

06-023

**BOOTLEG EXPLORATION INC.**

**REPORT ON THE 2006  
NORTH CANOL SEDEX RECONNAISSANCE PROGRAM  
IN THE ITSI LAKE AREA, YUKON**

**Report By**

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**For**

**Bootleg Exploration Inc.  
Suite 200, 11 – 11<sup>th</sup> Avenue South  
Cranbrook, BC, V1C 2P1**

**Project Location: Latitude 62° 53' N, Longitude 130° 21' W  
Mining District: Watson Lake  
NTS sheets: 105J/16  
Date: January 15, 2007**

## SUMMARY

This report documents a reconnaissance exploration program to explore for SEDEX potential in the Itsi Lake area south of the North Canol Highway in eastern Yukon on NTS map sheet 105J/16. The area was identified by researching government Regional Geochemical Survey (RGS) data, the regional geology and the Yukon Minfile database. This exploration program was partially funded by Yukon Mineral Incentive Program (YMIP) under the Focused Regional module.

The Itsi Lake area is in the central part of the Selwyn Basin, which hosts the Faro Mine, the Howards Pass, Tom and Jason Deposits. The Selwyn Basin has been extensively explored for SEDEX Pb-Zn deposit types, however the Itsi Lake Area appears to have experienced very little exploration activity as there is very little work documented for the area.

Aurora Geosciences Ltd was contracted by Bootleg Exploration Ltd to conduct the exploration program. Aurora provided a crew of 2 persons with the necessary gear for the program. The crew spend six days on site and collected 12 rock samples and 223 soil samples.

The soil sampling program returned values up to 1200 ppm Zn and 159.3 ppm Pb. Two areas in particular returned significant results; one at the western part of the grid; and one on the far eastern part grid. These areas are characterized by anomalous associations of Pb-Zn-Cd-Ag-Cu and minor Au.

The prospecting program returned one highly anomalous rock sample that contained 3.85% zinc and 12.6 g/t silver. This result is considered significant considering the short time that the crew was on site and the limited number of samples collected in the area.

Recommendations for further work in the area are to:

- 1 Conduct more soil sampling by filling-in the sample density in anomalous areas on the western and eastern part of the grid and expand the grid to the east and south.
- 2 Additional prospecting and sampling in the immediate area to determine the source of the 3.85% zinc sample.
- 3 Expand the regional prospecting and sampling.
- 4 Geological mapping of the prospect area.

A budget of \$75,000 is estimated for the follow-up program.

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## 1.0 INTRODUCTION

Aurora Geosciences was contracted by Bootleg Exploration Inc. to conduct a reconnaissance exploration program in the Itsi Lake Area off the North Canol Highway on NTS maps sheet 105J/16 to explore for SEDEX-style lead-zinc-silver potential. The exploration program was partially funded by the Yukon Mineral Incentive Program (YMIP), a program that assists companies and individuals with mineral exploration costs. This report documents the exploration program.

The prospecting crew consisted of Casey Adshead (geological technician) and Michael Mark (field assistant). The program was conducted from September 7 through September 17, 2006.

The crew mobilized from Whitehorse by truck to the area and, after over-nighting in Ross River on the first night, flew to the area by helicopter and established a small fly camp. The work was conducted by foot traverse from the camp. The crew evaluated the area by soil sampling, prospecting and rock sampling.

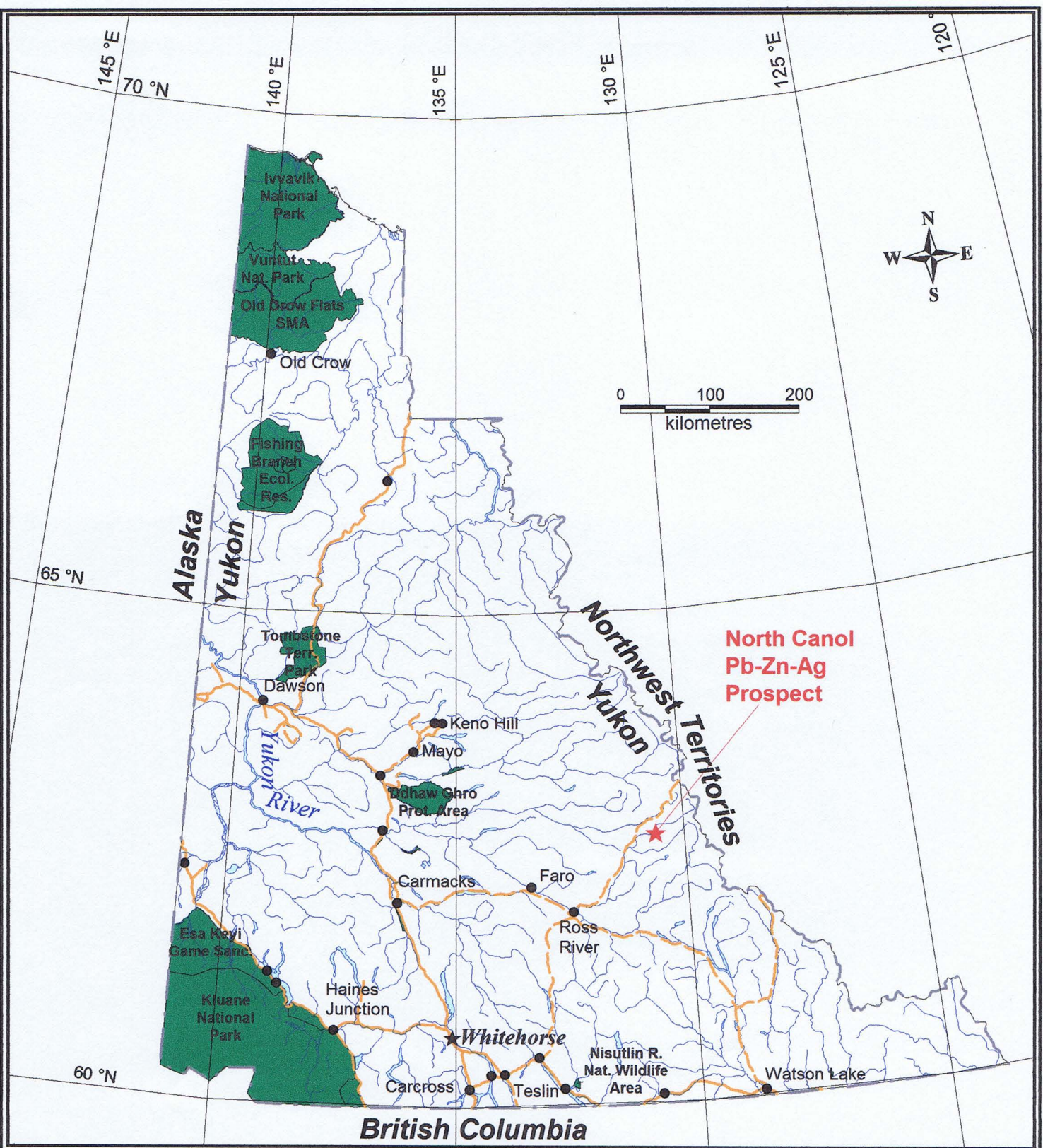
## 2.0 LOCATION AND ACCESS

The North Canol SEDEX Reconnaissance area is located 150 km northeast of Ross River in east-central Yukon on NTS map 105J16. It is 8 km south of the point where the North Canol highway crosses the MacMillan River and is centered at 62° 53' N Latitude, 130° 21' W Longitude. The area lies within the Watson Lake Mining District. The location is plotted on Figure 1.

Access to the area is by the vehicle on the North Canol Highway from Ross River to the MacMillan River. From there, the area can be accessed by foot, however helicopter is recommended. The nearest helicopter base is located in Ross River.

## 3.0 LAND STATUS

The project area is on Crown Land and falls under the jurisdiction of the Government of Yukon. There are no First Nation Class A, Class B lands or private land in the immediate area. The area is open for quartz claim staking. Active mineral claims in the area are shown on the Land Status Map in Figure 2.



S.G. CASSELMAN  
 PROFESSIONAL GEOSCIENTIST  
 BRITISH COLUMBIA  
 JANUARY 2007

**BOOTLEG EXPLORATION  
 North Canal Pb-Zn-Ag Prospect  
 Location Map**

Figure 1

February 24, 2006



Quartz claims



Project area

15 January, 2007  
 S. CASSELMAN  
 PROFESSIONAL  
 BRITISH COLUMBIA  
 GEOSCIENCE

**BOOTLEG EXPLORATION INC.**  
**NORTH CANOL RECONNAISSANCE PROJECT**  
**Figure 2 - Land Status Map**

NTS: 105J16  
 Datum: NAD83

Date: January 5, 2007

Mining District: Watson Lake  
 Projection: UTM, zone 9

Job: BEI-06-03-YT

scale 1:150,000

**AURORA GEOSCIENCES LTD**

#### 4.0 PHYSIOGRAPHY AND CLIMATE

The project area is in the eastern Yukon in the Selwyn Mountains. The area is comprised of steep mountainous terrain with broad, treed valleys. Elevations range from 1,300 to 1,900 metres above sea level. The area is treed with spruce, pine, poplar and willow at lower elevations and alpine terrain at higher elevations.

The area experiences cold dry winters and warm moist summers. Snow usually begins accumulating in September and is generally melted by June. Temperatures range from highs in the mid 20<sup>0</sup>'s in summer to lows of -50<sup>0</sup> C in winter.

#### 5.0 REGIONAL GEOLOGICAL SETTING

The regional geology of the project area is taken from the Yukon Digital Geology Map (Gordey, et. al., 2003) and is plotted on Figure 3.

The North Canol area is in the central part of the Selwyn Basin, a recognized Sedex Pb-Zn-Ag mining and exploration region. The Selwyn Basin is defined by Gordey, 1993 as "a region of deep-water offshore sedimentation that persisted from late Precambrian to Middle Devonian time. Its basal deposits consist of late Precambrian rift (-) clastics; it is overlain by rift clastics of late Devonian age. On its northeastern side are time-equivalent shallow shelf strata of Mackenzie Platform. Along its southwestern margin there developed in the Siluro-Devonian a carbonate-clastic shelf, the Cassiar Platform... Its southwestern limit is essentially the limit of the miogeocline as presently preserved (.)"

The basin formed by passive margin sedimentation, it is characterized by thick accumulations of clastic sediments, with a significant component of deepwater black shales and cherts. These basinal rocks interfinger with and are bound by shallower water platformal carbonates (Heon, 2007). It is bounded to the north by the Dawson Fault and grades into platformal facies to the east (Mackenzie Platform) and southwest (Cassiar Platform). It may be bounded by a Mesozoic thrust fault separating it from Yukon-Tanana Terrane in the Anvil district and it is offset to the southwest by the Tintina Fault.

