

December 16, 2016

File No.:VA101-00640/02-A.01
Cont. No.:VA16-01820



FS 64925
EMS 550121
OHS 550122

Mr. Jim Newton
Mining Engineer
BMC Minerals (No. 1) Ltd.
530 - 1130 West Pender Street
Vancouver, British Columbia
Canada, V6E 4A4

Dear Jim,

Re: Kudz Ze Kayah PFS – Geotechnical Site Characterization Summary

1 – INTRODUCTION

This letter presents a summary of the available information on geotechnical and permafrost conditions for the Kudz Ze Kayah Project. The Kudz Ze Kayah Project is a proposed copper-zinc-lead-gold mine that BMC Minerals (No.1) Ltd. (BMC) is currently developing to a Pre-Feasibility Study (PFS) level.

The majority of the available geotechnical information is from site investigations conducted by Cominco Ltd. (Cominco) and Golder Associates (Golder) in 1995 and 1996. The program included a total of 136 test pits and 43 drillholes to support the historic site layout which included a tailings storage facility location in Geona Creek. Additional geotechnical and hydrogeology information was collected by Tetra Tech EBA (Tetra Tech) and Knight Piésold Ltd. (KP) in 2015 and 2016 to support an updated mine plan. The current mine site general arrangement is shown on Drawing C210 in Appendix A. This letter presents a summary of the available information on geotechnical and permafrost conditions for the Kudz Ze Kayah Project for the updated 2016 General Arrangement.

2 – PREVIOUS WORK AND BACKGROUND INFORMATION

The following site investigations have been conducted in the project area since 1995:

- 1995 Golder Feasibility Level Geotechnical and Hydrogeological Site Investigation. The program included 75 geotechnical drillholes and 87 test pits, piezometer installation, temperature measurements, and laboratory testing of overburden samples (Golder, 1996a).
- 1996 Golder Geotechnical Site Investigations for the ABM Deposit. The program included 49 test pits and laboratory testing of overburden samples (Golder, 1996b).
- 2015 Tetra Tech Monitoring Well Installation Program. The program included installation of 11 monitoring wells.
- 2015 KP Geotechnical Site Investigation. The program included six geotechnical and hydrogeological drillholes with SPTs, hydraulic conductivity testing and thermistor installations (KP, 2016a).
- 2016 KP Geotechnical Site Investigation. The program included 16 geotechnical and hydrogeological drillholes with SPTs, hydraulic conductivity testing and thermistor installations, and 53 test pits, with laboratory testing of rock and soil samples (KP, 2016b).

Geotechnical data from all the site investigation programs listed above were utilized for the geotechnical site characterization summarized in this letter. The locations of all test pits and drillholes are shown on Figure 1. Appended Tables B.1 and B.2 present details of all available test pits and drillholes conducted at the project site to date.

3 – SITE DESCRIPTION

3.1 PHYSIOGRAPHY

The project is located in the Saint Cyr Range area of the Pelly Mountains approximately 250 km northeast of Whitehorse, Yukon Territory, Canada. The topography of the area consists of rolling hills, with lakes occupying valley bottoms. Elevations range from approximately 1,400 meters above sea level (masl) at the valley floor to approximately 1,700 masl at the hill tops in the immediate vicinity of the deposit. The valley floor is occupied by a small north flowing stream known as Geona Creek which connects shallow bedded lakes.

3.2 SURFICIAL GEOLOGY

Glacial, periglacial and fluvial processes are the main processes that have been involved in the creation of landforms and are the origin of surficial deposits in the project area. Alexco Environmental Group (AEG) summarized the available surficial geology (AEG, 2015). The main surficial deposits in the project area are as follows:

- Alluvial deposits – geologically recent and result from water processes reworking the sediments deposited during the last ice age.
- Glaciofluvial deposits – the result of water processes from the melting of glaciers and ice sheets. The valley bottoms are infilled generally with sand and gravel deposits from alluvial and glaciofluvial processes to depths of up to 20 m. There are some glaciofluvial deposits on the west side of Geona Creek near the confluence with Finlayson Creek where a deposit in excess of 40 m thick are present.
- Glacial till deposits – the result of the direct glacial action. These silty sand and gravel deposits overlie much of the area, ranging in thickness from less than 1 m to up to 10 m. The thickness of these deposits generally decreases with increasing elevation.
- Colluvium deposits – the result of frost loosening of bedrock which is then transported by debris and avalanche flows to the base of steep slopes. Colluvium is generally deposited above about 1,500 m elevation.
- Organic material – generally less than 0.5 m thick overlies colluvium and glacial till deposits.

A desk-top terrain analysis was completed by KP to develop geomorphic and geological models for the site, provide a preliminary overview of the geohazards at the site and aid the planning of future borrow area assessments. The findings of this study are summarized in KP Letter VA16-00636, dated November 18, 2016.

3.3 PERMAFROST CONDITIONS

The current understanding of the permafrost conditions within the Kudz Ze Kayah project area is derived primarily from geotechnical test pitting investigations and thermal monitoring of boreholes. The 1995 field program identified 35 test pits that reported permafrost, a further 40 test pits observed ice lenses and ice segregation which is interpreted as an active layer rather than permafrost.

The 2015 and 2016 KP site investigation programs included installation of thirteen 10-node thermistor cables in select drillholes to provide ground temperature profiles. A data logger was installed at each thermistor location to collect and record temperature measurements at regular intervals. No evidence of permafrost or frozen soils was encountered during the 2015 drilling site investigation (KP, 2016a). Thermistor K16-330, located on the eastern hillside of Geona Creek, is the only instrument that has shown sub-freezing temperatures at any point since its installation in February 2016. None of the thermistors installed during the 2016 site investigation program confirm the presence of frozen ground (KP, 2016b). It should be noted that the thermistors were installed during the summer of 2016 and a full year of data has not been recorded at this time of this assessment.

Test pit details are summarized in Table A.1, including any permafrost details noted in the test pit logs. Permafrost has previously reported as being present on north and west facing slopes, especially above 1,400 masl elevation, although permafrost had been observed as low as 1,250 masl (Golder, 1995). The locations of the referenced test pits with logged permafrost conditions from the Golder 1995 report are presented on Figures 2 and 3.

4 – GEOTECHNICAL SITE CHARACTERIZATION

This section provides specific information on the foundation characteristics and permafrost conditions for the following proposed mine infrastructure components, based on the December 2016 general arrangement:

- Lower Water Management Pond
- Class A Storage Facility
- Class B Storage Facility
- Class C Storage Facility
- Overburden Stockpile
- Mill Site, and
- Open Pit.

4.1 LOWER WATER MANAGEMENT POND EMBANKMENT AREA

The Lower Water Management Pond Embankment Area is located in the Geona Creek valley at the northern end of the project. 24 test pits (TP 101 to TP 109, TP 111, TP95B-11, TP-96-S1 to TP-96-S3, and TP-96-D1 to TP-96-D10) and 16 drillholes (BH95G-11, BH95G-12, BH95G-13D, BH95G-14D, BH95G-17D, BH95G-18D, BH95G-21D, MW15-08S/D, MW15-09S/D, MW15-10S/D, K15-330, K15-334, and K15-336) have been completed in the area of the Lower Water Management Pond embankment. All test pits and drillholes are summarized in Table 1.

The overburden in the area of the proposed Lower Water Management Pond Embankment Area consists of interlayered alluvial, glaciofluvial, and glaciolacustrine sediments ranging between 14 m to 20 m thick on the west slopes, 11 m to 16 m thick in the valley bottom, and 4 m to 7 m thick on the east slopes. Low density soils with potential for liquefaction were observed on the west slopes and valley bottom. Ground water level measurements indicated the water table was at or near surface in the valley bottom and increasingly depressed up the valley slopes with depths greater than 15 m below ground surface. The upper 6 m to 8 m of bedrock was generally highly weathered and fractured on the east and west slopes with measured hydraulic conductivities on the order of 10-7 m/s.

Frozen soils were observed ranging between 0.9 m to 5 m deep, with ice contents ranging between 5 to 40% (KP, 2015). The minimum ground temperature measurements within the drillholes were generally above freezing with the exception of one drillhole located on the west hillside with sub-zero temperatures between depths of 3 m to 14 m below ground surface.

4.2 UPPER WATER MANAGEMENT POND EMBANKMENT AREA

The Upper Water Management Pond Embankment Area is located to the south of the Lower Water Management Pond, in the Geona Creek valley. There have been no test pits or drillholes completed in the area of the Upper Water Management Pond.

4.3 CLASS A STORAGE FACILITY AND COLLECTION POND

The Class A Storage Facility and Collection Pond are located at the northern end of the western slope of the project valley. Thirty-one test pits (TP95-08 to TP95-10, TP95B-14, TP95B-17 to TP95B-19, TP-96-B3 to TP-96-B15, TP16-17 to TP16-24, and TP16-49 to TP16-53) and seven drillholes (BH95G-35, K16-387, KP16-389, K16-390, MW16-13, and MW16-14S/D) were completed in the vicinity of the proposed Class A Storage Facility and Collection Pond. Nine test pit logs (TPON-2 to TPON-9) were not located in reports provided and are not summarized. Test pits and drillholes in the vicinity of the Class A Storage Facility and Collection Pond are summarized in Table 2.

Test pits completed within the Class A Storage Facility footprint did not report permafrost. Monitoring well MW16-13 was discovered to be frozen at approximately 6 mbgs shortly after installation. A temperature probe inserted down the well confirmed near freezing temperatures at this location. None of the thermistors installed in

the Class A Facility indicate freezing conditions in their data records, however, these thermistors were all installed lower in the Geona Creek valley.

Measured groundwater levels within the footprint of the facility range from 0.4 to 5.0 m depth. Bedrock was intercepted at 0.2 m to 10.4 m. Bedrock was described as weathered and fractured interbedded argillite mudstone, mafic tuff, and chlorite calcite schist. The overburden was generally found to consist of glacial till described as loose to compact silty sandy gravel with cobbles, with occasional localized pockets of fine-grained silts and clays. Organic silt and moss were often noted at surface up to 0.5 m thick.

The Class A Collection Pond is located below the Class A Storage Facility. Five test pits (TP95B-19, TP-96-B3, and TP-96-B8 to TP-96-B10) and two drillholes (MW16-14S/D) were completed in the vicinity of the proposed Class A Collection Pond, and are summarized in Table 2. Test pit TP-96-B10 encountered ice inclusions and lenses from 0.5 to 1.15 m depth. Bedrock was intercepted from 1.15 to 4.8 m. The overburden consists of glacioluvial deposits, typically compact to dense sand and some gravel.

4.4 CLASS B STORAGE FACILITY AND COLLECTION POND

The Class B Storage Facility is north of the Open Pit, along the west slope of the valley at the southern end. The Class B Storage Facility is located in the original location shown in the 1996 feasibility design, and also includes the Low Grade Ore (LGO) and Run of Mine (ROM) pad, as well as the Collection Pond downstream of the facility. Twenty test pits (TP95G-10 to TP95G-12, TP-96-G1 to TP-96-G5, TP16-11 to TP16-15, TP16-25 to TP16-27, TP16-32 to TP16-34, TP16-48), and five drillholes (BH95G-33, MW15-01, MW15-02, and MW16-12S/D) were completed in the vicinity of the proposed Class B Storage Facility, LGO and ROM pad, and Collection Pond. Test pits and drillholes in the vicinity of the Class B Storage Facility and Collection Pond are summarized in Table 3.

The overburden material consists of glacioluvial, glaciolacustrine, and glacial till, typically compact to dense, varying from sand with some silt, to sandy gravel with some silt and trace cobbles. Frozen ground conditions were observed in test pits TP95G-10 and TP-96-G5, at 3.3 m and 1.7 m, respectively. Test pits TP-96-G2 and TP-96-G4 reported ice lenses between 0.4 and 0.8 m depth. Bedrock was intercepted from 0.1 to 10 m. Bedrock is described as weathered and fractured chlorite calcite schist with tuff fragments. Measured groundwater level ranged from artesian to 6.2 m below ground surface.

4.5 CLASS C STORAGE FACILITY AND COLLECTION POND

The Class C Storage Facility is located in a small valley along the eastern slopes of the project area. Two test pits (TP95-01C and TP95-02C) and six drillholes (MW15-03S/D, MW15-04S/D, K16-402, and K16-410 to K16-412) were completed in the vicinity of the proposed Class C Storage Facility. Test pits and drillholes at the Class C Storage Facility are summarized in Table 4.

The overburden within the proposed Class C Storage Facility consists of glacioluvial and weathered colluvium deposits, typically compact to dense gravelly, silty, sands with trace clay. Drillhole K16-410 in the Class C Facility encountered frozen soil and ice in the SPT samples at approximately 1.5 and 5 m depth. Bedrock was intercepted at 4.7 m to 19.2 m. Bedrock was described as weathered and fractured interbedded argillite mudstone, mafic tuff, and chlorite calcite schist. Measured groundwater level ranged from 2.4 m to 13.3 m.

4.6 OVERBURDEN STOCKPILE AND COLLECTION POND

Overburden stripped from the Open Pit excavation is required for initial construction and for closure activities. Overburden material not required for initial construction will be placed in a stockpile along the valley's eastern slope, north of the Class C Storage Facility. Five test pits (TP95-03C, TP95-04C, TP95-05C, TP95-06C, and TP95-07C) and two monitoring wells (MW15-05S/D and MW16-16) were completed in the vicinity of the proposed Overburden Stockpile footprint. Test pits and the monitoring well at the Overburden Stockpile are summarized in Table 5. Permafrost was reported in three of the test pits (TP95-03C, TP95-04C, and TP95-06C) between 0.6 and 1.8 m depth. Bedrock was intercepted between 2.4 and 8.4 m depth. Bedrock was described

as weathered and fractured interbedded argillite mudstone, mafic tuff, and chlorite calcite schist. Test pits and monitoring well installations found the overburden was glacial till and glaciolacustrine sediments, comprised of compact to very dense sandy silt to silty sand and gravel with occasional cobbles and boulders. Measured groundwater levels ranged from 0.6 to 8.1 m below ground surface.

4.7 MILL SITE

The Mill Site is located on the western slopes of the project valley between the Class A and Class B Storage Facilities. Fourteen test pits (TP112, T95-06, TP95-07, TP95B-12, TP95B-13, TP95B-15, TP95B-16, TPT95B-20, TP-96-B17 to TP-96-B19, TP16-28, TP16-29, and TP16-31) and eight drillholes (BH95G-36, 37, BH95G-20M, K15-335, MW15-07D/S, K16-392, K16-395, and MW16-17) were completed in the vicinity of the proposed Mill Site. Test pits and drillholes at the Mill Site are summarized in Table 6.

The overburden within the proposed Mill Site location consists of glacial till deposits, typically compact to dense silty sandy gravel. Test pits TP95-06, TP95B-13, TP-96-B15, TP-96-B16 and TP96B-18 observed ice lenses approximately 0.1 to 0.8 m. Bedrock was intercepted at 1.2 m to 13.9 m. Bedrock is described as weathered and fractured interbedded argillite mudstone, mafic volcaniclastic, and chlorite calcite schist. Measured groundwater levels ranged from 1 m to 9.9 m, with artesian conditions encountered in drillholes K16-392 and K16-395. A detailed geotechnical characterization of the Mill Site area is included in KP Letter VA16-01536 (KP, 2016e).

4.8 OPEN PIT

Thirty-seven test pits (TP95B-21 to TP95B-27, TP95G-01, TP95G-03, TP95P-01 to TP95P-06, TP-96-B20, TP-96-B21, TP16-01 to TP16-10, TP16-36 to TP16-38, and TP16-41 to TP16-47) and seventeen drillholes (BH95G-20 to BH95G-24, BH95G-25S/D, BH95G-26, BH95G-28, DDH95-129, DDH95-131, DDH95-135, DDH95-146, DDH95-148, DDH95-150, K16-379, and MW16-15D/S) were completed in the vicinity of the ultimate Open Pit footprint. Test pits and drillholes at the Open Pit are summarized in Table 7. A detailed characterization of the Open Pit area is included in KP letter VA16-00636, Findings of Terrain Analysis (KP, 2016d).

5 – SUMMARY

Site investigations completed to date at the Kudz Ze Kayah project include:

- 1995 Golder Feasibility Level Geotechnical and Hydrogeological Site Investigation
- 1996 Golder Geotechnical Site Investigations for the ABM Deposit
- 2015 Tetra Tech Monitoring Well Installation Program
- 2015 KP Geotechnical Site Investigation, and
- 2016 KP Geotechnical Site Investigation.

The following projects areas from the KP 2016 PFS general arrangement have been characterized based on the site investigation data collected to date:

- Lower Water Management Pond
- Class A Storage Facility
- Class B Storage Facility
- Class C Storage Facility
- Overburden Stockpile
- Mill Site, and
- Open Pit.

Discontinuous permafrost has been identified across the project area, with a high degree of variability. The majority of recorded permafrost conditions were identified during the 1995 and 1996 Golder site investigations. It is recommended the approximate permafrost line presented by Golder be re-assessed with a test pitting program scheduled in the late summer or early fall to better understand seasonal ice lenses and active permafrost layers.

The 2016 thermistor data was recorded and downloaded from July through September 2016. It is recommended the thermistors are downloaded during Q3 or Q4 2017 to provide a full year of data, to additionally support the characterization of potential seasonal active layers.

Please do not hesitate to contact the undersigned if you have any questions or require additional information.

Yours truly,
Knight Piésold Ltd.

