of activated carbon over a period of 24 hours to recover the gold and silver in solution. After passing through the bottle of activated carbon, the solution was re-assayed for pH, NaCN, Au and Ag. Sodium cyanide was then added, if necessary, to maintain the solution at "target" levels (discussed in the History section). The leach solution was then recycled to the material for another 24 hour leach period. Two (2) batches of leach solution were used so that while one batch was applied to the column, the other was run through the carbon.

Figure 6-1.
Eagle Gold Project
Column Leach Test Apparatus



6.3 History of Cyanide Column Leach Tests

6.3.1 Start-up of Tests

The initial leach solution for the column tests contained 1.0 grams sodium cyanide per liter of solution.

6.3.2 Solution Color and Clarity

The initial and final solution color and clarity were monitored for each column test.

The solution color and clarity for the column tests are summarized in Table 6-9.

Table 6-9.
Eagle Gold Project
Master Composite
Cyanide Column Leach Test Work
Effluent Solutions, Color and Clarity

KCA Sample No.	KCA Test No.	Color and Clarity of Initial Column Effluent	Color and Clarity of Final Column Effluent
42979	43276	Clear and Yellow	Clear and Yellow

A "colorless and clear" solution exiting the columns is indicative of the fact that no fines migrated within the column of ore. Metal buildup in solution is usually denoted by a significant color change in the solution (i.e. a yellow color is typically indicative of higher levels of iron and a light blue solution might be indicative of a solution containing higher levels of copper). The absence of color could be indicative that no build up of metals in solution occurred during leach.

6.4 Copper Analyses in Solutions

Interim pregnant (effluent) cyanide leach solutions were assayed (solution analysis by flame atomic absorption spectrophotometer methods) periodically for copper content.

The lowest and highest copper values in solution data obtained over the leach period are summarized in Table 6-10.

Table 6-10.
Eagle Gold Project
Master Composite
Cyanide Column Leach Test Work
Copper Concentration in Column Leach Solutions

KCA Sample No.	KCA Test No.	Low Copper, mg/L	High Copper, mg/L
42979	43276	3.87	21.8

Copper minerals dissolve in cyanide solutions at varying rates and to varying degrees. Copper in cyanide leach solutions is not desirable as copper can consume sodium cyanide, consume dissolved oxygen, decrease precious metal dissolution rates, interfere with solution processing techniques and end up in the final doré. At ambient temperatures copper dissolution is generally highest for the carbonate copper minerals Azurite and Malachite going to lower dissolutions for copper silicates (Chrysocolla) and copper iron sulfides (Chalcopyrite). In cyanide starved systems the presence of Chalcopyrite can act to remove gold from solution (preg-rob). Chalcocite mineralization typically shows a copper dissolution of greater than 90%.

The range of copper in solution obtained for this series of column leach tests would be considered low and generally not note worthy in relationship to the processing of the material. The low copper in solution values obtained during the column leach tests confirmed the results obtained for copper in the head analyses.

6.5 Cyanide Strength and Alkalinity

The initial leach solution for the column test contained 1.0 grams sodium cyanide per liter of leach solution. Cyanide strength of the on-flow solutions was then maintained at 0.5 grams per liter sodium cyanide. Protective alkalinity in the tests was maintained by the initial addition of hydrated lime. The leach solution was monitored to ensure that it was in the pH range of 10-11.

Reagent consumption data for the column leach tests are summarized in Table 6-11.

Table 6-11.
Eagle Gold Project
Master Composite
Cyanide Column Leach Test Work
Column Leach Tests, Reagent Consumptions

KCA Sample No.	KCA Test No.	NaCN Consumed, kg/MT	Hydrated Lime Added, kg/MT	Cement Added, kg/MT
42979	43276	0.40	0.00	2.00

6.6 Mercury Analyses

The granular activated carbon samples utilized for the column tests for precious metal adsorption were air dried and then assayed for mercury as well as precious metal content.

The results of the mercury and gold analyses on the individual carbon samples are summarized in Table 6-12. The ratio of gold adsorbed to mercury adsorbed is also presented.

Table 6-12.
Eagle Gold Project
Master Composite
Cyanide Column Leach Test Work
Mercury Concentrations

KCA Sample No.	KCA Test No.	Carbon Period	Carbon Weight, grams	Carbon Assay, grams Au/MT	Carbon Assay, gms Hg/MT	Ratio Au : Hg
42979	43276	C-1	185.57	180.26	0.98	184
		C-2	167.98	20.43	0.59	35
		C-3	182.19	10.83	0.29	37

6.7 Percent Slump and Final Apparent Bulk Density

The height of material in the column test was measured before and after leaching. This height was utilized to calculate the "slump" during leaching as well as to calculate the final apparent bulk density for the material in the column.

The height, slump and final apparent bulk density from the column leach tests are summarized in Table 6-13.

The percent slump of a column gives an indication of potential permeability problems in production heaps. KCA typically classifies slumps larger than 10% as high. The calculated percent slump values for the Eagle Gold column leach tests were low, ranging from 0% to 0.8%.

Table 6-13.
Eagle Gold Project
Master Composite
Cyanide Column Leach Test Work
Percent Slump and Final Apparent Bulk Density

KCA Sample No.	KCA Test No.	Crush Size, mm	Initial Ht., meters	Final Ht., meters	Slump, %	Final Apparent Bulk Density, MTdry/m^3
42979	43276	-12.5	1.702	1.702	0.0%	1.449

7.0 Detoxification Test Work

7.1 Leachate Chemistry

As outlined in Section 6.0 of this report, the cyanide column leach test was conducted as a two (2) batch leach solution closed circuit test.

Alkaline cyanide solution was continuously distributed onto the material through a header of Tygon tubing with glass-capillary drip tubes utilizing a peristaltic pump.

The leachate or pregnant leach solution (PLS) exiting the leach column was collected in the bottom tank. The PLS was checked each cycle for pH, gold, silver and sodium cyanide.

The solution was then passed through a bottle of activated carbon over a period of 24 hours to recover the gold and silver in solution. After passing through the bottle of activated carbon, the solution was re-assayed for pH, gold silver and sodium cyanide. Sodium cyanide was then added, if necessary, to maintain the solution at "target" levels. The leach solution was then recycled to the material for another 24 hour leach period.

Two (2) batches of leach solution were used so that while one batch was applied to the column, the other was run through the carbon.

A portion of the PLS from the Eagle Gold Master Composite HPGR crushed product column test was sampled twice weekly for Profile II analysis beginning on day 10 of the column leach test.

Following the active leach period (the period where the PLS was passed through activated carbon to recover the gold and silver in solution) the PLS from the column leach test was continuously recycled through the column at an application rate of 10 $L/hr/M^2$ for four (4) consecutive days (day 33-36 of the column leach test).

The recycled PLS (Batch 2) was then combined with the final barren solution from the active leach period (Batch 1). A portion of the combined solution was submitted for a Profile II analysis.

The remaining combined solution was then continuously applied to the column at an application rate of 10 $L/hr/M^2$. The PLS was sampled daily for a Profile II analysis. The PLS was recycled until the solution constituents approached equilibrium.

The final recycled PLS was combined with the remaining feed solution. The composite solution was measured and assayed for copper, iron, Weak Acid Dissociable (WAD) cyanide and total cyanide. A portion of the composite solution was submitted for a designated suite analysis. The remaining solution was utilized for detoxification test work.

The Profile II analyses for the PLS are presented in Table 7-1.