The regional geology of the project area consists of sedimentary rocks of the Upper Cambrian to Ordovician Rabbitkettle Formation; Ordovician to Lower Devonian Road River Group; and Devonian to Mississippian Earn Assemblage of the Selwyn Basin. These rocks are overlain by Carboniferous to Permian rocks of the Mount Christie Formation. All these rocks are intruded by the mid-Cretaceous Selwyn Suite in the eastern part of the prospect area

The Rabbitkettle Formation (COR) consists of thin bedded, wavy banded, silty limestone and grey lustrous calcareous phyllite; limestone intraclast breccia and

conglomerate; massive to laminated, grey quartzose siltstone and chert and rare black slate; local mafic flows, breccia, and tuff.

The Road River Group (ODR) consists of black, gun-blue, or silvery white weathering black graptolitic shale and black chert; resistant grey weathering, thin to medium bedded, light grey to black, greenish grey or turquoise chert; and minor argillaceous limestone.

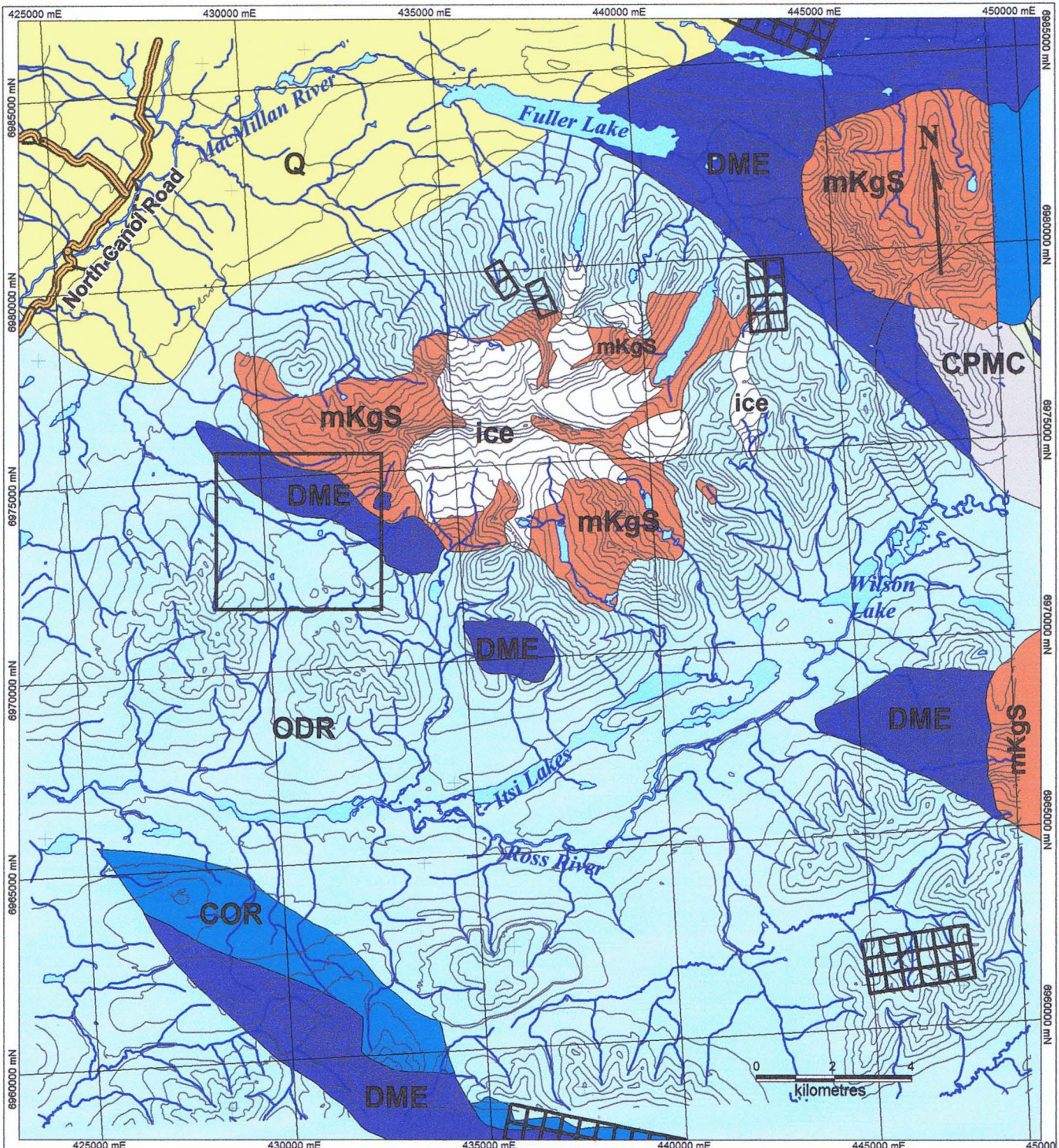
The Earn Group (DME) consists of thin bedded, laminated slate with thin to thickly interbedded fine to medium grained chert-quartz arenite and wacke; thick members of chert pebble conglomerate; black siliceous siltstone; nodular and bedded barite; and rare limestone.

The Mount Christie Formation (CPMC) consists of burrowed, interbedded greenish grey cherty shale and green shale; thin to medium bedded, light grey-green to black chert; black siliceous slate and siltstone; minor quartzite, limestone and dolostone; and locally abundant, large grey barite nodules.

The Selwyn Suite intrusions (mKgS) in the area are resistant, blocky, fine to coarse grained equigranular to porphyritic (K-feldspar) biotite quartz monzonite and granodiorite and minor quartz diorite with minor leuco-quartz monzonite and syenite.

The Rabbitkettle Formation, Road River Group and Earn Group Rocks host numerous lead-zinc and silver deposits and mineral occurrences including the Faro, Howards Pass, Tom and Jason Deposits. Much of the Selwyn Basin has been explored for SEDEX Pb-Zn deposit types, however the North Canol Prospect Area appears to have experienced very little exploration activity as there is very little work documented for the area. The only documented exploration activity near the prospect area is at the Canol Occurrence (minfile 105J 032), which was evaluated by Silver Sceptre Resources Ltd in 1980. Silver Sceptre focused on an airborne magnetic anomaly associated with the nearby intrusion and it appears they were not focused on the SEDEX potential.





**LEGEND**

- Q** Quaternary sediments
- mKgs** mid Cretaceous Selwyn Suite granodiorite
- CPMC** Carboniferous to Permian Mount Christie Formation shale and siltstone
- DME** Devonian to Mississippian Earn Group shale and argillite
- ODR** Ordovician to Lower Devonian Road River Group shale and siltstone
- COR** Cambrian to Ordovician Rabbitkettle Formation limestone and phyllite

scale 1:150,000

**BOOTLEG EXPLORATION INC.  
NORTH CANOL RECONNAISSANCE PROJECT  
Figure 3 - Regional Geology Map**

NTS: 105J16      Mining District: Watson Lake  
 Datum: NAD83      Projection: UTM, zone 9  
 Date: January 5, 2007      Job: BEI-06-03-YT

## 6.0 2006 EXPLORATION PROGRAM

The North Canol SEDEX Reconnaissance Project was identified by researching the government Regional Geochemical Survey (RGS) data, regional geology and minfile occurrences to look for lead-zinc-silver SEDEX-style potential in the Selwyn Basin. The research identified the area as having anomalous Pb-Zn-Ag-Cd and Ba in stream sediments in an area underlain by Selwyn Basin rocks and that had been previously under explored. The exploration program consisted of establishing broad spaced soil sampling grid to cover prospective stratigraphy (500 m line spacing 50 m sample spacing), prospecting the prospective the area and collecting rock samples.

The crew conducted six days of reconnaissance traverses and soil sampling and collected 12 rock samples and 223 soil samples.

## 7.0 GEOCHEMICAL ANALYTICAL PROCEDURE

All samples were sent to Acme Analytical Laboratories in Vancouver for processing. Acme is an ISO 9002 accredited facility.

The analytical procedure for the soil samples consisted of drying the samples then sieving to -80 mesh. A 15.0 gm sample of the -80-mesh material was then digested in aqua-regia solution and diluted to 300 ml with distilled water. This solution was then analyzed for 36 elements by Inductively Coupled Plasma Mass Spectrometry (ICP-MS) according to the Acme Group 1DX analytical package.

Rock samples were processed by crushing and pulverizing to -150 mesh. A 0.50 gm sample of the -150 mesh material was then digested in aqua-regia solution and diluted to 10 ml with distilled water. This solution was then analyzed for 37 elements by Inductively Coupled Plasma Mass Spectrometry (ICP-MS) according to the Acme Group 1F analytical package. One rock sample returned over limits for zinc (<10,000 ppm). This sample was later assayed by dissolving 1.0 gram of the pulverized material in aqua regia and diluting to 100 ml with distilled water. The solution was then analysed by ICP-ES for zinc and silver according to the Acme Group 7AR analytical package. Geochemical Analytical Certificates for the 2006 program are included in Appendix II.

## 8.0 RESULTS

The reconnaissance program provided for a brief visit to the project area. The crew evaluated the site with a goal of determining whether there is potential for SEDEX-style Pb-Zn-Ag mineralization. The RGS data of the surrounding area indicated the presence of anomalous Pb-Zn-Ag, as well as pathfinder elements Cd and Ba.

The soil sampling program returned a number of scattered anomalous lead and zinc values up to 1200 ppm Zn and 159.3 ppm Pb from throughout the survey area (Figures 5 and 6). Two areas in particular are of greater interest; the first is at the western part of the grid on lines L1N and L3N where anomalous zinc values can be traced from line to line and a lead value of 43.7 ppm on line L3N occurs; the other anomalous area is on the far eastern part of the survey grid where anomalous stretches of lead and zinc occur on lines L3N and L7N. Here there is reasonably good correlation between the lead and zinc values with lead up to 159.3 ppm and zinc to 1161 ppm. Both of these areas are also highly anomalous in cadmium and copper and weakly to mildly anomalous in silver and gold (Figures 8, 9, 7 and 10, respectively).

The prospecting and rock sampling program returned significant results. Rock sample ITSI-RS-12 contained 3.85% zinc, 343 ppm copper and 12.6 g/t silver. This result is considered significant considering the short time that the crew was on site and the limited number of samples collected in the area. Unfortunately, the mineralization in the sample was not described and its form is not known. This sample also has anomalous cadmium and copper, but the lead content is not considered anomalous at 6.53 ppm.