Prepared:

Madeline Pease, EIT
Staff Engineer

Reviewed:



Approval that this document adheres to Knight Piésold Quality Systems:

Attachments:

| | |
|----------------|---|
| Table 1 Rev 0 | Lower Water Management Pond |
| Table 2 Rev 0 | Class A Storage Facility Drillhole and Test Pit Summary |
| Table 3 Rev 0 | Class B Storage Facility Drillhole and Test Pit Summary |
| Table 4 Rev 0 | Class C Storage Facility Drillhole and Test Pit Summary |
| Table 5 Rev 0 | Overburden Stockpile Drillhole and Test Pit Summary |
| Table 6 Rev 0 | Mill Site Drillhole and Test Pit Summary |
| Table 7 Rev 0 | Open Pit Drillhole and Test Pit Summary |
| Figure 1 Rev 0 | Site Investigation General Arrangement Plan |
| Figure 2 Rev 0 | Site Investigations and Approximate Permafrost Boundary, Sheet 1 of 2 |
| Figure 3 Rev 0 | Site Investigations and Approximate Permafrost Boundary, Sheet 2 of 2 |
| Appendix A | Drawing C210_r0 General Arrangement |
| Appendix B | Test Pit and Drillhole Summary |

References:

- Alexco Environmental Group, 2015. Memorandum, KZK Project – DRAFT Summary of Available Surficial Geology and Permafrost Information. Theriault, J.
- Golder Associates., 1996a. Feasibility Level Geotechnical and Hydrogeological Site Investigation, Ref. No. 952-1523I, January 31, 1996.
- Golder Associates., 1996b. 1996 Geotechnical Site Investigations for the ABM Deposit, Kudz Ze Kayah Project, Ref. No. 952-1523I, October 18, 1996.
- Knight Piésold Ltd., 2015. Geotechnical Investigations Assessment - Kudz Ze Kayah Project Tailings Storage Facility, Ref. No. VA15-03193, Rev.0, September 29, 2015.
- Knight Piésold Ltd., 2016a. Geotechnical Site Investigation Data Report, Ref. No. VA101-640/2-1, Rev.0, October 5, 2016.

Knight Piésold Ltd., 2016b. Geotechnical Site Investigation Data Report, Ref. No. VA101-640/3-1, Rev.0, October 20, 2016.

Knight Piésold Ltd., 2016c. Prefeasibility Design Report, Ref. No. VA101-640/2-3, Rev.0, October 24, 2016.

Knight Piésold Ltd., 2016d. Findings of Terrain Analysis Letter, Ref. No. VA16-00636, Rev.0, November 18, 2016.

Knight Piésold Ltd., 2016e. Mill Site Area Geotechnical Characterization, Ref. No. VA16-01536, Rev.0, November 21, 2016.

TABLE 1

**BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT**

**GEOTECHNICAL SITE CHARACTERIZATION
LOWER WATER MANAGEMENT POND**

Print Dec/16/16 9:35:55

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|--|--|
| TP 101 | 6,819,229 | 414,749 | 1,316 | 4.9 | - | - | 0.6 | - | 0 - 0.3 m SILT 0.3 - 0.6 m SAND 0.6 - 4.0 m silty SAND to gravelly SAND 4.0 - 4.9 m silty SAND and some GRAVEL | some ice at 0.6 m |
| TP 102 | 6,819,072 | 414,741 | 1,316 | 5.50 | - | - | 0.4 | - | 0 - 0.3 m SILT 0.3 - 5.5 m silty SAND | ice lenses |
| TP 103 | 6,819,048 | 414,686 | 1,328 | 5.6 | - | 0.5 | - | - | 0 - 0.3 m SILT 0.5 - 4.3 m SAND and GRAVEL 4.3 - 5.6 m SAND | permafrost at 0.5 m |
| TP 104 | 6,819,190 | 414,631 | 1,333 | 2.70 | - | - | 0.30 | - | 0 - 0.3 m SILT 0.3 - 1.0 m gravelly SAND 1.0 - 2.7 m silty to gravelly SAND | frozen at 0.3 m, ice lenses at 1.0 - 2.7 m |
| TP 105 | 6,819,250 | 414,732 | 1,315 | 4.00 | - | 3.60 | 0.40 | 1.7 | 0 - 0.2 m SILT 0.2 - 1.7 m fine SAND and SILT 1.7 - 4.0 m fine to silty SAND | refusal on permafrost, ice lenses at 1.7 m |
| TP 106 | 6,819,300 | 414,738 | 1,315 | 5.60 | - | 5.60 | 0.40 | 0.4 | 0 - 0.2 m SILT 0.2 - 0.4 m fine SAND 0.4 - 5.4 m SILT 5.4 - 5.6 m fine SAND | refusal on permafrost, ice lenses at 0.4 m |
| TP 107 | 6,819,452 | 414,729 | 1,311 | 3.80 | - | 3.80 | 0.40 | 0.40 | 0 - 0.2 m SILT 0.2 - 0.4 m silty SAND and some GRAVEL 0.4 - 3.8 m fine SAND and some GRAVEL | refusal on permafrost, ice lenses at 0.4 m |
| TP 108 | 6,819,012 | 414,713 | 1,319 | 5.4 | - | - | - | - | 0 - 0.3 m SILT 0.3 - 5.4 m silty SAND and some GRAVEL | |
| TP 109 | 6,818,950 | 414,631 | 1,349 | 4.6 | - | - | - | 4.3 | 0 - 0.5 m SILT 0.5 - 4.6 m SAND and GRAVEL | |
| TP 111 | 6,819,030 | 414,991 | 1,370 | 2.6 | - | 2.6 | - | - | 0 - 0.3 m SILT 0.3 - 2.6 m SAND and GRAVEL | refusal on permafrost |
| TP95B-11 | 6,819,124 | 414,800 | 1,318 | 4 | - | - | - | - | 0 - 0.2 m topsoil 0.2 - 4.0 m SILT to silty SAND | |
| BH95G-11 | 6,819,256 | 414,713 | 1,317 | 14.94 | - | - | | | 0 - 0.61 m topsoil 0.61 - 14.94 m SAND and SILT | |
| BH95G-12 | 6,819,258 | 414,715 | 1,316 | 22.56 | - | - | | | 0 - 0.30 m topsoil 0.30 - 3.50 m SAND 3.50 - 10.06 m SAND and sandy silt 10.06 - 22.56 m SILT and GRAVEL | |
| BH95G-13D | 6,819,010 | 414,711 | 1,320 | 50.3 | 10.67 | - | | | 0 - 0.30 m topsoil 0.30 - 5.80 m silty SAND and gravel 5.80 - 10.67 m GRAVEL and some sand 10.67 - 50.3 m bedrock | |
| BH95G-14D | 6,818,998 | 414,651 | 1,340 | 28.65 | 19.35 | - | | | 0 - 4.88 m silty SAND and GRAVEL 4.88 - 6.10 m sandy SILT and GRAVEL 6.10 - 12.34 m SILT to silty SAND 12.34 - 15.85 m SAND and sandy GRAVEL 15.85 - 19.35 m GRAVEL and some SILT 19.35 - 28.65 m bedrock | |
| BH95G-17D | 6,819,049 | 414,913 | 1,345 | 16.46 | 7.62 | - | | | 0 - 3.35 m fine SAND and GRAVEL 3.35 - 7.62 m sandy SILT and GRAVEL 7.62 - 16.46 m bedrock | |
| BH95G-18D | 6,819,067 | 414,980 | 1,364 | 11.9 | 3.96 | - | | | 0 - 3.96 m silty SAND and GRAVEL 3.96 - 11.9 m bedrock | |
| BH95G-21D | 6,819,032 | 414,816 | 1,321 | 24.7 | 15.8 | - | | | 0 - 0.30 m topsoil 0.30 - 15.80 m silty SAND and GRAVEL 15.8 - 24.7 m bedrock | |
| TP-96-S1 | 6,819,070 | 414,581 | 1,355 | 5.5 | 4.00 | - | 0.40 | - | 0 - 0.4 m topsoil 0.4 - 4 m silty SAND to SANDY silt | 0.4 - 1.4 m frozen ice inclusions (Vx). |
| TP-96-S2 | 6,819,113 | 414,647 | 1,341 | 4.0 | - | - | - | - | 0 - 0.2 m topsoil 0.2 - 4 m SAND | |
| TP-96-S3 | 6,819,141 | 414,700 | 1,326 | 2.8 | - | - | 0.25 | 2.8 | 0 - 0.25 m topsoil 0.25 - 0.9 m silty SAND to sandy SILT 0.9 - 2.8 m fine SAND 2.8 - 5.5 m SILT to some CLAY | 0.25 - 0.9 m frozen, ice lenses (Vs) up to 1 mm thick |
| TP-96-D1 | 6,819,035 | 414,650 | 1,342 | 6.0 | - | - | 1.20 | - | 0 - 0.25 m topsoil 0.25 - 1.2 m silty SAND 1.2 - 1.5 m SAND and GRAVEL 1.5 - 4.8 m SAND to silty SAND and GRAVEL 4.8 - 6.0 m clayey SILT | 1.2 - 1.5 ice inclusions (Vx) |
| TP-96-D2 | 6,819,037 | 414,680 | 1,335 | 5.3 | - | 2.7 | 0.4 | - | 0 - 0.4 m topsoil 0.4 - 2.0 m SILT and some SAND 2.0 - 2.9 m frozen, silty SAND and some GRAVEL 2.9 - 4.0 m fine to medium SAND 4.0 - 5.3 m clayey SILT and some SAND | 0.4 - 2 m ice coatings (Vc) and inclusions (Vx), 2 - 2.9 m ice lenses (Vr), 2.7 m no visible ice, well bonded, no excess ice (Nbn) |
| TP-96-D3 | 6,819,075 | 414,723 | 1,324 | 5 | - | - | 0.4 | - | 0 - 0.4 m topsoil (SILT) 0.4 - 1.0 m silty SAND 1.0 - 2.1 m SAND (frozen) 2.1 - 5.0 m SAND | 0.4 - 1.0 m poorly bonded, friable ice (Nf) and coatings (Vc) |
| TP-96-D4 | 6,819,070 | 414,685 | 1,331 | 5.8 | - | - | 0.45 | - | 0 - 0.45 m topsoil (SILT) 0.45 - 2.7 m frozen SILT and pockets of SILT and SAND 2.7 - 3.5 m sandy SILT 3.5 - 5.0 m SAND and GRAVEL 5.0 - 5.8 m SILT | 0.45 - 2.7 m no visible ice, well bounded, no excess ice (Nbn) |

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|--|---|
| TP-96-D5 | 6,818,960 | 414,710 | 1,329 | 6 | - | - | 0.4 | - | 0 - 0.4 m topsoil (SILT) 0.4 - 1.8 m frozen SAND 1.8 - 6.0 m SAND and GRAVEL | 0.4 - 1.8 m ice coating (Vc) and inclusions (Vx) |
| TP-96-D6 | 6,819,080 | 414,825 | 1,328 | 5.8 | - | - | 0.35 | - | 0 - 0.35 m topsoil (SILT) 0.35 - 5.0 m frozen, silty SAND 5.0 - 5.8 m silty SAND | 0.35 - 5.0 m ice lenses, below 3 m ice content reduces |
| TP-96-D7 | 6,819,040 | 414,875 | 1,338 | 5.6 | - | - | 0.35 | - | 0 - 0.35 m topsoil 0.35 - 2.4 m frozen silty SAND to sandy SILT 2.4 - 3.3 m SAND 3.3 - 3.6 m SAND and GRAVEL 3.6 - 4.2 m SILT 4.2 - 4.4 m SAND and GRAVEL 4.4 - 5.6 m SAND to sandy SILT | 0.35 - 2.4 m poorly bonded to friable (Nf) to ice lenses (Vs) 1 - 2 mm thick |
| TP-96-D8 | 6,818,950 | 414,860 | 1,332 | 5.50 | - | - | - | 2 - 3 m | 0 - 0.5 m silty SAND 0.5 - 1.7 m silty SAND and GRAVEL 1.7 - 5.5 m silty SAND to sandy SILT | rapid water seepage |
| TP-96-D9 | 6,819,000 | 414,856 | 1,332 | 5.5 | - | - | - | 3 - 3 m | 0 - 0.5 m topsoil 0.5 - 3.0 m SAND to sandy SILT 3.0 - 5.5 m silty SAND | |
| TP-96-D10 | 6,819,020 | 414,950 | 1,360 | 3.70 | - | 3.70 | - | - | 0 - 0.3 m topsoil 0.3 - 1.4 m SAND 1.4 - 1.7 m SAND and GRAVEL 1.7 - 2.9 m frozen, silty SAND 2.9 - 3.7 m frozen, silty SAND and some GRAVEL | 0.3 - 1.4 m ice inclusion (Vs), 1.7 - 2.9 m ice lenses. Refusal on frozen ground. |
| MW15-08S | 6,818,520 | 414,902 | N/A | 11.63 | - | - | - | Flowing | 0 - 11.63 m SAND and GRAVEL | |
| MW15-08D | 6,818,520 | 414,902 | N/A | 36 | 14.9 | - | - | 0.97 | 0 - 13.7 m SAND and GRAVEL 13.7 - 36 m interlayered CHLORITE and argillitic MUDSTONE | |
| MW15-09S | 6,819,176 | 414,705 | N/A | 17.27 | - | - | - | -0.4 | 0 - 17.27 m SAND and GRAVEL | |
| MW15-09D | 6,819,176 | 414,705 | N/A | 42 | 21 | - | - | Flowing | 0 - 21.0 m SAND and GRAVEL 21.0 - 42.0 m interlayered CHLORITE and argillitic MUDSTONE | |
| MW15-10S | 6,819,204 | 414,788 | N/A | 9.55 | - | - | - | -0.84 | 0 - 9.55 m overburden | |
| MW15-10D | 6,819,204 | 414,788 | N/A | 36 | 21 | - | - | -0.88 | 0 - 21.0 m overburden 21.0 - 36.0 m interlayered CHLORITE and argillitic MUDSTONE | |
| K15-330 | 6,818,696 | 414,924 | 1,347 | 50.95 | 10.6 | - | - | 14.5 | 0 - 10.6 m GRAVEL 10.6 - 50.95 sedimentary mudstone schist | |
| K15-334 | 6,819,164 | 414,781 | 1,317 | 50.5 | 18.1 | - | - | 0.8 | 0 - 0.4 m organics, CLAY and SILT 0.4 - 18.1 m clayey SILT 18.1 - 50.5 m sedimentary mudstone schist | |
| K15-336 | 6,819,016 | 414,792 | 1,318 | 50.5 | 17.5 | - | - | 1.0 | 0 - 2.0 m organics, PEAT and SILT 2.0 - 16.0 m sandy SILT and some GRAVEL 16.0 - 17.5 m silty GRAVEL 17.5 - 50.5 m sedimentary mudstone schist | |

\KPL\VA-Prj\\$101\00640\02\A\Correspondence\VA16-01820 - Geotechnical Characterization with 2016 SI Data\Tables\Tables 1 to 6_Test Pit and Drillhole Summary.XLSX\Table 1_lower.wmp

| | | | | |
|-----|---------|-------------------------------|-------|------|
| 0 | 16DEC16 | ISSUED WITH LETTER VA16-01820 | JAG | LIG |
| REV | DATE | DESCRIPTION | PREPD | RWWD |

TABLE 2

**BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT**

**GEOTECHNICAL SITE CHARACTERIZATION
CLASS A STORAGE FACILITY DRILLHOLE AND TEST PIT SUMMARY**

Print Dec/16/16 9:35:55

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|---|--|
| TP95-08 | 6,817,780 | 414,619 | 1,416 | 4.50 | 4.50 | - | 0.40 | 1.40 | 0 - 0.4 topsoil 0.4 - 1.4 SAND and GRAVEL 1.4 - 4.5 clayey SILT | frozen at 0.4 to 1.0 m in thin ice lenses |
| TP95-09 | 6,818,261 | 414,448 | 1,412 | 6.00 | 5.00 | - | - | 4.00 | 0 - 0.3 topsoil 0.3 - 5.0 silty SAND and GRAVEL 5.0 - 6.0 weak metasediments | |
| TP95-10 | 6,818,799 | 414,281 | 1,414 | 4.30 | 4.00 | - | - | - | 0 - 0.2 topsoil 0.2 - 1.5 SAND, some silt 1.5 - 4.3 weathered bedrock | |
| TP95B-14 | 6,817,711 | 414,651 | 1,410 | 4.70 | - | - | - | - | 0 - 0.8 SAND 0.8 - 4.5 SILT 4.5 - 4.7 SILT some sand | |
| TP95B-17 | 6,818,112 | 414,577 | 1,405 | 3.30 | - | - | - | - | 0 - 2.2 silty SAND some gravel 2.2 - 3.3 silty SAND to SAND some gravel | |
| TP95B-18 | 6,818,112 | 414,801 | 1,363 | 3.50 | - | - | - | - | 0 - 1.8 SAND some silt 1.8 - 3.5 SAND | |
| TP95B-19 | 6,818,499 | 414,599 | 1,373 | 3.30 | - | - | - | - | 0 - 0.2 topsoil 0.2 - 3.3 silty SAND, some gravel | |
| BH95G-35 | 6,817,696 | 414,572 | 1,422 | 16.15 | 6.1 | - | - | - | 0 - 6.1 SAND and GRAVEL 6.1 - 16.15 mafic volcanic (tuff) bedded chlorite-calcite schist and argillite | |
| TP-96-B3 | 6,818,430 | 414,690 | 1,358 | 3.80 | - | - | - | 2.1 | 0 - 0.3 organic SILT 0.3 - 2.1 silty SAND and GRAVEL 2.1 - 3.8 sandy SILT and GRAVEL | |
| TP-96-B4 | 6,818,020 | 414,840 | 1,365 | 4.20 | - | - | 0.20 | 1.50 | 0 - 1.5 silty SAND and GRAVEL 1.5 - 2.1 silty SAND 2.1 - 4.2 SILT with sand and gravel | 0.2 - 1.5 m ice inclusions (Vx) and ice coatings. |
| TP-96-B6 | 6,817,842 | 414,729 | 1,395 | 2.50 | 2.50 | - | 0.20 | - | 0 - 2.5 silty SAND and GRAVEL 2.5 highly weathered bedrock | 0.2 - 1.0 m ice coatings (Vc) |
| TP-96-B7 | 6,818,000 | 414,721 | 1,390 | 3.50 | - | - | 0.20 | - | 0 - 3.5 SILT and SAND some gravel | 0.2 - 1.1 m ice not visible, well bonded, no excess Nbn) |
| TP-96-B8 | 6,818,230 | 414,650 | 1,385 | 4.50 | - | - | | - | 0 - 0.5 SAND and GRAVEL 0.5 - 2.0 silty SAND 2.0 - 4.5 SAND some gravel | |
| TP-96-B9 | 6,818,300 | 414,565 | 1,390 | 4.10 | - | - | - | 1.9 and 4.0 m | 0 - 0.9 silty SAND 0.9 - 2.5 SAND some silt 2.5 - 4.1 SILT and SAND | |
| TP-96-B10 | 6,818,443 | 414,565 | 1,390 | 1.15 | - | 0.50 | - | - | 0 - 0.4 organic silt 0.4 - 1.5 SAND some gravel 1.5 - 3.5 SILT and SAND | 0.5 - 1.15 m ice inclusions (Vx) and random ice lenses (Vr). Refusal in frozen ground. |
| TP-96-B11 | 6,818,540 | 414,500 | 1,395 | 3.50 | - | - | - | 0.4 to 1.5 m | 0 - 0.4 organic silt 0.4 - 1.5 fine SAND, some gravel | |
| TP-96-B12 | 6,818,680 | 414,576 | 1,378 | 4.00 | - | - | - | - | 0 - 0.4 organic silt 0.4 - 3.7 silty SAND, some gravel 3.7 boulders | Refusal on boulders. |
| TP-96-B14 | 6,818,630 | 414,306 | 1,420 | 1.80 | 0.6 | - | - | - | 0 - 0.2 organic SILT 0.2 - 0.6 silty SAND 0.6 - 1.8 weathered bedrock | |
| TP-96-B15 | 6,818,769 | 414,445 | 1,395 | 2.90 | 1.5 | - | 0.30 | - | 0 - 0.3 organic SILT 0.3 - 0.9 silty SAND, some gravel 0.9 - 1.5 sandy SILT, some gravel with lenses of organic silt 1.5 - 2.9 weathered bedrock | 0.3 - 0.9 m frozen well bounded, ice inclusions (Vx to Nbe) |
| TP16-17 | 6,817,760 | 414,139 | 1,478 | 1.3 | 0.3 | - | - | - | 0 - 0.2 organics 0.2 - 0.3 SAND, some silt and gravel 0.3 - 1.3 weathered bedrock | |
| TP16-18 | 6,817,985 | 414,045 | 1,479 | 2.3 | 0.2 | - | - | 0.5 | 0 - 0.2 organics 0.2 - 2.3 SAND and GRAVEL, some clay | |
| TP16-19 | 6,818,170 | 414,021 | 1,470 | 2.8 | 2.8 | - | - | - | 0 - 0.1 organics 0.1 - 0.2 SILT 0.2 - 2.8 silty SAND, some gravel 2.8 weathered bedrock | |
| TP16-20 | 6,818,271 | 414,181 | 1,441 | 2 | 0.6 | - | - | - | 0 - 0.3 organics 0.3 - 0.6 sandy SILT, some gravel 0.6 - 2.0 weathered bedrock | |
| TP16-21 | 6,818,971 | 414,331 | 1,395 | 2.3 | 2.3 | - | - | - | 0 - 0.1 organics 0.1 - 2.4 silty SAND 2.4 weathered bedrock | |
| TP16-22 | 6,818,989 | 414,423 | 1,386 | 4.5 | - | - | - | - | 0 - 0.3 organics 0.3 - 4.5 gravelly SILT and SAND | |
| TP16-23 | 6,818,370 | 414,428 | 1,412 | 2.4 | 2.4 | - | - | - | 0 - 0.1 organics 0.1 - 2.4 silty SAND 2.4 weathered bedrock | |
| TP16-24 | 6,818,145 | 414,409 | 1,423 | 1.5 | 0.3 | - | - | - | 0 - 0.3 organics 0.3 - 1.5 weathered bedrock | |