Table 7-1
Eagle Gold Project
Master Composite
KCA Sample No. 42979
KCA Test No. 43276
Leachate Chemistry

Parameter	Units	1-Dec	4-Dec	8-Dec	15-Dec	18-Dec	22-Dec	24-Dec	28-Dec	29-Dec	30-Dec	31-Dec	1-Jan	2-Jan	3-Jan	4-Jan	5-Jan	5-Jan Comp
Aluminum	mg/L	0.3	<0.3	<0.3	<0.3	<0.2	<0.2	0.1	0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Antimony	mg/L	0.012	0.015	0.013	0.031	0.036	0.059	0.054	0..062	0.068	0.075	0.076	0.080	0.085	0.094	0.092	0.099	0.095
Arsenic	mg/L	0.02	0.03	0.03	0.15	0.17	0.11	0.14	0.12	0.28	0.31	0.24	0.30	0.31	0.35	0.33	0.30	0.27
Barium	mg/L	0.71	0.058	0.057	0.083	0.064	0.072	0.06	0.051	0..061	0.065	0.056	0.062	0.061	0.070	0.076	0.067	0.069
Beryllium	mg/L	<0.005	<0.005	<0.005	<0.005	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004	<0.004
Bismuth	mg/L	<0.5	<0.5	<0.5	<0.5	<0.4	<0.4	<0.2	<0.2	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4
Boron	mg/L	<0.3	<0.3	<0.3	<0.3	<0.2	<0.2	<0.1	<0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Cadmium	mg/L	0.019	0.009	0.012	0.007	0.007	0.007	0.007	0.008	0.009	0.009	0.009	0.009	0.009	0.010	0.010	0.010	0.010
Calcium	mg/L	260	220	200	240	220	180	180	140	190	200	170	170	170	190	210	200	200
Chromium	mg/L	0.035	0.03	0.027	0.02	0.013	0.012	0.014	0.014	0.013	0.013	0.010	0.010	0.009	0.009	0.008	0.008	0.008
Cobalt	mg/L	0.9	0.86	0.9	0.83	0.30	0.69	0.65	0.85	0.73	0.77	0.74	0.82	0.72	0.76	0.81	0.74	0.73
Copper	mg/L	8.8	7.9	9	6.6	5.3	7.5	7.7	8.6	9.0	9.1	9.2	9.3	9.3	9.3	9.8	8.3	8.3
Gallium	mg/L	<0.5	<0.5	<0.5	<0.5	<0.4	<0.4	<0.2	<0.2	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4
Iron	mg/L	1.7	1.7	1.8	1.9	1.6	2.1	1.9	2.2	2.3	2.4	2.2	2.2	2.2	2.2	2.4	2.6	2.5
Lanthanum	mg/L	<0.3	<0.3	<0.3	<3	<0.2	<0.2	<0.1	<0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Lead	mg/L	0.017	0.009	0.007	0.006	0.008	0.005	0.004	<0.004	<0.004	0.010	<0.004	0.008	0.004	<0.004	<0.004	<0.004	0.006
Lithium	mg/L	<0.5	<0.5	<0.5	<0.5	<0.4	<0.4	<0.2	<0.2	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4
Magnesium	mg/L	<3	<3	<3	<3	<2	<2	<1	<1	<2	<2	<2	<2	<2	<2	<2	<2	<2
Manganese	mg/L	0.01	<0.01	0.01	<0.01	<0.004	<0.004	<0.004	0.008	<0.004	<0.004	0.019	<0.008	<0.008	0.017	<0.008	<0.004	<0.004
Mercury	mg/L	0.0023	0.0012	0.001	0.0014	0.0012	<0.0002	0.0008	0.0003	0.0006	0.0008	0.0003	0.0005	0.0006	0.0010	0.0013	0.0009	0.0011
Molybdenum	mg/L	0.22	0.21	0.23	0.22	0.21	0.22	0.22	0.25	0.24	0.24	0.23	0.24	0.24	0.25	0.25	0.25	0.25
Nickel	mg/L	0.1	0.062	0.056	0.053	0.048	0.033	0.040	0.037	0.068	0.058	0.064	0.079	0.080	0.091	0.10	0.10	0.10
Potassium	mg/L	26	25	23	27	27	26	25	25	24	25	25	25	26	28	31	32	32
Scandium	mg/L	<0.3	<0.3	<0.3	<0.3	<0.2	<0.2	<0.1	<0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Selenium	mg/L	0.09	0.08	0.08	0.06	0.06	0.06	0.06	0.07	0.074	0.076	0.07	0.073	0.076	0.078	0.079	0.07	0.08
Silver	mg/L	0.017	0.01	0.009	0.006	<0.004	<0.004	<0.004	<0.004	0.004	<0.004	<0.004	0.006	0.005	0.006	0.007	0.007	0.007
Sodium	mg/L	400	390	380	520	570	640	700	730	650	660	610	630	650	690	770	760	780
Strontium	mg/L	8.4	6.7	6.1	3.2	6.1	5.5	5.6	5.2	5.2	5.4	4.9	5.1	5.1	5.5	6.2	6.0	6.1
Thallium	mg/L	<0.003	<0.003	<0.003	<0.003	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002	<0.002
Tin	mg/L	<0.5	<0.5	<0.5	<0.5	<0.4	<0.4	<0.2	<0.2	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4	<0.4
Titanium	mg/L	<0.3	<0.3	<0.3	<0.3	<0.2	<0.2	<0.1	<0.1	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Vanadium	mg/L	0.046	0.061	0.082	0.11	0.12	0.1	0.11	0.12	0.11	0.1	0.11	0.11	0.11	0.11	0.10	0.097	0.096
Zinc	mg/L	8.8	6.7	7.8	5.7	6.0	6.2	6.2	6.7	7.5	7.7	7.4	7.8	7.7	7.8	8.0	7.8	7.8
pH	units	11.3	10.9	10.9	10.7	10.8	10.7	10.7	10.6	10.2	10.3	10.4	10.6	10.5	10.6	10.3	10.3	--
Free NaCN	g/L	0.58	0.44	0.38	0.53	0.55	0.48	0.45	0.37	0.43	0.45	0.31	0.36	0.33	0.46	0.59	0.41	--
Volume	L	10.83	9.37	10.11	8.46	9.43	8.85	9.38	16.1	8.44	8.11	7.34	7.99	6.51	9.09	8.02	6.65	--
Type	2 Batch System	P	P	P	P	P	P	P	P/B	P	P	P	P	P	P	P	P	P
Comments									Feed	Effluent 1	Effluent 2	Effluent 3	Effluent 4	Effluent 5	Effluent 6	Effluent 7	Effluent 8	Effluent 8 + Remaining Feed

Note: P/B - preg and barren combined - 28 December 2009.

Note: Metals Analyses only.

7.2 Detoxification Test Work

Detoxification test work utilizing a hydrogen peroxide (copper catalyzed peroxide) detoxification method was conducted on the column leach test residue.

The final recycled PLS was combined with the remaining feed solution. The combined solution was measured and assayed for copper, iron, Weak Acid Dissociable (WAD) cyanide and total cyanide. A portion of the combined solution was submitted for a designated suite analysis.

Based upon the copper and total cyanide analysis, copper sulfate pentahydrate ($CuSO_4.5H_2O$) and hydrogen peroxide (35% H_2O_2) were added to the remaining composite solution from the column leach test to reduce the WAD cyanide to less than 0.2 mg/L.

Copper sulfate pentahydrate ($CuSO_4.5H_2O$) was added to the composite solution to produce an overall copper level in solution of 20% of the WAD cyanide concentration. Hydrogen peroxide was added at a level equivalent to 300% of theoretical based upon the total cyanide level. The solution was then sparged with air and mixed for a period of four hours in an open vessel. After the four hour time period the solution was assayed for residual hydrogen peroxide and WAD cyanide before being cycled onto the column (Phase I).

The detoxification effluent was measured daily (days 1-6). Hydrogen peroxide and copper were added daily to the effluent based upon the initial total cyanide and copper levels. The effluents from day 7 and 8 of the detoxification period were measured, combined, assayed for copper, iron, Weak Acid Dissociable (WAD) cyanide, total cyanide and sampled for the designated suite analysis.

Based upon the copper and total cyanide analysis, copper sulfate pentahydrate was added to the composite solution to produce an overall copper level in solution of 20% of the WAD cyanide concentration. Hydrogen peroxide was added at a level equivalent to 500% of theoretical based upon the total cyanide level. The solution was sparged with air and mixed for a period of four hours in an open vessel. After the four hour time period the solution was assayed for residual hydrogen peroxide and WAD cyanide before being cycled onto the column (Phase II).