## 9.0 CONCLUSIONS AND RECOMMENDATIONS

The prospecting and soil sample program in the Itsi Lake area south of the North Canol Highway was successful in locating significantly anomalous zinc values in rock and soil samples and moderately to highly anomalous lead, cadmium, copper, silver and gold. The most significant result being a rock sample that returned 3.85% Zn and 12.6 g/t Ag. The soil sample survey identified two areas; one on the western part of the grid and one on the eastern part of the grid that demonstrate SEDEX-type metal associations and warrant further work. As well, there are a number of isolated soil anomalies that should be examined to determine their significance.

In general, lead-in-soil is the best indicator of proximity to source because it is much less mobile than the other SEDEX-associated indicator elements. Follow-up work may be expedited by focusing on the higher lead anomalies.

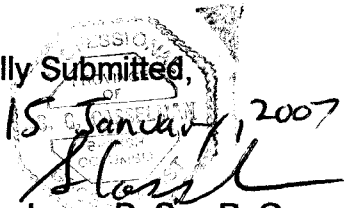
The metal association is that which be expected from SEDEX-style mineralization, however it could also be skarn-related. The proximity of the eastern soil anomaly and rock sample ITSI-RS-12 to the large Selwyn Suite granodiorite makes a skarn-related source a possibility. Follow-up work should attempt to determine the style of mineralization, which will aid in the search for the source of the mineralization.

Recommendations for further work in the area are to:

- 1 Conduct more soil sampling by filling-in the sample density in anomalous areas on the western and eastern part of the grid (100 m line spacing and 25 m station spacing) and expand the grid to the east and south.
- 2 Additional prospecting and sampling in the immediate area to determine the source of the 3.85% zinc sample.
- 3 More regional prospecting and sampling to be directed by reviewing the RGS data to look for other anomalies.
- 4 Geological mapping of the prospect area.

A budget of \$75,000 is estimated for the follow-up program.

Respectfully Submitted,



15 January, 2007

Scott Casselman, B. Sc., P. Geo.



## 11.0 REFERENCES

- Casselmann, S. 2006. Yukon Mineral Incentive Program (YMIP) Application For a Focused Regional Exploration Program In the North Canal Road Area, , Yukon Territory. Private Report.
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- Heon, Danielle, 2007. Selwyn Basin Metallogeny. Yukon Geological Survey website, <http://www.geology.gov.yk.ca/metallogeny/selwyn/intro.html#definition>
- Gordey, S. P. and Anderson, R. G., 1993. Evolution of the northern Cordilleran Miogeocline, Nahanni map area [105I], Yukon and Northwest Territories. Geological Survey of Canada, Memoir 428.
- Gordey, S. P. and Makepeace, A. J., 2003. Yukon Digital Geology. Geological Survey of Canada, Open File D3826.

**APPENDIX I**

**STATEMENT OF QUALIFICATIONS**

### Statement of Qualifications

I, Scott Casselman, P. Geo., certify that:

- 1) I reside at 33 Firth Road, Whitehorse, Yukon Territory, Y1A 4R5
- 2) I am a geologist employed by Aurora Geosciences Ltd. of Whitehorse, Yukon Territory.
- 3) I graduated from Carleton University in Ottawa, Ontario with a Bachelor of Science Degree in Geology in 1985 and have worked as a geologist since that time.
- 4) I am a member of the Association of Professional Engineers and Geoscientists of British Columbia, Registration No. 20032.
- 5) I compiled this report from data collected by Aurora Geosciences staff on the North Canal Reconnaissance Project area during the summer of 2006.
- 6) I have not visited the project area.

Dated this 15<sup>th</sup> day of January, 2007, at Whitehorse, Yukon Territory.

  
Scott G. Casselman, BSc., P. Geo.



**APPENDIX II**

**GEOCHEMICAL ANALYTICAL CERTIFICATES**



GEOCHEMICAL ANALYSIS CERTIFICATE



Aurora Geosciences Ltd. (Whitehorse) PROJECT North Canol File # A608826

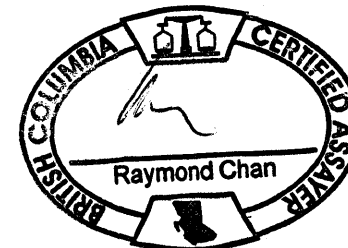
108 Gold Road, Whitehorse YT Y1A 2W3 Submitted by: Scott Casselman

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Sc	Tl	S	Hg	Se	Te	Ga
	ppm	ppm	ppm	ppm	ppb	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppm	ppm	%	ppb	ppm	ppm	ppm
G-1	1.38	2.59	2.84	41.1	11	4.4	4.3	524	1.84	<1	2.7	<2	4.5	53.9	.01	.03	.09	36	53	.072	7.7	14.1	.57	200.0	.120	5	.89	.059	.45	2.7	1.9	.37	<.01	<5	<1	<.02	4.7
ITSI-RS-1	.85	12.03	16.09	112.7	1806	10.8	12.3	387	3.32	5.6	1.9	1.4	10.3	128.4	.30	4.58	.12	39	2.20	.051	13.7	33.8	1.06	79.7	.123	4	4.01	.372	.39	.4	4.1	.95	1.87	7	16.7	.11	10.9
ITSI-RS-2	1.08	38.97	10.31	320.3	1966	27.6	11.6	330	3.08	3.4	1.6	1.6	9.6	124.6	3.88	2.20	.37	48	2.21	.049	11.2	51.9	1.23	114.7	.113	5	4.34	.352	.41	1.5	6.5	1.07	1.72	10	32.6	.11	11.4
RE ITSI-RS-2	1.08	39.20	10.25	323.7	1998	28.0	11.8	335	3.13	4.2	1.7	2.2	9.7	127.5	3.93	2.11	.38	49	2.24	.049	11.6	53.3	1.25	109.9	.113	5	4.40	.355	.42	1.4	6.5	1.09	1.74	10	33.5	.11	11.8
ITSI-RS-3	.68	48.23	11.39	96.6	2065	5.8	14.4	415	4.08	22.8	.9	1.8	6.2	128.1	1.21	2.60	1.62	30	2.26	.067	11.4	12.9	.95	39.1	.145	5	4.34	.402	.13	.5	2.3	.16	2.13	<5	35.0	.12	11.6
ITSI-RS-4	1.60	224.84	30.48	35.4	3894	292.8	64.8	365	9.20	2.3	.1	3.7	.6	479.5	.70	11.09	.40	60	3.81	.109	4.7	147.4	1.05	17.9	.290	6	6.17	.122	.43	.4	1.9	1.90	6.31	<5	106.6	.48	16.1
ITSI-RS-5	1.43	200.90	17.62	498.6	3163	320.9	63.9	519	11.18	13.0	2.8	6.1	.6	16.2	5.66	58.86	.20	32	.74	.116	1.8	80.0	.98	18.7	.033	4	2.19	.005	.26	<.1	2.8	.89	6.51	8	63.0	.37	7.0
ITSI-RS-6	1.11	48.37	13.16	60.5	2252	8.0	7.9	179	2.22	3.5	2.8	1.3	15.6	62.0	1.15	2.22	.21	17	.93	.053	13.9	18.2	.68	39.2	.087	7	1.91	.170	.11	2.9	3.7	.14	1.10	5	33.9	.05	6.4
ITSI-RS-7	.70	48.68	9.05	686.5	1115	76.6	10.7	287	2.52	27.8	3.5	1.0	14.3	50.0	1.99	1.59	.50	25	.84	.052	27.0	27.2	.84	74.6	.087	6	2.30	.206	.28	.2	5.1	.56	1.17	6	11.1	.06	8.7
ITSI-RS-8	1.77	169.59	5.26	100.1	742	12.8	8.6	93	2.70	73.0	1.8	6.4	10.3	253.3	.69	1.43	1.65	41	2.59	.048	13.8	35.0	1.07	79.5	.133	6	4.94	.203	.11	1.6	6.4	.18	1.22	<5	52.6	.09	13.7
ITSI-RS-9	.58	4.31	20.12	40.7	192	8.1	11.8	318	3.25	79.7	1.3	3.7	6.9	38.2	.15	13.73	.22	40	.65	.043	7.1	43.7	1.01	47.1	.079	4	1.55	.091	.11	.3	3.6	.08	3.00	<5	16.4	.04	5.4
ITSI-RS-10	3.53	76.92	10.71	148.8	688	33.7	6.2	296	2.81	5.3	.4	1.6	1.5	75.3	.92	2.04	.09	66	1.12	.014	3.8	43.9	.18	43.8	.009	3	1.78	.044	.11	6.1	2.2	.65	2.24	24	6.4	.05	7.8
ITSI-RS-11	8.34	178.86	2.44	22.0	2198	79.5	6.6	49	2.60	3.4	2.0	2.0	1.7	157.7	.30	.22	.32	134	1.64	.121	10.9	49.3	.09	115.1	.061	4	2.17	.028	.03	.7	1.5	.04	1.39	<5	69.3	.15	11.2
ITSI-RS-12	8.42	343.04	6.53	>10000	12600	97.8	13.5	2102	9.65	1.6	2.1	32.7	.1	2.3	382.63	.78	5.83	182	32	130	.9	53.1	.04	9.6	.074	10	3.32	.007	.08	40.6	1.3	.16	7.29	262	258.0	1.45	41.0
STANDARD DS7	20.47	106.64	68.97	395.3	858	55.4	9.4	617	2.37	47.0	5.2	64.5	4.8	76.6	6.25	5.44	4.56	82	.95	.076	14.4	246.6	1.03	375.2	.125	41	1.02	.095	.44	3.7	2.6	4.13	.19	191	3.3	1.04	5.0

GROUP 1F - 0.50 GM SAMPLE LEACHED WITH 3 ML 2-2-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR, DILUTED TO 10 ML, ANALYSED BY ICP/ES & MS.  
(>) CONCENTRATION EXCEEDS UPPER LIMITS. SOME MINERALS MAY BE PARTIALLY ATTACKED. REFRACTORY AND GRAPHITIC SAMPLES CAN LIMIT AU SOLUBILITY.  
- SAMPLE TYPE: ROCK R150 Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DEC 1 1 2006

Data 1 FA \_\_\_\_\_ DATE RECEIVED: NOV 24 2006 DATE REPORT MAILED: .....



