YEIP
2001
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Geophysical and Geochemical Report:
Dunn Claims 1-24
YC20619-YC20642
NTS 115-0-11
Dawson Mining District

Prepared by 19651 Yukon Inc

In Compliance with YMIP#01-070

January 30, 2002

YEIP
01-070
2002

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GRID DATA OF MAG & GRADIENT VALUES

YUKON ENERGY, MINES
& RESOURCES LIBRARY
PO Box 2703
Whitehorse Yukon Y1A 2C6

SUMMARY & RECOMMENDATIONS

The program on the Indian River Dunite covered by DUN 1 to 24 consisted of hand trenching and minor sampling, along with a geophysical survey that covered the center of the intrusion The sampling showed elevated levels of chromium but only trace amounts of PGEs along left limit or west side of Bishop Cr The 2000 sampling program identified anomalous PGE values on the right limit or east side of Bishop Cr going into the thicker section of the intrusive The geophysics identified some gradient anomalies within along side the magnetic anomalies The VLF survey showed a mildly conductive zone coincidental with a gradient anomaly and local mag high running off the edge of the ultramafic This was on L 102+00E @ 93+12 5N to L 101+50E @ 93+75N and over to L 101+00E @ 93+75N Another mild conductor was on L 101+00E @ 99+00N on the edge of a magnetic high which is most likely the edge of the ultramafic The Cutler VLF station was used as the transmitter for L 102+00E & L 101+50E This transmitter could not be picked up the next day and the Seatle station was used This station signal was a strong signal but a weaker dip needle response was recorded The null was recorded facing SW for the Cutler station and facing E for the Seatle station

The gradient showed some intense swings within the ultramafic (as identified with the mag), which signifies segregations of magnetic material This signature is highly suspect of a layered ultramafic The most intense gradient anomaly in the magnetic anomaly of the ultramafic is, starting at L 100+00E @ 91+00N to L 100+50E @ 90+87 5N to L 101+00E @ 90+62 5N Another is at L 102+00E @ 96+00N to L 101+50E @ 96+12 5N The drill and Cat will be now used for exposing and sampling these anomalies and others More geophysics is also warranted to close off and delimiate the extensions of the ultramafic and the anomalies within it

Location and Access to Indian River Dunite

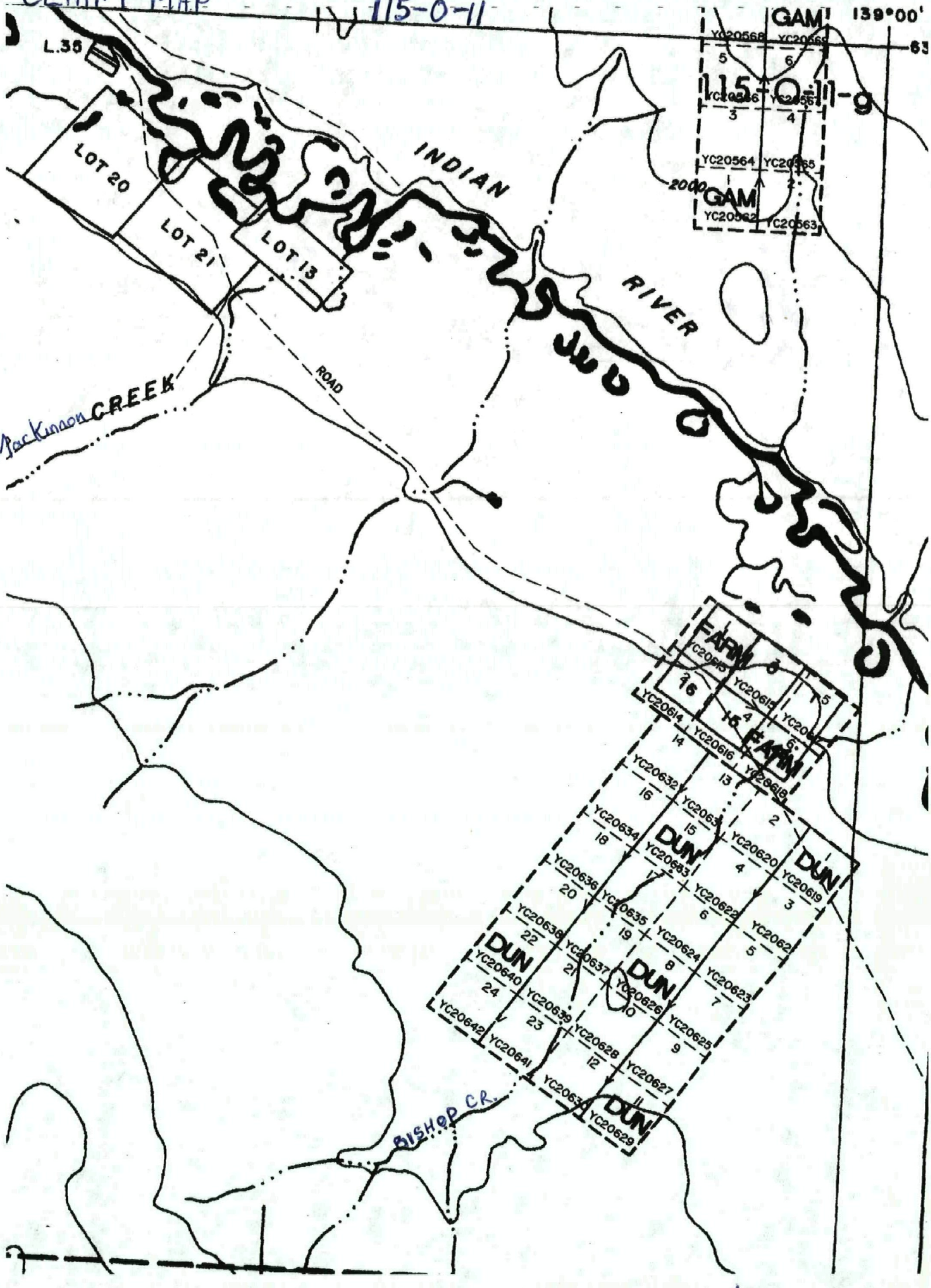
The Indian River Dunite prospect is covered by Dun 1 to 24 and is located approximately 45 km by road south and east from Dawson City It is on map sheet 115-O-11 in the Dawson Mining District The prospect is accessed from Dawson City via the Hunker or Bonanza Creek roads off the Klondike Highway east of Dawson City Either of these roads are taken 20 km to Quartz Cr turn off to the south The Quartz Cr Road is followed 12 km downstream to the mouth of Quartz Cr to the old sunken dredge The road takes off here to the left and goes upstream along the Indian River 9 km to the Indian River Hay Farm From here one travels south along a cat trail 1 5 km to edge of the Dun claims at Bishop Cr by ATV 4 wheeler The 4 wheeler trail is followed another 1 5 km up the right limit of Bishop Cr through the geophysics grid done this year

SUMMARY OF WORK DONE

The work on the Indian River Dunite covered by claims DUN 1 to 24 consisted of hand trenching and blasting 8 sample sites over a three-day period in June and a geophysical survey over a 12-day period in January The drilling and trenching part of the program could not be completed due to time constraints This follow up part of the program on the identified anomalies will be completed as soon as time allows, since we have the use of the drill for the next couple months The geophysics program was broken up into 8 days of line cutting, and picketing and 4 days of running the geophysical equipment During this time 9 4 km of grid was put in, 8 4 km of mag / gradient was run and 4 5 km of VLF was run The grid had lines coming off a baseline every 50 m, with stations marked every 25 m The mag / gradient survey had readings taken every 12 5 m along the line while the VLF had readings taken every 25 m on these lines Due to the extremely dense bush and time constraints only the center portion of the intrusion complex, identified through the aeromag, was covered by grid and the resulting geophysics The grid work was performed by Vern Matkovich, Carl Jonas, and Tom Morgan, and the mag / gradient survey was completed by Shawn Ryan with his Scintrex mag / gradient instrument Tom Morgan put in the VLF survey with the Geophonics dip needle unit Shawn and Vern spent a day defining target anomalies between lines and stations after everything had been plotted The ground survey worked well for showing detail within the ultramafic that the aeromag blended together in an amalgamated high Some cross lines need to be run to see if the orientation of the lines are giving a proper VLF profile of a conductor cross over More grid work and geophysics is needed on this intrusion and its edges, to be followed up by drilling and maybe trenching to see if correlations do exist

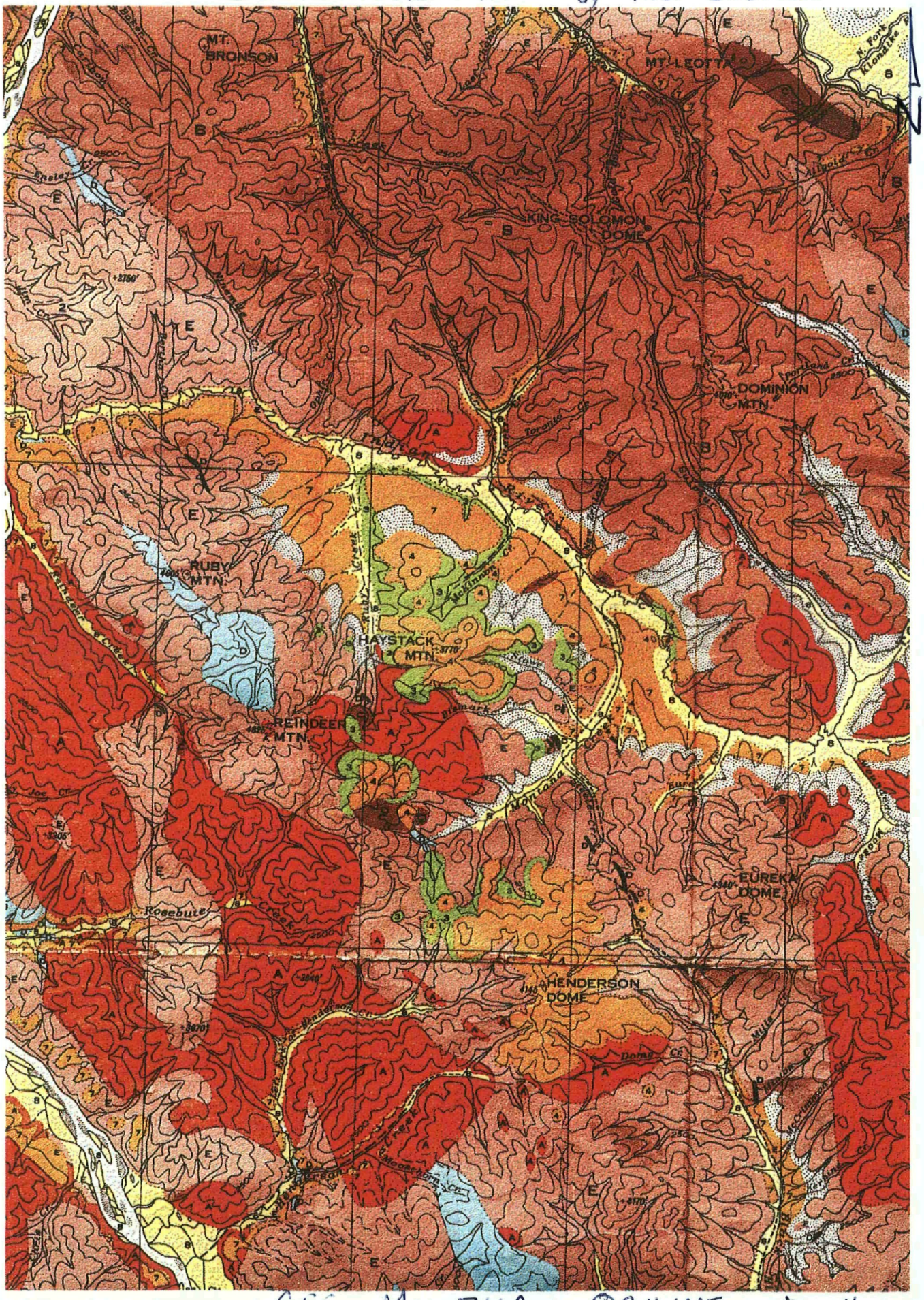
CLAIM MAP

115-0-11



1 in. = ½ mi.