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|--|------------------------|
| TP16-49 | 6,818,821 | 414,317 | 1,407 | 4.2 | 0.7 | - | - | - | 0 - 0.1 organics 0.1 - 0.7 silty SAND and GRAVEL 0.7 - 4.2 weathered bedrock | |
| TP16-50 | 6,818,848 | 414,482 | 1,379 | 5 | - | - | - | - | 0 - 0.2 organics 0.2 - 0.4 SILT 0.4 - 3.0 SAND and GRAVEL, some silt 3.0 - 5.0 sandy SILT, some gravel | |
| TP16-51 | 6,818,617 | 414,346 | 1,409 | 1.7 | 0.3 | - | - | - | 0 - 0.2 organics 0.2 - 0.3 SILT 0.3 - 0.4 SILT and SAND 0.4 - 1.7 weathered bedrock | |
| TP16-52 | 6,818,631 | 414,474 | 1,390 | 2.5 | 2.5 | - | - | - | 0 - 0.2 organics 0.2 - 2.5 silty, gravelly SAND 2.5 weathered bedrock | |
| TP16-53 | 6,819,075 | 414,236 | 1,398 | 3.5 | - | - | - | - | 0 - 0.1 organics 0.1 - 0.3 SILT 0.3 - 3.5 silty, gravelly SAND | |
| K16-387 | 6,817,991 | 414,571 | 1,411 | 34 | 3.3 | - | - | 4.57 | 0 - 3.3 SILT and SAND, some gravel 3.3 - 34.0 interlayered carbonaceous mudstone and mafic volcanoclastics | |
| K16-389 | 6,818,334 | 414,361 | 1,421 | 42 | 10.4 | - | - | 3.48 | 0 - 10.4 sandy, gravelly SILT and CLAY 10.4 - 42.0 interlayered carbonaceous mudstone and mafic volcanoclastics | |
| K16-390 | 6,818,779 | 414,323 | 1,409 | 38.6 | 2.1 | - | - | 4.95 | 0 - 2.1 SILT and SAND, some clay 2.1 - 38.6 interlayered carbonaceous mudstone and mafic volcanoclastics | |
| MW16-13 | 6,817,774 | 414,011 | 1,503 | 27.9 | 1.1 | - | - | 1.68 | 0 - 1.1 silty SAND, some gravel 1.1 - 27.9 interlayered carbonaceous mudstone and mafic volcanoclastics | |
| MW16-14D | 6,818,386 | 414,779 | 1,342 | 40.2 | 4.8 | - | - | -0.73 | 0 - 0.2 organics 0.2 - 4.8 clayey, sandy SILT, some gravel 4.8 - 40.2 interlayered carbonaceous mudstone and mafic volcanoclastics | |
| MW16-14S | 6,818,383 | 414,780 | 1,341 | 4.5 | - | - | - | 3.18 | 0 - 0.2 organics 0.2 - 4.5 clayey, sandy SILT, some gravel | |

\KPL\VA-Prj\\$1101\00640\02\ACorrespondence\VA16-01820 - Geotechnical Characterization with 2016 SI DataTables[Tables 1 to 6_Test Pit and Drillhole Summary.XLSX]Table 2_class A waste

| | | | | |
|-----|----------|-------------------------------|-------|------|
| 0 | 16DEC'16 | ISSUED WITH LETTER VA16-01820 | JAG | LJG |
| REV | DATE | DESCRIPTION | PREPD | RVWD |

TABLE 3

**BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT**

**GEOTECHNICAL SITE CHARACTERIZATION
CLASS B STORAGE FACILITY DRILLHOLE AND TEST PIT SUMMARY**

Print Dec/16/16 9:35:55

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|---|---|
| TP95G-10 | 6,816,779 | 415,123 | 1,391 | 3.30 | - | 3.30 | - | - | 0 - 0.15 topsoil 0.15 - 3.3 silty SAND some gravel | frozen soil difficult to penetrate with excavator, no mention of permafrost term. |
| TP95G-11 | 6,816,579 | 415,101 | 1,391 | 1.30 | 1.30 | - | - | - | 0 - 0.15 topsoil 0.15 - 1.3 SAND 1.3 bedrock | refusal on bedrock |
| TP95G-12 | 6,816,332 | 415,053 | 1,391 | 1.30 | 1.30 | - | - | - | 0 - 0.1 topsoil 0.1 - 0.35 silty SAND 0.35 - 1.3 highly weathered bedrock | refusal on bedrock |
| TP-96-G1 | 6,816,824 | 414,955 | 1,410 | 3.90 | 3.50 | - | - | - | 0 - 0.5 SILT and SAND 0.5 - 1.35 SAND some gravel 1.35 - 3.9 gravelly SAND | |
| TP-96-G2 | 6,816,631 | 414,952 | 1,411 | 4.00 | 3.50 | - | 0.40 | 2.10 | 0 - 0.4 organic silt 0.4 - 0.8 silty SAND 0.8 - 2.1 SAND 2.1 - 3.0 silt SAND and GRAVEL | 0.4 - 0.8 m frozen ice lenses (Vs) 2 - 4 mm thick |
| TP-96-G3 | 6,816,355 | 414,850 | 1,423 | 3.00 | - | - | - | - | 0 - 0.4 silty SAND 0.4 - 2.5 SAND 2.5 - 3.0 cobbles and boulders | |
| TP-96-G4 | 6,816,090 | 414,810 | 1,417 | 3.00 | 2.50 | - | 0.40 | 2.80 | 0 - 0.1 organics 0.1 - 0.4 SAND, some silt 0.4 - 2.5 gravelly SILT and SAND 2.5 - 3.0 weathered bedrock | 0.4 - 0.55 m frozen ice inclusions (Vx) |
| TP-96-G5 | 6,817,000 | 414,640 | 1,440 | 5.30 | - | 1.70 | 0.00 | - | 0 - 1.7 silty SAND and GRAVEL 1.7 - 5.3 silty SAND and GRAVEL | frozen throughout pit |
| BH95G-33 S/D | 6,816,742 | 415,133 | 1,390 | 13.1 | 7.32 | - | - | - | 0 - 1.52 silty SAND 1.52 - 7.32 SAND some gravel 7.32 - 13.1 chlorite calcite schist | |
| MW15-01 | 6,816,750 | 414,347 | - | 20.00 | 1.80 | - | - | artesian | 0 - 1.8 overburden 1.8 - 8.2 argillitic mudstone 8.2 - 8.5 siliceous rhyolite 8.5 - 14.8 schist | |
| MW15-02 | 6,816,270 | 414,808 | - | 32.00 | 6.50 | - | - | 5.42 | 0 - 6.5 overburden 6.5 - 10.5 mafic ash or volcanoclastic 10.5 - 19.8 argillitic mudstone 19.8 - 32.0 mafic ash or dyke | |
| TP16-11 | 6,816,429 | 414,690 | 1,447 | 3.50 | 0.80 | - | - | 2 | 0 - 0.4 organics 0.4 - 0.8 silty SAND 0.8 - 3.5 weathered bedrock | |
| TP16-12 | 6,816,591 | 414,480 | 1,485 | 1.60 | 0.10 | - | - | - | 0 - 0.1 organics 0.1 - 1.6 weathered bedrock | |
| TP16-13 | 6,816,764 | 414,546 | 1,452 | 2.00 | 0.20 | - | - | - | 0 - 0.2 organics 0.2 - 2.0 weathered bedrock | |
| TP16-14 | 6,816,917 | 414,472 | 1,457 | 2.00 | 0.50 | - | - | - | 0 - 0.3 organics 0.3 - 0.5 SILT and SAND 0.5 - 2.0 weathered bedrock | |
| TP16-15 | 6,817,229 | 414,310 | 1,466 | 4.80 | - | - | - | - | 0 - 0.3 organics 0.3 - 0.4 SAND and GRAVEL 0.4 - 4.8 SILT and SAND, some gravel | |
| TP16-25 | 6,816,453 | 414,805 | 1,425 | 1.90 | 1.60 | - | - | - | 0 - 0.2 organics 0.2 - 1.6 silty, gravelly SAND 1.6 - 1.9 weathered bedrock | |
| TP16-26 | 6,816,975 | 414,944 | 1,394 | 4.00 | - | - | - | - | 0 - 0.2 organics 0.2 - 4.0 silty, gravelly SAND | |
| TP16-27 | 6,816,889 | 414,896 | 1,413 | 2.90 | - | - | - | - | 0 - 0.3 organics 0.3 - 2.9 silty SAND and GRAVEL | |
| TP16-32 | 6,816,895 | 415,051 | 1,389 | 5.00 | - | - | - | - | 0 - 0.2 organics 0.2 - 5.0 silty, gravelly SAND | |
| TP16-33 | 6,816,478 | 415,010 | 1,395 | 3.40 | - | - | - | - | 0 - 0.4 organics 0.4 - 3.4 SILT and SAND, some gravel | |
| TP16-34 | 6,816,353 | 414,999 | 1,391 | 4.90 | - | - | - | - | 0 - 0.1 organics 0.1 - 0.3 SILT and COBBLES 0.3 - 4.9 silty, gravelly SAND | |
| TP16-48 | 6,816,478 | 415,140 | 1,375 | 4.00 | - | - | - | - | 0 - 0.1 organics 0.1 - 0.4 SILT 0.4 - 4.0 SILT and SAND, some gravel | |
| MW16-12D | 6,816,530 | 415,278 | 1,369 | 28.20 | 7.20 | - | - | artesian | 0 - 0.1 organics 0.1 - 7.2 gravelly CLAY, some silt 7.2 - 28.2 interlayered carbonaceous mudstone and mafic volcaniclastics | |
| MW16-12S | 6,816,530 | 415,274 | 1,369 | 8.00 | 7.20 | - | - | -0.01 | 0 - 0.1 organics 0.1 - 7.2 gravelly CLAY, some silt 7.2 - 8.0 interlayered carbonaceous mudstone and mafic volcaniclastics | |

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|--------------------------|------------------------|
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|--------------------------|------------------------|

\KPL\VA-Prj\\$1101\0640\02\A\Correspondence\VA16-01820 - Geotechnical Characterization with 2016 SI Data\Tables\Tables 1 to 6_Test Pit and Drillhole Summary.XLSX\Table 3_class B waste

| | | | | |
|-----|---------|-------------------------------|-------|------|
| 0 | 16DEC16 | ISSUED WITH LETTER VA16-01820 | JAG | LJG |
| REV | DATE | DESCRIPTION | PREPD | RWWD |

TABLE 4

**BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT**

**GEOTECHNICAL SITE CHARACTERIZATION
CLASS C STORAGE FACILITY DRILLHOLE AND TEST PIT SUMMARY**

Print Dec/16/16 9:35:55

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|---|------------------------|
| TP95-01C | 6,816,397 | 415,895 | 1,442 | 3.05 | 3.05 | - | - | - | 0 - 3.05 silty SAND with gravel 3.05 carbonaceous argillite | refusal on bedrock |
| TP95-02C | 6,816,458 | 415,867 | 1,445 | 4.60 | 4.60 | - | - | 2.40 | 0 - 4.6 silty SAND with gravel 4.6 carbonaceous mudstone | refusal on bedrock |
| MW15-03 S/D | 6,816,049 | 416,314 | - | 18.51 | 10.4 | - | - | 3.27 (S) 7.89 (D) | 0 - 6.5 overburden 6.5 - 32.0 interbedded mafic ash and argillitic mudstone | |
| MW15-04 S/D | 6,816,158 | 415,782 | - | 18.51 | 4.5 | - | - | dry (S) 7.88 m (D) | 0 - 4.5 sand and gravel and cobbles 4.5 - 18.51 layered mudstone and chlorite, biotite and quartzite schist | |
| K16-402 | 6,816,485 | 415,844 | 1,443 | 70.60 | 6.30 | - | - | 13.25 | 0 - 6.3 SILT and SAND with gravel 6.3 - 70.5 interlayered carbonaceous mudstone and mafic volcanics | |
| K16-410 | 6,816,446 | 416,136 | 1,473 | 31.00 | 5.60 | - | - | 7.95 | 0 - 5.6 sandy, gravelly CLAY and SILT 5.6 - 18.7 carbonaceous mudstone 18.7 - 31.0 mafic volcanics | |
| K16-411 | 6,816,237 | 415,947 | 1,446 | 34.10 | 18.20 | - | - | 3.13 | 0 - 18.2 SILT and SAND with layers of clay and gravel 18.2 - 34.1 interlayered carbonaceous mudstone and mafic volcanics | |
| K16-412 | 6,816,061 | 416,070 | 1,464 | 38.70 | 19.20 | - | - | 6.8 | 0 - 19.2 SILT and SAND with clay 19.2 - 38.7 interlayered carbonaceous mudstone and mafic volcanics | |

\KPL\VA-Prj\\$1\01\00640\02\VA\Correspondence\VA16-01820 - Geotechnical Characterization with 2016 SI Data\Tables\Tables 1 to 6_Test Pit and Drillhole Summary.XLSX\Table 4_class C waste

| | | | | |
|-----|---------|-------------------------------|-------|------|
| 0 | 16DEC16 | ISSUED WITH LETTER VA16-01820 | JAG | LJG |
| REV | DATE | DESCRIPTION | PREPD | RVWD |

TABLE 5

**BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT**

**GEOTECHNICAL SITE CHARACTERIZATION
OVERBURDEN STOCKPILE DRILLHOLE AND TEST PIT SUMMARY**

Print Dec/16/16 9:35:55

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|---|------------------------|
| TP95-03C | 6,816,797 | 415,746 | 1,449 | 3.05 | 3.05 | 1.50 | - | - | 0 - 3.05 clayey SILT and SAND with gravel 3.05 felipatnic lapilli tuff with schistose character | permafrost at 1.5 m |
| TP95-04C | 6,817,505 | 415,551 | 1,440 | 1.82 | - | 1.82 | - | | 0 - 1.82 clayey SILT and SAND with gravel | refusal on permafrost |
| TP95-05C | 6,817,560 | 415,597 | 1,447 | 2.40 | 2.40 | - | - | - | 0 - 2.4 clayey SILT and SAND with gravel 2.4 mudstone/ argillite | refusal on bedrock |
| TP95-06C | 6,817,951 | 415,491 | 1,449 | 0.60 | - | 0.60 | - | 1.00 | 0.3 - 0.6 clayey silty SAND with gravel | refusal on permafrost |
| TP95-07C | 6,818,012 | 415,402 | 1,432 | 3.65 | 3.65 | - | - | - | 0 - 2.13 clayey SILT and SAND with gravel 2.13 - 3.65 chlorite-amphibole calcite schist | refusal on bedrock |
| MW15-05 S/D | 6,816,872 | 415,850 | - | 30.00 | 8.40 | - | - | 12.23 (S) 0 (D) | 0 - 8.4 overburden 8.4 - 30.0 carbonaceous mudstone | |
| MW16-16 | 6,817,229 | 415,395 | 1,393 | 40.30 | 3.90 | - | - | 19.82 | 0 - 13.9 gravelly SILT and SAND 13.9 - 40.3 interlayered carbonaceous mudstone and mafic volcaniclastics | |

\IKPL\VA-Prj\\$1\01\00640\02\VA\Correspondence\VA16-01820 - Geotechnical Characterization with 2016 SI Data\Tables\Tables 1 to 6_Test Pit and Drillhole Summary.XLSX\Table 5_OVB stockpile

| | | | | |
|-----|---------|-------------------------------|-------|------|
| 0 | 16DEC16 | ISSUED WITH LETTER VA16-01820 | JAG | LJG |
| REV | DATE | DESCRIPTION | PREPD | RWWD |