GEOCHEMICAL ANALYSIS CERTIFICATE

Aurora Geosciences Ltd. PROJECT North Caro/Recce File # A607087 Page 1

108 Gold Road, Whitehorse YT Y1A 2W3 Submitted by: Scott Casselman



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.2	2.0	3.4	44	<.1	3.8	4.0	520	1.84	<.5	2.0	.7	3.9	74	<.1	<.1	.1	36	.57	.080	9	7	.62	199	.127	1	1.11	.105	.52	.1	<.01	2.4	.3	<.05	5	<.5	15.0
L1E 1100N	18.5	83.2	31.9	281	.6	30.6	4.5	247	5.31	48.9	2.2	4.9	.2	38	.8	12.7	1.4	171	.03	.237	18	25	.15	408	.007	2	1.09	.008	.12	.3	.03	.6	.6	.24	6	9.0	15.0
L1E 1050N	17.5	80.2	27.5	232	1.5	28.7	4.0	197	3.55	56.3	4.1	9.5	.2	37	.8	13.0	.9	143	.09	.218	14	25	.22	417	.010	2	1.23	.010	.09	.3	.06	.7	.5	.17	5	11.3	15.0
L1E 1000N	13.0	35.9	26.7	87	1.3	11.6	.8	58	3.60	54.7	1.9	4.9	.5	41	.4	7.1	.7	111	.03	.175	20	22	.18	387	.005	3	.88	.009	.24	.2	.09	.9	.9	.54	3	12.0	15.0
L1E 950N	.2	7.2	.8	9	<.1	1.2	1.6	41	.53	.8	.2	.5	.1	10	.1	<.1	<.1	18	.12	.061	2	1	.03	59	.028	<1	.50	.027	.02	<.1	.01	.4	<.1	<.05	2	<.5	15.0
L1E 900N	15.2	26.1	29.9	158	1.3	10.2	1.2	36	2.42	61.8	1.3	27.9	1.5	12	.3	7.8	1.1	126	.01	.061	18	11	.02	293	.037	2	.31	.004	.09	.6	.08	.8	.3	.17	4	7.3	15.0
L1E 850N	16.5	35.4	109.6	94	1.2	7.1	1.0	27	3.91	70.7	.8	3.1	.2	47	.1	10.6	1.5	190	.01	.144	23	14	.05	720	.007	5	.44	.009	.18	.2	.05	.6	1.4	.30	5	10.9	7.5
L1E 800N	10.5	24.3	11.7	38	3.7	9.1	.4	21	1.40	23.5	7.2	3.2	1.3	189	.7	8.4	.2	317	1.18	1.112	13	55	.10	1395	.007	10	.97	.004	.14	.3	2.53	2.4	.9	.08	3	7.6	15.0
L1E 750N	13.4	19.5	40.2	74	1.1	9.4	3.0	82	1.79	19.8	1.8	1.6	.4	26	.2	5.6	1.4	144	.05	.097	14	21	.16	329	.069	2	.69	.006	.12	.6	.12	.7	.8	.09	13	4.4	15.0
L1E 700N	17.7	22.8	31.8	71	1.4	8.8	1.0	23	1.31	32.0	2.5	2.3	.1	31	.3	5.7	1.3	202	.02	.078	14	22	.04	454	.009	2	.53	.006	.08	.3	.10	.1	.8	.13	7	7.1	15.0
L1E 650N	4.4	20.6	23.5	23	6.8	9.0	.3	8	.44	6.4	4.6	4.8	.1	13	.3	2.6	.6	131	.04	.043	21	43	.02	295	.004	3	.36	.003	.06	.1	.30	.2	.7	.06	3	1.9	15.0
RE L1E 650N	4.1	21.0	23.8	23	7.1	9.3	.3	7	.44	6.0	4.4	3.3	.1	13	.4	2.6	.5	109	.04	.041	20	39	.02	278	.002	1	.33	.003	.04	.1	.29	.2	.7	<.05	3	2.1	7.5
L1E 600N	6.7	19.4	13.5	33	1.6	6.5	.4	11	.41	7.0	2.6	1.0	.1	35	.3	1.2	.2	98	.02	.092	19	35	.02	217	.002	3	.32	.005	.06	.1	.10	.1	.4	.06	2	2.8	15.0
L1E 550N	2.8	5.6	4.0	20	.9	2.6	1.4	93	.73	3.3	1.1	.7	<.1	17	.3	.8	.1	45	.05	.084	2	5	.03	117	.005	<1	.22	.022	.03	<.1	.07	.1	.2	.07	1	1.2	15.0
L1E 500N	15.7	22.9	11.7	237	3.2	84.4	1.5	116	1.61	32.8	4.2	3.9	<.1	132	2.7	8.7	.2	197	.39	.447	7	20	.10	862	.002	2	.70	.031	.10	.1	.44	.1	1.5	.31	3	7.2	15.0
L1E 450N	17.6	22.4	24.8	128	1.5	24.1	1.9	314	1.55	39.1	2.5	1.4	.1	53	1.0	5.4	.7	147	.10	.259	11	20	.09	642	.002	2	1.00	.011	.10	.2	.10	.1	.7	.17	5	5.0	15.0
L1E 400N	1.3	5.3	1.0	13	.5	5.7	.6	21	.31	3.0	.8	<.5	<.1	10	.2	.6	<.1	12	.10	.077	2	1	.03	50	.008	<1	.37	.023	.02	<.1	.08	.1	<.1	<.05	2	1.0	15.0
L1E 350N	13.5	20.5	11.6	419	.5	41.0	1.6	106	.96	70.4	2.3	1.0	<.1	42	1.2	11.2	.3	145	.25	.322	10	25	.18	557	.002	2	1.02	.006	.08	.1	.05	.2	1.0	.10	5	3.3	15.0
L1E 300N	2.8	16.4	4.5	100	3.1	26.5	1.0	33	.26	2.4	1.7	2.3	<.1	24	1.6	3.6	.1	37	.20	.115	4	8	.07	326	.005	<1	.51	.025	.03	.1	.24	.1	4	<.05	3	4.7	15.0
L1E 250N	.8	3.3	.9	41	<.1	6.7	.3	6	.04	1.1	.2	<.5	.1	9	<.1	.4	<.1	3	.06	.017	1	<1	.02	47	.019	<1	.29	.027	.01	<.1	<.01	.1	.1	.07	1	.9	15.0
L1E 200N	6.2	23.0	17.6	69	.2	9.0	.7	25	1.20	26.6	1.9	2.8	<.1	11	.1	4.0	.5	128	.02	.112	10	20	.05	141	.004	<1	.63	.004	.04	.3	.11	.1	.3	.07	5	2.8	15.0
L1E 150N	4.4	47.3	14.7	316	3.3	44.4	1.0	49	1.14	10.4	5.8	5.3	.2	31	3.7	3.4	.3	83	.22	.314	8	28	.18	881	.005	1	1.38	.007	.05	.2	.56	.5	.9	.20	4	4.6	15.0
L1E 100N	12.3	26.7	5.4	509	.9	64.4	10.7	499	1.76	115.5	4.0	2.4	.1	32	7.0	3.6	.2	92	.29	.190	9	21	.27	532	.009	2	1.24	.024	.04	.5	.17	.4	1.7	.10	4	4.7	15.0
L1E 50N	15.1	36.5	9.8	408	.7	32.9	4.2	404	2.40	68.4	3.1	2.5	.2	32	2.3	6.1	.4	157	.29	.206	10	25	.26	372	.011	2	1.04	.008	.06	.4	.07	.5	.5	.09	5	5.0	15.0
L1E ON	7.2	21.9	18.4	64	.3	8.6	1.6	75	1.82	26.8	1.2	1.7	<.1	16	.1	3.8	.4	122	.02	.072	9	13	.05	133	.011	2	.80	.008	.05	.3	.04	.2	.2	.06	6	3.1	15.0
L1E 50S	.2	1.1	.3	6	.4	.7	.6	15	.26	.5	.1	<.5	<.1	5	.1	.3	<.1	11	.02	.014	<1	1	.01	11	.013	<1	.07	.019	.01	<.1	.01	.1	<.1	<.05	<1	<.5	15.0
L1E 100S	10.0	23.4	9.9	93	<.1	13.9	2.0	59	1.38	24.7	.9	.5	.1	9	.1	5.9	.3	200	.01	.035	10	13	.04	83	.014	1	.47	.009	.05	.3	.02	.4	2	<.05	6	2.5	7.5
L1E 150S	10.1	45.8	22.7	146	.4	22.9	4.0	179	3.22	41.7	2.0	4.6	.2	16	.3	7.4	.3	150	.03	.183	10	20	.08	237	.006	3	.70	.005	.09	.4	.10	.3	.3	.08	4	5.0	15.0
L1E 200S	7.2	28.5	23.3	98	.6	15.3	2.0	58	2.02	42.9	2.7	3.9	.5	18	.7	6.6	.7	112	.10	.234	13	26	.13	303	.048	2	1.34	.006	.06	1.1	.10	.9	.3	.07	8	4.1	15.0
L1E 250S	6.1	16.3	20.2	58	.1	9.2	1.6	45	1.38	35.1	1.1	1.0	<.1	11	.1	4.0	.4	122	.01	.049	12	13	.04	111	.013	1	.54	.004	.05	.4	.02	.2	.3	<.05	6	2.0	15.0
L1E 300S	3.9	13.2	9.6	31	<.1	4.6	.9	26	.58	10.5	.6	.8	<.1	6	<.1	2.2	.3	75	.01	.021	12	9	.03	79	.011	1	.57	.005	.03	.4	.02	.2	.3	<.05	4	.7	15.0
L1E 350S	9.0	36.3	17.0	117	.7	18.5	3.6	180	2.58	38.8	2.1	1.7	.1	23	.3	6.6	.3	166	.02	.149	10	20	.08	237	.011	3	.73	.008	.07	.5	.08	.5	.3	.09	4	5.1	15.0
L1E 400S	10.2	26.6	18.1	117	.4	18.0	2.0	61	1.89	31.4	1.8	1.5	.1	19	.2	5.9	.3	190	.01	.099	11	21	.06	156	.005	2	.61	.005	.07	.4	.06	.2	.4	<.05	5	4.3	15.0
L1E 450S	6.9	19.4	9.8	88	2.2	14.7	1.8	84	2.18	28.0	1.7	2.5	.9	18	.2	4.6	.2	173	.05	.163	7	25	.07	164	.015	2	.97	.002	.05	.4	.18	1.0	.3	<.05	4	3.3	15.0
L1E 500S	12.7	33.5	23.8	148	.8	23.5	3.1	124	4.07	47.9	2.1	3.1	.5	21	.3	8.9	.4	369	.02	.157	11	35	.11	210	.017	2	1.02	.004	.08	.7	.12	1.0	.4	.06	8	5.3	15.0