GEOLOGICAL MAP by H.S. BOSTOCK



GSC MAP 711A OGILVIE 1in. = 4mi.

Regional Geological Legend
115-0-1 and 115-0-2

by H S. Bostock

RECENT
8-Stream deposits

TERTIARY AND MODERN
7-Stream deposits

SELKIRK SERIES
6-Basalt, andesite

TERTIARY
EOCENE OR LATER
5-Granite porphyry, syenite porphyry
4-Andesite, basalt, dacite, trachyte, rhyolite, breccia, tuff, agglomerate

EOCENE
3-Conglomerate, sandstone, shale, coal, tuff

JURASSIC OR LATER
2-Chiefly granite and granodiorite

ORDOVICIAN OR LATER
1-Argillite, sandstone, conglomerate

PRECAMBRIAN AND LATER
A-Chiefly gneissic granite
B-Klondike schist sericite schist, minor chlorite schist
C- Gabbro, pyroxene, peridotite, serpentine
D-Limestone
E-Gneiss, quartzite, schist, slate

MAP 711A
OGILVIE, YUKON
Scale 1 253,440
One inch to 4 miles

Sample Descriptions DUN 2001

June 8

DUN-21-R-001
Composite grab sample over 1 0 m from blasted, hand dug pit 1 0 m below moss in a decayed slightly serpentinized dunite This sample pit is on the left limit of Bishop Cr in the south west extension of dunite intrusion at a
UTM reading of 07V 0597584
7064398

DUN-21-R-002
0 5 m sample of subcrop material taken on top of permafrost at 1m deep, 30 m down slope or east of R-001 Dunite is a blocky uniform grained intrusive

June 9

DUN-21-R-003
Sample pit in a recessively decaying creek bank blasted and dug approximately 60 m NE along creek bank slope from R-002 Rust stained slightly serpentinized dunite material from 1 5 m deep over a 0 5 m long sample section from pit bottom UTM reading of 07V 0597652
7064404

DUN-21-R-004
Sample pit is at 35 m NE from R-003 at base of the slope The sample is in a hard blocky fine-grained dark dunite that was taken across 1 m from a depth of 1 m

DUN-21-R-005
Sample pit is located 30 m upslope from R-004 The dunite here is decayed and serpentinized and was sampled over 0 5 m in subcrop 1 m below surface

DUN-21-R-006
Channel sample of subcrop material taken from a black, fractured dunite with clay infillings (serpentinized), over 1 m, at a depth of 1 m UTM 07V 0597711
7064538

June 10

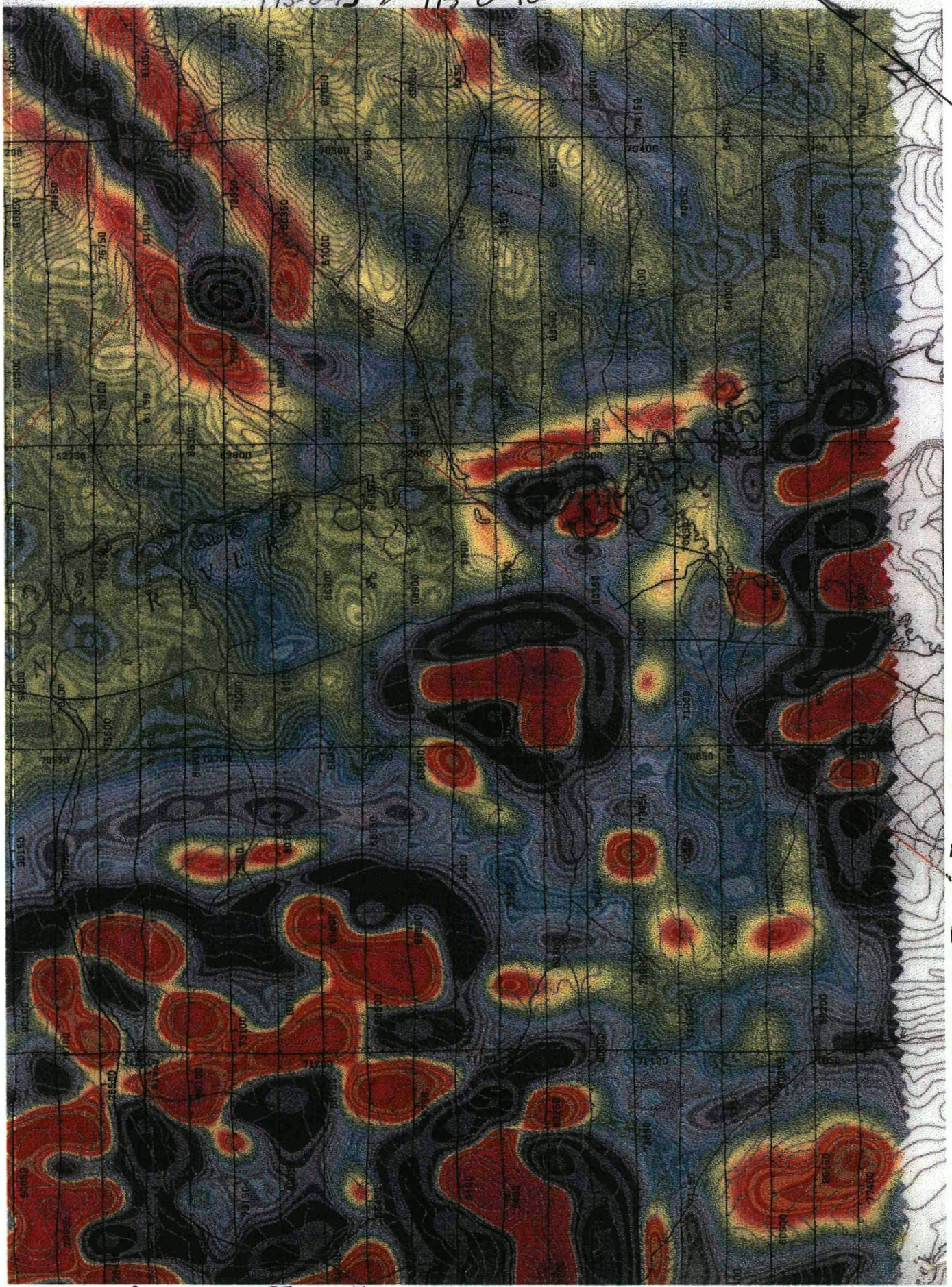
DUN-21-R-007
Channel sample in subcrop on edge of NE extension of dunite just before it becomes covered by gravel beds Sample section is over 0 75 m at a 1 m depth This sample is the same material as R-006 and is 30 m from it

DUN-21-R-008
1 m chip sample of hard dark green dunite outcrop on right limit bankof Bishop Cr Which is below Pin Hill

TABULATION OF RESULTS FOR 2001 DUN

	(~~~~~~~~~~~~~~~~~~ppm~~~~~~~~~~~~~~~~~~)(~~~~%~~~~)												
SAMPLE #	Au	Pd	Pt	Cu	Sb	Cd	Co	Ni	Cr	Mn	Ca	Fe	Mg
DUN-21-R-001	-	0 01	-	6	12	-	74	1304	1267	842	1 06	4 00	8 03
DUN-21-R-002	-	0 03	0 01	6	14	-	70	1272	1278	383	0 61	3 27	9 61
DUN-21-R-003	-	0 02	-	11	15	-	72	1509	1408	318	0 54	3 61	9 59
DUN-21-R-004	-	-	-	14	10	-	76	1395	920	448	1 00	2 98	11 0
DUN-21-R-005	-	-	-	14	12	-	98	1967	1494	671	0 03	4 61	14 0
DUN-21-R-006	-	-	-	25	13	-	104	1656	1265	766	0 04	4 05	10 0
DUN-21-R-007	-	0 01	-	21	12	-	101	1718	1285	917	0 05	4 85	8 93
DUN-21-R-008	0 01	0 02	-	15	11	-	75	1405	1107	368	0 02	3 73	9 56