TABLE 6

**BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT**

**GEOTECHNICAL SITE CHARACTERIZATION
MILL SITE DRILLHOLE AND TEST PIT SUMMARY**

Print Dec/16/16 9:35:55

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|------------------------|--|---|
| TP112 | 6,817,299 | 414,702 | 1,418 | 5.30 | - | - | - | 4 | 0 - 2.0 sandy SILT some gravel 2.0 - 4.6 sandy SILT and GRAVEL 4.6 - 5.3 weathered bedrock | |
| T95-06 | 6,817,261 | 414,773 | 1,410 | 4.00 | 4 | - | 0.1 | 1 | 0 - 4.0 silty SAND some gravel 4.0 weak metasediments | frozen at 0.1 to 0.15 m in thin ice lenses |
| TP95-07 | 6,817,540 | 414,680 | 1,414 | 2.80 | 1.2 | - | - | 2.3 | 0 - 0.6 topsoil 0.6 - 1.2 GRAVEL and SAND 1.2 - 2.8 weak metasediments | |
| TP95B-12 | 6,818,680 | 414,576 | 1,378 | 4.00 | - | - | - | - | 0 - 0.3 topsoil 0.3 - 1.8 silty SAND, some gravel 1.8 - 2.5 weathered bedrock | Refusal on boulders. |
| TP95B-13 | 6,818,620 | 414,450 | 1,404 | 3.70 | 3.4 | - | 0.5 | - | 0 - 0.5 topsoil 0.5 - 3.0 SAND, some silt, gravel | 0.5 - 1.3 frozen no visible ice, well bonded, no excess ice (Nbn) |
| TP95B-15 | 6,818,769 | 414,445 | 1,395 | 2.90 | 1.5 | - | 0.3 | - | 0 - 0.3 topsoil 0.3 - 0.5 SAND 0.5 - 2.3 sandy SILT 2.3 - 2.8 gravelly SAND, some silt, cobbles | 0.3 - 0.9 m frozen well bounded, ice inclusions (Vx to Nbe) |
| TP95B-16 | 6,818,680 | 414,660 | 1,360 | 4.70 | - | - | 0.65 | - | 0 - 0.3 topsoil 0.3 - 0.8 SAND and GRAVEL 0.8 - 1.8 gravelly SAND, some silt 1.8 - 3.0 sandy SAND, some gravel 3.0 - 3.8 SILT, some sand, gravel | 0.65 - 1.05 m frozen ice inclusions (Vx). |
| TP95B-20 | 6,817,199 | 414,848 | 1,404 | 2.90 | - | - | - | - | 0 - 2.9 silty SAND some gravel | |
| TP-96-B17 | 6,817,537 | 414,650 | 1,415 | 3.60 | - | - | - | 2.70 | 0 - 0.55 organic silt 0.55 - 0.8 SAND and GRAVEL 0.8 - 3.6 silty SAND some gravel | |
| TP-96-B18 | 6,817,610 | 414,800 | 1,393 | 5.00 | - | - | 0.80 | - | 0 - 0.5 organic silt 0.5 - 0.8 SAND and GRAVEL 0.8 - 5.0 silty SAND | 0.8 - 1.0 m frozen ice lenses (Vs) 1 - 2 mm thick |
| TP-96-B19 | 6,817,690 | 414,890 | 1,375 | 2.60 | - | - | - | 1.0 and 2.5 m | 0 - 0.5 organic gravelly SILT 0.5 - 1.0 fine SAND, some gravel 1.0 - 2.6 SILT and SAND, some gravel | |
| BH95G-36 | 6,817,449 | 414,628 | 1,418 | 10.08 | 3.35 | - | - | - | 0 - 3.35 silty SAND and GRAVEL 3.35 - 10.08 mafic volcanic (tuff) bedded chlorite-calcite schist with argillite | |
| BH95G-37 | 6,817,454 | 414,584 | 1,425 | 13.11 | 3.81 | - | - | 9.9 | 0 - 3.81 silty SAND and GRAVEL, cobbles 3.81 - 13.11 interbedded mafic tuff and argillite | |
| BH95G-20M | 6,817,263 | 414,725 | 1,416 | 12.5 | 3.81 | - | - | - | 0 - 3.81 silty, sandy GRAVEL 3.81 - 5.64 bedrock quartz vein 5.64 - 12.5 chlorite carbonate schist | |
| K15-335 | 6,817,327 | 414,667 | 1,421 | 32.33 | 2.5 | - | - | - | 0 - 2.5 silty, sandy GRAVEL 2.5 - 32.33 chlorite carbonate schist | |
| MW15-07D/S | 6,818,520 | 414,902 | - | 36 | 13.9 | - | - | 12.66 (S) 36.89 (D) | 0 - 13.9 sand and gravel 13.9 - 36.0 chlorite, biotite and calcite schist with layered argillitic mudstone | |
| TP16-28 | 6,817,432 | 414,783 | 1,401 | 2.7 | 2.2 | - | - | 2.5 | 0 - 0.1 organics 0.1 - 0.2 SILT 0.2 - 0.4 SAND and GRAVEL, some silt 0.4 - 2.2 silty SAND, some gravel 2.2 - 2.7 weathered bedrock | |
| TP16-29 | 6,817,465 | 414,894 | 1,386 | 2.3 | 2.3 | - | - | - | 0 - 0.2 organics 0.2 - 0.5 GRAVEL, some sand 0.5 - 2.3 silty, gravelly SAND 2.3 weathered bedrock | |
| TP16-31 | 6,817,555 | 414,605 | 1,412 | 4.5 | - | - | - | - | 0 - 0.5 organics 0.5 - 0.8 silty SAND and GRAVEL 0.8 - 4.5 silty, gravelly SAND | |
| K16-392 | 6,817,471 | 414,852 | 1,390 | 46.2 | 5 | - | - | artesian | 0 - 5.0 Silty SAND, some clay 5.0 - 46.2 interlayered mafic volcanoclastics and carbonaceous mudstone | |
| K16-395 | 6,817,251 | 414,822 | 1,406 | 46.2 | 2.3 | - | - | 0 | 0 - 0.1 organics 0.1 - 2.3 sandy SAND, some gravel 2.3 - 46.2 interlayered mafic volcanoclastics and carbonaceous mudstone | |
| MW16-17 | 6,817,489 | 414,634 | 1,418 | 31.1 | 1.6 | - | - | 2.61 | 0 - 0.1 organics 0.1 - 1.6 CLAY and SILT, some sand 1.6 - 31.1 interlayered mafic volcanoclastics and carbonaceous mudstone | |

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|-----------------|----------------|------------------|---------------------------------------|-------------------------|----------------------------|--|-----------------------------|--------------------------|------------------------|
|-------------------------|-----------------|----------------|------------------|---------------------------------------|-------------------------|----------------------------|--|-----------------------------|--------------------------|------------------------|

| | | | | |
|-----|----------|-------------------------------|-------|------|
| 0 | 18DEC'16 | ISSUED WITH LETTER VA16-01820 | JAG | LIG |
| REV | DATE | DESCRIPTION | PREPD | RW/D |

TABLE 7

**BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT**

**GEOTECHNICAL SITE CHARACTERIZATION
OPEN PIT DRILLHOLE AND TEST PIT SUMMARY**

Print Dec/16/16 9:35:55

| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|--|---|
| TP95B-21 | 6,815,095 | 414,941 | 1,383 | 2.2 | - | - | - | 0.3 | 0 - 0.3 gravelly SAND 0.3 - 1.0 silty SAND, some clay 1.0 - 2.2 silty SAND and GRAVEL | |
| TP95B-22 | 6,815,466 | 414,925 | 1,386 | 2.80 | - | - | - | 0.35 | 0 - 0.9 organics 0.9 - 1.8 SAND 1.8 - 2.8 silty SAND and GRAVEL | |
| TP95B-23 | 6,815,433 | 415,027 | 1,384 | 2.60 | - | - | - | - | 0 - 0.25 organics 0.25 - 2.6 sandy SILT | |
| TP95B-24 | 6,815,771 | 415,042 | 1,383 | 3.50 | - | - | - | - | 0 - 2.2 gravelly SAND 2.2 - 3.5 SILT and GRAVEL | |
| TP95B-25 | 6,815,756 | 414,950 | 1,382 | 3.00 | - | - | - | 0.30 | 0 - 0.3 organics 0.23 - 0.45 SILT 0.45 - 3.0 gravelly SAND | |
| TP95B-26 | 6,814,869 | 415,041 | 1,391 | 3.30 | - | - | - | 1.30 | 0 - 0.9 gravelly SAND 0.9 - 2.0 silty SAND 2.0 - 3.3 SILT same sand layered | |
| TP95B-27 | 6,815,080 | 414,983 | 1,383 | 1.80 | - | - | - | 0.30 | 0 - 0.2 organic SILT 0.2 - 1.8 gravelly SAND, some silt | |
| TP95G-01 | 6,814,899 | 415,141 | 1,388 | 5.00 | - | 1.5 | - | 1.50 | 0 - 0.5 topsoil 0.5 - 1.5 SAND, some silt, some gravel 1.5 - 2.0 gravelly SAND 2.0 - 5.0 silty SAND, some gravel | reach of excavator, ice lenses throughout |
| TP95G-03 | 6,814,800 | 415,198 | 1,394 | 4.50 | - | 2.2 | - | - | 0 - 0.5 topsoil 0.5 - 1.3 fine SAND, some silt, some gravel and cobbles 1.3 - 2.2 SAND, some silt, gravel 2.2 - 4.5 silty SAND, some gravel | no visible ice, poorly bonded |
| TP95P-01 | 6,815,498 | 414,777 | 1,403 | 2.50 | 2.50 | - | 0 | - | 0 - 0.4 organics 0.4 - 0.7 SAND 0.7 - 2.5 silty SAND layered 2.5 bedrock | frozen at surface no other mention of permafrost |
| TP95P-02 | 6,815,497 | 414,875 | 1,393 | 0.20 | 0.20 | - | - | - | 0 - 0.2 SAND 0.2 bedrock | |
| TP95P-03 | 6,815,501 | 414,916 | 1,387 | 2.00 | 1.50 | - | 0 | - | 0 - 0.25 organics 0.25 - 1.5 SAND some silt layered 1.5 - 2.0 quartz sericite schist | frozen at surface no other mention of permafrost |
| TP95P-04 | 6,815,422 | 414,950 | 1,383 | 3.50 | - | - | 0.70 | 1.10 | 0 - 0.2 organics 0.2 - 1.1 SILT and SAND 1.1 - 1.9 SAND and GRAVEL 1.9 - 3.5 SILT and SAND | frozen at surface, ice segregation at 0.7 m |
| TP95P-05 | 6,815,377 | 414,849 | 1,393 | 4.00 | - | - | - | - | 0 - 0.8 organics 0.8 - 4.0 SAND | |
| TP95P-06 | 6,815,336 | 415,027 | 1,385 | 1.50 | - | - | 0 | 1.10 | 0 - 0.5 organics 0.5 - 1.1 clayey SILT 1.1 - 1.5 silty SAND and GRAVEL | frozen at surface no other mention of permafrost |
| TP-96-B20 | 6,815,480 | 414,955 | 1,410 | 2.50 | - | - | 0.10 | 1.50 | 0 - 1.5 SILT 1.5 - 2.5 SAND | 0.1 - 1.5 m frozen no visible ice, well bonded, no excess (Nbn) |
| TP-96-B21 | 6,815,550 | 414,930 | 1,411 | 2.60 | 2.50 | - | - | 2.50 | 0 - 2.6 silty SAND 2.6 cobbles | |
| BH95G-20 | 6,815,497 | 414,845 | 1,396 | 10.06 | 1.52 | - | - | - | 0 - 1.5 GRAVEL and SAND 1.5 - 10.06 felsic tuffs and quartz sericite schist | |
| BH95G-21 | 6,815,640 | 414,801 | 1,402 | 10.08 | 2.00 | - | - | - | 0 - 2.0 SAND 2.0 - 10.06 schist | |
| BH95G-22 | 6,815,731 | 414,930 | 1,385 | 7.47 | 4.57 | - | - | 1.26 | 0 - 2.6 sand SILT 2.6 - 4.6 gravelly SAND 4.6 - 7.5 schist | |
| BH95G-23 | 6,815,275 | 414,906 | 1,386 | 14.63 | 14.17 | - | - | 0.44 | 0 - 1.0 SAND some silt 10.1 - 14.2 silty SAND and GRAVEL 14.2 - 14.6 chlorite calcite schist | |
| BH95G-24 | 6,815,259 | 415,039 | 1,384 | 9.75 | 8.53 | - | - | 5.05 | 0 - SAND some silt 5.0 - 6.9 silty SAND some gravel 6.9 - 8.5 SAND 8.5 - 9.75 weathered schist | |
| BH95G-25 S/D | 6,815,526 | 415,062 | 1,383 | 22.25 | 17.07 | - | - | 2.79 (S) - (D) | 0 - 1.5 sandy SILT 1.5 - 4.3 SAND and GRAVEL 4.3 - 17.1 SAND some silt and gravel 17.1 - 22.25 sericite quartz schist | |
| BH95G-26 | 6,815,664 | 415,061 | 1,382 | 14.63 | 13.40 | - | - | - | 0 - 1.8 silty SAND 1.5 - 5.5 gravelly SAND 5.5 - 14.6 felsic lapilli tuff and chlorite schist | |
| BH95G-28 | 6,814,946 | 415,143 | 1,389 | 17.68 | 17.07 | - | - | - | 0 - 0.4 topsoil 0.4 - 7.0 SAND, some silt, gravel 7.0 - 14.3 silty SAND and GRAVEL 14.3 - 17.1 GRAVEL, some silt, sand 17.1 - 17.7 weathered chlorite-calcite-biotite schist | |