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Sample	
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	gm
G-1	.2	2.0	3.4	44	<.1	3.7	4.1	523	1.88	<.5	2.0	.8	3.9	69	<.1	<.1	.1	37	.52	.080	8	7	.60	201	.124	2	1.05	.098	.53	.1	<.01	2.1	.4	<.05	5	<.5	15.0	
L1E 550S	6.7	21.6	22.8	77	.2	12.0	1.8	64	1.73	20.2	1.3	1.2	.1	20	.2	3.0	.3	160	.01	.125	12	21	.06	208	.005	2	.76	.006	.06	.2	.07	.2	.4	.07	6	2.3	15.0	
L1E 600S	5.5	16.8	12.5	52	.2	8.1	1.4	38	.96	10.8	.9	2.1	.1	14	.1	1.9	.2	131	.01	.052	13	19	.04	167	.004	3	.60	.005	.05	.1	.05	.1	.4	<.05	6	1.5	7.5	
L1E 650S	16.3	38.3	26.0	185	1.1	26.4	3.0	116	3.98	49.4	2.6	3.0	.4	46	.3	6.6	.4	460	.03	.203	11	43	.11	478	.011	2	1.16	.007	.09	.3	.17	1.0	.6	.10	8	6.4	7.5	
L1E 700S	30.6	84.3	37.4	400	3.1	56.2	6.0	250	7.96	106.1	6.5	6.0	1.0	83	.7	12.0	.5	1047	.07	.463	19	97	.23	597	.018	3	2.02	.013	.15	.5	.55	1.9	1.1	.20	14	13.6	7.5	
L1E 750S	26.8	43.9	34.1	150	5.0	24.8	3.6	227	5.90	51.8	3.6	3.7	.3	87	.4	12.0	.4	365	.07	.459	9	41	.05	314	.007	3	.74	.019	.16	.3	.98	.5	1.1	.45	5	13.6	7.5	
L1E 800S	11.5	48.0	26.2	143	6.2	23.6	.8	19	1.31	8.0	6.2	1.1	.1	63	3.3	5.1	.3	172	.15	.187	10	43	.02	436	.001	3	.46	.013	.11	.1	.25	.3	.7	.22	3	9.6	7.5	
L1E 850S	22.6	33.1	29.7	150	2.5	20.5	2.4	172	2.21	26.9	3.2	3.7	.1	35	1.0	6.9	.3	291	.03	.200	10	25	.03	426	.004	3	.46	.006	.09	.5	.84	.3	1.4	.12	5	5.8	15.0	
L1E 900S	13.6	81.3	13.7	359	2.1	47.9	6.4	280	3.06	39.5	5.3	9.1	.9	37	1.3	9.5	.2	204	.09	.287	11	26	.11	373	.007	3	.98	.005	.08	.3	.83	1.1	.5	.08	3	5.7	15.0	
L1E 950S	15.2	40.2	24.4	185	2.2	26.5	3.0	78	3.46	34.2	2.2	3.5	.1	20	.4	7.3	.3	212	.01	.127	11	23	.10	265	.014	3	.88	.008	.09	.2	.16	.5	.5	.10	7	4.6	15.0	
L1E 1000S	8.8	43.8	15.2	120	1.1	22.0	5.4	238	4.25	48.9	2.6	5.2	.2	94	.3	6.3	.2	107	.08	.292	7	16	.06	605	.006	3	.67	.019	.12	.2	.53	.5	.4	.29	3	6.1	7.5	
L1E 1050S	14.7	83.1	22.4	227	1.5	40.2	7.8	348	4.03	46.1	4.9	8.6	.7	85	.8	8.8	.3	158	.05	.188	10	20	.09	700	.008	2	.82	.015	.12	.2	.38	1.6	.5	.28	3	8.2	15.0	
L1E 1100S	7.7	34.8	13.2	109	.8	16.4	2.4	87	2.00	20.6	2.5	2.5	.1	16	.3	3.8	.2	88	.02	.156	7	15	.05	265	.002	2	.63	.009	.06	.2	.28	.3	.3	.11	3	3.1	7.5	
RE L1E 1100S	7.4	33.5	12.9	105	.7	15.8	2.3	85	1.95	20.4	2.4	2.1	<.1	15	.3	3.6	.2	80	.03	.149	6	13	.04	245	.002	2	.59	.008	.05	.2	.26	.2	.2	.12	3	2.9	.5	
L1E 1150S	4.0	13.1	4.3	56	.1	9.4	1.9	32	.82	9.9	.5	.8	<.1	6	.1	1.9	.1	62	.01	.029	11	8	.02	91	.005	2	.35	.006	.04	.2	.03	.1	.2	<.05	3	.8	15.0	
L1E 1200S	1.3	9.6	4.4	14	.5	2.6	.9	15	.50	2.4	1.0	.9	<.1	7	.1	.6	.1	26	.01	.052	4	5	.02	49	.007	1	.73	.016	.02	.2	.05	.2	.1	<.05	3	.7	15.0	
L1E 1250S	.8	4.8	2.7	11	.3	1.6	.7	14	.36	1.6	.4	<.5	<.1	5	.1	.3	.1	21	.01	.025	5	4	.02	51	.010	<.1	.46	.012	.02	.1	.03	.1	.1	<.05	3	<.5	15.0	
L1E 1300S	3.1	9.5	2.4	32	.3	5.6	1.1	21	.50	5.0	.5	.6	.1	5	.1	1.1	.1	47	<.01	.020	8	7	.02	78	.006	1	.21	.010	.03	.1	.03	.2	.1	<.05	2	<.5	15.0	
L1E 1350S	.4	2.7	.9	6	.1	.8	.9	16	.31	<.5	.2	<.5	<.1	6	.1	.1	<.1	12	.02	.015	1	1	.02	19	.010	<.1	.17	.023	.02	<.1	.01	.1	<.1	<.05	1	<.5	15.0	
L1E 1400S	40.1	164.7	16.0	1350	6.2	182.4	3.0	98	2.62	37.1	17.2	6.4	.6	161	23.1	25.5	.2	895	.78	.500	14	96	.16	779	.006	8	1.01	.008	.16	.3	1.15	2.4	2.1	.23	6	26.1	15.0	
L1E 1450S	15.5	42.1	5.9	172	.9	28.6	1.5	45	1.02	11.9	3.7	3.5	.2	28	2.3	8.4	.1	279	.05	.092	6	22	.04	526	.007	2	.33	.013	.04	.1	.22	.6	.5	.06	2	5.7	15.0	
L1E 1500S	34.2	81.3	13.5	387	2.8	62.5	2.5	58	2.03	21.8	8.3	4.2	.6	62	3.1	16.6	.2	504	.06	.231	13	45	.05	907	.004	3	.60	.006	.09	.3	.31	.9	1.1	.17	4	15.2	15.0	
L1E 1550S	45.0	189.3	14.9	689	4.1	126.9	5.8	170	2.63	39.4	14.2	5.7	2.1	124	15.2	29.2	.2	800	.35	.392	16	73	.10	1342	.007	6	.78	.004	.12	.3	.82	3.8	1.5	.17	4	18.0	15.0	
L1E 1600S	1.3	7.1	1.9	11	.9	2.5	.5	11	.28	1.1	.8	<.5	<.1	14	.2	.7	<.1	35	.02	.047	1	5	.02	277	.004	1	.29	.018	.02	<.1	.03	.1	.1	<.05	1	1.4	15.0	
L1E 1650S	16.2	36.6	15.6	148	1.7	18.5	1.4	37	1.72	11.8	5.9	2.6	.1	140	1.0	9.9	.2	306	.05	.278	11	41	.03	1816	.002	2	.82	.003	.07	.2	.08	.2	1.0	.11	5	14.1	15.0	
L1E 1700S	10.8	26.8	14.4	122	1.3	18.1	1.6	45	1.52	13.3	2.2	1.5	<.1	63	.5	6.4	.2	162	.03	.127	8	21	.04	524	.006	1	.72	.009	.05	.4	.07	.2	.5	.11	5	9.1	15.0	
L1E 1750S	9.9	17.3	16.8	100	1.0	11.5	.7	13	.68	5.9	1.3	.7	.1	63	.4	7.3	.2	119	.02	.069	8	13	.01	597	.005	2	.31	.007	.04	.2	.04	.2	.4	<.05	3	10.8	15.0	
L2E 1250N	31.0	62.2	32.6	248	2.1	28.9	2.2	78	3.89	125.0	4.5	7.4	.1	37	1.0	16.5	1.5	234	.20	.283	11	39	.20	778	.007	1	.87	.007	.12	.8	.10	.4	.5	.27	6	23.2	7.5	
L2E 1200N	27.8	44.2	31.1	121	2.7	14.8	1.9	169	4.14	164.6	4.7	7.8	.7	50	.3	25.0	1.4	137	.19	.322	12	29	.24	831	.011	<.1	1.38	.006	.12	.5	.20	.9	.7	.25	4	20.0	15.0	
L2E 1150N	21.3	44.9	25.7	104	2.0	14.5	1.3	69	3.86	116.3	3.0	3.9	.3	26	.3	15.7	.9	152	.06	.219	16	23	.25	455	.004	2	.96	.007	.13	.3	.10	.6	.6	.19	4	14.0	7.5	
L2E 1100N	2.8	27.1	6.2	165	.2	32.6	14.6	619	3.76	10.0	.7	.8	.2	196	2.6	1.2	.3	133	1.09	.146	2	75	.41	2048	.007	1	1.42	.010	.02	.1	.06	2.1	.1	.18	11	1.0	7.5	
L2E 1050N	7.3	74.0	18.9	122	.8	13.1	2.1	91	4.19	28.5	1.2	2.0	1.6	43	.4	4.9	.3	61	.01	.123	16	11	.04	517	.003	2	.50	.004	.15	<.1	.05	2.0	.3	.20	2	8.7	7.5	
L2E 1000N	7.8	33.3	23.4	94	.8	7.1	1.4	34	2.14	33.9	.8	2.3	.1	35	.2	6.7	.3	66	.01	.089	9	10	.03	479	.001	1	.35	.006	.09	.1	.05	.3	.4	.13	2	5.6	15.0	
L2E 950N	35.9	60.4	32.2	78	3.4	18.4	2.3	90	3.59	80.0	9.3	24.3	.3	265	.7	18.9	.4	190	.20	.494	23	30	.09	372	.004	4	.65	.004	.16	.4	1.21	2.0	.7	.23	4	38.6	.5	
L2E 900N	27.9	47.8	25.6	68	3.1	15.1	1.9	72	3.01	73.4	6.8	19.0	.3	217	.6	15.7	.3	157	.15	.448	17	26	.09	217	.005	3	.53	.003	.14	.4	1.17	2.8	.7	.21	4	30.7	7.5	
STANDARD DS7	20.7	108.3	70.6	408	.9	55.0	9.6	623	2.38	49.9	4.9	69.7	4.4	72	6.6	6.0	4.6	86	.93	.081	13	171	1.07	380	.122	41	.98	.078	.45	3.8	.20	2.5	4.2	.20	5	3.7	15.0	