The detoxification procedure was continued until a WAD cyanide value less than 0.2 mg/L was obtained for three (3) consecutive days (Phase I-III). Following detoxification, the column was allowed to completely drain down. The final detoxification solution (final effluent plus drain down solutions) was sampled for the designated suite analysis.

The column was allowed to rest for a seven (7) day period prior to initiating modified Humidity Cell Testing (HCT).

The initial and final values for total and WAD cyanide are presented in Table 7-2.

Table 7-2.
Eagle Gold Project
Master Composite
HPGR Crushed Material
Summary of Detoxification Test Results
Total and WAD Cyanide

KCA Sample No.	KCA Test No.	Description	Detoxification Period, Days	Initial Total Cyanide, mg/L	Final Total Cyanide, mg/L	Initial WAD Cyanide, mg/L	Final WAD Cyanide, mg/L
42979	43276	Master Composite	27	288.6	2.07	268.4	0.16

7.3 Detoxification Procedure

The Master Composite HPGR column leach test (KCA Test No. 43276) was treated as follows:

1. The final recycled PLS was combined with the remaining feed solution. The combined solution was measured and assayed for copper, iron, WAD and total cyanide. A portion of the combined solution was submitted for a designated suite analysis.

2. Based upon the total cyanide and copper analysis, hydrogen peroxide and copper, if needed, were added to detoxify the combined solution, (copper catalyzed peroxide). The solution was then sparged with air and mixed for a period of four hours in an open vessel. After the four hour time period the solution was assayed for residual hydrogen peroxide and WAD cyanide before being cycled onto the column.

3. The columns were then restarted with the detoxified solution. Daily additions of hydrogen peroxide and copper were added to the leach solution based on the initial total cyanide and copper values. Solution circulation through the column material was continued.

4. Every seven (7) days thereafter, the effluent solutions from the two batch cycle were combined, sampled and analyzed. The hydrogen peroxide and copper additions were adjusted accordingly. Detoxification continued until a WAD cyanide value less than 0.2 mg/L was obtained for three (3) consecutive days.

5. The final detoxification solution (final effluent plus drain down solutions) were combined, thoroughly mixed and sampled for the designated suite analysis, WAD and total cyanide analyses.

6. The column was allowed to rest for a seven (7) day period prior to initiating modified Humidity Cell Testing (HCT).

Total chemical additions are summarized in Table 7-3.

Table 7-3.
Eagle Gold Project
Master Composite
HPGR Crushed Material
Detoxification Test Work
Summary of Chemical Additions

KCA Sample No.	KCA Test No.	Column Weight, kg	35% H_2O_2 Applied, gms	10 gpL $CuSO_4.5H_2O$, mLs	100% H_2O_2 Applied, gms/MT	Copper Added, gms/MT
42979	43276	80	147.05	489	643	16

Daily detoxification data showing total and WAD cyanide analyses and chemical additions for the column are presented in Table 7-4 and Table 7-5.

Chemical additions of 35% H_2O_2 are reported in grams, (gms) added and copper, as 10g/L $CuSO_4.5H_2O$, are reported in milliliters, (mL), added. The complete results can be found in the Appendix.

The wet chemistry and metals analyses, total cyanide and weak acid dissociable cyanide analyses for the final recycled PLS solution, interim detoxification solutions and final detoxification solution are presented in Table 7-6.

Table 7-4.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
KCA Test No. 43276
HPGR Crushed Material (Calculated P_{80} = 3.641 millimeters)
Daily Detoxification Data

Date	Description	P/D*	Cycle	pH	Free NaCN, gpL	Volume, kg	100% H_2O_2, grams	Cu, grams	WAD, mg/L	WAD, grams	Total, mg/L	Cu, mg/L	Fe, mg/L	H_2O_2, mg/L	Sample mLs out	Add H_2O_2:WAD CN	$CuSO_4$, mLs	35% H_2O_2, grams	Volume, kg
5-Jan	Start Detox	P	0	10.3	0.40	14.67			268.40	3.937	288.60	8.79	2.29		900				
6-Jan	Detox w/ Anal.	P/1	1	10.3	0.40	13.69	15.57	0.61	268.40	3.674	288.60	8.79	2.29		--	4	240.00	44.50	
7-Jan		D	2	8.5	<0.01	13.93			3.22	0.045		5.01	0.00	8	125				
8-Jan	Detox 1	P	3	10.4	0.39	6.26	7.12	0.14				8.31	2.30		50		55	20.35	6.26
9-Jan		D		8.5	<0.01	6.34						6.61	1.24	12	50				
9-Jan	Detox 1	P	4	10.6	0.16	7.71	8.77	0.17				2.37	0.00		50		68	25.06	7.71
10-Jan		D		8.5	<0.01	7.72						3.62	0.01	12	50				
10-Jan	Detox 1	P	5	10.5	0.11	6.65	7.56	0.15				1.26	0.47		50		59	21.61	6.65
11-Jan		D		8.5	<0.01	6.70						3.68	0.02	12	50				
11-Jan	Detox 1	P	6	10.0	0.17	7.65	8.70	0.17				1.16	0.27		50		67	24.86	7.65
12-Jan		D		8.5	<0.01	7.74						3.25	0.00	2	50				
12-Jan	Period 2	P	7	10.6	0.03	6.41						0.59	0.11		50				6.41
13-Jan	Period 2	P		10.6	0.01	8.18						0.42	0.15		50				8.18
13-Jan	Detox w/ Anal.	P/2	8	10.6	0.01	14.60	0.61	0.00	2.79	0.041	5.98	0.59	0.16		850	15	0	1.74	
14-Jan		D		10.0	<0.01	14.38			0.57	0.008	4.00	0.03	0.00	<1	250				
15-Jan	Detox 2	P	9	10.2	0.04	6.44	0.27	0.00				0.32	0.08		50		0	0.77	6.44
16-Jan		D		10.0	<0.01	6.44						0.46	0.00	<1	50				
16-Jan	Detox 2	P	10	10.0	0.02	7.51	0.31	0.00				0.16	0.04		50		0	0.90	7.51
17-Jan		D		10.0	<0.01	7.51						0.08	0.00	<1	50				
17-Jan	Detox 2	P	11	10.1	0.01	5.88	0.25	0.00				0.21	0.06		50		0	0.71	5.88
18-Jan		D		8.5	<0.01	5.88						0.90	0.00	<1	50				
18-Jan	Detox 2	P	12	10.2	0.01	5.22	0.22	0.00				0.21	0.05		50		0	0.63	5.22
19-Jan		D		8.6	<0.01	5.22						0.51	0.02	<1	50				
19-Jan	Detox 2	P	13	10.1	0.02	6.07	0.26	0.00				0.36	0.04		50		0	0.73	6.07
20-Jan		D		8.5	<0.01	6.07						0.04	0.00	<1	50				
20-Jan	Detox 2	P	14	10.1	<0.01	4.22	0.18	0.00				0.96	0.00		50		0	0.51	4.22
21-Jan		D		8.6	<0.01	4.22						0.11	0.00	<1	50				
21-Jan	Period 3	P	15	9.9	<0.01	4.63						0.04	0.06		50				4.63
22-Jan	Period 3	P		9.9	<0.01	4.92						0.02	0.01		50				4.92
22-Jan	Detox w/ Anal.	P/3	16	9.9	<0.01	9.55	0.40	0.00	0.38	0.004	4.05	0.03	0.02		850	111	0	1.15	

Note: P = Pregnant Solution and D = Detox Solution.