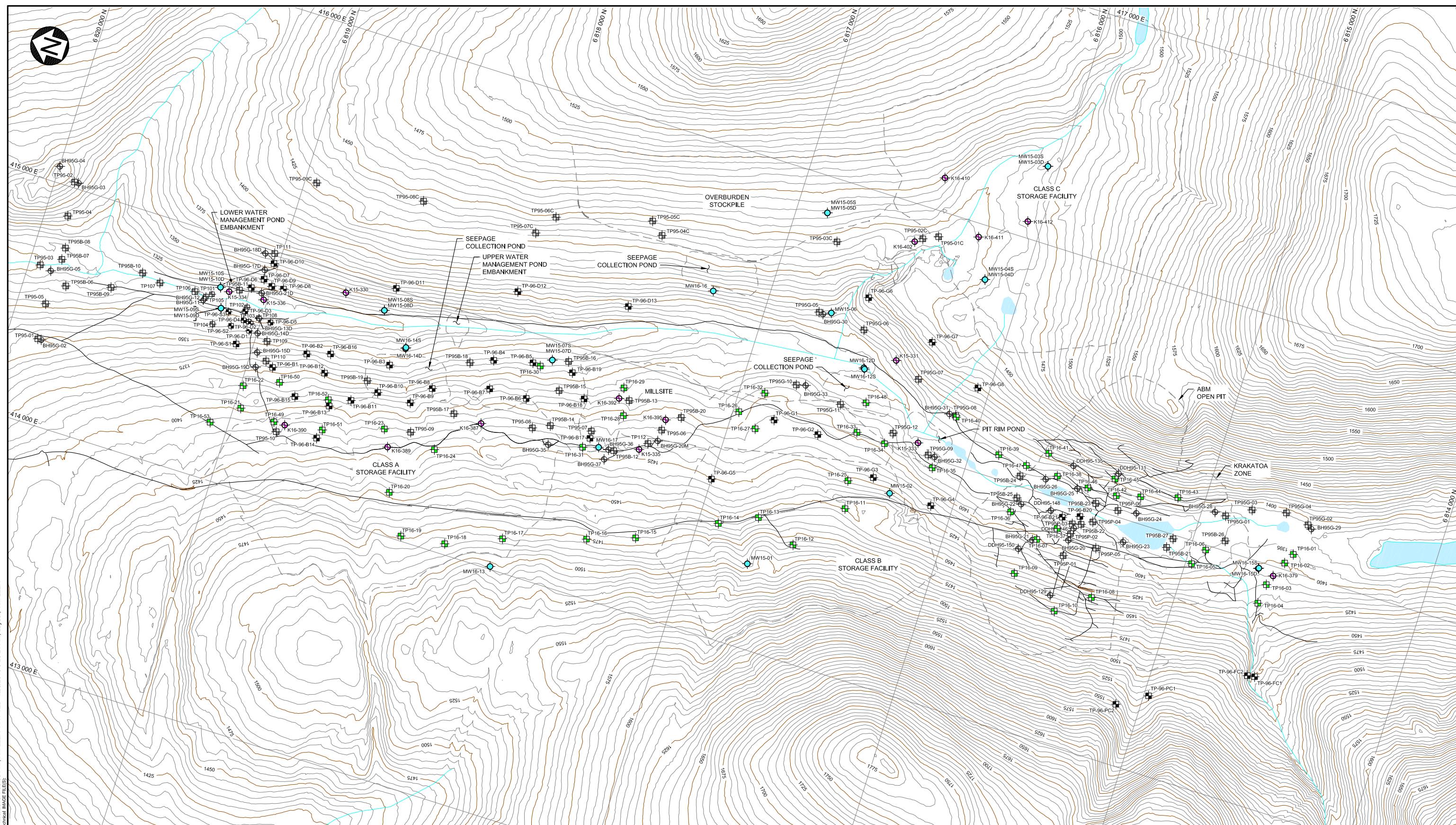
| Drillhole / Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | End of Test Pit / Drillhole (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Depth (m) | Geotechnical Description | Permafrost Description |
|-------------------------|--------------|-------------|---------------|---------------------------------|-------------------|----------------------|--|-----------------------|---|------------------------|
| DDH95-129 | 6,815,500 | 414,603 | 1,444 | - | - | - | - | - | see Note 1 | |
| DDH95-131 | 6,815,380 | 415,175 | 1,415 | - | - | - | - | - | see Note 1 | |
| DDH95-135 | 6,815,570 | 415,150 | 1,403 | - | - | - | - | - | see Note 1 | |
| DDH95-146 | 6,815,490 | 414,900 | 1,388 | - | - | - | - | - | see Note 1 | |
| DDH95-148 | 6,815,604 | 414,942 | 1,383 | - | - | - | - | - | see Note 1 | |
| DDH95-150 | 6,815,686 | 414,748 | 1,413 | - | - | - | - | - | see Note 1 | |
| TP16-01 | 6,814,580 | 415,073 | 1,398 | 4.5 | - | - | - | - | 0 - 0.2 organics 0.2 - 0.5 SAND and GRAVEL 0.5 - 4.5 gravelly SILT and SAND | |
| TP16-02 | 6,814,603 | 415,027 | 1,397 | 4.3 | 1.50 | - | - | - | 0 - 0.2 organics 0.2 - 0.4 sandy GRAVEL and COBBLES 0.4 - 1.5 gravelly SILT and SAND 1.5 - 4.3 silty SAND and GRAVEL | |
| TP16-03 | 6,814,649 | 414,918 | 1,409 | 3.2 | 2.10 | - | - | - | 0 - 0.3 organics 0.3 - 2.1 SAND 2.1 - 3.2 silty SAND and GRAVEL | |
| TP16-04 | 6,814,660 | 414,833 | 1,413 | 2.2 | 2.20 | - | - | 2.2 | 0 - 0.3 organics 0.3 - 2.2 SAND and GRAVEL 2.2 - 2.2 weathered bedrock | |
| TP16-05 | 6,814,974 | 414,907 | 1,380 | 3.3 | - | - | - | 0.5 | 0 - 0.5 organics 0.5 - 3.3 silty, sandy GRAVEL | |
| TP16-06 | 6,814,935 | 414,979 | 1,382 | 1.6 | - | - | - | 1.3 | 0 - 0.2 organics 0.2 - 1.6 SAND and GRAVEL | |
| TP16-07 | 6,815,624 | 414,809 | 1,398 | 2.4 | 0.50 | - | - | - | 0 - 0.3 organics 0.3 - 0.5 silty SAND 0.5 - 2.4 SAND and GRAVEL | |
| TP16-08 | 6,815,332 | 414,646 | 1,432 | 4.2 | 1.30 | - | - | 2 | 0 - 0.1 organics 0.1 - 1.3 gravelly SILT and SAND 1.3 - 4.2 weathered bedrock | |
| TP16-09 | 6,815,671 | 414,645 | 1,426 | 3.9 | - | - | - | 3.9 | 0 - 0.3 organics 0.3 - 0.7 organic SILT 0.7 - 3.9 silty, gravelly SAND | |
| TP16-10 | 6,815,463 | 414,544 | 1,453 | 3 | 0.60 | 0.30 | - | - | 0 - 0.3 organics 0.3 - 0.6 silty SAND and GRAVEL 0.6 - 3.0 weathered bedrock | |
| TP16-36 | 6,815,763 | 414,886 | 1,388 | 5.1 | - | - | - | - | 0 - 0.1 organics 0.1 - 0.5 SILT 0.5 - 5 SILT and SAND 5 - 5.1 sandy SILT | |
| TP16-37 | 6,815,556 | 414,878 | 1,391 | 2.3 | 0.30 | - | - | - | 0 - 0.1 organics 0.1 - 0.3 silty SAND 0.3 - 2.3 silty SAND | |
| TP16-38 | 6,815,621 | 415,088 | 1,381 | 5 | - | - | - | - | 0 - 0.2 organics 0.2 - 5.0 silty SAND | |
| TP16-41 | 6,815,684 | 415,168 | 1,402 | 3 | - | 0.50 | - | - | 0 - 0.2 organics 0.2 - 0.5 SILT, some sand 0.5 - 3.0 silty, gravelly SAND | |
| TP16-42 | 6,815,361 | 415,084 | 1,388 | 4.9 | - | - | - | - | 0 - 0.4 organics 0.4 - 4.9 SAND, some silt | |
| TP16-43 | 6,815,112 | 415,154 | 1,403 | 1.8 | 1.00 | - | - | - | 0 - 0.3 organics 0.3 - 1.0 silty GRAVEL, some sand 1.0 - 1.8 weathered bedrock | |
| TP16-44 | 6,815,262 | 415,110 | 1,386 | 4 | - | - | - | - | 0 - 0.3 organics 0.3 - 4.0 silty, gravelly SAND | |
| TP16-45 | 6,815,387 | 415,149 | 1,408 | 3.5 | 3.30 | - | - | - | 0 - 0.2 organics 0.2 - 1.1 SILT and COBBLES 1.1 - 3.3 silty, gravelly SAND 3.3 - 3.5 weathered bedrock | |
| TP16-46 | 6,815,484 | 415,079 | 1,383 | 4.1 | - | - | - | - | 0 - 0.2 organics 0.2 - 0.4 SILT, some gravel 0.4 - 4.1 silty, gravelly SAND | |
| TP16-47 | 6,815,758 | 415,091 | 1,382 | 4.5 | - | - | - | - | 0 - 0.5 organics 0.5 - 4.5 silty SAND, some clay | |
| K16-379 | 6,814,627 | 414,964 | 1,405 | 39.7 | 5.90 | - | - | 1.97 | 0 - 5.9 gravelly SILT and SAND 5.9 - 39.7 interlayered coherent and volcaniclastic rhyolite | |
| MW16-15D | 6,814,702 | 414,976 | 1,402 | 42.2 | 5.70 | - | - | 8.64 | 0 - 5.7 SILT and SAND with gravel 5.7 - 42.2 interlayered volcaniclastic and coherent rhyolite | |
| MW16-15S | 6,814,699 | 414,977 | 1,401 | 6 | 5.70 | - | - | 3.93 | 0 - 5.7 SILT and SAND with gravel 5.7 - 6.1 stringer and disseminated sulphide | |

\KPL\VA-Prj\\$1\0100640\02\Correspondence\VA16-01820 - Geotechnical Characterization with 2016 SI Data\Tables\Tables 1 to 6_Test Pit and Drillhole Summary.XLSX\Table 7_Open Pit

NOTES:

1. "DDH95" SERIES DRILLHOLE DATA WAS NOT FOUND.

| | | | | |
|-----|----------|-------------------------------|-------|------|
| 0 | 16DEC'16 | ISSUED WITH LETTER VA16-01820 | JAG | LJG |
| REV | DATE | DESCRIPTION | PREPD | RWWD |



SAVED: M:\101\00640\002\AVACad\FIGS\B48.126\2016\1:03:35 PM , KMILLER PRINTED: 12/6/2016 9:28:21 AM, Layout: KMILLER XREF FILE IS: V:\TRAIL\7\TOPCON\5dm\VA-HYDRO Geotechnical Image File.SIS

NOTES:

1. COORDINATE GRID IS UTM NAD 83 9N.
2. TOPOGRAPHIC DETAIL BASED ON INFORMATION PROVIDED BY BMC FEBRUARY 02, 2016.
3. CONTOUR INTERVAL IS 5 METRES.
4. ALL ELEVATIONS ARE IN METRES, UNLESS NOTED OTHERWISE.

LEGEND:

- GROUNDWATER MONITORING WELL (TETRA TECH)
- GEOTECHNICAL DRILLHOLE (KNIGHT PIESOLD)
- PREVIOUS DRILLHOLE (GOLDER)
- TEST PIT (KNIGHT PIESOLD)
- PREVIOUS TEST PIT (GOLDER)
- PREVIOUS TEST PIT (GOLDER 1995)
- TRAIL

PLAN
SCALE A

SCALE A 150 75 0 250 500 750 m

BMC MINERALS (NO.1) LTD.

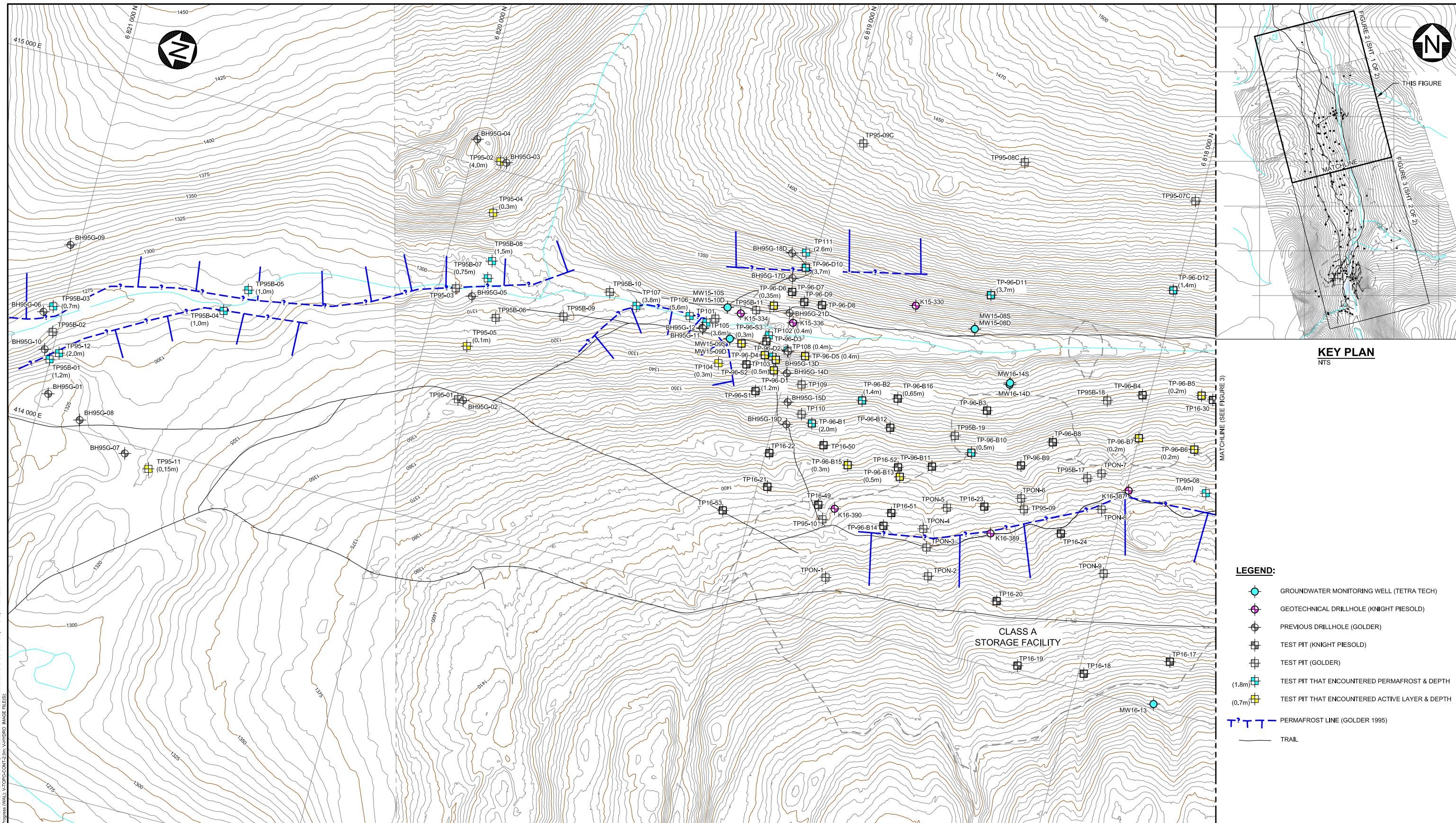
KUDZ ZE KAYAH PROJECT

SITE INVESTIGATIONS
GENERAL ARRANGEMENT
PLAN

Knight Piésold
CONSULTING

| FIGURE 1 | REV 0 |
|------------------------|-----------------------|
| P/A NO. VA101-640/2 | REF NO. VA16-01820 |

| 0 08DEC'16 | ISSUED WITH LETTER | JAS | KJM | LJG |
|------------|--------------------|----------|-------|----------|
| REV DATE | DESCRIPTION | DESIGNED | DRAWN | REVIEWED |



SAVED: M:\101\006400\2\Acad\FIGS\B49_12\8\2016 9:26:16 AM - KMILLER PRINTED: 12/8/2016 9:36:09 AM - KMILLER
XREF FILE IS: V-TRAIL.VTPR-CON-2dm.VAYIRO IMAGE FILE:

PLAN
SCALE A

SCALE A 100 50 0 100 200 300 400 500 m

BMC MINERALS (NO.1) LTD.

KUDZ ZE KAYAH PROJECT

SITE INVESTIGATIONS AND
APPROXIMATE PERMAFROST BOUNDARY
SHEET 1 OF 2

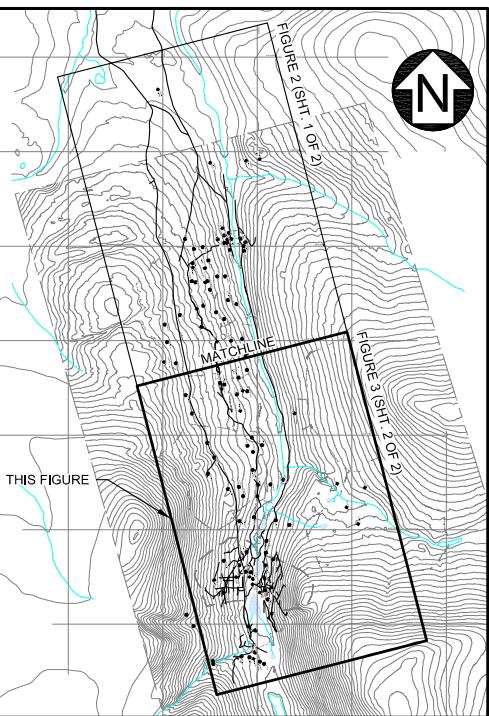
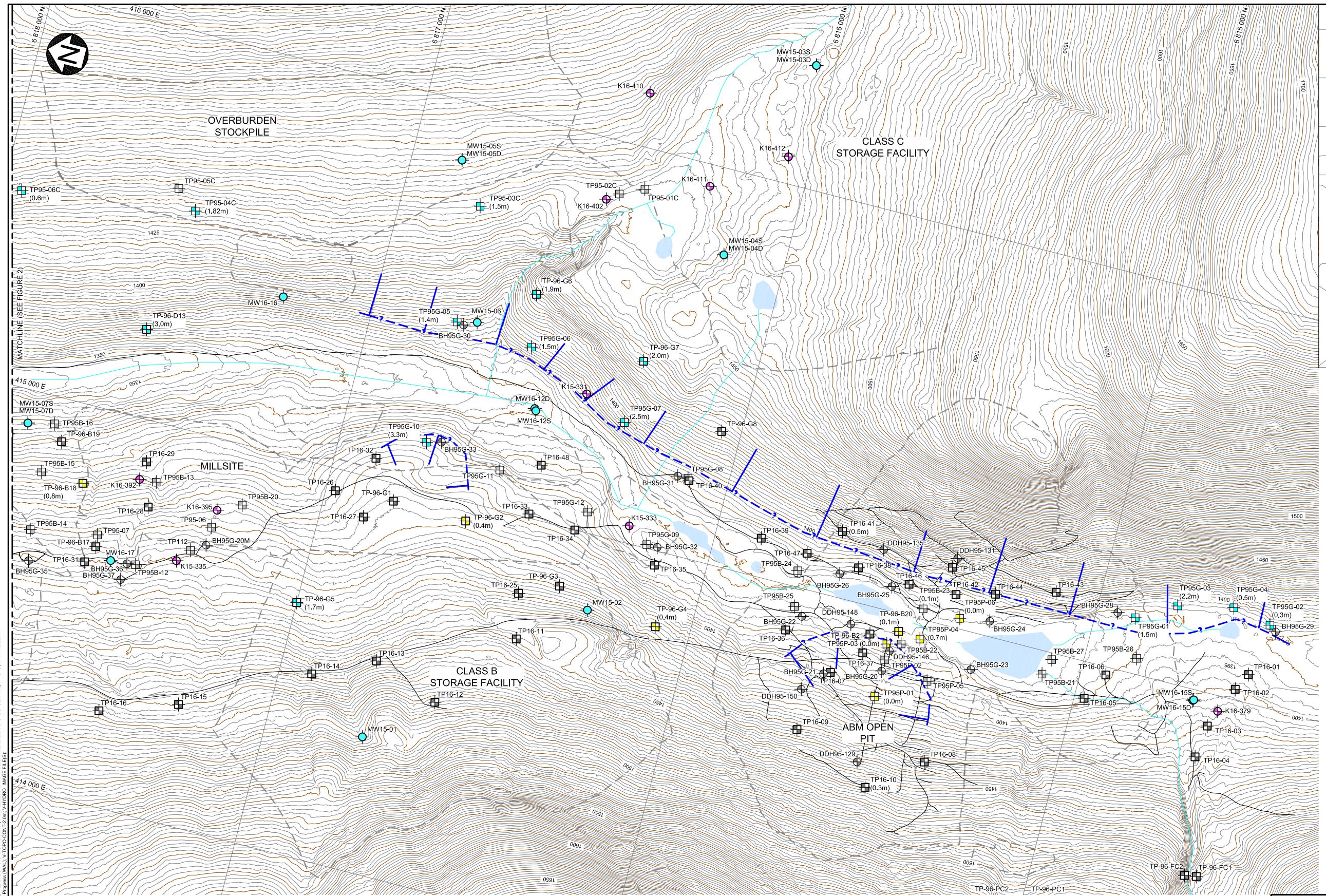
Knight Piésold
CONSULTING

P/A NO.
VA101-640/2 REF NO.
VA16-01820

REV 0

| 0 | 08DEC'16 | ISSUED WITH LETTER | JAS | KJM | LJG |
|-----|----------|--------------------|----------|-------|----------|
| REV | DATE | DESCRIPTION | DESIGNED | DRAWN | REVIEWED |

FIGURE 2 REV 0



LEGEND:

- GROUNDWATER MONITORING WELL (TETRA TECH)
- Geotechnical Drillhole (KNIGHT PIESOLD)
- Previous Drillhole (GOLDER)
- Test Pit (KNIGHT PIESOLD)
- Test Pit (GOLDER)
- (1.8m) ■ TEST PIT THAT ENCOUNTERED PERMAFROST & DEPTH
- (0.7m) ■ TEST PIT THAT ENCOUNTERED ACTIVE LAYER & DEPTH
- PERMAFROST LINE (GOLDER 1995)
- TRAIL