115-0-15 // 115-0-10



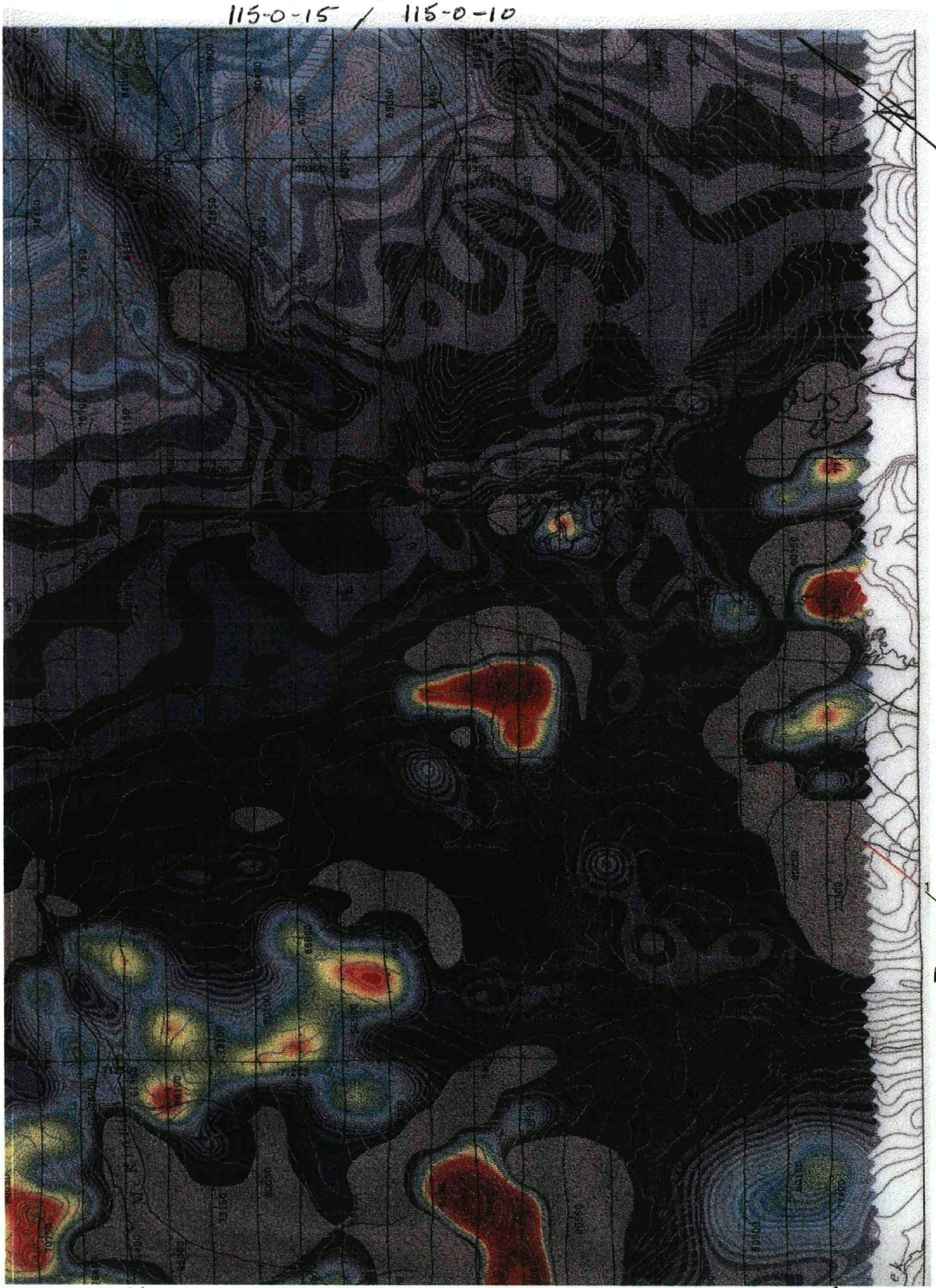
115-0-10

115-041

RESIDUAL TOTAL FIELD

1:50,000

115-0-15 / 115-0-10

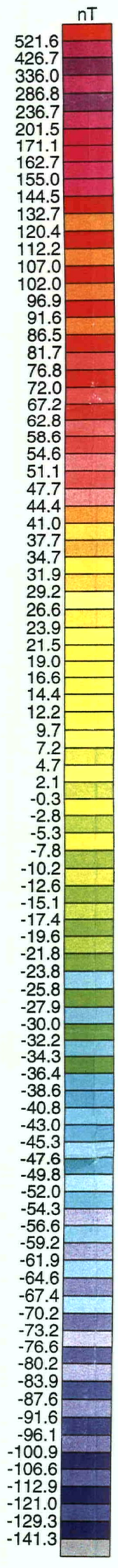


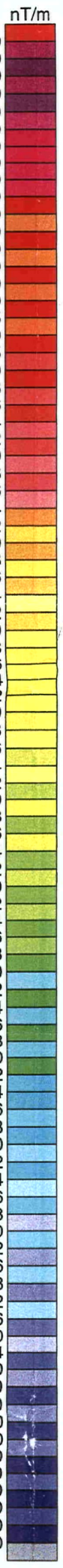
115-0-10

115-0-11

MAGNETIC FIRST DERIVATIVE

1:50,000





RESIDUAL TOTAL FIELD

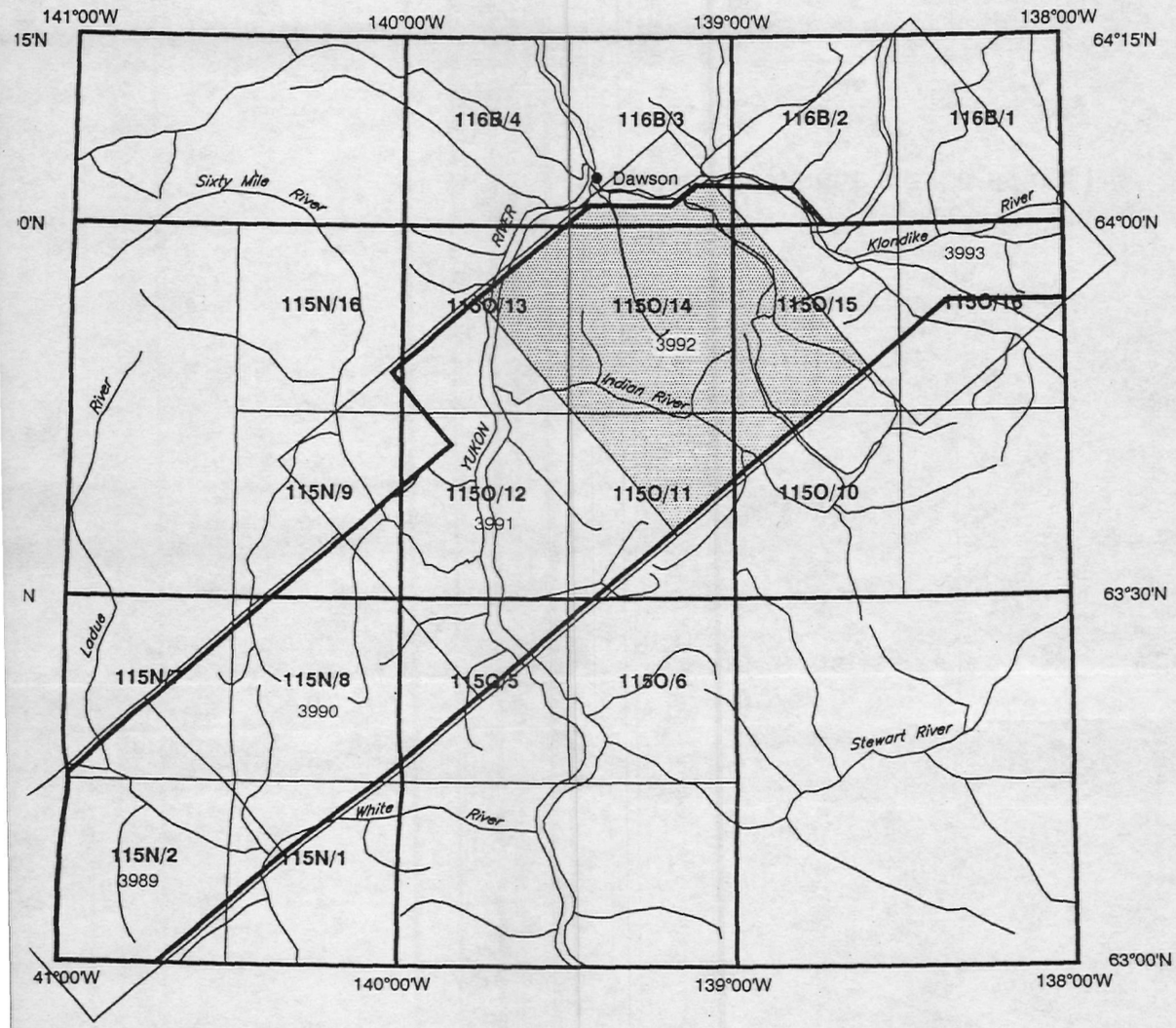
MAGNETIC FIRST DERIVATIVE

2001-8 GSC REPORT

Flight lines, fiducial / Lignes de vol, fiducie ..... 10100 < 42500

Recommended citation:
Shives, R.B.K., Carson, J.M., Ford, K.L., Holman, P.B., Gordey, S., Abbott, G., 2001
Geological Survey of Canada Open File 3992,
Exploration and Geological Services Division, Yukon, Indian and Northern Affairs Canada Open File 2001-8,
Magnetic Anomaly Map (Residual Total Field),
Stewart River Area - 115O/14,
Scale 1:50,000

Notation bibliographique conseillée;
Shives, R.B.K., Carson, J.M., Ford, K.L., Holman, P.B., Gordey, S., Abbott, G., 2001
Commission géologique du Canada Dossier Public 3992,
Affaires indiennes et du Nord, Région du Yukon, Exploration et services de géologies Dossier Public 2001-8,
Carte des anomalies magnétiques (Champ résiduel total),
Stewart River Area - 115O/14,
échelle 1/50 000



NATIONAL TOPOGRAPHICAL SYSTEM REFERENCE AND GEOPHYSICAL MAP INDEX

SYSTÈME NATIONAL DE RÉFÉRENCE CARTOGRAPHIQUE ET INDEX DES CARTES GÉOPHYSIQUES

(MAGNETIC FIRST DERIVATIVE)

MAGNETIC ANOMALY MAP (RESIDUAL TOTAL FIELD)

CARTE DES ANOMALIES MAGNÉTIQUES (CHAMP RÉSIDUEL TOTAL)

STEWART RIVER AREA
YUKON TERRITORY / TERRITOIRE DU YUKON

115 O/14

GEOLOGICAL SURVEY OF CANADA

COMMISSION GÉOLOGIQUE DU CANADA

This map was compiled from data acquired during an airborne geophysical survey (gamma ray spectrometer, magnetometer and VLF EM) carried out by Fugro utilizing an Aerospatiale AS350B2 helicopter (registration C FZTA) The survey operations were carried out from July 29 2000 to September 21 2000

Flight path was recovered using a post flight differential Global Positioning System A vertically mounted video camera was used for verification of the flight path The average traverse line spacing was 500 m with control lines flown at 3 5 km intervals Helicopter flight height was maintained at an average ground clearance of 120 m

The gamma ray spectrometry data were recorded at a 1 0 second sample rate into 256 channel main and radon spectra using an Exploranium GR820 spectrometry system The volume of NaI in the two detectors comprising the system were main detector 33 4L radon detector 8 4L Counts from the main detector were recorded in five windows corresponding to thorium (2410 2810 kev) uranium (1660 1860 kev) potassium (1370 1570 kev) total radioactivity (400 2815 kev) and cosmic radiation (3000 >6000 kev) Counts from the radon detector were recorded in the radon window (1660 1860 kev) The radon detection system was calibrated following methods outlined in AGSO 1995/60 After removal of the background the data were corrected for spectral interferences changes in temperature pressure and departures from the 120 m planned survey elevation The data were then converted to standard concentration units and ratios which were interpolated to a 125 m square grid for display as colour interval maps

The aeromagnetic data were recorded at a 0 1 second sample rate using a 0 01 nT sensitivity split beam cesium vapour magnetometer suspended 23 m below the helicopter The control line and traverse line magnetic data were corrected for variations in the magnetic field using the magnetic ground station magnetometer data After editing the survey data the intersections of traverse and control lines were established and the differences in the magnetic values were computer analysed to obtain the levelling network The levelled total field values were interpolated to a 125 m square grid Global Positioning System data were used to calculate the grid of International Geomagnetic Reference Field data circa 2000 7 which was subtracted from the total magnetic field grid The resulting residual magnetic field grid presented as a colour interval map The grid of the first vertical derivative of the magnetic field was then computed from the residual magnetic field and is presented as a colour interval map

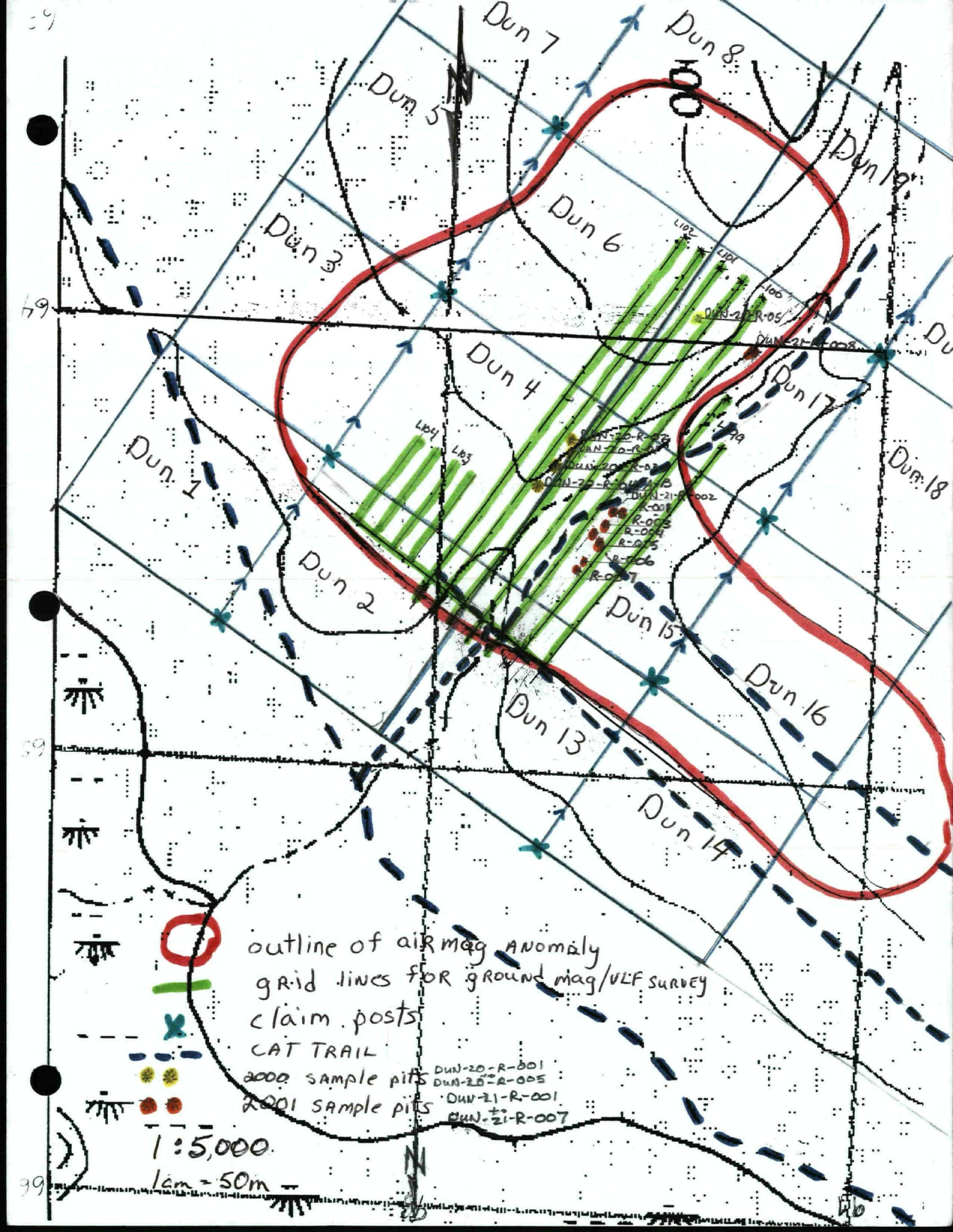
VLF total field and quadrature components for two frequencies were recorded using a Herz Totem 2A system The line station was tuned to station NAA at Cutler MA transmitting at 24 0 kHz The ortho station was tuned to the 24 8 kHz station NLK at Seattle WA VLF data were recorded 4 times per second VLF data will only be made available with the digital data