Table 7-5.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
KCA Test No. 43276
HPGR Crushed Material (Calculated P_{80} = 3.641 millimeters)
Daily Detoxification Data

Date	Description	P/D*	Cycle	pH	Free NaCN, gpL	Volume, kg	100% H_2O_2, grams	Cu, grams	WAD, mg/L	WAD, grams	Total, mg/L	Cu, mg/L	Fe, mg/L	H_2O_2, mg/L	Sample mLs out	Add H_2O_2:WAD CN		$CuSO_4$, mLs	35% H_2O_2, grams	Volume, kg
23-Jan		D		8.8	<0.01	8.70			0.11	0.001	3.14	0.00	0.00	<1	250					
24-Jan	Detox 3	P	17	10.2	<0.01	5.00	0.21	0.00				0.00	0.04		25			0	0.60	5.00
25-Jan		D		8.2	<0.01	5.00						0.27	0.00	<1	25					
25-Jan	Detox 3	P	18	10.1	<0.01	4.93	0.21	0.00				0.00	0.00		25			0	0.59	4.93
26-Jan		D		8.9	<0.01	4.93						0.00	0.00	<1	25					
26-Jan	Detox 3	P	19	9.9	<0.01	5.05	0.21	0.00				0.57	0.00		25			0	0.61	5.05
27-Jan		D		8.6	<0.01	5.05						0.00	0.00	<1	25					
27-Jan	Detox 3	P	20	9.6	<0.01	4.64	0.20	0.00				0.39	0.00		25			0	0.56	4.64
28-Jan		D		8.4	<0.01	4.64						0.03	0.00	<1	25					
28-Jan	Detox 3	P	21	9.8	<0.01	4.76	0.20	0.00				0.01	0.00		25			0	0.56	4.76
29-Jan		D		8.5	<0.01	4.76						0.08	0.00	<1	25					
29-Jan	Detox 3	P	22	9.8	<0.01	5.11	0.21	0.00				0.00	0.00					0	0.61	5.11
30-Jan		D		8.6	<0.01	5.11						0.00	0.00	<1	25					
30-Jan	Period 4	P	23	9.8	<0.01	5.00						0.08	0.00		25					5.00
31-Jan	Period 4	P		9.8	<0.01	4.87						0.08	0.00		25					4.87
1-Feb	Cycle w/ Anal.	P/4	24	9.8	<0.01	9.87			0.16	0.002	2.07	0.08	0.03			0				
Total -							51.44	1.24										489	147.05	127.11

Note: P = Pregnant Solution and D = Detox Solution.

Table 7-6.
Eagle Gold Project
Master Composite
KCA Sample No. 42979
KCA Test No. 43276
HPGR Crushed Material (Calculated P_{80} = 3.641 millimeters)
Detoxification Solution Analyses

Parameter	Units	WETLAB 1001034-001 5-Jan-10	WETLAB 1001094-001 13-Jan-10	WETLAB 1001201-001 22-Jan-10	WETLAB 1002002-001 1-Feb-10
Cyanate	mg/L	27	69	390	210
Thiocyanate	mg/L	120	310	<100	<100
Ammonia, as nitrogen	mg/L	46	44	71	60
pH	Units	10.38 (10.3)	10.00 (10.6)	9.18 (9.9)	9.85
Bicarbonate (HCO_3)	mg/L	<1.0	6.0	70.0	<1.0
Carbonate (CO_3)	mg/L	190	100	34	49
Hydroxide (OH)	mg/L	84	<1.0	<1.0	6.0
Total Alkalinity	mg/L as $CaCO_3$	570	170	110	99
Chloride	mg/L	35	30	39	44
Fluoride	mg/L	<1.0	<1.0	<0.50	<0.50
Sulfate	mg/L	990	1000	1400	1400
Nitrate Nitrogen	mg/L	<10	<10	2.9	2.9
Nitrite Nitrogen	mg/L	0.43	0.61	2.1	1.7
Total Kjeldahl Nitrogen	mg/L	74	130	130	99
Total Nitrogen	mg/L	75	130	140	100
Total Cyanide	mg/L	380 (288.60)	290 (5.98)	0.82 (4.05)	0.33 (2.07)
Total Dissolved Solids (TDS)	mg/L	2500	2300	2800	2600
WAD Cyanide	mg/L	280 (268.40)	1.3 (2.79)	0.3 (0.38)	0.11 (0.16)
Silica	mg/L	28	26	25	27
Aluminum	mg/L	0.090	0.072	<0.045	0.047
Barium	mg/L	0.061	0.049	0.059	0.056
Beryllium	mg/L	<0.0010	<0.0010	<0.0010	<0.0010
Bismuth	mg/L	<0.10	<0.10	<0.10	<0.10
Boron	mg/L	<0.10	<0.10	<0.10	<0.10
Cadmium	mg/L	0.0055	<0.0010	<0.0010	<0.0010
Calcium	mg/L	180	150	200	170
Chromium	mg/L	0.014	0.013	0.0057	0.0050
Cobalt	mg/L	0.86	0.81	1.0	0.96
Copper	mg/L	9.1 (8.79)	0.55 (0.59)	0.11 (0.03)	<0.050 (0.08)
Gallium	mg/L	<0.10	<0.10	<0.10	<0.10
Iron	mg/L	2.6 (2.29)	0.12 (0.16)	0.062 (0.02)	0.034 (0.03)
Lead	mg/L	<0.010	<0.010	<0.010	<0.010
Lithium	mg/L	<0.10	<0.10	<0.10	<0.10
Magnesium	mg/L	<0.50	<0.50	<0.50	<0.50
Manganese	mg/L	<0.0050	<0.0050	<0.0050	<0.0050
Molybdenum	mg/L	0.22	0.19	0.25	0.22
Nickel	mg/L	0.095	0.019	<0.010	<0.010
Phosphorous	mg/L	<0.50	<0.50	<0.50	<0.50
Potassium	mg/L	34	25	30	27
Scandium	mg/L	<0.10	<0.10	<0.10	<0.10
Silver	mg/L	0.0085	<0.0050	<0.0050	<0.0050
Sodium	mg/L	780	640	780	710
Strontium	mg/L	6.1	4.3	6.1	5.1
Tin	mg/L	<0.10	<0.10	<0.10	<0.10
Titanium	mg/L	<0.10	<0.10	<0.10	<0.10
Vanadium	mg/L	0.094	0.1	0.068	0.061
Zinc	mg/L	8.2	<0.010	<0.010	0.024
Mercury	mg/L	0.086	0.076	0.059	0.079
Antimony	mg/L	0.095	0.13	0.17	0.27
Arsenic	mg/L	0.15	0.56	0.45	0.67
Selenium	mg/L	0.068	0.055	0.070	0.069
Thallium	mg/L	<0.0010	<0.0010	<0.0010	<0.0010
Uranium	mg/L	<0.0020	<0.0020	<0.010	<0.010

Notes: KCA results shown in ( ). Increase in results shown in red. Analysis ? Shown in blue.

8.0 Humidity Cell Test Work

Following cyanidation and detoxification, the metallurgical column was converted to a large scale modified humidity column by SRK Consulting. The protocol for the modification and test work results are provided in the SRK Consulting report entitled Geochemical Characterization and Water Quality Predictions for the Eagle Gold Project prepared for Stantec and Victoria Gold Corp, November 2010.

9.0 Assaying Procedures

9.1 Heads and Tails

Head assays were run as one assay ton fire assays on duplicate splits for gold and silver. For gold analyses gravimetric and AA finish were utilized. The silver analyses were completed by gravimetric finish.

Tailings assays were run as one assay ton fire assays on duplicate splits for gold and silver analyses by standard fire assay methods with flame atomic absorption spectrophotometer (FAAS) finish for gold and gravimetric and four (4) acid digestion finish for silver.

9.2 Carbon Assays

The loaded granular activated carbon was dried and weighed. Two samples were split out and assayed and the remainder saved for reference. The carbon for assay was roasted to convert it to ash, then conventionally fire assayed.

9.3 Solution Assays

Solution assays were made every cycle on an atomic absorption spectrophotometer, using gold and silver standards. The solution assays were used merely to check on the progress of the column tests, since actual extractions were based on fire assays of the activated carbon.