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.2	2.2	3.2	44	<.1	3.7	4.4	525	1.96	<.5	1.9	.7	4.0	75	<.1	<.1	.1	37	.56	.077	8	7	.60	214	.131	1	1.07	.103	.54	.1	<.01	2.3	.4	<.05	5	<.5	15.0
L2E 850N	11.8	26.0	18.1	25	2.7	6.0	.6	16	.94	8.5	3.7	8.0	.1	159	.3	9.7	.2	64	.03	.176	7	15	.03	1072	.003	3	.38	.003	.06	.3	.82	.2	.8	.14	2	15.1	15.0
L2E 800N	13.9	25.9	22.5	28	1.7	6.2	1.0	19	1.02	5.4	2.1	2.6	.1	84	.3	6.0	.3	83	.02	.099	9	16	.02	378	.004	2	.29	.002	.07	.2	.21	.3	.9	.12	3	14.9	15.0
L2E 750N	34.4	192.1	46.3	18	2.5	14.3	.4	10	2.18	25.9	20.5	2.6	3.7	383	2.8	18.8	.2	187	.41	1.353	22	26	.04	1837	.006	1	1.42	.002	.06	.4	2.48	3.7	.4	.13	2	30.3	15.0
L2E 700N	25.1	32.4	31.5	50	3.8	8.4	.7	16	1.69	13.1	2.4	3.3	.1	72	.2	11.1	.5	154	.02	.155	11	20	.02	776	.003	3	.38	.004	.14	.3	.26	.3	.9	.27	4	25.4	7.5
L2E 650N	9.0	31.5	20.6	56	2.3	10.8	1.2	30	1.18	11.5	2.0	1.1	.1	118	.6	3.7	.6	83	.05	.166	7	25	.04	1048	.005	2	.47	.005	.05	.1	.20	.2	.2	.08	3	3.9	.5
L2E 600N	4.7	126.1	9.9	650	.4	60.2	6.5	74	6.12	12.8	1.9	3.0	1.2	11	.3	5.3	.4	54	.01	.114	5	21	.04	250	.003	4	.59	.003	.11	.1	.08	3.9	.2	.14	3	3.0	7.5
L2E 550N	5.3	31.7	13.6	79	.6	11.5	3.1	237	1.85	10.7	1.0	2.4	.1	43	.4	2.5	.2	38	.02	.099	4	7	.03	459	.003	2	.34	.011	.10	.1	.05	.3	.3	.21	2	1.9	7.5
RE L2E 300S	14.3	54.8	14.0	486	1.7	84.8	18.9	681	3.12	46.9	4.6	6.1	.5	58	4.7	8.8	.4	153	.33	.333	11	21	.18	1022	.016	2	1.45	.013	.08	.8	.39	1.1	.7	.11	4	6.2	15.0
L2E 500N	31.4	65.6	34.1	154	6.1	20.1	1.9	45	2.76	17.9	7.2	2.1	.1	100	2.4	7.9	.4	295	.02	.203	14	48	.03	405	.001	3	.48	.007	.22	.2	.28	.2	1.7	.53	3	24.6	7.5
L2E 450N	16.8	81.3	23.1	239	3.4	36.3	3.9	261	2.62	31.7	9.2	6.0	.4	77	2.2	9.2	.4	232	.10	.250	12	30	.06	627	.004	2	.59	.006	.13	.2	.32	.5	.8	.24	3	11.5	15.0
L2E 400N	10.2	52.4	11.2	169	1.9	25.9	2.1	184	1.71	18.2	5.8	2.3	.1	90	1.1	7.3	.2	108	.09	.194	8	21	.04	518	.002	2	.53	.008	.08	.1	.12	.3	.4	.16	2	10.4	15.0
L2E 350N	7.0	16.5	20.6	63	1.6	7.4	1.4	30	1.20	14.7	1.1	.7	.1	40	.3	2.7	.5	97	.03	.069	9	13	.04	267	.010	1	.46	.008	.06	.2	.10	.2	.4	.06	4	3.3	15.0
L2E 300N	16.9	72.3	18.0	183	2.5	23.7	1.7	50	1.96	14.9	6.8	1.9	.2	53	1.0	6.1	.3	149	.02	.158	10	19	.02	436	.003	1	.54	.007	.08	.1	.15	.4	.5	.21	2	9.5	.5
L2E 250N	13.4	34.7	9.2	155	1.2	20.1	1.2	16	1.08	9.1	3.1	.8	.2	111	.4	5.1	.2	228	.02	.078	7	21	.03	287	.003	3	.36	.007	.08	.1	.03	.2	.7	.13	3	4.5	7.5
L2E 200N	19.0	87.3	19.0	257	3.0	40.0	2.4	42	2.03	26.3	6.9	2.6	.4	93	1.5	10.7	.3	195	.03	.149	13	24	.04	607	.004	3	.43	.005	.09	.2	.20	1.0	.7	.15	2	8.2	7.5
L2E 150N	4.7	14.8	11.3	101	.5	8.8	2.6	269	.92	8.4	2.8	.6	.2	40	2.1	2.3	.3	97	.07	.147	9	14	.06	511	.005	1	.71	.009	.06	.2	.03	.3	.5	.06	3	2.2	15.0
L2E 100N	26.5	43.4	9.8	266	1.0	40.4	2.2	51	1.37	27.6	4.7	4.1	.1	16	1.3	8.1	.3	249	.03	.129	14	21	.05	236	.004	2	.64	.002	.06	.2	.12	.2	.7	<.05	3	4.3	15.0
L2E 50N	31.2	41.7	5.4	72	2.7	14.4	.7	15	.87	13.9	5.7	3.5	.1	39	3.1	4.6	.1	170	.04	.083	7	12	.03	526	.005	1	.35	.014	.07	.2	.34	.3	2.6	.12	2	7.2	15.0
L2E 0N	9.9	31.5	17.1	143	1.0	15.8	1.1	27	1.29	21.3	3.2	1.8	.1	28	.6	5.4	.4	156	.05	.120	11	20	.07	249	.006	2	.46	.005	.06	.2	.10	.2	.4	.06	4	3.9	7.5
L2E 50S	1.8	31.2	5.0	79	2.1	21.3	1.7	32	.74	5.2	5.1	6.5	.1	26	3.4	1.3	.1	29	.19	.090	6	6	.05	400	.012	1	.82	.017	.03	.1	.25	.5	.1	.07	3	2.8	15.0
L2E 100S	1.5	35.3	4.5	87	1.8	25.1	1.4	39	.71	4.4	5.8	4.9	.1	29	4.1	1.2	.1	27	.23	.092	6	6	.05	406	.011	1	.77	.019	.02	.1	.21	.5	.2	.08	2	2.9	15.0
L2E 150S	12.4	58.9	2.0	691	.5	144.1	34.8	3421	3.73	26.9	6.8	3.2	.2	198	28.0	4.4	.1	21	2.11	.209	2	4	.26	1449	.003	5	.53	.020	.05	.1	.15	.5	.2	.29	<.1	13.7	.5
L2E 200S	2.0	6.2	3.8	106	.2	8.9	2.5	362	.68	10.3	1.5	1.0	.1	22	1.1	.7	.1	38	.19	.141	4	5	.07	162	.006	1	.57	.018	.03	.1	.02	.1	.1	<.05	3	1.2	15.0
L2E 250S	4.3	11.6	8.4	194	.2	12.7	2.9	331	1.01	21.8	2.0	.9	.1	30	1.4	1.6	.2	86	.20	.144	7	10	.13	280	.008	1	.74	.015	.06	.3	.02	.2	.2	.08	4	1.8	15.0
L2E 300S	14.6	55.2	13.6	496	1.7	82.5	18.5	656	3.02	46.6	4.5	5.7	.4	57	4.6	8.6	.3	148	.32	.323	12	20	.18	1004	.016	2	1.48	.012	.08	.8	.37	1.1	.7	.09	3	6.7	15.0
L2E 350S	.1	2.5	.8	6	.2	.8	.9	17	.30	<.5	.1	<.5	<.1	7	<.1	.1	<.1	11	.03	.012	1	1	.02	16	.016	<.1	.13	.023	.02	<.1	.01	.1	<.1	<.05	1	<.5	15.0
L2E 400S	.5	3.9	1.7	8	.5	.8	.6	13	.29	1.1	.2	1.1	<.1	5	<.1	.3	<.1	21	.02	.015	3	3	.01	25	.010	<.1	.21	.014	.02	<.1	.02	.2	.1	<.05	2	<.5	15.0
L2E 450S	.4	4.5	1.4	7	.4	.8	.6	12	.27	.8	.2	<.5	<.1	5	<.1	.2	<.1	16	.02	.014	4	3	.01	24	.011	<.1	.25	.017	.02	<.1	.02	.1	.1	<.05	2	<.5	7.5
L2E 500S	2.3	10.4	6.6	17	.6	2.3	.6	16	.40	5.2	.7	2.4	.1	8	<.1	1.0	.1	58	.01	.027	12	9	.02	74	.010	1	.40	.006	.03	.2	.03	.3	.2	<.05	4	.9	15.0
L2E 550S	3.0	12.3	10.5	26	.6	3.6	.7	21	.64	9.3	.8	2.3	.1	12	.1	1.6	.2	84	.01	.048	11	12	.03	97	.012	1	.47	.006	.03	.2	.03	.4	.2	<.05	4	1.9	15.0
L2E 600S	.9	3.6	3.6	11	.6	1.7	.7	17	.37	2.8	.3	<.5	<.1	6	.1	.5	.1	29	.02	.022	2	3	.02	30	.007	<.1	.16	.014	.02	<.1	.02	.2	.1	<.05	1	.5	7.5
L2E 650S	1.6	4.4	3.9	16	.5	2.4	.8	18	.38	2.7	.4	1.1	<.1	6	.1	.7	.1	40	.01	.021	5	5	.02	36	.007	1	.24	.012	.03	.1	.03	.1	.1	<.05	3	<.5	7.5
L2E 700S	11.4	34.6	27.3	155	1.0	22.4	2.6	66	1.92	27.0	1.9	3.1	.1	23	.2	5.3	.4	206	.02	.086	10	22	.07	198	.004	1	.65	.005	.08	.3	.07	.3	.5	.09	8	3.8	7.5
L2E 750S	4.1	13.3	3.6	34	.3	4.5	.7	17	.46	5.8	.6	1.1	<.1	6	.1	1.6	.1	67	.01	.025	12	11	.02	70	.004	<.1	.28	.005	.03	.1	.02	.1	.2	<.05	3	.8	15.0