The base map was reproduced by Geological Survey of Canada Pacific from digital topographic files provided by Geomatics Canada

Les données utilisées pour la compilation de cette carte ont été enregistrées au cours d un leve geophysique aéroporte (spectrométrique gamma aeromagnétique et VLF EM) effectué par Fugro avec un hélicoptère Aerospatiale AS350B2 Immatricule C FZTA Le levé a été réalisé du 29 juillet au 21 septembre 2000

Le recouvrement des lignes de vol s'est fait à l aide de mesures de système de positionnement global corrigées en mode différentiel après vol Une caméra vidéo montée verticalement a été utilisée pour la vérification du plan de vol L espacement moyen des lignes de vol était de 500 m recoupées par des lignes de controle separées d environ 3 5 km les unes des autres L hélicoptère a maintenu une altitude moyenne de 120 m au dessus du sol

Les données spectrométriques des rayons gamma ont été enregistrées selon un taux



Dun 1
Dun 2
Dun 3
Dun 4
Dun 5
Dun 6
Dun 7
Dun 8
Dun 13
Dun 14
Dun 15
Dun 16
Dun 17
Dun 18
Dun 19
L102
L101
L100
L104
L103
L99
DUN-20-R-05
DUN-21-R-008
DUN-20-R-02
DUN-20-R-01
DUN-20-R-03
DUN-20-R-04A-B
DUN-21-R-002
R-001
R-003
R-004
R-005
R-006
R-007
outline of air mag anomaly
grid lines for ground mag/VLF survey
claim posts
CAT TRAIL
2000 sample pits DUN-20-R-001 to DUN-20-R-005
2001 sample pits DUN-21-R-001 to DUN-21-R-007
1:5,000
1cm = 50m

Date 02/01/23,24 Project Dun 02

Job No. part lines 9900, 9950, 10000, 10050, 10100, 10150, 10200 Mag.

GRID LINES RUNNING @ 225°SW, 45°NE

411D Strickland Street,
Whitehorse, Yukon
Y1A 2K3
Phone : (403) 667-4639
Fax : (403) 668-2734