9.4 Cyanide Assays

Sodium cyanide concentrations in leach solutions were determined using a colorimetric titration using a silver nitrate titrant and 5-[p-(Dimethylamino)- benzylidene]-rhodanine as the indicator. Free cyanide was determined by titrating 25 mL of the leach solution to the colorimetric end point. A few drops of 1N sodium hydroxide solution were then added to break up any base metal cyanide complexes and the titration continued until the end point was reached again to determine the "total" cyanide in solution.

9.5 Multi-Element and Whole Rock Assays

Material for a multi-element analysis was digested using a four acid digestion. This digestion provided a total digestion. The resulting solution was then assayed semi-quantitatively by means of a Perkin-Elmer 2000 DV ICAP-OES. Whole rock analysis was conducted using a lithium metaborate fusion followed by ICAP-OES analysis. Certified standards were utilized for both types of analyses.

9.6 Carbon and Sulfur Assays

Carbon and sulfur speciation were determined by means of a LECO CS 400 carbon/sulfur determinator with induction furnace. Each sample set included two quality control samples, a blank and a standard check.

Appendix

Project:	Eagle Gold																		Head Screen, gms Au/MT:	0.506		gms Ag/MT:	1.79		
Sample Description:	Master Composite																		Head Assay, gms Au/MT:	n/a		gms Ag/MT:	n/a		
Test No.:	43276																		Extracted, gms Au/MT:	0.395		gms Ag/MT:	0.10		
Sample I.D.:	42979																		Tail Assay, gms Au/MT:	n/a		gms Ag/MT:	n/a		
Initial Ht., meters:	1.7018																		Est. Calculated Head, gms Au/MT:	0.413		gms Ag/MT:	1.76		
Crush Size, mm:	12.5																		Weight of Sample, kg:	80.00					
Column I.D., meters:	0.203																		Column Surface Area, square meters:	0.032					
																			Cement Addition, grams:	160.00		kg/MT:	2.00		
																			Hydrated Lime Addition, grams:	0.00		kg/MT:	0.00		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26
Date	pH, units	Free NaCN, gpL	Total NaCN, gpL	$Ca(OH)_2$ Added, grams	Cum. Lime Added, kg/MT	NaCN Added, grams	Cum. NaCN Consumed, kg/MT	Days Run	Water Added, grams	Carbon Bottle	Au, mg/L	Ag, mg/L	Cu, mg/L	Volume, mLs	Flow Rate Preg, L/Hr/M^2	Cum. T Sol'n. / T Ore	Solution, gms Au/MT	Solution Cumulative Recov., gms Au/MT	Recovered Gold Solution	Cumulative Recovered Gold Solution	Percent of Total Recovered Gold	Solution, gms Ag/MT	Solution Cumulative Recov., gms Ag/MT	Recovered Silver Solution	Cumulative Recovered Silver Solution
21-Nov	---	---	---	0.00	0.00	14.15	0.00		14,150	---	---	---	---	---			0.00	0.000	0.0%			0.00	0.00	0.0%	
21-Nov	---	---	---	---	---	---		0	---	---	---	---	---	---	0.00	0.09	0.00	0.000	0.0%	0%	0%	0.00	0.00	0.0%	0%
22-Nov	---	---	---	0.00	0.00	9.30	0.18		9,300	---	---	---	---	---			0.00	0.000	0.0%			0.00	0.00	0.0%	
22-Nov	11.5	0.73	0.73	---	---	---		1	---	C-1	2.11	0.71	21.8	7,190	9.24	0.09	0.19	0.190	45.9%	46%	48%	0.06	0.06	3.6%	4%
23-Nov	10.4	0.47	0.47	0.00	0.00	2.10	0.23		2,100	---	0.00	0.01	---	7,190			0.00	0.190	0.0%			0.00	0.06	-0.1%	
23-Nov	11.3	1.00	1.00	---	---	---		2	---	---	0.52	0.10	3.87	9,400	12.08	0.21	0.06	0.251	14.8%	61%	64%	0.01	0.07	0.7%	4%
24-Nov	10.9	0.95	0.95	0.00	0.00	0.00	0.14		---	---	0.00	0.01	---	9,400			0.00	0.251	0.0%			0.00	0.07	-0.1%	
24-Nov	11.2	0.59	0.59	---	---	---		3	---	---	0.26	0.03	4.63	8,460	10.87	0.31	0.03	0.278	6.7%	67%	71%	0.00	0.08	0.2%	4%
25-Nov	11.2	0.57	0.57	0.00	0.00	0.73	0.12		800	---	0.00	0.00	---	8,460			0.00	0.278	0.0%			0.00	0.08	0.0%	
25-Nov	11.5	0.63	0.63	---	---	---		4	---	---	0.15	0.03	9.8	8,590	11.04	0.42	0.02	0.294	3.9%	71%	75%	0.00	0.08	0.2%	5%