STANDARD DS7	20.5	105.8	67.9	405	.9	54.9	9.6	621	2.41	49.9	4.9	61.6	4.3	71	6.5	6.2	4.5	85	.92	.080	12	172	1.04	371	.122	39	.96	.079	.44	3.9	.20	2.5	4.2	.20	5	3.6	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.4	1.7	2.4	45	<1	5.2	4.2	474	1.67	<.5	1.7	<.5	3.4	42	<.1	<.1	.1	32	.38	.075	5	37	.56	196	.104	1	.82	.042	.45	.1	<.01	1.7	.3	<.05	4	<.5	15.0
L2E 800S	6.1	29.9	5.8	108	1.0	21.6	1.2	33	.98	10.8	.9	1.1	.1	11	.6	2.8	.1	92	.05	.069	4	11	.02	189	.003	2	.30	.011	.05	.1	.04	.2	<.05	2	1.6	15.0	
L2E 850S	4.2	21.9	4.2	75	1.2	14.5	1.0	23	.78	8.1	.6	<.5	<.1	9	.4	2.1	.1	68	.04	.061	3	7	.02	145	.004	1	.31	.014	.04	.1	.05	.2	<.05	2	1.2	15.0	
L2E 900S	6.0	15.8	3.9	52	.6	7.0	1.1	29	.67	7.0	.6	<.5	.1	7	.2	2.1	.1	85	.01	.032	11	9	.02	92	.004	1	.29	.008	.03	.2	.04	.1	<.05	3	1.2	15.0	
L2E 950S	7.5	15.4	10.6	77	.9	11.1	1.3	25	.83	11.6	1.0	1.1	.1	12	.1	3.3	.2	121	.01	.054	13	17	.03	106	.004	1	.48	.004	.04	.2	.05	.2	<.05	5	1.7	15.0	
L2E 1000S	1.2	5.6	2.2	10	1.2	1.7	.6	12	.29	1.4	.3	<.5	<.1	4	.1	.4	.1	20	.01	.019	6	5	.01	46	.007	1	.21	.012	.02	.1	.03	.1	<.05	2	<.5	15.0	
L2E 1050S	9.2	31.0	12.7	144	.6	20.9	3.0	152	1.74	23.2	2.5	2.5	.2	16	.4	4.5	.2	127	.02	.091	9	16	.08	166	.004	1	.62	.007	.05	.3	.16	.2	<.05	4	2.8	15.0	
L2E 1100S	3.2	11.6	5.4	41	.2	6.4	1.3	40	.67	7.4	.6	<.5	<.1	7	.2	1.3	.1	54	.01	.047	6	7	.02	80	.004	1	.43	.011	.03	.1	.03	.1	<.05	3	.8	15.0	
L2E 1150S	8.2	29.4	11.5	134	.4	20.6	2.6	55	1.65	22.5	1.6	1.9	.1	15	.3	4.2	.2	118	.01	.109	8	16	.04	174	.002	2	.41	.007	.06	.1	.08	.2	<.05	3	2.4	15.0	
L2E 1200S	2.1	5.1	2.9	26	.1	3.8	.8	15	.41	3.7	.7	<.5	<.1	6	.4	1.1	<.1	63	.02	.043	3	5	.02	124	.003	1	.24	.014	.03	.1	.03	.1	<.05	2	.6	15.0	
L2E 1250S	12.8	88.8	15.7	332	1.2	60.2	12.5	468	2.77	39.2	6.4	7.5	.8	55	1.7	9.4	.2	137	.21	.262	15	21	.15	409	.008	2	1.10	.006	.09	.5	.65	1.3	.4	.06	3	4.9	15.0
L2E 1300S	1.4	5.9	2.3	23	4	3.2	.9	16	.43	3.3	.3	<.5	<.1	6	.1	.7	<.1	26	.02	.032	2	4	.01	45	.004	1	.19	.014	.02	.1	.03	.2	<.05	1	.5	15.0	
L2E 1350S	.3	2.2	1.9	5	.3	.9	.6	14	.32	<.5	.3	<.5	<.1	5	.1	.1	<.1	10	.02	.030	1	2	.02	14	.007	<.1	.31	.023	<.05	.1	<.05	.1	<.05	2	<.5	15.0	
L2E 1400S	1.0	4.3	1.3	181	<.1	36.9	1.3	167	.33	.9	1.3	.5	<.1	12	3.5	.3	<.1	17	.16	.081	3	2	.03	81	.014	<.1	.61	.024	.02	<.1	.02	.3	.1	<.05	2	1.0	15.0
RE L2E 1400S	1.0	4.6	1.4	178	<.1	38.4	1.4	176	.36	1.0	1.3	<.5	.1	13	3.6	.3	<.1	18	.16	.084	3	2	.03	83	.014	<.1	.66	.024	.02	<.1	.03	.3	.1	<.05	2	1.1	15.0
L2E 1450S	4.0	8.7	3.3	46	<.1	6.7	.8	16	.47	3.2	.5	<.5	<.1	9	.1	1.2	.1	45	.03	.038	5	7	.02	105	.004	<.1	.51	.016	.03	.1	.02	.1	<.05	2	1.0	15.0	
L2E 1500S	42.9	24.0	2.3	147	1.1	53.8	2.0	303	.56	5.4	7.1	1.9	.1	16	1.8	2.5	.1	42	.26	.195	5	5	.05	318	.003	1	.83	.022	.02	.1	.35	.2	.1	.10	3	2.0	15.0
L3E 1700N	95.8	202.0	40.5	771	4.8	91.6	3.5	170	5.44	276.5	27.1	20.0	3.4	77	4.1	50.1	6.0	346	1.23	.979	19	44	.34	363	.020	1	1.88	.012	.13	.6	.06	2.4	.9	.18	6	49.2	15.0
L3E 1650N	100.3	250.3	42.0	583	3.8	59.8	3.9	375	11.79	443.1	22.6	38.0	5.1	80	2.2	45.7	8.3	288	.44	.714	23	46	.30	533	.038	1	1.96	.022	.20	.8	.05	4.0	1.3	.44	11	54.6	15.0
L3E 1600N	78.0	203.9	33.1	533	4.1	69.1	4.7	307	6.16	403.1	21.3	34.7	1.7	83	2.8	53.0	9.8	355	.51	.678	25	38	.33	493	.018	1	1.98	.017	.15	.6	.09	1.6	1.1	.22	7	36.8	15.0
L3E 1550N	46.8	140.0	22.7	327	7.1	39.9	4.3	539	5.07	101.1	11.5	22.7	.4	53	1.7	23.0	1.9	193	.20	.392	14	31	.19	543	.009	1	1.57	.019	.11	.5	.09	.7	.7	.25	6	21.6	15.0
L3E 1500N	13.9	70.3	8.9	317	1.6	39.6	3.0	164	.80	23.8	2.9	1.2	<.1	31	6.7	2.3	.7	30	.35	.206	5	15	.12	266	.003	2	.65	.015	.08	.2	.06	.1	.5	.13	2	16.5	.5
L3E 1450N	31.0	34.7	16.7	206	3.6	18.9	1.6	125	2.23	112.9	8.5	13.4	.7	36	.7	6.6	1.4	177	.37	.494	19	23	.15	240	.008	1	1.24	.007	.10	.8	.29	.6	.6	.10	4	21.6	15.0
L3E 1400N	8.5	14.2	3.6	69	.9	8.1	1.8	167	.93	82.7	2.1	6.5	.1	17	.3	2.7	.4	82	.21	.185	6	10	.06	138	.008	<.1	.82	.018	.04	.3	.08	.2	<.05	3	6.0	15.0	
L3E 1350N	9.7	11.4	5.9	63	.2	5.8	1.2	329	.71	23.7	.9	1.3	.1	7	.2	1.6	.4	47	.03	.099	5	6	.02	94	.003	<.1	.29	.015	.03	.1	.02	.1	<.05	2	2.6	15.0	
L3E 1300N	1.6	17.4	2.4	18	.9	3.9	.8	19	.49	20.3	2.0	1.6	<.1	7	.5	.6	.1	23	.04	.087	5	3	.03	41	.004	<.1	.52	.023	.03	.1	.04	.2	.1	<.05	2	1.9	15.0
L3E 1250N	.9	4.0	2.2	8	.1	1.1	.6	14	.38	1.9	.5	<.5	<.1	4	.1	.2	.1	12	.03	.032	2	2	.02	21	.014	<.1	.46	.019	.02	.1	.02	.1	<.05	2	<.5	15.0	
L3E 1200N	8.7	24.8	18.5	69	.2	11.5	2.3	52	2.24	48.3	1.5	99.5	.1	13	.4	4.4	.9	86	.04	.083	13	15	.09	154	.015	1	.69	.009	.06	.4	.03	.3	.3	.08	7	5.2	15.0
L3E 1150N	.7	3.6	1.8	12	.2	2.3	.8	17	.34	1.7	.5	<.5	<.1	7	.2	.2	.1	10	.04	.047	2	3	.03	58	.006	<.1	.22	.021	.03	.1	.02	.1	<.05	1	<.5	15.0	
L3E 1100N	2.2	73.4	1.0	56	.3	10.4	1.4	25	.45	1.0	.7	<.5	<.1	6	1.8	.2	.1	17	.04	.041	3	3	.03	16	.016	<.1	.20	.023	.02	<.1	.02	.1	<.05	1	1.4	15.0	
L3E 1050N	.5	1.5	2.0	7	<.1	1.2	.6	13	.29	1.6	.3	<.5	<.1	6	.1	.2	.1	13	.03	.031	1	2	.02	23	.006	<.1	.19	.025	.02	.1	.01	.1	<.05	1	<.5	15.0	
L3E 1000N	.4	2.6	1.7	15	.2	2.0	.5	13	.30	1.6	.4	<.5	<.1	8	.5	.1	.1	9	.04	.039	1	2	.02	66	.006	<.1	.29	.024	.02	.1	.02	.1	<.05	1	.7	15.0	
L3E 950N	1.7	3.9	1.9	14	1	2.1	.8	14	.35	5.5	.4	.8	.1	4	.1	.5	.1	16	.02	.036	5	2	.01	29	.006	<.1	.23	.015	.02	.1	.02	.1	<.05	2	.6	15.0	
L3E 900N	.2	1.5	.9	7	<.1	.8	.9	17	.32	<.5	.2	<.5	<.1	7	<.1	.1	<.1	12	.04	.018	<.1	1	.02	17	.012	<.1	.13	.025	.02	<.1	.01	.1	<.05	1	<.5	15.0	
L3E 850N	.3	2.8	.9	28	.1	4.2	.7	13	.22	.7	.3	<.5	<.1	7	1.4	.1	<.1	7	.04	.027	1	1	.02	82	.007	<.1	.21	.024	.02	<.1	.01	.1	<.05	1	.7	15.0	
STANDARD DS7	20.0	107.0	66.7	411	.9	54.4	9.5	613	2.35	49.0	4.7	79.7	4.3	68	6.2	5.8	4.4	82	.92	.078	12	167	1.01	360	.116	37	.92	.075	.43	3.7	.19	2.4	4.1	.20	4	3.2	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject R