Project Dun. 02

20 Mag.

57,000 +

Abour 2500

2000-2500

1500-2000

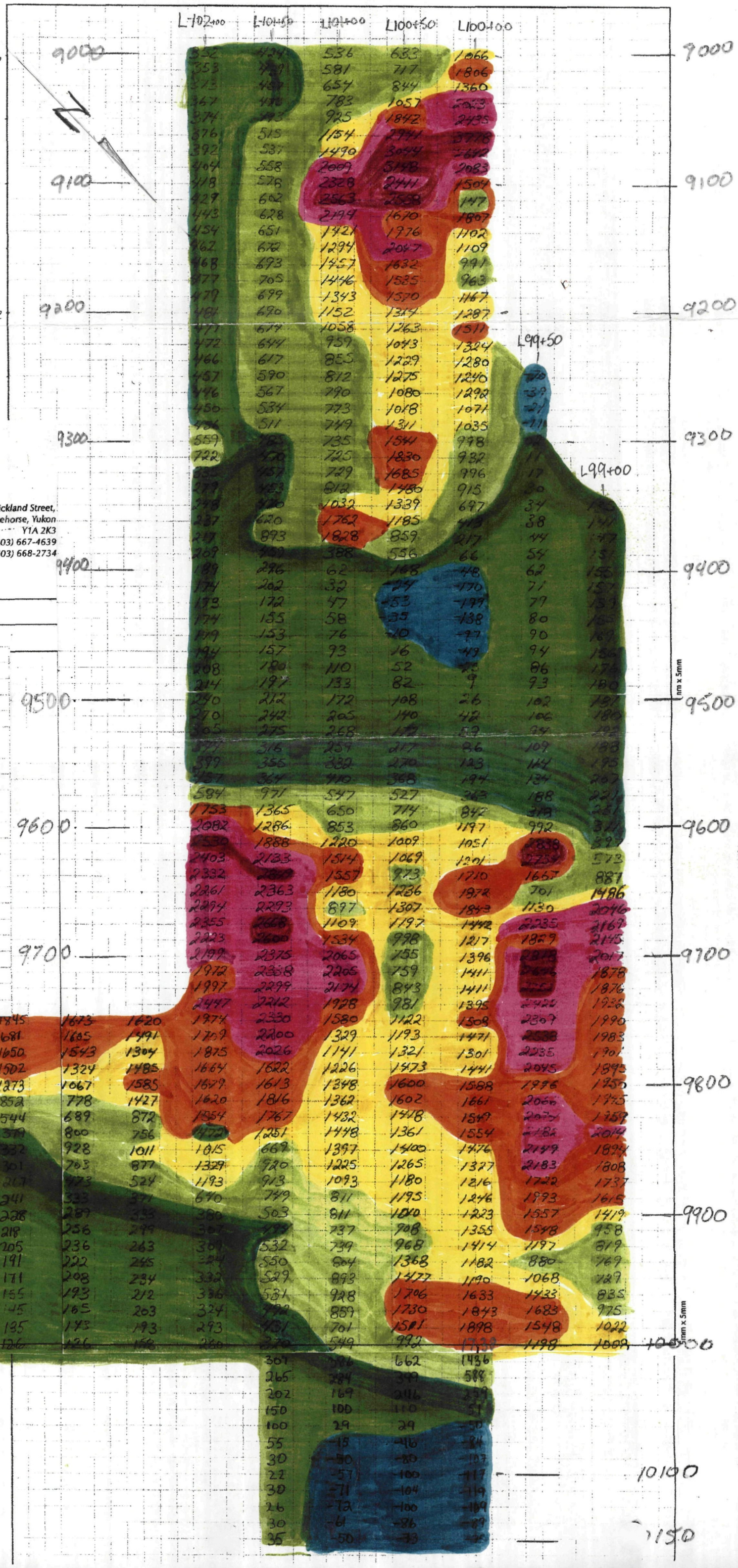
1000-1500

500-1000

0-500

below 0

1cm. = 25m



Job No PART LINES 7900, 9950, 10000, 10050 GRADIENT
10100, 10150, 10200

GRID LINES RUNNING @
225° SW / 45° NE

411D Strickland
Whitehorse,
Y
Phone (403) 66
Fax (403) 66

Project Dan 92
GRADIENT

1cm = 25m

9000	9100	9200	9300	9400	9500	9600	9700	9800	9900	10000	10100	10150
2	1	-2	-9	-14								
1.2	5	-2	-10	106								
29	7	-4	-16	-10								
2	7	-5	-29	92								
2	-.7	-6	-4	22								
.1	.2	46	86	484								
1	.6	-44	-86	78								
.4	-.3	41	149	32								
1.	.6	53	-59	266								
1	14	71	37	-320								
1	.9	54	-61	93								
1	2	-38	81	-7								
.7	2	-34	64	.6								
.4	3	-23	-21	-18								
1	3	-2	35	-14								
1	2	5	19	-3								
1.	2	-.4	-16	9								
-.1	3	3	29	42								
-.4	1	2	4	55								
-.1	.5	6	30	38								
-3	.1	1	19	32	-5							
-2	.9	1	4	54	-1							
-1	-.4	2	-5	13	-1							
-2	-.1	.7	31	15	-1							
7	-1	-.9	47	8	-1							
60	-.8	-2	-87	5	-1							
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-9	-.8	.7	41	18	-.6							
-3	-.4	5	28	-.1	-.4	-1						
-2	.3	107	26	-16	-.7	.2						
-4	66	116	6	-22	-.9	.1						
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-4	-8	-27	-21	-23	-.4	.3						
-5	-7	-14	-18	-25	-.2	-1						
-2	-6	-8	-12	-16	-.2	-2						
-3	-4	-6	-8	-7	-.2	-.4						
-2	-4	-4	-6	-7	.2	.2						
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-9	-4	-7	-6	-7	-8	2						
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-47	21	6	5	-11	-19	-4						
94	5	24	-.9	23	-39	-6						
-145	-19	8	-4	44	-89	-9						
110	-84	16	3	-3	175	-15						
3	49	32	-6	3	146	-10						
11	207	34	-21	52	-5	-16						
8	.7	-21	9	52	-98	30						
11	-16	-35	-13	57	-40	55						
36	61	17	3	23	130	51						
8	27	-23	-7	-14	-65	41						
26	-13	-44	-40	7	121	26						
22	8	-10	20	4	36	12						
-6.6	22	45	-18	2	81	12						
607	9	7	-10	-3	16	14						
-641	77	-12	-2	10	4	19						
-264	74	27	9	-4	67	22						
413	32	-33	5	-33	6	8						
40	-67	-15	14	-6	-12	10						
469	-34	7	20	-1	-12	19						
25	-64	3	18	9	14	19						
525	54	18	5	-7	9	21						
-1083	28	20	-1	-.8	29	31						
257	-58	17	9	-8	21	16						
297	-33	5	3	-15	68	19						
378	-14	5	3	-16	-4	20						
-135	-12	-6	13	-2	63	20						
-21.1	-27	-6	-5	-11	-10	22						
-139	-9	-5	-13	12	31	-22						
-8.0	3	-3	-9	30	-2	-12						
-39	3	3	19	-6	-34	-5						
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.7	1	9	54	38	47	18						
.8	⊙	4	31	50	33	18						
5	2	-2	1		6	18						
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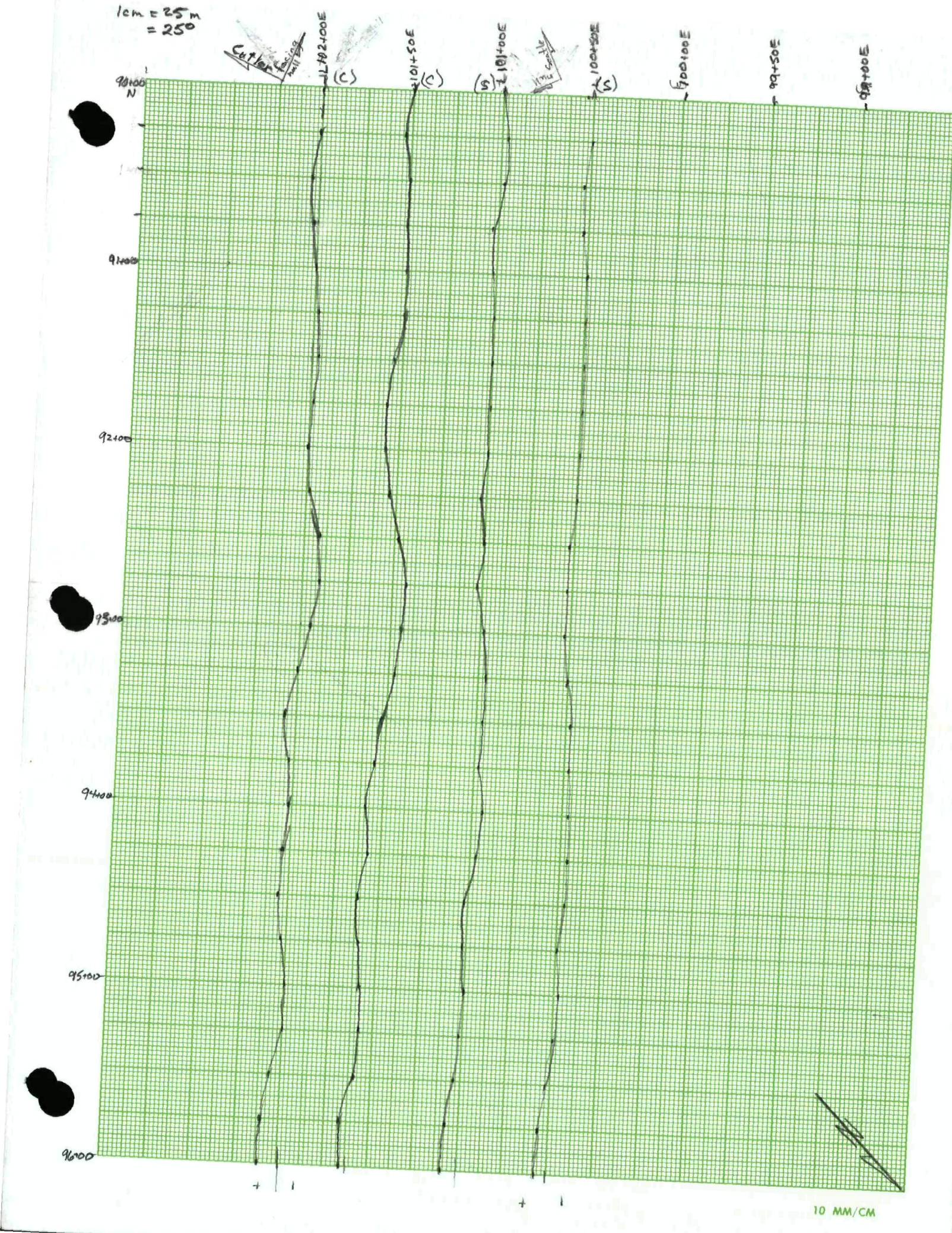
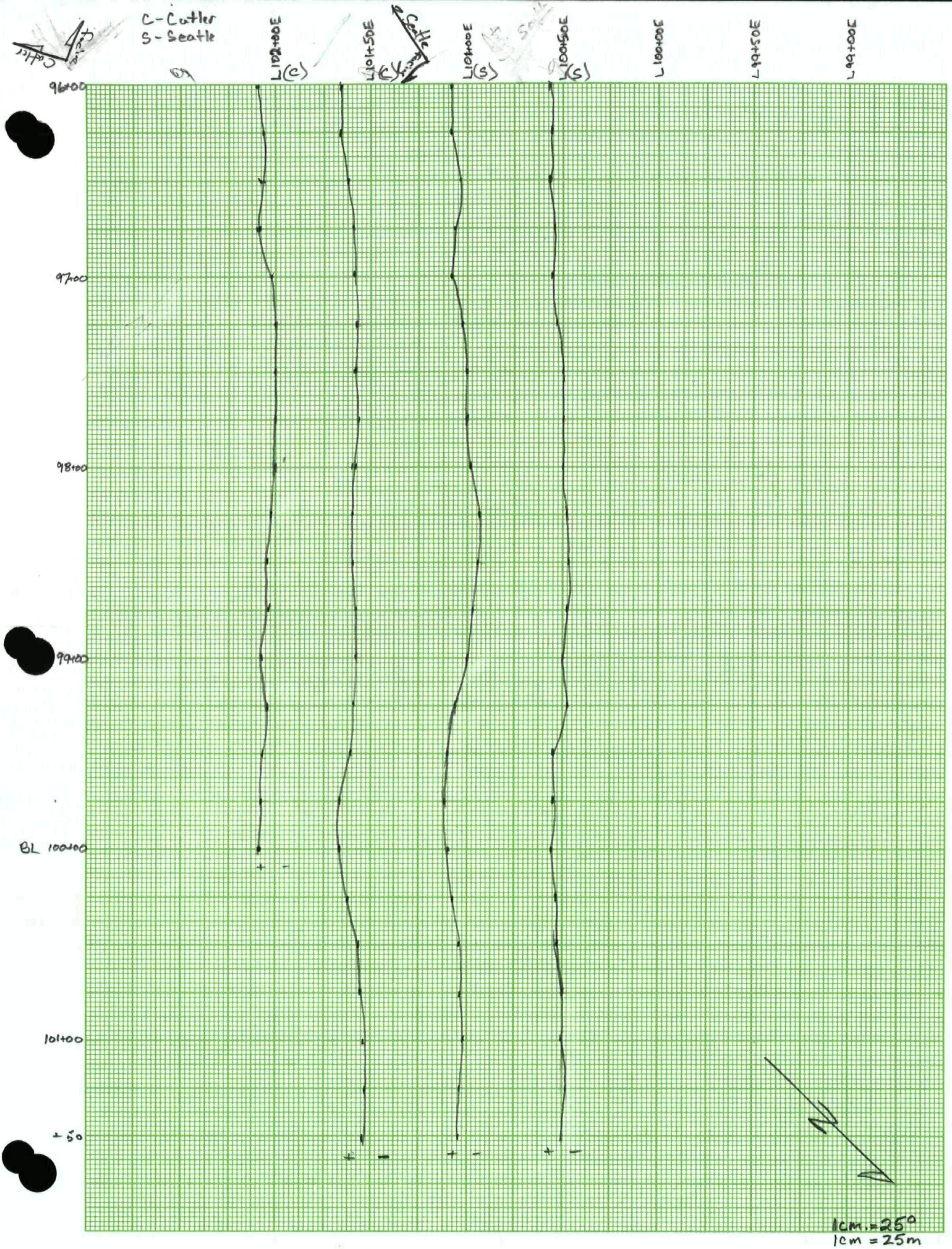
	3	-5	-8	-1								
	-.	-6	-8	-17								
	-.4	-5	-7	-12								
	-1	-6	-8	-9								
	-2	-5	-9	-8								
	-2	-5	-7	-5								
	.2	-3	-6	-4								
	2	-4	-3	-3								
	-.2	-4	-4	-3								
	-1	-2	-2	-2								
	3	-5	-2	-3								
				1								

9000 7000m
9100 9100
9200 9200
9300 9300
9400 9400
9500 9500
9600 9600
9700 9700
9800 9800
9900 9900
10000 10000
10100 10100
10150 10150

1mm x 5mm


1cm = 25m
= 25°
Cutler
facing wall
102+00E
(C)
101+50E
(C)
(S)
101+00E
Line Seattle
100+50E
(S)
100+00E
99+50E
99+00E
90+00 N
91+00
92+00
93+00
94+00
95+00
96+00
10 MM/CM

C-Cutler
S-Seattle



Northern Analytical Laboratories ltd

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Fax (867) 668-4890
E-mail NAL@yknet yk ca

Invoice for Analytical Services

To

19651 Yukon Ltd, Tom Morgan

Invoice Date 11/07/2001

WO# 00175

QTY	DESCRIPTION	UNIT PRICE	AMOUNT
	Sample Preparation		
8	Rock/D C Sample Preparation	5 50	44 00
	Analyses		
8	Au, Pt, Pd 30g FA/AAS	25 00	200 00
8	ICP 30 Elements	8 00	64 00

Subtotal	308 00
GST @7% (R 121285662)	21 56
Total due on receipt of invoice	$329 56

2% per month charged on overdue accounts

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19/07/2001

Certificate of Analysis

# of pages (not including this page) 1

19651 Yukon Ltd, Tom Morgan

WO# 00175

Certified by
Justin Lemphers (Senior Assayer)

Date Received 21/06/01

SAMPLE PREPARATION

Code	# of Samples	Type	Preparation Description (All wet samples are dried first)
r	8	rock	Crush to -10 mesh, riffle split 200g, pulverize to -100 mesh

ANALYTICAL METHODS SUMMARY.

Symbol	Units	Element	Method (A assay) (G geochem)	Fusion/Digestion	Lower Limit	Upper Limit

1000ppb = 1ppm = 1g/mt = 0 0001% = 0 029166oz/ton

CERTIFICATE OF ANALYSIS
iPL 01G0695

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[069511 43 45 10071701]

Northern Analytical Laboratories
Project MO#00175
Shipper Norm Smith
Shipment PO# 568114
Analysis
Au/Pd/Pt(FA/AAS 30g)g/mt
ICP(AqR)30
Comment

8 Samples Out Jul 17 2001 In Jul 10 2001

CODE	AMOUNT	TYPE	PREPARATION DESCRIPTION	PULP	REJECT
B31100	8	Pulp	Pulp received as it is no sample prep	12M/Dis	00M/Dis
B82100	1	Std iPL	Standard iPL no charge	00M/Dis	00M/Dis

NS=No Sample Rep=Replicate M=Month Dis=Discard

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Analytical Summary

##	Code	Method	Units	Description	Element	Limit Low	Limit High
01	0368	FA/AAS	g/mt	Au (FA/AAS 30g) g/mt	Gold	0 01	9999 00
02	0341	FA/AAS	g/mt	Pd FA/AAS finish g/mt	Palladium	0 01	9999 00
03	0331	FA/AAS	g/mt	Pt FA/AAS finish in g/mt	Platinum	0 01	99999 00
04	0721	ICP	ppm	Ag ICP	Silver	0 1	100 0
05	0711	ICP	ppm	Cu ICP	Copper	1	20000
06	0714	ICP	ppm	Pb ICP	Lead	2	20000
07	0730	ICP	ppm	Zn ICP	Zinc	1	20000
08	0703	ICP	ppm	As ICP	Arsenic	5	10000
09	0702	ICP	ppm	Sb ICP	Antimony	5	1000
10	0732	ICP	ppm	Hg ICP	Mercury	3	10000
11	0717	ICP	ppm	Mo ICP	Molybdenum	1	1000
12	0747	ICP	ppm	Tl ICP (Incomplete Digestion)	Thallium	10	1000
13	0705	ICP	ppm	Bi ICP	Bismuth	2	10000
14	0707	ICP	ppm	Cd ICP	Cadmium	0 1	100 0
15	0710	ICP	ppm	Co ICP	Cobalt	1	10000
16	0718	ICP	ppm	Ni ICP	Nickel	1	10000
17	0704	ICP	ppm	Ba ICP (Incomplete Digestion)	Barium	2	10000
18	0727	ICP	ppm	W ICP (Incomplete Digestion)	Tungsten	5	1000
19	0709	ICP	ppm	Cr ICP (Incomplete Digestion)	Chromium	1	10000
20	0729	ICP	ppm	V ICP	Vanadium	2	10000
21	0716	ICP	ppm	Mn ICP	Manganese	1	10000
22	0713	ICP	ppm	La ICP (Incomplete Digestion)	Lanthanum	2	10000
23	0723	ICP	ppm	Sr ICP (Incomplete Digestion)	Strontium	1	10000
24	0731	ICP	ppm	Zr ICP	Zirconium	1	10000
25	0736	ICP	ppm	Sc ICP	Scandium	1	10000
26	0726	ICP	%	Ti ICP (Incomplete Digestion)	Titanium	0 01	1 00
27	0701	ICP	%	Al ICP (Incomplete Digestion)	Aluminum	0 01	10 00
28	0708	ICP	%	Ca ICP (Incomplete Digestion)	Calcium	0 01	10 00
29	0712	ICP	%	Fe ICP	Iron	0 01	10 00
30	0715	ICP	%	Mg ICP (Incomplete Digestion)	Magnesium	0 01	10 00
31	0720	ICP	%	K ICP (Incomplete Digestion)	Potassium	0 01	10 00
32	0722	ICP	%	Na ICP (Incomplete Digestion)	Sodium	0 01	5 00
33	0719	ICP	%	P ICP	Phosphorus	0 01	5 00

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* Our liability is limited solely to the analytical cost of these analyses

BC Certified Assayer David Chu

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CERTIFICATE OF ANALYSIS
iPL 01G0695

Client Northern Analytical Laboratories **8 Samples**
Project WO#00175 8=Pulp 1=Std iPL [069511 51 07 10071701]