26-Nov	11.3	0.60	0.60	0.00	0.00	0.70	0.17		700	---	0.02	0.01	---	8,590			0.00	0.292	-0.5%			0.00	0.08	-0.1%	
26-Nov	11.4	0.76	0.76	---	---	---		5	---	---	0.14	0.02	---	9,120	11.72	0.53	0.02	0.308	3.9%	75%	78%	0.00	0.08	0.1%	5%
27-Nov	11.3	0.71	0.71	0.00	0.00	0.00	0.15		---	---	0.02	0.00	---	9,120			0.00	0.306	-0.6%			0.00	0.08	0.0%	
27-Nov	11.5	0.60	0.60	---	---	---		6	---	---	0.16	0.01	---	7,690	9.88	0.63	0.02	0.321	3.7%	78%	81%	0.00	0.08	0.1%	5%
28-Nov	11.1	0.60	0.60	0.00	0.00	1.60	0.16		1,600	---	0.01	0.00	---	7,690			0.00	0.320	-0.2%			0.00	0.08	0.0%	
28-Nov	11.4	0.62	0.62	---	---	---		7	---	---	0.07	0.01	8.27	10,650	13.68	0.76	0.01	0.330	2.3%	80%	84%	0.00	0.08	0.1%	5%
29-Nov	11.3	0.56	0.56	0.00	0.00	0.00	0.18		---	---	0.00	0.00	---	10,650			0.00	0.330	0.0%			0.00	0.08	0.0%	
29-Nov	11.5	0.68	0.68	---	---	---		8	---	---	0.08	0.01	8.48	8,390	10.78	0.87	0.01	0.338	2.0%	82%	86%	0.00	0.08	0.1%	5%
30-Nov	11.2	0.63	0.63	0.00	0.00	0.72	0.16		1,600	---	0.00	0.00	---	8,390			0.00	0.338	0.0%			0.00	0.08	0.0%	
30-Nov	11.5	0.57	0.57	---	---	---		9	---	---	0.04	0.01	---	10,280	13.21	1.00	0.01	0.343	1.2%	83%	87%	0.00	0.09	0.1%	5%
1-Dec	11.1	0.55	0.55	0.00	0.00	0.00	0.17		---	XC-1	0.00	0.00	---	10,280			0.00	0.343	0.0%			0.00	0.09	0.0%	
1-Dec	11.3	0.58	0.58	---	---	---		10	---	C-2	0.02	0.01	---	10,830	13.91	1.13	0.00	0.346	0.7%	84%	88%	0.00	0.09	0.1%	5%
2-Dec	10.9	0.45	0.45	0.00	0.00	0.00	0.16		---	---	0.00	0.00	---	10,830			0.00	0.346	0.0%			0.00	0.09	0.0%	
2-Dec	11.4	0.57	0.57	---	---	---		11	---	---	0.06	0.01	7.98	9,590	12.32	1.25	0.01	0.353	1.7%	85%	89%	0.00	0.09	0.1%	5%
3-Dec	11.0	0.50	0.50	0.00	0.00	0.00	0.16		---	---	0.00	0.00	---	9,590			0.00	0.353	0.0%			0.00	0.09	0.0%	
3-Dec	11.4	0.54	0.54	---	---	---		12	---	---	0.04	0.01	---	10,630	13.66	1.39	0.01	0.358	1.3%	87%	91%	0.00	0.09	0.1%	5%
4-Dec	10.6	0.47	0.47	0.00	0.00	0.00	0.15		---	---	0.00	0.00	---	10,630			0.00	0.358	0.0%			0.00	0.09	0.0%	
4-Dec	10.9	0.44	0.44	---	---	---		13	---	---	0.03	0.01	---	9,370	12.04	1.50	0.00	0.362	0.9%	88%	92%	0.00	0.09	0.1%	5%
5-Dec	10.9	0.69	0.69	0.00	0.00	0.00	0.16		---	---	0.00	0.00	---	9,370			0.00	0.362	0.0%			0.00	0.09	0.0%	
5-Dec	11.1	0.71	0.71	---	---	---		14	---	---	0.03	0.01	---	8,660	11.13	1.61	0.00	0.365	0.8%	88%	93%	0.00	0.09	0.1%	5%
6-Dec	10.9	0.42	0.42	0.00	0.00	0.00	0.15		---	---	0.00	0.00	---	8,660			0.00	0.365	0.0%			0.00	0.09	0.0%	
6-Dec	11.1	0.43	0.43	---	---	---		15	---	---	0.01	0.00	---	10,670	13.71	1.74	0.00	0.366	0.3%	89%	93%	0.00	0.09	0.0%	5%
7-Dec	10.5	0.44	0.44	0.00	0.00	0.00	0.17		---	---	0.00	0.00	---	10,670			0.00	0.366	0.0%			0.00	0.09	0.0%	
7-Dec	10.9	0.38	0.38	---	---	---		16	---	---	0.02	0.01	---	8,610	11.06	1.85	0.00	0.369	0.5%	89%	93%	0.00	0.09	0.1%	5%
8-Dec	10.5	0.43	0.43	0.00	0.00	0.00	0.17		---	---	0.00	0.00	---	8,460			0.00	0.369	0.0%			0.00	0.09	0.0%	
8-Dec	10.9	0.38	0.38	---	---	---		17	---	---	0.00	0.00	---	10,110	12.99	1.98	0.00	0.369	0.0%	89%	93%	0.00	0.09	0.0%	5%
9-Dec	10.6	0.34	0.34	0.00	0.00	2.60	0.19		---	---	0.01	0.00	---	10,110			0.00	0.367	-0.3%			0.00	0.09	0.0%	
9-Dec	10.9	0.34	0.34	---	---	---		18	---	---	0.03	0.01	6.82	8,650	11.11	2.09	0.00	0.371	0.8%	90%	94%	0.00	0.09	0.1%	5%
10-Dec	10.5	0.34	0.34	0.00	0.00	2.90	0.23		600	---	0.01	0.00	---	8,650			0.00	0.370	-0.3%			0.00	0.09	0.0%	
10-Dec	10.9	0.33	0.33	---	---	---		19	---	---	0.03	0.00	---	9,150	11.76	2.20	0.00	0.373	0.8%	90%	95%	0.00	0.09	0.0%	5%
11-Dec	10.4	0.30	0.30	0.00	0.00	2.80	0.27		---	---	0.00	0.00	---	9,150			0.00	0.373	0.0%			0.00	0.09	0.0%	
11-Dec	10.8	0.54	0.54	---	---	---		20	---	---	0.00	0.01	---	9,760	12.54	2.32	0.00	0.373	0.0%	90%	95%	0.00	0.10	0.1%	5%
12-Dec	10.6	0.45	0.45	0.00	0.00	0.00	0.27		---	XC-2	0.00	0.01	---	9,760			0.00	0.373	0.0%			0.00	0.09	-0.1%	