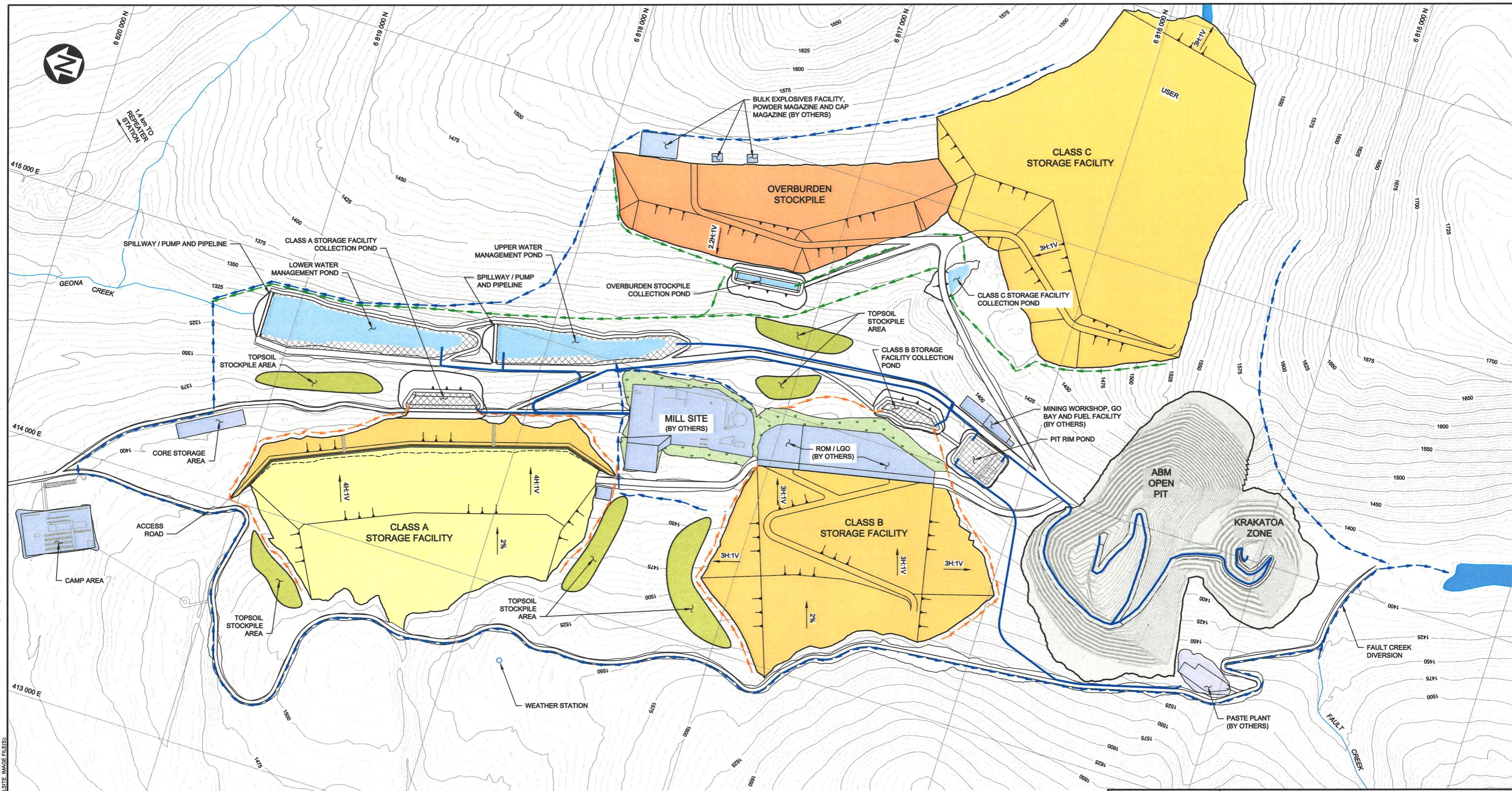
BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT
SITE INVESTIGATIONS AND APPROXIMATE PERMAFROST BOUNDARY SHEET 2 OF 2

| | | |
|-------------------------------------|------------------------|-----------------------|
| Knight Piésold CONSULTING | P/A NO. VA101-640/2 | REF NO. VA16-01820 |
| FIGURE 3 REV 0 | | |

APPENDIX A

GENERAL ARRANGEMENT DRAWING C210

(Page A-1)


NOTES:

1. COORDINATE GRID IS UTM NAD 83 9N.
2. TOPOGRAPHIC DETAIL BASED ON INFORMATION PROVIDED BY BMC FEBRUARY 02, 2016.
3. PIT SHELLS PROVIDED BY BMC MINERALS (NO.1) LTD. APRIL 8, 2016.
4. CONTOUR INTERVAL IS 5 METRES.
5. ALL ELEVATIONS ARE IN METRES, UNLESS NOTED OTHERWISE.
6. CONCURRENT RECLAMATION OF CLASS A STORAGE FACILITY NOT SHOWN.
7. CULVERTS ARE REQUIRED WHERE DITCHES CROSS ROADS.

LEGEND:

| | |
|--|---------------------------------|
| | WATER |
| | CLASS A STORAGE FACILITY |
| | CLASS B & C STORAGE FACILITIES |
| | OVERBURDEN STOCKPILE |
| | TOPSOIL STOCKPILE AREA |
| | OPEN PIT |
| | RECLAIMED / PROGRESSIVE CLOSURE |
| | FACILITIES BY OTHERS |

PLAN

SCALE A

150 75 0 250 500 750 m

| DRG. NO. | DESCRIPTION | REV | DATE | DESCRIPTION | DESIGNED | DRAWN | REVIEWED | APPROVED | REV | DATE | DESCRIPTION | MAP | KJM | Jed |
|----------|--------------------|-----|------|-------------|----------|-------|----------|----------|-----|------|-------------|-----|-----|-----|
| | REFERENCE DRAWINGS | | | REVISIONS | | | | | | | REVISIONS | | | |

**FOR INFORMATION ONLY
NOT FOR CONSTRUCTION**

DISCLAIMER

THIS DRAWING WAS PREPARED BY KNIGHT PIÉSOLD LTD. AS AN ACCOUNT OF THE INFORMATION TESTED ON THIS DRAWING. THE INFORMATION ON THIS DRAWING IS KNIGHT PIÉSOLD'S BEST JUDGEMENT IN THE LIGHT OF THE INFORMATION AVAILABLE TO IT AT THE TIME OF PREPARATION. KNIGHT PIÉSOLD LTD. AND ANY OTHER PARTY MAKES NO CLAIMS OF THIS DRAWING, OR ANY RELIANCE ON OR DECISIONS MADE BASED ON IT, ARE THE RESPONSIBILITY OF THE USER. KNIGHT PIÉSOLD LTD. AND ANY OTHER PARTY MAKE NO RESPONSIBILITY FOR DAMAGES AND EXPENSES WHICH MAY RESULT AS A RESULT OF DECISIONS MADE OR ACTUALS BASED ON THIS DRAWING. KNIGHT PIÉSOLD LTD. AND ANY OTHER PARTY BASED ON THIS DRAWING GOES RESULTING FROM DELAYING THE COMMENCEMENT AND COMPLETION OF THIS DRAWING, OR UNCONTROLLED AND UNPREDICTABLE FACTORS. THE MOST RECENT VERSION OF THIS DRAWING IS THE MOST RECENT VERSION OF THIS DRAWING.

**Knight Piésold
CONSULTING**

BMC MINERALS (NO. 1) LTD.

KUDZ ZE KAYAH PROJECT

**GENERAL ARRANGEMENT
ULTIMATE LAYOUT**



VA101-640/2 DRAWING NO. **C210** REVISION **0**

APPENDIX B
TEST PIT AND DRILL HOLE SUMMARY
(Pages B-1 to B-5)

TABLE B.1

BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT

TEST PIT SUMMARY

Print Dec/16/16 9:32:50

| Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | Depth of Test Pit (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Seepage Depth (m) | Comments |
|-------------|-----------------|----------------|------------------|-----------------------------|-------------------------|----------------------------|--|--|--|
| TP 101 | 6819229.28 | 414749.29 | 1315.54 | 4.90 | - | - | 0.6 | - | some frost at 0.6 m |
| TP 102 | 6819072.49 | 414741.00 | 1315.92 | 5.50 | - | - | 0.40 | - | permafrost and ice lenses |
| TP 103 | 6819047.76 | 414685.89 | 1327.85 | 5.60 | - | 0.50 | - | - | permafrost at 0.5 m |
| TP 104 | 6819189.75 | 414630.66 | 1332.57 | 2.70 | - | - | 0.30 | - | frozen at 0.3 m, ice lenses at 1.0 - 2.7 m |
| TP 105 | 6819250.43 | 414732.28 | 1315.26 | 4.00 | - | 3.60 | 0.40 | 1.70 | refusal on permafrost, ice lenses at 1.7 m |
| TP 106 | 6819300.49 | 414738.28 | 1314.99 | 5.60 | - | 5.60 | 0.40 | 0.40 | refusal on permafrost, ice lenses at 0.4 m |
| TP 107 | 6819451.57 | 414728.76 | 1311.45 | 3.80 | - | 3.80 | 0.40 | 0.40 | refusal on permafrost, ice lenses at 0.4 m |
| TP 108 | 6819011.69 | 414712.84 | 1319.21 | 5.40 | - | - | - | - | |
| TP 109 | 6818949.87 | 414630.59 | 1348.56 | 4.60 | - | - | - | 4.30 | |
| TP 110 | 6818929.20 | 414550.39 | 1370.30 | 5.60 | - | - | - | 0.3 and 3.4 | |
| TP 111 | 6819029.75 | 414990.87 | 1370.02 | 2.60 | - | 2.60 | - | - | refusal on permafrost |
| TP 112 | 6817298.66 | 414701.99 | 1418.46 | 5.30 | - | - | - | 4.0 | |
| TP95-01 | 6819869.47 | 414351.61 | 1348.68 | 4.00 | 0.40 | - | - | - | |
| TP95-02 | 6819919.91 | 415024.34 | 1362.86 | 4.00 | - | - | 4.00 | - | small boulders at bottom of test pit frozen |
| TP95-03 | 6819952.54 | 414650.18 | 1299.91 | 5.00 | - | - | - | 3.0 | |
| TP95-04 | 6819904.07 | 414880.33 | 1337.42 | 4.00 | - | - | 0.30 | - | frozen at 0.3 m in thin ice lenses |
| TP95-05 | 6819882.39 | 414501.52 | 1321.77 | 2.00 | - | - | 0.10 | - | frozen at 0.3 m in thin ice lenses |
| TP95-06 | 6817260.63 | 414773.11 | 1410.32 | 4.00 | 4.00 | - | 0.10 | 1.00 | frozen at 0.1 to 0.15 m in thin ice lenses |
| TP95-07 | 6817540.48 | 414680.48 | 1413.72 | 2.80 | 1.20 | - | - | 2.30 | |
| TP95-08 | 6817780.45 | 414619.00 | 1416.03 | 4.50 | 4.50 | - | 0.40 | 1.40 | frozen at 0.4 to 1.0 m in thin ice lenses |
| TP95-09 | 6818261.24 | 414448.28 | 1412.10 | 6.00 | 5.00 | - | - | 4.00 | |
| TP95-10 | 6818799.32 | 414280.94 | 1413.81 | 4.30 | 4.00 | - | - | - | |
| TP95-11 | 6820658.17 | 413947.46 | 1305.00 | 5.00 | - | - | 0.15 | - | frozen at 0.15 to 0.3 m in thin ice lenses |
| TP95-12 | 6820980.54 | 414198.07 | 1270.00 | 2.00 | - | 2.00 | 0.10 | - | frozen at 0.1 to 0.3 m and 1.4 to 2.0 m in thin ice lenses |
| TP95B-01 | 6821002.19 | 414174.79 | 1270.00 | 2.00 | - | 1.20 | - | - | refusal on permafrost |
| TP95B-02 | 6821012.65 | 414250.85 | 1255.00 | 3.00 | - | - | - | 0.7 and 1.5 | |
| TP95B-03 | 6821028.98 | 414320.44 | 1259.00 | 1.00 | - | 0.70 | - | - | refusal on permafrost |
| TP95B-04 | 6820564.91 | 414426.73 | 1270.00 | 1.30 | - | 1.00 | - | - | refusal on permafrost |
| TP95B-05 | 6820512.55 | 414500.67 | 1270.00 | 1.60 | - | 1.00 | - | - | refusal on permafrost |
| TP95B-06 | 6819824.10 | 414598.08 | 1311.10 | 4.50 | - | - | - | - | |
| TP95B-07 | 6819873.10 | 414699.39 | 1302.38 | 1.20 | - | 0.75 | - | 0.70 | refusal on permafrost |
| TP95B-08 | 6819873.33 | 414749.13 | 1304.43 | 2.50 | - | 1.50 | - | 1.50 | permafrost at 1.5 m no visible ice |
| TP95B-09 | 6819641.33 | 414648.97 | 1308.85 | 4.50 | - | - | - | - | |
| TP95B-10 | 6819533.22 | 414747.12 | 1309.68 | 3.80 | - | - | - | 0.30 | |
| TP95B-11 | 6819124.49 | 414800.34 | 1318.01 | 4.00 | - | - | - | - | |
| TP95B-12 | 6817426.50 | 414630.50 | 1419.25 | 2.50 | 1.80 | - | - | - | |
| TP95B-13 | 6817427.81 | 414849.90 | 1390.04 | 3.00 | - | - | - | - | |
| TP95B-14 | 6817711.49 | 414650.58 | 1410.34 | 4.70 | - | - | - | - | |
| TP95B-15 | 6817720.31 | 414801.57 | 1393.61 | 4.20 | - | - | - | - | |
| TP95B-16 | 6817719.10 | 414929.84 | 1361.52 | 3.80 | - | - | - | - | |
| TP95B-17 | 6818111.71 | 414576.85 | 1404.71 | 3.30 | - | - | - | - | |
| TP95B-18 | 6818111.76 | 414800.80 | 1362.55 | 3.50 | - | - | - | - | |
| TP95B-19 | 6818499.30 | 414599.18 | 1373.29 | 3.30 | - | - | - | - | |
| TP95B-20 | 6817198.55 | 414848.08 | 1403.51 | 2.90 | - | - | - | - | |
| TP95B-21 | 6815094.85 | 414940.73 | 1382.69 | 2.20 | - | - | - | 0.30 | |
| TP95B-22 | 6815465.65 | 414925.13 | 1385.69 | 2.80 | - | - | - | 0.35 | |
| TP95B-23 | 6815433.32 | 415027.07 | 1383.73 | 2.60 | - | - | - | - | |
| TP95B-24 | 6815770.54 | 415041.55 | 1383.16 | 3.50 | - | - | - | - | |
| TP95B-25 | 6815755.70 | 414950.23 | 1382.45 | 3.00 | - | - | - | 0.30 | |
| TP95B-26 | 6814868.91 | 415040.67 | 1390.82 | 3.30 | - | - | - | 1.30 | |
| TP95B-27 | 6815080.06 | 414983.14 | 1382.68 | 1.80 | - | - | - | 0.30 | |
| TP95-01C | 6816397.45 | 415894.76 | 1441.70 | 3.05 | 3.05 | - | - | - | refusal on bedrock |
| TP95-02C | 6816458.11 | 415866.60 | 1444.54 | 4.60 | 4.60 | - | - | 2.40 | refusal on bedrock |
| TP95-03C | 6816797.15 | 415746.38 | 1448.54 | 3.05 | 3.05 | 1.50 | - | - | permafrost at 1.5 m |
| TP95-04C | 6817504.56 | 415551.34 | 1440.39 | 1.82 | - | 1.82 | - | - | refusal on permafrost |
| TP95-05C | 6817560.17 | 415597.27 | 1447.48 | 2.40 | 2.40 | - | - | - | refusal on bedrock |
| TP95-06C | 6817951.01 | 415490.58 | 1449.10 | 0.60 | - | 0.60 | - | - | refusal on permafrost |
| TP95-07C | 6818012.39 | 415401.97 | 1432.39 | 3.65 | 3.65 | - | - | - | refusal on bedrock |
| TP95-08C | 6818500.94 | 415387.74 | 1442.38 | 3.65 | 3.65 | - | 0.90 | - | ice lenses in upper 0.9 m, refusal on bedrock |
| TP95-09C | 6818950.85 | 415326.17 | 1427.37 | 0.60 | 0.60 | - | - | - | |
| TP95G-01 | N/A | N/A | 5.00 | - | 1.50 | - | - | 1.50 | reach of excavator, ice lenses throughout |
| TP95G-02 | 6814557.86 | 415209.26 | 1393.86 | 5.50 | - | 0.30 | - | 5.00 | mentions frozen, but no permafrost term used |
| TP95G-03 | 6814800.23 | 415197.95 | 1394.31 | 4.50 | - | 2.20 | - | - | mentions no visible ice and poorly bonded, but no permafrost term used. |
| TP95G-04 | 6814659.26 | 415229.61 | 1397.15 | 4.70 | - | 0.50 | - | 4.70 | mentions no visible ice and poorly bonded, but no permafrost term used. |
| TP95G-05 | 6816780.05 | 415442.89 | 1388.00 | 3.50 | - | 1.40 | - | - | permafrost at 1.4 m with visible ice crystals |
| TP95G-06 | 6816578.45 | 415428.13 | 1388.67 | 1.50 | - | 1.50 | - | - | mentions no visible ice and poorly bonded. Ended test pit due to melting permafrost. |
| TP95G-07 | 6816298.37 | 415299.85 | 1395.87 | 4.20 | - | 2.50 | - | 3.80 | permafrost at 2.5 m with no visible ice crystals, poorly bonded. |

| Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | Depth of Test Pit (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Seepage Depth (m) | Comments |
|-------------|-----------------|----------------|------------------|-----------------------------|-------------------------|----------------------------|---|--|--|
| TP95G-08 | 6816103.82 | 415201.58 | 1391.92 | 3.90 | - | - | - | 3.00 | |
| TP95G-09 | 6816164.14 | 415009.56 | 1385.57 | 5.00 | - | 0.15 | - | 4.90 | mentions no visible ice and poorly bonded, but no permafrost term used. Soil frozen and difficult to excavate. |
| TP95G-10 | 6816779.28 | 415123.26 | 1391.13 | 3.30 | - | 0.15 | - | - | frozen soil difficult to penetrate with excavator, no mention of permafrost term. |
| TP95G-11 | 6816578.54 | 415100.93 | 1391.44 | 1.30 | 1.30 | - | - | - | refusal on bedrock |
| TP95G-12 | 6816332.36 | 415052.72 | 1391.47 | 1.30 | 1.30 | - | - | - | refusal on bedrock |
| TP95P-01 | 6815497.89 | 414777.31 | 1403.42 | 2.50 | 2.50 | - | 0 | - | frozen at surface no other mention of permafrost |
| TP95P-02 | 6815496.57 | 414874.83 | 1393.03 | 0.20 | 0.20 | - | - | - | |
| TP95P-03 | 6815501.37 | 414915.88 | 1387.41 | 2.00 | 1.50 | - | 0 | - | frozen at surface no other mention of permafrost |
| TP95P-04 | 6815421.94 | 414949.53 | 1383.33 | 3.50 | - | - | 0.70 | 1.10 | frozen at surface, ice segregation at 0.7 m |
| TP95P-05 | 6815376.88 | 414848.59 | 1392.81 | 4.00 | - | - | - | - | |
| TP95P-06 | 6815335.90 | 415026.94 | 1384.60 | 1.50 | - | - | 0 | 1.10 | frozen at surface no other mention of permafrost |
| TP-96-B1 | 6818895.00 | 414533.00 | 1376.00 | 2.00 | - | 2.00 | - | 1.80 | 0.2 - 2.0 m ice coatings (Vc) and ice crystals (Vx) . Refusal on frozen ground. |
| TP-96-B2 | 6818775.00 | 414630.00 | 1364.00 | 2.40 | - | 1.40 | - | 0.40 | 1.4 m ice lenses (Vs). Refusal on frozen ground. |
| TP-96-B3 | 6818430.00 | 414690.00 | 1358.00 | 3.80 | - | - | - | 2.10 | |
| TP-96-B4 | 6818020.00 | 414840.00 | 1365.00 | 4.20 | - | - | 0.20 | 1.50 | 0.2 - 1.5 m ice inclusions (Vx) and ice coatings. |
| TP-96-B5 | 6817860.00 | 414880.00 | 1365.00 | 2.60 | 2.60 | - | - | 2.40 | |
| TP-96-B6 | 6817842.00 | 414729.00 | 1395.00 | 2.50 | 2.50 | - | 0.20 | - | 0.2 - 1.0 m ice coatings (Vc) |
| TP-96-B7 | 6818000.00 | 414721.00 | 1390.00 | 3.50 | - | - | 0.20 | - | 0.2 - 1.1 m ice not visible, well bonded, no excess Nbn) |
| TP-96-B8 | 6818230.00 | 414650.00 | 1385.00 | 4.50 | - | - | - | - | |
| TP-96-B9 | 6818300.00 | 414565.00 | 1390.00 | 4.10 | - | - | - | 1.9 and 4.0 m | |
| TP-96-B10 | 6818443.00 | 414565.00 | 1390.00 | 1.15 | - | 0.50 | - | - | 0.5 - 1.15 m ice inclusions (Vx) and random ice lenses (Vr). Refusal in frozen ground. |
| TP-96-B11 | 6818540.00 | 414500.00 | 1395.00 | 3.50 | - | - | - | 0.40 | |
| TP-96-B12 | 6818680.00 | 414576.00 | 1378.00 | 4.00 | - | - | - | - | Refusal on boulders. |
| TP-96-B13 | 6818620.00 | 414450.00 | 1404.00 | 3.70 | 3.40 | - | 0.50 | - | 0.5 - 1.3 frozen no visible ice, well bonded, no excess ice (Nbn) |
| TP-96-B14 | 6818630.00 | 414306.00 | 1420.00 | 1.80 | 0.60 | - | - | - | |
| TP-96-B15 | 6818769.00 | 414445.00 | 1395.00 | 2.90 | 1.50 | - | 0.30 | - | 0.3 - 0.9 m frozen well bounded, ice inclusions (Vx to Nbe) |
| TP-96-B16 | 6818680.00 | 414660.00 | 1360.00 | 4.70 | - | - | 0.65 | - | 0.65 - 1.05 m frozen ice inclusions (Vx). |
| TP-96-B17 | 6817537.00 | 414650.00 | 1415.00 | 3.60 | - | - | - | 2.70 | |
| TP-96-B18 | 6817610.00 | 414800.00 | 1393.00 | 5.00 | - | - | 0.80 | - | 0.8 - 1.0 m frozen ice lenses (Vs) 1 - 2 mm thick |
| TP-96-B19 | 6817690.00 | 414890.00 | 1375.00 | 2.60 | - | - | - | 1.0 and 2.5 m | |
| TP-96-B20 | 6815480.00 | 414955.00 | 1410.00 | 2.50 | - | - | 0.10 | 1.50 | 0.1 - 1.5 m frozen no visible ice, well bonded, no excess (Nbn) |
| TP-96-B21 | 6815550.00 | 414930.00 | 1411.00 | 2.60 | 2.50 | - | - | 2.50 | |
| TP-96-S1 | 6819070.00 | 414581.00 | 1355.00 | 5.50 | 4.00 | - | 0.40 | - | 0.4 - 1.4 m frozen ice inclusions (Vx). |
| TP-96-S2 | 6819113.00 | 414647.00 | 1341.00 | 4.00 | - | - | - | - | |
| TP-96-S3 | 6819141.00 | 414700.00 | 1326.00 | 2.80 | - | - | 0.25 | 2.80 | 0.25 - 0.9 m frozen, ice lenses (Vs) up to 1 mm thick |
| TP-96-D1 | 6819035.00 | 414650.00 | 1342.00 | 6.00 | - | - | 1.20 | - | 1.2 - 1.5 ice inclusions (Vx) |
| TP-96-D2 | 6819037.00 | 414680.00 | 1335.00 | 5.30 | - | 2.70 | 0.40 | - | 0.4 - 2 m ice coatings (Vc) and inclusions (Vx), 2 - 2.9 m ice lenses (Vr), 2.7 m no visible ice, well bonded, no excess ice (Nbn) |
| TP-96-D3 | 6819075.00 | 414723.00 | 1324.00 | 5.00 | - | - | 0.40 | - | 0.4 - 1.0 m poorly bonded, friable ice (Nf) and coatings (Vc) |
| TP-96-D4 | 6819070.00 | 414685.00 | 1331.00 | 5.80 | - | - | 0.45 | - | 0.45 - 2.7 m no visible ice, well bounded, no excess ice (Nbn) |
| TP-96-D5 | 6818960.00 | 414710.00 | 1329.00 | 6.00 | - | - | 0.40 | - | 0.4 - 1.8 m ice coating (Vc) and inclusions (Vx) |
| TP-96-D6 | 6819080.00 | 414825.00 | 1328.00 | 5.80 | - | - | 0.35 | - | 0.35 - 5.0 m ice lenses, below 3 m ice content reduces |
| TP-96-D7 | 6819040.00 | 414875.00 | 1338.00 | 5.60 | - | - | 0.35 | - | 0.35 - 2.4 m poorly bonded to friable (Nf) to ice lenses (Vs) 1 - 2 mm thick |
| TP-96-D8 | 6818950.00 | 414860.00 | 1332.00 | 5.50 | - | - | - | 2 - 3 m | rapid water seepage |
| TP-96-D9 | 68190000.00 | 414856.00 | 1332.00 | 5.50 | - | - | - | 3 - 3 m | |
| TP-96-D10 | 6819020.00 | 414950.00 | 1360.00 | 3.70 | - | 3.70 | - | - | 0.3 - 1.4 m ice inclusion (Vs), 1.7 - 2.9 m ice lenses. Refusal on frozen ground. |
| TP-96-D11 | 6818500.00 | 415005.00 | 1368.00 | 4.50 | - | 3.70 | 0.20 | | 0.2 - 1.3 m ice lenses (Vs) friable ice (Nf), 1.7 - 2.9 m ice lenses (Vs) 2.9 - 3.7 m ice inclusions (Vx) and ice lenses (Vs). Refusal on frozen ground. |
| TP-96-D12 | 6818010.00 | 415145.00 | 1374.00 | 1.50 | - | 1.40 | 0.45 | - | 0.45 - 1.5 m no visible ice, well bonded, excess ice (Nbn) 1.4 m ice inclusions (Vx). Refusal on frozen ground. |
| TP-96-D13 | 6817550.00 | 415225.00 | 1368.00 | 3.70 | - | 3.00 | 0.40 | - | 0.4 - 0.8 m ice inclusions (Vx) and ice coatings (Vc), 0.8 - 3.7 m ice inclusions (Vx) ice coatings (Vc) and ice lenses (Vs). Refusal on frozen ground. |
| TP-96-G1 | 6816824.00 | 414955.00 | 1410.00 | 3.90 | 3.50 | - | - | - | |
| TP-96-G2 | 6816631.00 | 414952.00 | 1411.00 | 4.00 | 3.50 | - | 0.40 | 2.10 | 0.4 - 0.8 m frozen ice lenses (Vs) 2 - 4 mm thick |
| TP-96-G3 | 6816355.00 | 414850.00 | 1423.00 | 3.00 | - | - | - | - | |
| TP-96-G4 | 6816090.00 | 414810.00 | 1417.00 | 3.00 | 2.50 | - | 0.40 | 2.80 | 0.4 - 0.55 m frozen ice inclusions (Vx) |
| TP-96-G5 | 6817000.00 | 414640.00 | 1440.00 | 5.30 | - | 1.70 | 0.00 | | frozen throughout pit |
| TP-96-G6 | 6816600.00 | 415563.00 | 1420.00 | 2.30 | - | 1.90 | 0.50 | - | 0.5 - 0.8 m ice coatings (Vc), 0.8 - 1.9 m no visible ice (Nf), 1.9 - 2.3 m ice inclusions (Vx) and coatings (Vc). Refusal on frozen ground. |
| TP-96-G7 | 6816290.00 | 415465.00 | 1440.00 | 2.00 | - | 2.00 | 0.10 | - | 0.1 - 0.4 m no visible ice, well bonded, no excess (Nbn), 1.5 - 2.0 m ice lenses (Vs) |
| TP-96-G8 | 6816050.00 | 415340.00 | 1426.00 | 3.30 | - | - | - | - | |
| TP-96-FC1 | 6814580.00 | 414535.00 | 1454.00 | 0.40 | - | - | - | - | |
| TP-96-FC2 | 6814610.00 | 414530.00 | 1454.00 | 0.10 | 0.00 | - | - | - | |
| TP-96-PC1 | 6814980.00 | 414325.00 | 1535.00 | 0.20 | - | - | - | - | |
| TP-96-PC2 | 6815100.00 | 414250.00 | 1525.00 | 0.10 | 0.10 | - | - | - | |
| TP16-01 | 6814580.00 | 415073.00 | 1398.00 | 4.50 | - | - | - | - | |
| TP16-02 | 6814603.00 | 415027.00 | 1397.00 | 4.30 | 1.50 | - | - | - | |
| TP16-03 | 6814649.00 | 414918.00 | 1409.00 | 3.20 | 2.10 | - | - | - | |

| Test Pit ID | Northing (m) | Easting (m) | Elevation (m) | Depth of Test Pit (m) | Bedrock Depth (m) | Permafrost Depth (m) | Active Layer / Seasonal Permafrost (m) | Groundwater Seepage Depth (m) | Comments |
|-------------|-----------------|----------------|------------------|-----------------------------|-------------------------|----------------------------|---|--|--|
| TP16-04 | 6814660.00 | 414833.00 | 1413.00 | 2.20 | 2.20 | - | - | 2.20 | |
| TP16-05 | 6814974.00 | 414907.00 | 1380.00 | 3.30 | - | - | - | 0.50 | |
| TP16-06 | 6814935.00 | 414979.00 | 1382.00 | 1.60 | - | - | - | 1.30 | |
| TP16-07 | 6815624.00 | 414809.00 | 1398.00 | 2.40 | 0.50 | - | - | - | |
| TP16-08 | 6815332.00 | 414646.00 | 1432.00 | 4.20 | 1.30 | - | - | 2.00 | |
| TP16-09 | 6815671.00 | 414645.00 | 1426.00 | 3.90 | - | - | - | 3.90 | |
| TP16-10 | 6815463.00 | 414544.00 | 1453.00 | 3.00 | 0.60 | 0.30 | - | - | |
| TP16-11 | 6816429.00 | 414690.00 | 1447.00 | 3.50 | 0.80 | - | - | 2.00 | |
| TP16-12 | 6816591.00 | 414480.00 | 1485.00 | 1.60 | 0.10 | - | - | - | |
| TP16-13 | 6816764.00 | 414546.00 | 1452.00 | n/a | 0.20 | - | - | - | Logged cut slope of Tote Road |
| TP16-14 | 6816917.00 | 414472.00 | 1457.00 | n/a | 0.50 | - | - | - | Logged cut slope of Tote Road |
| TP16-15 | 6817229.00 | 414310.00 | 1466.00 | 4.80 | - | - | - | - | |
| TP16-16 | 6817424.00 | 414243.00 | 1472.00 | 1.50 | 0.20 | - | - | - | |
| TP16-17 | 6817760.00 | 414139.00 | 1478.00 | 1.30 | 0.30 | - | - | - | |
| TP16-18 | 6817985.00 | 414045.00 | 1479.00 | 2.30 | 0.20 | - | - | 0.50 | |
| TP16-19 | 6818170.00 | 414021.00 | 1470.00 | 2.80 | 2.80 | - | - | - | |
| TP16-20 | 6818271.00 | 414181.00 | 1441.00 | 2.00 | 0.60 | - | - | - | |
| TP16-21 | 6818971.00 | 414331.00 | 1395.00 | 2.30 | 2.30 | - | - | - | |
| TP16-22 | 6818989.00 | 414423.00 | 1386.00 | 4.50 | - | - | - | - | |
| TP16-23 | 6818370.00 | 414428.00 | 1412.00 | 2.40 | 2.40 | - | - | - | |
| TP16-24 | 6818145.00 | 414409.00 | 1423.00 | 1.50 | 0.30 | - | - | - | |
| TP16-25 | 6816453.00 | 414805.00 | 1425.00 | 1.90 | 1.60 | - | - | - | |
| TP16-26 | 6816975.00 | 414944.00 | 1394.00 | 4.00 | - | - | - | - | |
| TP16-27 | 6816889.00 | 414896.00 | 1413.00 | 2.90 | - | - | - | - | |
| TP16-28 | 6817432.00 | 414783.00 | 1401.00 | 2.70 | 2.20 | - | - | 2.50 | |
| TP16-29 | 6817465.00 | 414894.00 | 1386.00 | 2.30 | 2.30 | - | - | - | Water seeping in at 0.5m from upper layer, but lower zone not saturated, possible barrier or seep from melting ice |
| TP16-30 | 6817827.00 | 414876.00 | 1368.00 | 3.80 | - | - | - | - | |
| TP16-31 | 6817555.00 | 414605.00 | 1412.00 | 4.50 | - | - | - | - | |
| TP16-32 | 6816895.00 | 415051.00 | 1389.00 | 5.00 | - | - | - | - | |
| TP16-33 | 6816478.00 | 415010.00 | 1395.00 | 3.40 | - | - | - | - | |
| TP16-34 | 6816353.00 | 414999.00 | 1391.00 | 4.90 | - | - | - | - | |
| TP16-35 | 6816132.00 | 414963.00 | 1381.00 | 4.50 | 4.50 | - | - | 4.00 | |
| TP16-36 | 6815763.00 | 414886.00 | 1388.00 | 5.10 | - | - | - | - | |
| TP16-37 | 6815556.00 | 414878.00 | 1391.00 | 2.30 | 0.30 | - | - | - | |
| TP16-38 | 6815621.00 | 415088.00 | 1381.00 | 5.00 | - | - | - | - | |
| TP16-39 | 6815883.00 | 415099.00 | 1381.00 | 4.00 | - | - | - | 2.00 | |
| TP16-40 | 6816100.00 | 415196.00 | 1384.00 | 4.50 | - | - | - | 4.00 | |
| TP16-41 | 6815684.00 | 415168.00 | 1402.00 | 3.00 | - | 0.50 | - | - | |
| TP16-42 | 6815361.00 | 415084.00 | 1388.00 | 4.90 | - | - | - | - | |
| TP16-43 | 6815112.00 | 415154.00 | 1403.00 | 1.80 | 1.00 | - | - | - | |
| TP16-44 | 6815262.00 | 415110.00 | 1386.00 | 4.00 | - | - | - | - | |
| TP16-45 | 6815387.00 | 415149.00 | 1408.00 | 3.50 | 3.30 | - | - | - | |
| TP16-46 | 6815484.00 | 415079.00 | 1383.00 | 4.10 | - | - | - | - | |
| TP16-47 | 6815758.00 | 415091.00 | 1382.00 | 4.50 | - | - | - | - | |
| TP16-48 | 6816478.00 | 415140.00 | 1375.00 | 4.00 | - | - | - | - | Water seeping in at 0.5m from upper layer, lower zone not saturated |
| TP16-49 | 6818821.00 | 414317.00 | 1407.00 | 4.20 | 0.70 | - | - | - | |
| TP16-50 | 6818848.00 | 414482.00 | 1379.00 | 5.00 | - | - | - | - | |
| TP16-51 | 6818617.00 | 414346.00 | 1409.00 | 1.70 | 0.30 | - | - | - | |
| TP16-52 | 6818631.00 | 414474.00 | 1390.00 | 2.50 | 2.50 | - | - | - | |
| TP16-53 | 6819075.00 | 414236.00 | 1398.00 | 3.50 | - | - | - | - | |

\KPL\VA-Prj\\$110100640\02\A\Correspondence\VA16-01820 - Geotechnical Characterization with 2016 SI Data\Appendix B\Tables B.1 and B.2_Test Pit and Drillhole Summary.xlsx\Table B1 _test pits

| | | | | |
|-----|----------|-------------------------------|-------|------|
| 0 | 16DEC'16 | ISSUED WITH LETTER VA16-01820 | JAG | LJG |
| REV | DATE | DESCRIPTION | PREPD | RW/D |