Out Jul 17 2001 Page 1 of 1
In Jul 10 2001 Section 1 of 2

Sample Name	Type	Au g/mt	Pd g/mt	Pt g/mt	Ag ppm	Cu ppm	Pb ppm	Zn ppm	As ppm	Sb ppm	Hg ppm	Mo ppm	Tl ppm	Bi ppm	Cd ppm	Co ppm	Ni ppm	Ba ppm	W ppm
DUN21R001	Pulp	<0 01	0 01	<0 01	0 1	6	6	24	<5	12	<3	3	<10	<2	<0 1	74	1304	281	<5
DUN21R002	Pulp	<0 01	0 03	0 01	<0 1	6	6	20	<5	14	<3	3	<10	<2	<0 1	70	1272	62	<5
DUN21R003	Pulp	<0 01	0 02	<0 01	<0 1	11	6	20	<5	15	<3	3	<10	<2	<0 1	72	1509	28	<5
DUN21R004	Pulp	<0 01	<0 01	<0 01	<0 1	14	2	16	<5	10	<3	3	<10	<2	<0 1	76	1395	100	<5
DUN21R005	Pulp	<0 01	<0 01	<0 01	<0 1	14	5	31	<5	12	<3	3	<10	<2	<0 1	98	1967	75	<5
DUN21R006	Pulp	<0 01	<0 01	<0 01	<0 1	25	6	24	<5	13	<3	3	<10	<2	<0 1	104	1656	56	<5
DUN21R007	Pulp	<0 01	0 01	<0 01	0 1	21	4	28	<5	12	<3	2	<10	<2	<0 1	101	1718	112	<5
DUN21R008	Pulp	0 01	0 02	<0 01	0 1	15	7	22	<5	11	<3	3	<10	<2	<0 1	75	1405	4	<5
STD101	Std iPL	0 08	0 53	0 25	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Minimum Detection		0 01	0 01	0 01	0 1	1	2	1	5	5	3	1	10	2	0 1	1	1	2	5
Maximum Detection		9999 00	9999 00	99999 00	100 0	20000	20000	20000	10000	1000	10000	1000	1000	10000	100 0	10000	10000	10000	1000
Method		FA/AAS	FA/AAS	FA/AAS	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP

——=No Test Ins=Insufficient Sample Del=Delay Max=No Estimate Rec=ReCheck m=x1000 %=Estimate % NS=No Sample

CERTIFICATE OF ANALYSIS
iPL 01G0695

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Client Northern Analytical Laboratories **8 Samples**
Project WO#00175 8=Pulp 1=Std iPL [069511 51 07 10071701]

Out Jul 17 2001
In Jul 10 2001

Sample Name	Cr ppm	V ppm	Mn ppm	La ppm	Sr ppm	Zr ppm	Sc ppm	Ti %	Al %	Ca %	Fe %	Mg %	K %	Na %	P %
DUN21R001	1267	23	842	2	21	2	2	0 01	0 26	1 06	4 00	8 03	0 01	0 01	<0 01
DUN21R002	1278	24	383	<2	6	1	3	0 01	0 34	0 61	3 27	9 61	0 01	0 01	<0 01
DUN21R003	1408	32	318	<2	8	1	5	0 01	0 54	0 54	3 61	9 59	<0 01	0 01	<0 01
DUN21R004	920	22	448	<2	10	1	4	0 01	0 60	1 00	2 98	11%	<0 01	0 01	<0 01
DUN21R005	1494	31	671	<2	3	2	4	0 01	0 42	0 03	4 61	14%	0 01	0 01	<0 01
DUN21R006	1265	26	766	<2	3	2	4	0 01	0 48	0 04	4 05	10%	0 01	0 01	<0 01
DUN21R007	1285	31	917	<2	5	3	4	0 02	0 57	0 05	4 85	8 93	0 01	0 01	<0 01
DUN21R008	1107	27	368	<2	1	1	3	0 01	0 31	0 02	3 73	9 56	<0 01	0 01	<0 01
STD101	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Minimum Detection	1	2	1	2	1	1	1	0 01	0 01	0 01	0 01	0 01	0 01	0 01	0 01
Maximum Detection	10000	10000	10000	10000	10000	10000	10000	1 00	10 00	10 00	10 00	10 00	10 00	5 00	5 00
Method	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP

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[002014 46 44 10011001]

Northern Analytical Laboratories

Project None Given
Shipper Norm Smith
Shipment PO# 568108
Analysis
Au/Pt/Pd(FA/AAS 30)
ICP(AqR)30
Comment

6 Samples Out Jan 10 2001 In Jan 08 2001

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CODE	AMOUNT	TYPE	PREPARATION DESCRIPTION	PULP	REJECT
B211	6	Rock	crush split & pulverize	12M/Dis	03M/Dis

NS=No Sample Rep=Replicate M=Month Dis=Discard

Analytical Summary

##	Code	Method	Units	Description	Element	Limit Low	Limit High
01	0368	FA/AAS	g/mt	Au (FA/AAS 30g) g/mt	Gold	0 01	9999 00
02	0331	FA/AAS	g/mt	Pt FA/AAS finish in g/mt	Platinum	0 01	99999 00
03	0341	FA/AAS	g/mt	Pd FA/AAS finish g/mt	Palladium	0 01	9999 00
04	0721	ICP	ppm	Ag ICP	Silver	0 1	100 0
05	0711	ICP	ppm	Cu ICP	Copper	1	20000
06	0714	ICP	ppm	Pb ICP	Lead	2	20000
07	0730	ICP	ppm	Zn ICP	Zinc	1	20000
08	0703	ICP	ppm	As ICP	Arsenic	5	10000
09	0702	ICP	ppm	Sb ICP	Antimony	5	1000
10	0732	ICP	ppm	Hg ICP	Mercury	3	10000
11	0717	ICP	ppm	Mo ICP	Molybdenum	1	1000
12	0747	ICP	ppm	Tl ICP (Incomplete Digestion)	Thallium	10	1000
13	0705	ICP	ppm	Bi ICP	Bismuth	2	10000
14	0707	ICP	ppm	Cd ICP	Cadmium	0 1	100 0
15	0710	ICP	ppm	Co ICP	Cobalt	1	10000
16	0718	ICP	ppm	Ni ICP	Nickel	1	10000
17	0704	ICP	ppm	Ba ICP (Incomplete Digestion)	Barium	2	10000
18	0727	ICP	ppm	W ICP (Incomplete Digestion)	Tungsten	5	1000
19	0709	ICP	ppm	Cr ICP (Incomplete Digestion)	Chromium	1	10000
20	0729	ICP	ppm	V ICP	Vanadium	2	10000
21	0716	ICP	ppm	Mn ICP	Manganese	1	10000
22	0713	ICP	ppm	La ICP (Incomplete Digestion)	Lanthanum	2	10000
23	0723	ICP	ppm	Sr ICP (Incomplete Digestion)	Strontium	1	10000
24	0731	ICP	ppm	Zr ICP	Zirconium	1	10000
25	0736	ICP	ppm	Sc ICP	Scandium	1	10000
26	0726	ICP	%	Ti ICP (Incomplete Digestion)	Titanium	0 01	1 00
27	0701	ICP	%	Al ICP (Incomplete Digestion)	Aluminum	0 01	10 00
28	0708	ICP	%	Ca ICP (Incomplete Digestion)	Calcium	0 01	10 00
29	0712	ICP	%	Fe ICP	Iron	0 01	10 00
30	0715	ICP	%	Mg ICP (Incomplete Digestion)	Magnesium	0 01	10 00
31	0720	ICP	%	K ICP (Incomplete Digestion)	Potassium	0 01	10 00
32	0722	ICP	%	Na ICP (Incomplete Digestion)	Sodium	0 01	5 00
33	0719	ICP	%	P ICP	Phosphorus	0 01	5 00

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BC Certified Assayer: David Chiu

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Client Northern Analytical Laboratories **6 Samples**
Project None Given 6=Roc

[002014 46 44 10011001] Out Jan 10 2001 In Jan 08 2001

Sample Name	Type	Au g/mt	Pt g/mt	Pd g/mt	Ag ppm	Cu ppm	Pb ppm	Zn ppm	As ppm	Sb ppm	Hg ppm	Mo ppm	Tl ppm	Bi ppm	Cd ppm	Co ppm	Ni ppm	Ba ppm	W ppm
Dun 20 01	Rock	0 02	<0 01	<0 01	<0 1	20	40	30	<5	5	<3	4	<10	<2	1 1	53	1252	205	<5
Dun 20 02	Rock	0 02	<0 01	0 12	<0 1	9	19	28	<5	6	<3	2	<10	<2	2 1	66	1266	23	<5
Dun 20 03	Rock	<0 01	0 05	0 01	<0 1	12	18	21	<5	<5	<3	3	<10	<2	1 2	73	1403	40	<5
Dun 20 04A	Rock	0 01	<0 01	0 01	<0 1	11	11	24	<5	7	<3	3	<10	<2	1 8	66	1292	42	<5
Dun 20 04B	Rock	<0 01	<0 01	0 01	<0 1	16	10	29	<5	<5	<3	2	<10	<2	2 2	77	1669	116	<5
Dun 20 05	Rock	0 01	0 01	0 01	<0 1	4	14	22	<5	6	<3	3	<10	<2	1 6	66	1313	22	<5
Minimum Detection		0 01	0 01	0 01	0 1	1	2	1	5	5	3	1	10	2	0 1	1	1	2	5
Maximum Detection		9999 00	99999 00	9999 00	100 0	20000	20000	20000	10000	1000	10000	1000	1000	10000	100 0	10000	10000	10000	1000
Method		FA/AAS	FA/AAS	FA/AAS	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP	ICP

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Client Northern Analytical Laboratories
Project None Given

6 Samples
6=Rock

[002014 46 44 10011001]

Out Jan 10, 2001
In Jan 08, 2001

Sample Name	Cr ppm	V ppm	Mn ppm	La ppm	Sr ppm	Zr ppm	Sc ppm	Ti %	Al %	Ca %	Fe %	Mg %	K %	Na %	P %
Dun 20 01	697	20	303	<2	3	<1	1	0 01	0 22	0 03	3 08	5 92	<0 01	0 01	<0 01
Dun 20 02	759	21	744	<2	6	1	2	0 01	0 13	0 68	3 77	8 96	<0 01	0 01	<0 01
Dun 20 03	568	16	571	<2	1	1	2	<0 01	0 11	0 11	3 47	7 18	<0 01	0 01	<0 01
Dun 20 04A	978	24	752	<2	12	1	2	0 01	0 19	0 41	4 28	7 44	<0 01	0 01	<0 01
Dun 20 04B	856	23	972	<2	3	2	2	0 01	0 31	0 04	4 27	5 31	<0 01	0 01	<0 01
Dun 20 05	470	10	452	<2	6	1	2	<0 01	0 10	0 49	3 14	12%	<0 01	0 01	<0 01
Minimum Detection	1	2	1	2	1	1	1	0 01	0 01	0 01	0 01	0 01	0 01	0 01	0 01
Maximum Detection	10000	10000	10000	10000	10000	10000	10000	1	0 00	10 00	10 00	10 00	10 00	5 00	5 00
Method	ICP	ICP	ICP	ICP	ICP	ICP	ICP	[illegible]	ICP	ICP	ICP	ICP	ICP	ICP	ICP

[illegible] Sample Dpl=Dpls Max=No Estimate Rec=ReCheck m=x1000 %=Estimate % NS=No Sample

Dun Data 23

??ý???ü

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10200 9962.5 57336.4 0.08 12.460556 1 0.1
10200 9950 57332.3 0.08 12.473333 1 -1.5
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10200 9850 58015.9 0.09 12.631111 1 25.9
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Plotted.

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10200 9325 57335.7 0.08 13.805556 1 -12.4
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10200 9300 57559.0 0.08 13.821944 1 7.6
10200 9287.5 57456.5 0.07 13.830278 1 -2.4
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10200 9262.5 57446.0 0.08 13.848611 1 -2.1
10200 9250 57457.7 0.08 13.856389 1 -0.3
10200 9237.5 57466.6 0.08 13.864444 1 -0.1
10200 9225 57472.4 0.08 13.872222 1 -0.4
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10200 9200 57481.2 0.07 13.887222 1 1.0
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10200 9162.5 57468.9 0.08 13.909167 1 0.4
10200 9150 57462.2 0.08 13.916944 1 0.7
10200 9137.5 57454.2 0.07 13.924722 1 1.1
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Plotted.