Project:	Eagle Gold																		Head Screen, gms Au/MT:	0.506		gms Ag/MT:	1.79		
Sample Description:	Master Composite																		Head Assay, gms Au/MT:	n/a		gms Ag/MT:	n/a		
Test No.:	43276																		Extracted, gms Au/MT:	0.395		gms Ag/MT:	0.10		
Sample I.D.:	42979																		Tail Assay, gms Au/MT:	n/a		gms Ag/MT:	n/a		
Initial Ht., meters:	1.7018																		Est. Calculated Head, gms Au/MT:	0.413		gms Ag/MT:	1.76		
Crush Size, mm:	12.5																		Weight of Sample, kg:	80.00					
Column I.D., meters:	0.203																		Column Surface Area, square meters:	0.032					
																			Cement Addition, grams:	160.00		kg/MT:	2.00		
																			Hydrated Lime Addition, grams:	0.00		kg/MT:	0.00		

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26
Date	pH, units	Free NaCN, gpL	Total NaCN, gpL	$Ca(OH)_2$ Added, grams	Cum. Lime Added, kg/MT	NaCN Added, grams	Cum. NaCN Consumed, kg/MT	Days Run	Water Added, grams	Carbon Bottle	Au, mg/L	Ag, mg/L	Cu, mg/L	Volume, mLs	Flow Rate Preg, L/Hr/M^2	Cum. T Sol'n. / T Ore	Solution, gms Au/MT	Solution Cumulative Recov., gms Au/MT	Recovered Gold Solution	Cumulative Recovered Gold Solution	Percent of Total Recovered Gold	Solution, gms Ag/MT	Solution Cumulative Recov., gms Ag/MT	Recovered Silver Solution	Cumulative Recovered Silver Solution
12-Dec	10.6	0.45	0.45	0.00	0.00	0.00	0.27		---	XC-2	0.00	0.01	---	9,760			0.00	0.373	0.0%			0.00	0.09	-0.1%	
12-Dec	10.9	0.55	0.55	---	---	---		21	---	C-3	0.03	0.01	---	8,300	10.66	2.43	0.00	0.376	0.8%	91%	95%	0.00	0.10	0.1%	5%
13-Dec	10.0	0.33	0.33	0.00	0.00	3.20	0.25		1,000	---	0.00	0.00	---	8,300			0.00	0.376	0.0%			0.00	0.10	0.0%	
13-Dec	10.9	0.37	0.37	---	---	---		22	---	---	0.03	0.01	---	8,750	11.24	2.54	0.00	0.380	0.8%	92%	96%	0.00	0.10	0.1%	5%
14-Dec	10.3	0.37	0.37	0.00	0.00	2.00	0.31		---	---	0.00	0.00	---	8,750			0.00	0.380	0.0%			0.00	0.10	0.0%	
14-Dec	10.6	0.44	0.44	---	---	---		23	---	---	0.01	0.01	---	10,510	13.50	2.67	0.00	0.381	0.3%	92%	97%	0.00	0.10	0.1%	6%
15-Dec	10.6	0.41	0.41	0.00	0.00	0.00	0.31		---	---	0.00	0.01	---	10,510			0.00	0.381	0.0%			0.00	0.10	-0.1%	
15-Dec	10.7	0.53	0.53	---	---	---		24	---	---	0.02	0.01	---	8,460	10.87	2.77	0.00	0.383	0.5%	93%	97%	0.00	0.10	0.1%	6%
16-Dec	10.4	0.49	0.49	0.00	0.00	1.70	0.29		800	---	0.00	0.01	---	8,460			0.00	0.383	0.0%			0.00	0.10	-0.1%	
16-Dec	10.5	0.39	0.39	---	---	---		25	---	---	0.01	0.01	7.63	10,170	13.07	2.90	0.00	0.384	0.3%	93%	97%	0.00	0.10	0.1%	6%
17-Dec	10.5	0.35	0.35	0.00	0.00	2.50	0.32		---	---	0.00	0.00	---	10,170			0.00	0.384	0.0%			0.00	0.10	0.0%	
17-Dec	10.7	0.40	0.40	---	---	---		26	---	---	0.02	0.00	---	9,190	11.81	3.01	0.00	0.387	0.6%	94%	98%	0.00	0.10	0.0%	6%
18-Dec	10.6	0.35	0.35	0.00	0.00	2.30	0.35		---	---	0.00	0.00	---	9,190			0.00	0.387	0.0%			0.00	0.10	0.0%	
18-Dec	10.8	0.55	0.55	---	---	---		27	---	---	0.01	0.01	---	9,430	12.12	3.13	0.00	0.388	0.3%	94%	98%	0.00	0.10	0.1%	6%
19-Dec	10.6	0.43	0.43	0.00	0.00	0.00	0.36		---	---	0.00	0.01	---	9,430			0.00	0.388	0.0%			0.00	0.10	-0.1%	
19-Dec	10.8	0.46	0.46	---	---	---		28	---	---	0.00	0.01	---	8,990	11.55	3.25	0.00	0.388	0.0%	94%	98%	0.00	0.10	0.1%	6%
20-Dec	10.6	0.37	0.37	0.00	0.00	2.10	0.35		---	---	0.00	0.00	---	8,990			0.00	0.388	0.0%			0.00	0.10	0.0%	
20-Dec	10.7	0.48	0.48	---	---	---		29	---	---	0.01	0.00	---	9,420	12.10	3.36	0.00	0.389	0.3%	94%	99%	0.00	0.10	0.0%	6%
21-Dec	10.7	0.41	0.41	0.00	0.00	0.00	0.37		---	---	0.01	0.00	---	9,420			0.00	0.388	-0.3%			0.00	0.10	0.0%	
21-Dec	10.7	0.42	0.42	---	---	---		30	---	---	0.03	0.01	---	8,200	10.54	3.47	0.00	0.391	0.7%	95%	99%	0.00	0.10	0.1%	6%
22-Dec	10.6	0.44	0.44	0.00	0.00	2.40	0.37		1,100	---	0.00	0.01	---	8,200			0.00	0.391	0.0%			0.00	0.10	-0.1%	
22-Dec	10.7	0.48	0.48	---	---	---		31	---	---	0.00	0.01	---	8,850	11.37	3.58	0.00	0.391	0.0%	95%	99%	0.00	0.10	0.1%	6%
23-Dec	10.7	0.38	0.38	0.00	0.00	2.00	0.39		---	---	0.00	0.01	---	8,850			0.00	0.391	0.0%			0.00	0.10	-0.1%	
23-Dec	10.7	0.45	0.45	---	---	---		32	---	---	0.00	0.01	6.93	9,380	12.05	3.69	0.00	0.391	0.0%	95%	99%	0.00	0.10	0.1%	6%
24-Dec	10.5	0.39	0.39	0.00	0.00	0.00	0.41		---	---	0.00	0.00	---	9,380			0.00	0.391	0.0%			0.00	0.10	0.0%	
24-Dec	10.6	0.53	0.53	---	---	---		33	---	---	0.02	0.01	---	7,490	9.62	3.79	0.00	0.393	0.5%	95%	100%	0.00	0.10	0.1%	6%
28-Dec	10.5	0.33	0.33	0.00	0.00	2.00	0.40		---	XC-3	0.00	0.00	---	7,490			0.00	0.393	0.0%			0.00	0.10	0.0%	
28-Dec	10.6	0.41	0.41	---	---	---		37	---	---	0.02	0.00	---	8,610	11.06	3.89	0.00	0.395	0.5%	96%	100%	0.00	0.10	0.0%	6%
29-Dec	10.6	0.41	0.41	0.00	0.00	0.00	0.43		---	---	0.02	0.00	---	8,610			0.00	0.393	-0.5%			0.00	0.10	0.0%	
29-Dec	10.2	0.43	0.43	---	---	---		38	---	---	0.02	0.01	---	8,440	10.84	4.00	0.00	0.395	0.5%	96%	100%	0.00	0.10	0.1%	6%
30-Dec	10.2	0.43	0.43	0.00	0.00	0.00	0.42		---	---	0.02	0.01	---	8,440			0.00	0.393	-0.5%			0.00	0.10	-0.1%	
30-Dec	10.3	0.45	0.45	---	---	---		39	---	---	0.03	0.01	8.00	8,110	10.42	4.10	0.00	0.396	0.7%	96%	100%	0.00	0.10	0.1%	6%
31-Dec	10.3	0.45	0.45	0.00	0.00	0.00	0.42		---	---	0.03	0.01	---	8,110			0.00	0.393	-0.7%			0.00	0.10	-0.1%	
31-Dec	10.4	0.31	0.31	---	---	---		40	---	---	0.02	0.01	---	7,340	9.43	4.19	0.00	0.395	0.4%	96%	100%	0.00	0.10	0.1%	6%
1-Jan	10.4	0.31	0.31	0.00	0.00	4.00	0.43		---	---	0.02	0.01	---	7,340			0.00	0.393	-0.4%			0.00	0.10	-0.1%	

Project:	Eagle Gold																									
Sample Description:	Master Composite																									
Test No.:	43276																									
Sample I.D.:	42979																									
Initial Ht., meters:	1.7018																									
Crush Size, mm:	12.5																									
Column I.D., meters:	0.203																									

Head Screen, gms Au/MT:	0.506		gms Ag/MT:	1.79																						
Head Assay, gms Au/MT:	n/a		gms Ag/MT:	n/a																						
Extracted, gms Au/MT:	0.395		gms Ag/MT:	0.10																						
Tail Assay, gms Au/MT:	n/a		gms Ag/MT:	n/a																						
Est. Calculated Head, gms Au/MT:	0.413		gms Ag/MT:	1.76																						
Weight of Sample, kg:	80.00																									
Column Surface Area, square meters:	0.032																									
Cement Addition, grams:	160.00		kg/MT:	2.00																						
Hydrated Lime Addition, grams:	0.00		kg/MT:	0.00																						