TABLE B.2

BMC MINERALS (NO.1) LTD.
KUDZ ZE KAYAH PROJECT

DRILLHOLE SUMMARY

Print Dec/16/16 9:32:50

| Drillhole ID | Northing (m) | Easting (m) | Elevation (m) | End of Drillhole (m) | Bedrock Depth (m) | Measured Water Level (m) | Date of Water Level Measurement | Installations | Completion Zone | | Instrumentation/Well Status | |
|--------------|-----------------|----------------|------------------|----------------------------|-------------------------|--------------------------------|---------------------------------------|-----------------|-----------------|------------|------------------------------------|------------|
| | | | | | | | | | (m) | (m) | | |
| BH95G-01 | 6,820,981.59 | 414,080.36 | 1,305.00 | 28.04 | - | - | - | standpipe | 15.20 | 19.80 | Unknown | |
| BH95G-02 | 6,819,854.47 | 414,351.88 | 1,349.69 | 21.33 | 4.87 | 7.22 | Nov. 2016 | standpipe | 4.50 | 6.00 | Functional | |
| BH95G-2A | 6,819,834.00 | 414,339.00 | 1,360.00 | 8.09 | 4.87 | - | - | standpipe | 23.00 | 27.43 | Unknown | |
| BH95G-03 | 6,819,903.05 | 415,025.00 | 1,357.89 | 27.43 | 22.55 | - | - | standpipe | 18.30 | 22.86 | Unknown | |
| BH95G-04 | 6,819,998.26 | 415,068.36 | 1,377.41 | 22.88 | 9.75 | - | - | - | - | - | - | |
| BH95G-05 | 6,819,903.36 | 414,639.80 | 1,302.69 | 68.88 | 39.62 | - | - | - | - | - | - | |
| BH95G-06 | 6,821,051.58 | 414,299.06 | 1,257.00 | 67.05 | 25.90 | - | - | - | - | - | - | |
| BH95G-6A | 6,820,695.00 | 413,599.00 | 1,360.00 | 18.30 | - | - | - | standpipe | 48.80 | 53.34 | Unknown | |
| BH95G-07 | 6,820,732.85 | 413,972.50 | 1,305.00 | 53.34 | 28.95 | - | - | - | - | - | - | |
| BH95G-7A | 6,820,912.16 | 414,015.10 | 1,315.00 | 19.80 | - | - | - | standpipe | Unknown | Unknown | Unknown | |
| BH95G-08 | 6,820,878.38 | 414,031.35 | 1,305.00 | 32.30 | 23.16 | - | - | standpipe | 20.80 | 22.30 | Unknown | |
| BH95G-08A | 6,820,878.38 | 414,031.35 | 1,320.00 | 22.30 | - | - | - | - | - | - | - | |
| BH95G-09 | 6,821,025.09 | 414,498.91 | 1,324.00 | 24.68 | 15.54 | 10.65 | May 2015 | standpipe | 35.70 | 40.23 | Functional | |
| BH95G-10 | 6,821,022.22 | 414,198.41 | 1,258.00 | 40.23 | - | - | - | standpipe | Unknown | Unknown | Unknown | |
| BH95G-10A | 6,821,022.22 | 414,198.41 | 1,258.00 | 40.23 | - | - | - | - | - | - | - | |
| BH95G-11 | 6,819,256.20 | 414,713.46 | 1,316.60 | 14.94 | - | - | - | - | - | - | - | |
| BH95G-12 | 6,819,258.07 | 414,715.15 | 1,316.49 | 22.56 | - | - | - | - | - | - | - | |
| BH95G-13D | 6,819,009.63 | 414,711.34 | 1,319.51 | 50.30 | 10.67 | - | - | standpipe | 24.20 | 28.65 | Unknown | |
| BH95G-14D | 6,818,997.64 | 414,651.03 | 1,339.97 | 28.65 | 19.35 | - | - | standpipe | 14.70 | 17.60 | Unknown | |
| BH95G-14S | 6,819,000.00 | 414,650.00 | 1,339.97 | 28.65 | 19.35 | - | - | standpipe | 19.00 | 22.00 | Unknown | |
| BH95G-15D | 6,818,975.33 | 414,573.51 | 1,357.83 | 22.58 | 11.90 | - | - | standpipe | Unknown | Unknown | Unknown | |
| BH95G-16 | N/A | N/A | 1,356.00 | 50.30 | 49.70 | - | - | standpipe | 13.00 | 16.00 | Unknown | |
| BH95G-17D | 6,819,048.91 | 414,912.56 | 1,345.16 | 16.46 | 7.62 | - | - | standpipe | 6.00 | 9.00 | Unknown | |
| BH95G-17S | 6,819,051.00 | 414,911.00 | 1,345.16 | 16.46 | 7.62 | - | - | standpipe | 8.40 | 11.40 | Unknown | |
| BH95G-18D | 6,819,067.08 | 414,979.85 | 1,364.21 | 11.90 | 3.96 | - | - | standpipe | 19.00 | 22.00 | Unknown | |
| BH95G-19D | 6,818,963.15 | 414,513.01 | 1,371.60 | 22.56 | 14.32 | - | - | standpipe | 4.80 | 7.80 | Unknown | |
| BH95G-19S | 6,818,964.00 | 414,510.00 | N/A | 22.56 | 14.32 | - | - | standpipe | 9.00 | 12.00 | Unknown | |
| BH95G-20M | 6,817,262.95 | 414,724.80 | 1,415.76 | 12.50 | 3.81 | - | - | standpipe | 21.20 | 24.20 | Unknown | |
| BH95G-21D | 6,819,032.19 | 414,816.21 | 1,320.83 | 24.70 | 15.80 | - | - | standpipe | 7.50 | 10.50 | Unknown | |
| BH95G-21S | 6,819,032.19 | 414,816.21 | 1,320.83 | 24.70 | 15.80 | - | - | standpipe | 6.50 | 9.50 | Unknown | |
| BH95G-20 | 6,815,497.02 | 414,845.41 | 1,395.89 | 10.06 | 1.52 | 2.11 | Nov. 2015 | standpipe | 6.10 | 9.10 | Functional | |
| BH95G-21 | 6,815,640.29 | 414,801.00 | 1,402.45 | 10.08 | 2.00 | 1.60 | Nov. 2016 | standpipe | 2.80 | 5.80 | Functional | |
| BH95G-22 | 6,815,730.99 | 414,929.87 | 1,384.66 | 7.47 | 4.57 | 2.70 | Nov. 2016 | standpipe | 9.80 | 12.80 | Functional | |
| BH95G-23 | 6,815,275.39 | 414,906.38 | 1,385.99 | 14.63 | 14.17 | -0.28 | Sept. 2015 | standpipe | 6.40 | 9.40 | Functional | |
| BH95G-24 | 6,815,259.11 | 415,038.91 | 1,384.36 | 9.75 | 8.53 | Flowing | Sept. 2016 | standpipe | 17.80 | 20.80 | Functional | |
| BH95G-25D | 6,815,525.79 | 415,062.39 | 1,383.38 | 22.25 | 17.07 | 4.29 | Nov. 2016 | standpipe | 8.50 | 11.50 | Functional | |
| BH95G-25S | 6,815,521.00 | 415,074.00 | N/A | 22.25 | 17.07 | 2.13 | Nov. 2016 | standpipe | 10.60 | 13.60 | Functional | |
| BH95G-26 | 6,815,663.92 | 415,060.56 | 1,382.34 | 14.63 | 13.40 | - | - | - | - | - | - | |
| BH95G-27 | 6,812,634.00 | 414,758.00 | 1,377.78 | 19.80 | 16.76 | - | - | - | - | - | - | |
| BH95G-28 | 6,814,945.68 | 415,142.87 | 1,389.47 | 17.68 | 17.07 | 0.73 | Nov. 2015 | standpipe | 15.60 | 18.60 | Functional | |
| BH95G-29 | 6,814,539.60 | 415,196.16 | 1,391.33 | 19.20 | 18.40 | - | Flowing | Sept. 2016 | standpipe | 16.20 | 19.20 | Functional |
| BH95G-30 | 6,816,762.07 | 415,439.70 | 1,386.14 | 19.20 | 12.80 | -0.24 | Oct. 2016 | standpipe | 7.00 | 10.00 | Functional | |
| BH95G-31 | 6,816,130.84 | 415,200.47 | 1,390.91 | 10.06 | 4.57 | -0.84 | Sept. 2016 | standpipe | 12.20 | 15.20 | Functional | |
| BH95G-32 | 6,816,136.36 | 415,009.74 | 1,386.46 | 16.15 | 10.06 | 4.18 | Nov. 2016 | standpipe | 9.10 | 12.10 | Functional | |
| BH95G-33D | 6,816,741.79 | 415,133.19 | 1,389.53 | 13.10 | 7.35 | 5.29 | Nov. 2016 | standpipe | 2.80 | 5.80 | Functional | |
| BH95G-33S | 6,816,743.00 | 415,130.00 | N/A | N/A | N/A | 4.96 | Nov. 2016 | standpipe | Unknown | Dry | - | |
| BH95G-34 | 6,817,200.00 | 419,365.00 | N/A | 22.86 | - | - | - | - | - | - | - | |
| BH95G-35 | 6,817,695.94 | 414,571.80 | 1,421.58 | 16.15 | 6.10 | - | - | standpipe | 7.00 | 10.00 | destroyed by bentonite within well | |
| BH95G-36 | 6,817,448.51 | 414,627.62 | 1,417.63 | 10.08 | 3.35 | - | - | standpipe | 10.00 | 13.00 | Unknown | |
| BH95G-37 | 6,817,454.03 | 414,583.84 | 1,424.54 | 13.11 | 3.81 | 9.90 | Nov. 2015 | standpipe | 154.50 | 160.00 | Functional | |
| DDH95-129 | 6,815,499.87 | 414,602.77 | 1,443.90 | N/A | N/A | 9.39 | Nov. 2016 | standpipe | 123.50 | 128.00 | Functional | |
| DDH95-131 | 6,815,379.60 | 415,174.76 | 1,414.60 | N/A | N/A | 31.21 | Nov. 2016 | standpipe | Unknown | Functional | Frozen, artesian | |
| DDH95-135 | 6,815,569.80 | 415,149.51 | 1,402.83 | N/A | N/A | 0.00 | Nov. 2015 | standpipe | 134.10 | 138.70 | - | |
| DDH95-146 | 6,815,490.28 | 414,889.98 | 1,388.30 | N/A | N/A | Flowing | Oct. 2016 | standpipe | - | - | Functional | |
| DDH95-148 | 6,815,604.02 | 414,942.47 | 1,383.31 | N/A | N/A | - | - | standpipe | 174.30 | 178.90 | Unknown | |
| DDH95-150 | 6,815,685.77 | 414,748.12 | 1,413.00 | N/A | N/A | 12.88 | Nov. 2015 | monitoring well | 10.00 | 18.80 | Functional | |
| K15-330 | 6,818,696.00 | 414,924.00 | 1,347.00 | 50.95 | 10.60 | - | - | thermistors | - | - | Functional | |
| K15-331 | 6,816,411.00 | 415,347.00 | 1,387.00 | 32.00 | 13.50 | - | - | thermistors | - | - | Functional | |
| K15-333 | 6,816,220.00 | 415,045.00 | 1,381.00 | 71.35 | 6.35 | - | - | - | - | - | - | |
| K15-334 | 6,819,164.00 | 414,781.00 | 1,317.00 | 50.50 | 18.10 | - | - | - | - | - | - | |
| K15-335 | 6,817,327.00 | 414,667.00 | 1,421.00 | 32.33 | 2.50 | - | - | thermistors | - | - | Functional | |
| K15-336 | 6,819,016.00 | 414,792.00 | 1,318.00 | 50.50 | 17.50 | - | - | thermistors | - | - | Functional | |
| MW15-01 | 6,816,750.00 | 414,347.00 | N/A | 20.00 | 1.70 | 12.21 | March 2016 | monitoring well | 23.00 | 31.70 | Functional | |
| MW15-02 | 6,816,270.00 | 414,808.00 | N/A | 32.00 | 1.60 | Flowing | Sept. 2015 | monitoring well | 4.10 | 7.10 | Functional | |
| MW15-03S | 6,816,049.00 | 416,314.00 | N/A | 7.06 | 6.70 | 6.35 | March 2016 | monitoring well | 10.10 | 16.00 | Functional | |
| MW15-03D | 6,816,049.00 | 416,314.00 | N/A | 18.51 | 6.70 | 3.05 | March 2016 | monitoring well | 11.20 | 14.10 | Functional | |
| MW15-04S | 6,816,156.00 | 415,782.00 | N/A | 14.10 | 11.90 | 9.44 | March 2016 | monitoring well | 27.10 | 32.90 | Functional | |
| MW15-04D | 6,816,158.00 | 415,782.00 | N/A | 18.51 | 11.90 | 9.27 | March 2016 | monitoring well | 4.60 | 7.60 | Functional | |
| MW15-05S | 6,816,872.00 | 415,850.00 | N/A | 30.00 | 8.50 | 11.72 | March 2016 | monitoring well | 6.50 | 9.40 | Functional | |
| MW15-05D | 6,816,872.00 | 415,850.00 | N/A | 9.70 | 10.90 | Flowing | Sept. 2015 | monitoring well | 8.10 | 11.00 | Functional | |
| MW15-06 | 6,816,730.00 | 415,455.00 | N/A | 42.00 | 21.00 | - | Flowing | March 2016 | monitoring well | 26.30 | 32.10 | Functional |
| MW15-07S | 6,817,786.00 | 414,915.00 | N/A | 9.55 | - | -0.84 | Aug/Sep 2015 | monitoring well | 25.70 | 31.50 | Functional | |
| MW15-08D | 6,818,550.00 | 414,902.00 | N/A | 33.00 | 14.20 | Flowing | Sept. 2015 | monitoring well | 8.70 | 11.60 | Functional | |
| MW15-08S | 6,818,520.00 | 414,902.00 | N/A | 11.63 | - | Flowing | Sept. 2015 | monitoring well | 29.80 | 35.60 | Functional | |
| MW15-08D | 6,818,520.00 | 414,902.00 | N/A | 36.00 | 14.90 | 0.97 | Nov. 2015 | monitoring well | 11.40 | 17.30 | Functional | |
| MW15-09S | 6,819,176.00 | 414,705.00 | N/A | 17.27 | - | -0.40 | Sept. 2015 | monitoring well | 35.10 | 40.90 | Functional | |
| MW15-09D | 6,819,176.00 | 414,705.00 | N/A | 42.00 | 21.00 | Flowing | Sept. 2015 | monitoring well | 6.60 | 9.60 | Functional | |
| MW15-10S | 6,819,204.00 | 414,788.00 | N/A | 9.55 | - | -0.84 | Aug/Sep 2015 | monitoring well | 25.70 | 31.50 | Functional | |
| MW15-10D | 6,819,204.00 | 414,788.00 | N/A | 36.00 | 21.00 | -0.88 | March 2016 | monitoring well | 4.15 | 7.05 | Functional | |
| MW15-11S | N/A | N/A | N/A | 7.00 | - | 1.90 | March 2016 | monitoring well | 20.60 | 35.20 | Functional | |
| MW15-11D | N/A | N/A | N/A | 35.20 | 7.50 | - | Flowing | Nov. 2015 | N/A | N/A | Functional | |
| K16-379 | 6,814,627.00 | 414,964.00 | 1,405.00 | 39.70 | 5.90 | 1.97 | July 2016 | viv piezometers | - | - | Functional | |
| K16-387 | 6,817,991.00 | 414,571.00 | 1,411.00 | 34.00 | 3.30 | 4.57 | July 2016 | thermistors | - | - | Functional | |
| K16-389 | 6,818,334.00 | 414,361.00 | 1,421.00 | 42.00 | 10.40 | 3.48 | July 2016 | thermistors | - | - | Functional | |
| K16-390 | 6,818,779.00 | 414,323.00 | 1,409.00 | 38.60 | 2.10 | 4.95 | July 2016 | thermistors | - | - | Functional | |
| K16-392 | 6,817,471.00 | 414,852.00 | 1,399.00 | 46.20 | | | | | | | | |

| Drillhole ID | Northing (m) | Easting (m) | Elevation (m) | End of Drillhole (m) | Bedrock Depth (m) | Measured Water Level (m) | Date of Water Level Measurement | Installations | Completion Zone | | Instrumentation/Well Status |
|--------------|-----------------|----------------|------------------|----------------------------|-------------------------|--------------------------------|---------------------------------------|-----------------|-----------------|-------|-----------------------------|
| | | | | | | | | | (m) | (m) | |
| K16-411 | 6,816,237.00 | 415,947.00 | 1,446.00 | 34.10 | 18.20 | 3.13 | July 2016 | thermistor | - | - | Functional |
| K16-412 | 6,816,061.00 | 416,070.00 | 1,464.00 | 38.70 | 19.20 | 6.80 | July 2016 | thermistor | - | - | Functional |
| MW16-12D | 6,816,530.00 | 415,278.00 | 1,369.00 | 28.20 | 7.20 | Flowing | July 2016 | monitoring well | 20.50 | 27.60 | Functional |
| MW16-12S | 6,816,530.00 | 415,274.00 | 1,369.00 | 8.00 | 7.20 | -0.01 | July 2016 | monitoring well | 2.60 | 4.30 | Functional |
| MW16-13 | 6,817,774.00 | 414,011.00 | 1,503.00 | 27.90 | 1.10 | Frozen | July 2016 | monitoring well | 19.10 | 27.00 | Frozen |
| MW16-14D | 6,818,386.00 | 414,779.00 | 1,342.00 | 40.20 | 4.80 | -0.73 | July 2016 | monitoring well | 30.80 | 38.80 | Functional |
| MW16-14S | 6,818,383.00 | 414,780.00 | 1,341.00 | 4.50 | - | 3.18 | July 2016 | monitoring well | 2.30 | 4.60 | Functional |
| MW16-15D | 6,814,702.00 | 414,976.00 | 1,402.00 | 42.20 | 5.70 | 8.64 | July 2016 | monitoring well | 28.80 | 36.60 | Functional |
| MW16-15S | 6,814,699.00 | 414,977.00 | 1,401.00 | 6.00 | 5.70 | 3.93 | July 2016 | monitoring well | 3.10 | 5.30 | Functional |
| MW16-16 | 6,817,229.00 | 415,395.00 | 1,393.00 | 40.30 | 3.90 | 19.82 | July 2016 | monitoring well | 31.50 | 38.80 | Functional |
| MW16-17 | 6,817,489.00 | 414,634.00 | 1,418.00 | 31.10 | 1.60 | 2.61 | July 2016 | monitoring well | 20.30 | 27.70 | Functional |

\KPL\VA-Pr\\$1\0100640\02\A\Correspondence\VA16-01820 - Geotechnical Characterization with 2016 SI Data\Appendix B\Tables B.1 and B.2_Test Pit and Drillhole Summary.xlsx\Table B2_drillholes

| | | | | |
|-----|---------|-------------------------------|-------|------|
| 0 | 16DEC16 | ISSUED WITH LETTER VA16-01820 | JAG | LJG |
| REV | DATE | DESCRIPTION | PREPD | RWWD |