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10150 9500 57212.8 0.09 14.449167 1 -3.4
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Whitehorse, Yukon Y1A 2C6

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plotted.

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plotted

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Plotted.

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Plotted.

Plotted

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Plotted

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10150 10050 57150.0 0.08 17.579444 1 -0.4
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9900 9800 58950.6 0.09 13.180278 1 19.8
9900 9787.5 58895.6 0.09 13.187222 1 10.4
9900 9775 58901.3 0.09 13.194444 1 8.6
9900 9762.5 58983.2 0.10 13.200278 1 22.1
9900 9750 58990.5 0.10 13.208333 1 19.7
9900 9737.5 58932.6 0.10 13.216389 1 14.8
9900 9725 58876.1 0.09 13.222778 1 12.1
9900 9712.5 58878.4 0.09 13.229167 1 12.0
9900 9700 59017.5 0.11 13.240000 1 26.6
9900 9687.5 59145.8 0.09 13.246944 1 40.9
9900 9675 59169.3 0.10 13.253333 1 51.0
9900 9662.5 59046.4 0.09 13.259722 1 55.3
9900 9650 58486.1 0.13 13.268333 1 30.6
9900 9637.5 57887.9 0.10 13.274722 1 -16.3
9900 9625 57573.6 0.08 13.286111 1 -9.9
9900 9612.5 57397.2 0.09 13.296667 1 -15.3
9900 9600 57311.1 0.09 13.304167 1 -9.8
9900 9587.5 57251.7 0.09 13.311944 1 -6.5
9900 9575 57221.6 0.09 13.319167 1 -4.0
9900 9562.5 57207.6 0.09 13.328333 1 -2.7
9900 9550 57195.0 0.09 13.337778 1 -1.8
9900 9537.5 57188.3 0.09 13.344167 1 -2.3
9900 9525 57192.2 0.09 13.351667 1 0.2
9900 9512.5 57180.6 0.09 13.357778 1 -1.9
9900 9500 57181.1 0.09 13.365278 1 -0.7
9900 9487.5 57180.7 0.10 13.373889 1 0.7
9900 9475 57176.0 0.09 13.381389 1 1.1
```

plotted

```
9900 9462.5 57156.6 0.09 13.389167 1 -1.1
9900 9450 57169.6 0.09 13.405833 1 1.8
9900 9437.5 57155.6 0.09 13.413889 1 -0.4
9900 9425 57159.9 0.09 13.423056 1 -1.6
9900 9412.5 57157.6 0.09 13.429444 1 -1.1
9900 9400 57155.2 0.09 13.436389 1 0.3
9900 9387.5 57151.4 0.10 13.446667 1 0.2
9900 9375 57147.0 0.09 13.453333 1 0.1
9900 9362.5 57141.5 0.09 13.461389 1 0.2
9900 9350 57135.6 0.09 13.470278 1 -1.0
```

plotted

S.W. end

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    9950.00 +
/!  Date____:    02/01/24
/!  Job_____:    0
/!  Operator:
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
9950 9250 56930.6 0.08 13.656389 1 -4.5
9950 9262.5 56961.3 0.08 13.673889 1 -1.1
9950 9275 56979.1 0.08 13.681111 1 -1.2
9950 9287.5 56988.9 0.08 13.688056 1 -1.4
9950 9300 57002.2 0.08 13.695833 1 -1.0
9950 9312.5 57011.4 0.08 13.703056 1 -1.1
9950 9325 57017.2 0.09 13.711667 1 -1.2
9950 9337.5 57030.2 0.09 13.720556 1 -0.6
9950 9350 57034.1 0.08 13.727778 1 -0.4
9950 9362.5 57038.9 0.09 13.735000 1 -0.7
9950 9375 57044.2 0.08 13.744167 1 -0.9
9950 9387.5 57054.2 0.08 13.750833 1 -0.5
9950 9400 57062.5 0.08 13.758333 1 -0.4
9950 9412.5 57071.5 0.09 13.767500 1 -0.2
9950 9425 57079.3 0.08 13.775278 1 -0.2
9950 9437.5 57080.6 0.09 13.782222 1 -0.2
9950 9450 57090.5 0.09 13.791389 1 0.2
9950 9462.5 57094.5 0.09 13.797778 1 0.0
9950 9475 57086.9 0.08 13.810833 1 -1.6
9950 9487.5 57093.3 0.09 13.819722 1 -1.7
9950 9500 57102.1 0.11 13.828889 1 -2.1
9950 9512.5 57106.3 0.09 13.837778 1 -17.0
9950 9525 57094.2 0.09 13.848889 1 -5.9
9950 9537.5 57109.8 0.09 13.860000 1 -4.9
9950 9550 57114.9 0.09 13.868333 1 -8.0
9950 9562.5 57134.0 0.09 13.880000 1 -11.8
9950 9575 57188.0 0.09 13.888611 1 -19.3
9950 9587.5 57318.5 0.08 13.897778 1 -38.8
9950 9600 57992.7 0.11 13.905556 1 -89.2
9950 9612.5 59838.6 0.12 13.923333 1 174.9
9950 9625 59754.1 0.10 13.931667 1 146.4
9950 9637.5 58667.9 0.11 13.939444 1 -4.9
9950 9650 57701.6 0.11 13.947500 1 -98.2
9950 9662.5 58130.7 0.10 13.956667 1 -39.7
9950 9675 59235.3 0.11 13.966667 1 130.0
9950 9687.5 58829.6 0.11 13.977500 1 -64.5
9950 9700 59818.7 0.18 13.986389 1 121.2
9950 9712.5 59646.4 0.08 13.993889 1 36.3
9950 9725 59752.3 0.09 14.003611 1 81.0
9950 9737.5 59422.4 0.08 14.011944 1 15.7
9950 9750 59309.9 0.08 14.019167 1 4.1
9950 9762.5 59538.5 0.10 14.026944 1 66.9
9950 9775 59235.2 0.08 14.034722 1 6.4
9950 9787.5 59045.5 0.09 14.042500 1 -12.4
9950 9800 58996.4 0.09 14.050833 1 -12.3
9950 9812.5 59066.4 0.09 14.058056 1 13.6
```

SW end of line.

plotted.

```
9950 9825 59074.5 0.09 14.065000 1 8.7
9950 9837.5 59182.1 0.09 14.071667 1 29.2
9950 9850 59149.2 0.09 14.079167 1 20.7
9950 9862.5 59183.2 0.09 14.089722 1 68.3
9950 9875 58722.2 0.11 14.098611 1 -3.6
9950 9887.5 58993.7 0.09 14.105278 1 63.0
9950 9900 58557.6 0.12 14.114722 1 -9.7
9950 9912.5 58548.6 0.08 14.121667 1 30.7
9950 9925 58197.6 0.09 14.129722 1 -2.4
9950 9937.5 57880.2 0.10 14.137500 1 -33.5
9950 9950 58068.9 0.09 14.144722 1 -3.2
9950 9962.5 58433.2 0.08 14.151667 1 27.6
9950 9975 58683.6 0.09 14.160556 1 47.3
9950 9987.5 58548.3 0.08 14.170000 1 32.7
9950 10000 58198.5 0.08 14.178333 1 6.1
```

Plotted.

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    10000.0 +
/!  Date____:    02/01/24
/!  Job_____:    0
/!  Operator:
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
10000 9987.5 58898.5 0.09 14.277778 1 50.4
10000 9975 58843.0 0.09 14.289722 1 38.2
10000 9962.5 58633.7 0.09 14.303611 1 31.0
10000 9950 58190.7 0.09 14.311667 1 -10.8
10000 9937.5 58182.6 0.09 14.321667 1 -5.8
10000 9925 58414.6 0.08 14.335278 1 29.9
10000 9912.5 58355.7 0.08 14.342222 1 12.0
10000 9900 58223.3 0.08 14.351667 1 -11.0
10000 9887.5 58246.3 0.08 14.359167 1 -2.4
10000 9875 58216.4 0.09 14.368889 1 -15.9
10000 9862.5 58327.8 0.08 14.377222 1 -14.5
10000 9850 58476.9 0.08 14.385278 1 -7.5
10000 9837.5 58554.8 0.08 14.398056 1 -0.8
10000 9825 58549.3 0.08 14.410556 1 -7.3
10000 9812.5 58661.0 0.08 14.421111 1 8.9
10000 9800 58588.6 0.08 14.430000 1 -1.3
10000 9787.5 58441.0 0.08 14.444167 1 -6.4
10000 9775 58301.7 0.09 14.486667 1 -33.0
10000 9762.5 58471.5 0.09 14.499722 1 -3.7
10000 9750 58508.0 0.08 14.508056 1 9.9
10000 9737.5 58395.1 0.08 14.514444 1 -3.4
10000 9725 58411.8 0.08 14.523611 1 1.8
10000 9712.5 58411.7 0.08 14.533056 1 4.0
10000 9700 58396.6 0.08 14.540000 1 6.8
10000 9687.5 58217.0 0.09 14.551111 1 -13.8
10000 9675 58442.6 0.08 14.558333 1 23.1
10000 9662.5 58843.1 0.09 14.568611 1 57.4
10000 9650 58872.2 0.09 14.580000 1 51.8
10000 9637.5 58710.8 0.09 14.589444 1 52.0
10000 9625 58201.2 0.09 14.597500 1 3.0
10000 9612.5 58051.9 0.09 14.607500 1 -2.7
10000 9600 58197.0 0.09 14.615833 1 44.4
10000 9587.5 57842.4 0.11 14.626389 1 22.7
10000 9575 57363.9 0.09 14.635833 1 -11.0
10000 9562.5 57194.8 0.09 14.646389 1 -11.1
10000 9550 57123.8 0.09 14.654444 1 -6.7
10000 9537.5 57086.6 0.09 14.664722 1 -5.7
10000 9525 57059.6 0.08 14.672778 1 -5.0
10000 9512.5 57042.0 0.09 14.681389 1 -4.8
10000 9500 57026.5 0.09 14.691389 1 -3.1
10000 9487.5 57009.4 0.08 14.705833 1 -1.8
10000 9475 56975.2 0.09 14.714722 1 -3.3
10000 9462.5 56951.3 0.08 14.725278 1 -2.8
10000 9450 56903.9 0.08 14.737500 1 -6.5
10000 9437.5 56862.8 0.09 14.747778 1 -7.3
10000 9425 56801.6 0.08 14.757222 1 -15.6
```

Plotted.

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    10400.0 +
/!  Date____:    02/01/24
/!  Job_____:    0
/!  Operator:
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
10400 9750 58710.3 0.08 17.251389 1 35.4
10400 9762.5 58695.9 0.09 17.261389 1 30.8
10400 9775 58487.4 0.09 17.270833 1 17.9
10400 9787.5 58237.9 0.09 17.278333 1 5.8
10400 9800 57990.4 0.09 17.286389 1 7.1
10400 9812.5 57712.4 0.08 17.295278 1 -5.3
10400 9825 57411.4 0.08 17.303889 1 -15.7
10400 9837.5 57305.0 0.09 17.311667 1 -11.8
10400 9850 57275.6 0.09 17.319444 1 -6.2
10400 9862.5 57254.1 0.09 17.328056 1 -3.7
10400 9875 57240.5 0.10 17.335278 1 -4.6
10400 9887.5 57231.9 0.14 17.343611 1 -2.4
10400 9900 57229.4 0.09 17.351944 1 -0.3
10400 9912.5 57217.4 0.09 17.359722 1 -0.4
10400 9925 57203.0 0.09 17.367500 1 -0.9
10400 9937.5 57189.2 0.09 17.374722 1 -0.7
10400 9950 57172.4 0.09 17.383056 1 -1.5
10400 9962.5 57163.2 0.09 17.390556 1 -1.6
10400 9975 57158.9 0.09 17.398611 1 0.4
10400 9987.5 57148.3 0.10 17.407500 1 -0.1
10400 10000 57139.6 0.10 17.416944 1 -0.6
```