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26
Date	pH, units	Free NaCN, gpL	Total NaCN, gpL	$Ca(OH)_2$ Added, grams	Cum. Lime Added, kg/MT	NaCN Added, grams	Cum. NaCN Consumed, kg/MT	Days Run	Water Added, grams	Carbon Bottle	Au, mg/L	Ag, mg/L	Cu, mg/L	Volume, mLs	Flow Rate Preg, L/Hr/M^2	Cum. T Sol'n. / T Ore	Solution, gms Au/MT	Solution Cumulative Recov., gms Au/MT	Recovered Gold Solution	Cumulative Recovered Gold Solution	Percent of Total Recovered Gold	Solution, gms Ag/MT	Solution Cumulative Recov., gms Ag/MT	Recovered Silver Solution	Cumulative Recovered Silver Solution
1-Jan	10.6	0.36	0.36	---	---	---		41	---	---	0.05	0.01	8.36	4,990	6.41	4.26	0.00	0.396	0.8%	96%	100%	0.00	0.10	0.0%	6%
2-Jan	10.6	0.36	0.36	0.00	0.00	0.00	0.51		---	---	0.05	0.01	---	4,990			0.00	0.393	-0.8%			0.00	0.10	0.0%	
2-Jan	10.5	0.33	0.33	---	---	---		42	---	---	0.04	0.01	8.60	6,510	8.36	4.34	0.00	0.396	0.8%	96%	100%	0.00	0.10	0.0%	6%
3-Jan	10.5	0.33	0.33	0.00	0.00	1.80	0.51		---	---	0.04	0.01	---	6,510			0.00	0.393	-0.8%			0.00	0.10	0.0%	
3-Jan	10.6	0.46	0.46	---	---	---		43	---	---	0.04	0.01	8.43	9,090	11.68	4.45	0.00	0.397	1.1%	96%	101%	0.00	0.10	0.1%	6%
4-Jan	10.6	0.46	0.46	0.00	0.00	0.00	0.50		---	---	0.04	0.01	---	9,090			0.00	0.393	-1.1%			0.00	0.10	-0.1%	
4-Jan	10.3	0.59	0.59	---	---	---		44	---	---	0.04	0.01	---	8,020	10.30	4.55	0.00	0.397	1.0%	96%	101%	0.00	0.10	0.1%	6%
5-Jan	10.3	0.59	0.59	0.00	0.00	0.00	0.47		---	---	0.04	0.01	---	8,020			0.00	0.393	-1.0%			0.00	0.10	-0.1%	
5-Jan	10.3	0.41	0.41	---	---	---		45	---	---	0.06	0.01	---	6,650	8.54	4.63	0.00	0.398	1.2%	96%	101%	0.00	0.10	0.0%	6%
8-Jan	10.3	0.41	0.41	0.00	0.00	0.00	0.49		---	---	0.06	0.01	---	6,650			0.00	0.393	-1.2%			0.00	0.10	0.0%	
8-Jan	10.4	0.39	0.39	---	---	---		48	---	---	0.06	0.02	8.31	6,260	8.04	4.71	0.00	0.397	1.1%	96%	101%	0.00	0.10	0.1%	6%
11-Jan	10.4	0.39	0.39	0.00	0.00	0.00	0.51		---	---	0.06	0.02	---	6,260			0.00	0.393	-1.1%			0.00	0.10	-0.1%	
11-Jan	10.0	0.17	0.17	---	---	---		51	---	---	0.05	0.01	1.16	7,650	9.83	4.81	0.00	0.397	1.2%	96%	101%	0.00	0.10	0.1%	6%
12-Jan	10.0	0.17	0.17	0.00	0.00	0.00	0.53		---	---	0.05	0.01	---	7,650			0.00	0.393	-1.2%			0.00	0.10	-0.1%	
12-Jan	10.6	0.03	0.03	---	---	---		52	---	---	0.03	0.01	0.59	6,410	8.24	4.89	0.00	0.395	0.6%	96%	100%	0.00	0.10	0.0%	6%
13-Jan	10.6	0.01	0.01	0.00	0.00	0.00	0.56		---	---	0.03	0.01	---	6,410			0.00	0.393	-0.6%			0.00	0.10	0.0%	
13-Jan	10.6	0.01	0.01	---	---	---		53	---	---	0.05	0.01	0.42	8,190	10.52	4.99	0.01	0.398	1.2%	96%	101%	0.00	0.10	0.1%	6%
15-Jan	10.2	0.04	0.04	0.00	0.00	0.00	0.58		---	---	0.05	0.01	---	8,190			-0.01	0.393	-1.2%			0.00	0.10	-0.1%	
15-Jan	10.2	0.04	0.04	---	---	---		55	---	---	0.03	0.00	0.32	6,440	8.27	5.07	0.00	0.395	0.6%	96%	100%	0.00	0.10	0.0%	6%
16-Jan	10.0	0.02	0.02	0.00	0.00	0.00	0.57		---	---	0.03	0.00	---	6,440			0.00	0.393	-0.6%			0.00	0.10	0.0%	
16-Jan	10.0	0.02	0.02	---	---	---		56	---	---	0.02	0.01	0.16	7,510	9.65	5.16	0.00	0.395	0.5%	96%	100%	0.00	0.10	0.1%	6%
17-Jan	10.1	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.02	0.01	---	7,510			0.00	0.393	-0.5%			0.00	0.10	-0.1%	
17-Jan	10.1	0.01	0.01	---	---	---		57	---	---	0.04	0.01	0.21	5,880	7.55	5.24	0.00	0.396	0.7%	96%	100%	0.00	0.10	0.0%	6%
18-Jan	10.2	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.04	0.01	---	5,880			0.00	0.393	-0.7%			0.00	0.10	0.0%	
18-Jan	10.2	0.01	0.01	---	---	---		58	---	---	0.07	0.00	0.21	5,220	6.71	5.30	0.00	0.397	1.1%	96%	101%	0.00	0.10	0.0%	6%
19-Jan	10.1	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.07	0.00	---	5,220			0.00	0.393	-1.1%			0.00	0.10	0.0%	
19-Jan	10.1	0.01	0.01	---	---	---		59	---	---	0.02	0.00	0.36	6,070	7.80	5.38	0.00	0.394	0.4%	95%	100%	0.00	0.10	0.0%	6%
20-Jan	9.9	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.04	0.01	---	6,070			0.00	0.391	-0.7%			0.00	0.10	0.0%	
20-Jan	9.9	0.01	0.01	---	---	---		60	---	---	0.04	0.01	0.41	4,630	5.95	5.44	0.00	0.393	0.6%	95%	100%	0.00	0.10	0.0%	6%
21-Jan	10.1	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.04	0.00	---	4,630			0.00	0.391	-0.6%			0.00	0.10	0.0%	
21-Jan	10.1	0.01	0.01	---	---	---		61	---	---	0.04	0.00	0.04	4,220	5.42	5.49	0.00	0.393	0.5%	95%	100%	0.00	0.10	0.0%	6%
22-Jan	8.8	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.05	0.00	---	4,220			0.00	0.391	-0.6%			0.00	0.10	0.0%	
22-Jan	8.8	0.01	0.01	---	---	---		62	---	---	0.05	0.00	0.02	4,920	6.32	5.55	0.00	0.394	0.7%	95%	100%	0.00	0.10	0.0%	6%
24-Jan	10.2	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.04	0.00	---	4,920			0.00	0.391	-0.6%			0.00	0.10	0.0%	
24-Jan	10.2	0.01	0.01	---	---	---		64	---	---	0.04	0.00	0	5,000	6.42	5.61	0.00	0.394	0.6%	95%	100%	0.00	0.10	0.0%	6%
25-Jan	10.1	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.05	0.01	---	5,000			0.00	0.391	-0.8%			0.00	0.10	0.0%	
25-Jan	10.1	0.01	0.01	---	---	---		65	---	---	0.05	0.00	1.27	4,930	6.33	5.68	0.00	0.394	0.7%	95%	100%	0.00	0.10	0.0%	6%
26-Jan	9.9	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.02	0.00	---	4,930			0.00	0.392	-0.3%			0.00	0.10	0.0%	
26-Jan	9.9	0.01	0.01	---	---	---		66	---	---	0.02	0.00	0.57	5,050	6.49	5.74	0.00	0.394	0.3%	95%	100%	0.00	0.10	0.0%	6%
27-Jan	9.6	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.06	0.00	---	5,050			0.00	0.390	-0.9%			0.00	0.10	0.0%	
27-Jan	9.6	0.01	0.01	---	---	---		67	---	---	0.06	0.00	0	4,640	5.96	5.80	0.00	0.393	0.8%	95%	100%	0.00	0.10	0.0%	6%
28-Jan	9.8	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.04	0.00	---	4,640			0.00	0.391	-0.6%			0.00	0.10	0.0%	
28-Jan	9.8	0.01	0.01	---	---	---		68	---	---	0.04	0.00	0.01	4,760	6.12	5.86	0.00	0.394	0.6%	95%	100%	0.00	0.10	0.0%	6%
29-Jan	9.8	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.04	0.00	---	4,760			0.00	0.391	-0.6%			0.00	0.10	0.0%	
29-Jan	9.8	0.01	0.01	---	---	---		69	---	---	0.04	0.00	0.08	5,110	6.57	5.92	0.00	0.394	0.6%	95%	100%	0.00	0.10	0.0%	6%
3-Feb	9.7	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.04	0.00	---	5,100			0.00	0.391	-0.6%			0.00	0.10	0.0%	
3-Feb	9.7	0.01	0.01	---	---	---		74	---	---	0.04	0.00	0.05	7,110	9.14	6.01	0.00	0.395	0.9%	96%	100%	0.00	0.10	0.0%	6%
4-Feb	9.7	0.01	0.01	0.00	0.00	0.00	0.58		---	---	0.06	0.00	---	7,110			-0.01	0.389	-1.3%			0.00	0.10	0.0%	
4-Feb	9.7	0.01	0.01	---	---	---		75	---	---	0.06	0.00	0	6,970	8.96	6.10	0.01	0.395	1.3%	96%	100%	0.00	0.10	0.0%	6%