Plotted

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    10350.0 +
/!  Date____:    02/01/24
/!  Job_____:    0
/!  Operator:
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
10350 10000 57126.7 0.09 17.021389 1 -1.1
10350 9987.5 57135.1 0.09 17.033889 1 -0.7
10350 9975 57145.4 0.08 17.044444 1 -0.9
10350 9962.5 57155.2 0.09 17.051111 1 -1.6
10350 9950 57171.5 0.09 17.060000 1 -2.3
10350 9937.5 57190.7 0.09 17.069167 1 -0.6
10350 9925 57205.5 0.09 17.077222 1 -1.1
10350 9912.5 57218.4 0.09 17.084444 1 -1.3
10350 9900 57227.7 0.09 17.094444 1 -3.2
10350 9887.5 57240.8 0.09 17.101111 1 -3.6
10350 9875 57267.1 0.09 17.109444 1 -4.1
10350 9862.5 57301.6 0.09 17.121389 1 -5.3
10350 9850 57331.9 0.08 17.129722 1 -9.4
10350 9837.5 57378.9 0.08 17.136389 1 -12.6
10350 9825 57544.3 0.09 17.144722 1 -14.0
10350 9812.5 57852.4 0.08 17.153611 1 -2.3
10350 9800 58273.2 0.10 17.162222 1 16.7
10350 9787.5 58502.5 0.09 17.170556 1 20.2
10350 9775 58650.4 0.09 17.185556 1 21.9
10350 9762.5 58680.9 0.09 17.193611 1 1.6
10350 9750 58844.9 0.09 17.206111 1 28.7
```

Plotted.

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    10250.0 +
/!  Date____:    02/01/24
/!  Job_____:    0
/!  Operator:
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
10250 10000 57158.2 0.09 16.574444 1 -3.8
10250 9987.5 57192.9 0.09 16.584722 1 2.4
10250 9975 57202.8 0.10 16.593611 1 -1.0
10250 9962.5 57211.6 0.09 16.600556 1 -2.3
10250 9950 57234.4 0.09 16.616389 1 -0.9
10250 9937.5 57245.5 0.09 16.623889 1 -2.0
10250 9925 57263.1 0.08 16.631389 1 -4.9
10250 9912.5 57299.0 0.09 16.639167 1 -5.4
10250 9900 57333.2 0.08 16.646667 1 -6.8
10250 9887.5 57371.3 0.08 16.654722 1 -10.1
10250 9875 57524.1 0.08 16.676944 1 -16.4
10250 9862.5 57877.2 0.08 16.683333 1 14.7
10250 9850 58011.5 0.09 16.691667 1 22.9
10250 9837.5 57755.9 0.08 16.699722 1 -11.8
10250 9825 57872.1 0.09 16.707500 1 -30.5
10250 9812.5 58427.6 0.11 16.715833 1 55.3
10250 9800 58585.3 0.08 16.723611 1 21.7
10250 9787.5 58485.8 0.08 16.733333 1 4.6
10250 9775 58303.9 0.08 16.741667 1 -38.4
10250 9762.5 58491.1 0.08 16.749444 1 16.0
10250 9750 58620.3 0.08 16.762500 1 -43.2
```

plotted.

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    10300.0 +
/!  Date____:    02/01/24
/!  Job_____:    0
/!  Operator:
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
10300 9750 58673.1 0.08 16.806389 1 -14.9
10300 9762.5 58605.8 0.08 16.820000 1 -4.0
10300 9775 58543.8 0.08 16.829167 1 15,5
10300 9787.5 58324.1 0.08 16.836389 1 5.3
10300 9800 58067.6 0.09 16.843889 1 -8.4
10300 9812.5 57778.7 0.11 16.850556 1 -26.5
10300 9825 57688.9 0.08 16.857778 1 -16.3
10300 9837.5 57800.3 0.09 16.865556 1 -1.1
10300 9850 57928.2 0.08 16.875278 1 24.6
10300 9862.5 57703.4 0.08 16.883611 1 6.6
10300 9875 57473.1 0.09 16.893611 1 -9.1
10300 9887.5 57332.8 0.09 16.903056 1 -8.7
10300 9900 57288.7 0.09 16.910556 1 -4.3
10300 9912.5 57256.1 0.09 16.916944 1 -3.3
10300 9925 57235.9 0.09 16.923889 1 -2.1
10300 9937.5 57221.8 0.09 16.931667 1 -2.3
10300 9950 57208.1 0.09 16.938611 1 0.2
10300 9962.5 57192.9 0.09 16.945000 1 0.4
10300 9975 57165.2 0.09 16.951944 1 -0.4
10300 9987.5 57143.1 0.09 16.959167 1 -2.0
10300 10000 57125.8 0.09 16.967778 1 -1.3
```

S.W. end of line

Plotted.

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    10050.0 +
/!  Date____:    02/01/24
/!  Job_____:    4444
/!  Operator: shawn,line redid for magnetic levelling with 02/01/23 files
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
10050 10000 57989.4 0.10 18.027500 1 2.2
10050 10012.5 57634.0 0.08 18.038611 1 -4.2
10050 10025 57400.8 0.09 18.047222 1 -7.1
10050 10037.5 57246.2 0.09 18.057778 1 -8.1
10050 10050 57111.2 0.09 18.065833 1 -7.6
10050 10062.5 57025.8 0.09 18.073889 1 -7.6
10050 10075 56955.4 0.08 18.082222 1 -8.2
10050 10087.5 56921.3 0.08 18.090000 1 -6.5
10050 10100 56900.4 0.08 18.097222 1 -5.3
```

à

```
10000 9412.5 56830.8 0.08 14.766944 1 -24.5
10000 9400 56952.7 0.08 14.778611 1 -22.6
10000 9387.5 57066.2 0.09 14.851944 1 -21.9
10000 9375 57217.1 0.09 14.862778 1 -21.6
10000 9362.5 57413.8 0.08 14.873056 1 -16.4
10000 9350 57697.2 0.09 14.882500 1 -0.1
10000 9337.5 57915.5 0.09 14.895278 1 17.6
10000 9325 57996.1 0.09 14.908056 1 19.4
10000 9312.5 57932.8 0.09 14.919722 1 5.1
10000 9300 57998.3 0.09 14.930556 1 7.6
10000 9287.5 58035.7 0.09 14.946111 1 14.7
10000 9275 58071.7 0.09 14.955556 1 13.1
10000 9262.5 58292.3 0.09 14.966667 1 54.2
10000 9250 58240.8 0.09 14.975000 1 32.4
10000 9237.5 58280.7 0.09 14.982778 1 37.5
10000 9225 58324.7 0.09 14.989444 1 35.0
10000 9212.5 58511.7 0.09 15.007500 1 41.9
10000 9200 58287.1 0.08 15.137778 1 9.0
10000 9187.5 58167.7 0.09 15.153889 1 -3.1
10000 9175 57963.0 0.10 15.164722 1 -13.7
10000 9162.5 57991.7 0.09 15.175556 1 -18.2
10000 9150 58109.3 0.10 15.191667 1 0.6
10000 9137.5 58102.7 0.09 15.203611 1 -6.7
10000 9125 58807.4 0.11 15.217778 1 93.1
10000 9112.5 57147.0 0.23 15.239722 1 -320.1
10000 9100 58504.8 0.27 15.253611 1 265.9
10000 9087.5 59083.8 0.10 15.263056 1 31.9
10000 9075 59642.8 0.09 15.280556 1 78.4
10000 9062.5 60778.9 0.39 15.295556 1 494.2
10000 9050 59435.6 0.15 15.306111 1 22.2
10000 9037.5 59023.0 0.11 15.317778 1 92.1
10000 9025 58360.4 0.09 15.330278 1 -9.7
10000 9012.5 58806.1 0.10 15.339167 1 105.8
10000 9000 58066.7 0.10 15.348889 1 -13.6
```

S. W end.

```
10000 10150 56925.1 0.08 16.073611 1 -3.0
10000 10137.5 56913.4 0.08 16.085278 1 -1.6
10000 10125 56891.7 0.08 16.092778 1 -2.7
10000 10112.5 56881.7 0.08 16.099167 1 -2.9
10000 10100 56883.5 0.08 16.108056 1 -3.9
10000 10087.5 56893.3 0.08 16.116944 1 -5.4
10000 10075 56916.3 0.09 16.125833 1 -8.1
10000 10062.5 56950.7 0.09 16.134444 1 -8.8
10000 10050 57050.7 0.09 16.144722 1 -11.9
10000 10037.5 57259.1 0.09 16.153889 1 -17.0
10000 10025 57588.0 0.08 16.161111 1 -13.9
10000 10012.5 58436.6 0.08 16.180833 1 46.9
```

plotted.

12.5 m. from 10000-00

```
/--------------------------    S C I N T R E X    ----------------------------
/!  Revision:    4.3F
/!  Line____:    10000.0 +
/!  Date____:    02/01/24
/!  Job_____:    2222
/!  Operator:
/!  Serial__:    0
/!  Basefld_:    58775
/!  Duration:    2.0
/!  Mag_Data:    X/Y/TotFld/Noise/Hours/0=Uncor/Grad
/-------------------------------------------------------------------------------
10000 10400 57140.0 0.10 17.476111 1 -0.0
10000 10387.5 57138.4 0.09 17.485000 1 0.5
10000 10375 57133.8 0.09 17.495278 1 0.4
10000 10362.5 57131.7 0.09 17.501944 1 -1.0
10000 10350 57125.9 0.09 17.509444 1 -2.0
10000 10337.5 57125.5 0.09 17.516111 1 -1.7
10000 10325 57120.0 0.09 17.523333 1 -2.6
10000 10312.5 57125.6 0.09 17.530278 1 -1.4
10000 10300 57125.3 0.09 17.538333 1 -1.8
10000 10287.5 57133.2 0.09 17.546667 1 -1.7
10000 10275 57140.6 0.09 17.553611 1 -2.3
10000 10262.5 57150.9 0.09 17.561667 1 -2.0
10000 10250 57159.2 0.10 17.573056 1 -1.7
10000 10237.5 57177.7 0.09 17.579722 1 -2.5
10000 10225 57207.7 0.09 17.587222 1 -1.4
10000 10212.5 57231.8 0.09 17.593611 1 0.4
10000 10200 57258.0 0.09 17.601944 1 0.4
10000 10187.5 57300.3 0.09 17.609167 1 -0.4
10000 10175 57346.7 0.09 17.621111 1 1.1
10000 10162.5 57350.0 0.08 17.631667 1 -3.0
10000 10150 57370.0 0.09 17.643611 1 0.7
10000 10137.5 57401.9 0.08 17.653333 1 -2.2
10000 10125 57448.9 0.09 17.660278 1 -0.5
10000 10112.5 57523.1 0.08 17.669444 1 1.3
10000 10100 57550.1 0.08 17.676389 1 0.0
10000 10087.5 57604.3 0.08 17.686111 1 -3.6
10000 10075 57696.4 0.08 17.692500 1 -3.9
10000 10062.5 57827.7 0.08 17.699444 1 -1.8
10000 10050 57987.9 0.09 17.711389 1 0.8
10000 10037.5 58269.7 0.10 17.721111 1 5.7
10000 10025 58624.0 0.08 17.730556 1 42.4
10000 10012.5 58759.5 0.08 17.742222 1 59.4
10000 9987.5 58588.7 0.08 17.776111 1 33.5
10000 9975 58383.0 0.09 17.789167 1 22.8
10000 9962.5 58226.1 0.09 17.796944 1 4.9
10000 9950 58197.0 0.09 17.803333 1 6.9
10000 9937.5 58254.2 0.09 17.812222 1 21.8
10000 9925 58258.6 0.09 17.820000 1 31.1
10000 9912.5 58126.9 0.09 17.827222 1 25.6
10000 9900 58007.6 0.10 17.835000 1 20.5
10000 10000 58738.7 0.09 17.894444 1 50.5
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