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se	Sample
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	ppm	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm	gm	
G-1	.3	1.8	2.6	45	<1	5.1	4.1	498	1.76	<.5	1.7	<.5	3.4	51	<.1	<.1	.1	35	.42	.076	6	33	.59	192	.112	1	.94	.064	.50	.1	<.01	2.0	.3	<.05	5	<.5	15
L3E 800N	11.6	33.9	30.0	85	1.7	10.8	1.2	63	1.63	32.6	4.9	2.0	.4	68	1.0	8.9	.6	87	.08	.271	16	17	.14	593	.004	1	.80	.008	.10	.3	.59	.3	.8	.26	4	10.7	15
L3E 750N	37.9	20.3	21.7	82	1.7	14.8	5.7	2756	.96	26.7	2.5	1.3	.2	34	.7	7.3	.3	113	.06	.208	11	15	.05	595	.003	2	.46	.008	.09	.3	.15	.2	3.8	.13	3	5.6	15
L3E 700N	16.6	53.9	10.2	115	1.5	21.9	5.0	968	1.20	17.0	4.1	1.7	.2	31	1.1	7.4	.2	83	.08	.124	8	7	.03	252	.003	1	.85	.017	.04	.1	.21	.2	.4	.10	4	3.9	15
L3E 650N	32.1	232.7	36.7	1062	2.6	149.0	9.7	895	5.68	81.2	19.6	3.9	.5	142	15.9	16.4	.5	104	.66	.515	19	25	.16	1002	.005	3	1.20	.012	.19	.1	.36	2.1	1.1	.38	3	14.3	15
L3E 600N	27.0	48.1	16.6	215	.7	36.1	1.0	47	1.23	16.7	2.2	1.0	.2	76	.4	4.2	.3	149	.04	.156	6	28	.03	385	.003	2	.39	.013	.08	.2	.04	.3	.8	.14	3	7.0	15
L3E 550N	4.3	13.2	8.8	43	.4	5.0	.5	18	.52	10.1	1.3	1.2	.1	11	.3	2.4	.2	87	.02	.071	5	10	.03	120	.003	1	.29	.013	.03	.1	.08	.2	.2	<.05	2	1.3	15
L3E 500N	8.7	20.5	18.9	75	.3	8.6	1.3	42	1.84	41.5	1.3	2.0	.1	16	.2	6.5	.4	133	.02	.088	11	14	.05	188	.004	<1	.41	.007	.06	.2	.04	.2	.2	.06	5	3.2	15
L3E 450N	6.4	78.2	30.6	698	1.2	66.2	8.8	454	2.34	126.2	12.3	5.8	4.2	29	9.3	6.4	1.9	86	.35	.104	18	30	.54	479	.109	2	1.97	.040	.11	.7	.05	3.0	.5	<.05	6	2.9	15
RE L3E 450N	6.3	82.9	31.4	737	1.2	70.7	9.6	480	2.52	129.5	12.4	7.2	4.4	29	9.1	6.4	2.0	88	.37	.110	18	31	.57	462	.115	2	2.09	.041	.11	.6	.05	3.2	.5	<.05	6	2.9	15
L3E 400N	.7	14.1	7.0	39	.2	4.0	.8	20	.29	16.0	1.7	.9	.7	10	.3	1.1	.2	19	.13	.059	5	4	.07	46	.041	<1	.56	.022	.02	.2	.01	.7	.1	<.05	2	1.2	15
L3E 350N	11.1	37.6	19.7	39	1.2	5.6	.9	65	4.85	60.7	3.0	6.7	.6	22	.4	9.2	.4	171	.11	.438	9	37	.12	399	.014	1	1.29	.015	.07	.5	.15	.8	.4	.19	6	11.5	15
L3E 300N	4.9	13.8	18.7	38	.4	6.1	1.3	26	1.19	18.3	.6	1.6	<.1	9	.1	3.5	.3	85	.02	.055	7	9	.02	153	.006	<1	.53	.010	.03	.2	.03	.2	.2	<.05	4	2.0	15
L3E 250N	13.2	30.7	44.1	61	1.3	9.8	1.4	53	4.77	87.2	2.2	4.5	.2	27	.1	13.3	.7	253	.04	.386	10	38	.11	450	.019	1	.98	.011	.10	.3	.13	.7	.5	.24	12	9.1	15
L3E 200N	.3	2.0	.9	.9	.6	1.3	.9	26	.41	<.5	.1	.5	<.1	7	<.1	<.1	<.1	14	.03	.026	1	2	.02	18	.006	<1	.20	.023	.02	<.1	.01	.1	<.1	<.05	1	<.5	15
L3E 150N	8.2	30.1	40.5	72	.9	12.8	2.7	200	4.33	61.3	1.7	3.9	.2	20	.2	15.8	.6	163	.04	.150	11	39	.43	207	.021	1	1.27	.010	.08	.2	.06	1.2	.4	.11	8	6.1	15
L3E 100N	2.9	10.1	5.8	21	.4	3.3	1.0	26	.76	5.6	.4	1.3	<.1	6	.1	1.4	.1	42	.02	.059	4	6	.03	73	.004	<1	.31	.016	.03	.1	.01	.2	.2	<.05	2	.9	15
L3E 50N	.3	3.5	1.5	5	.3	1.4	.8	18	.40	.7	.2	<.5	<.1	6	.1	.1	<.1	11	.03	.022	1	3	.02	18	.012	<1	.62	.025	.02	<.1	<.01	.3	<.1	<.05	3	<.5	15
L3E 0N	5.2	22.9	19.3	59	.2	8.6	1.4	29	1.50	19.9	.6	1.0	.1	12	.1	4.5	.4	65	.03	.060	6	7	.03	166	.007	1	.80	.013	.07	.1	.02	.3	.3	<.05	5	4.4	15
L3E 50S	17.3	102.8	43.1	489	1.3	64.1	14.3	690	3.32	79.8	14.2	6.0	1.6	43	4.2	18.1	.7	164	.27	.170	18	30	.37	467	.037	3	1.65	.019	.12	1.1	.32	2.6	.5	.09	4	7.1	15
L3E 100S	.1	1.0	1.6	6	.3	.7	.6	14	.27	<.5	.4	<.5	<.1	8	.1	.1	<.1	8	.03	.023	1	2	.02	15	.009	<1	.28	.024	.02	<.1	.01	.2	<.1	<.05	1	<.5	15
L3E 150S	8.4	23.8	24.0	73	.2	10.7	2.1	127	1.53	22.2	.7	.8	.1	12	.1	4.5	.3	119	.01	.064	13	10	.03	173	.005	2	.45	.005	.07	.3	.02	.2	.3	.06	4	2.7	15
L3E 200S	8.1	41.8	22.0	93	.3	13.0	3.6	448	2.56	28.5	2.4	3.0	.3	14	.3	6.5	.3	113	.02	.186	7	19	.09	216	.005	1	.65	.010	.06	.2	.13	.3	.3	.11	4	4.9	15
L3E 250S	10.5	66.8	16.6	219	1.8	40.1	3.0	72	2.03	31.4	5.3	8.6	.5	40	.9	8.7	.3	173	.26	.196	14	28	.18	450	.011	3	1.32	.008	.10	.4	.44	1.1	.5	<.05	4	8.8	15
L3E 300S	6.2	54.8	12.3	192	1.4	30.7	7.3	431	1.78	20.4	2.8	5.2	.3	27	1.5	4.3	.2	121	.12	.169	8	19	.10	288	.005	3	.99	.014	.09	.2	.21	.6	.3	<.05	3	2.7	15
L3E 350S	7.9	15.8	20.9	84	.2	12.8	1.9	61	1.21	19.4	1.2	1.8	.1	15	.1	3.5	.4	171	.02	.037	14	22	.08	151	.019	2	.79	.004	.07	.2	.04	.5	.4	<.05	9	1.9	15
L3E 400S	2.5	5.4	4.1	27	.2	3.5	.8	21	.39	3.5	.5	<.5	<.1	9	.1	.8	.1	51	.03	.026	8	8	.03	148	.003	<1	.30	.009	.04	.1	.03	.1	.2	<.05	3	.6	15
L3E 450S	10.0	34.5	19.0	159	.6	26.0	2.8	105	2.70	34.5	2.5	2.1	.1	23	.4	6.2	.3	242	.03	.152	11	33	.11	184	.007	1	.96	.006	.08	.4	.10	.4	.4	.07	6	4.8	15
L3E 500S	4.0	14.8	12.4	48	.3	8.0	1.1	31	.95	9.3	1.0	1.3	.1	13	.1	1.7	.2	110	.02	.065	11	19	.06	148	.005	1	.73	.009	.05	.1	.05	.2	.4	<.05	6	1.6	15
L3E 550S	.3	5.2	1.6	6	1.5	1.9	.6	12	.24	.5	.4	.5	<.1	6	.1	.1	<.1	13	.03	.031	1	3	.02	37	.008	<1	.47	.027	.03	<.1	.04	.2	<.1	<.05	2	.6	15
L3E 600S	9.6	34.9	29.4	106	.6	16.6	3.2	285	4.22	48.7	1.9	2.3	.3	22	.2	7.8	.5	382	.03	.164	12	39	.56	179	.026	1	1.29	.005	.10	.2	.11	1.7	.5	.09	9	4.2	15
L3E 650S	3.8	14.1	11.1	39	.5	6.7	1.4	47	1.01	9.0	1.0	1.3	.1	13	<.1	1.4	.2	106	.02	.069	9	18	.07	94	.004	1	.81	.013	.05	.2	.05	.2	.3	<.05	5	1.2	15
L3E 700S	.6	4.6	1.1	7	.9	3.1	.6	10	.25	<.5	.5	.5	<.1	9	.3	.3	<.1	14	.03	.032	1	3	.02	118	.004	<1	.27	.026	.02	<.1	.04	.2	.1	<.05	1	1.0	15
L3E 750S	1.3	5.3	2.4	12	1.5	1.7	.6	13	.33	1.3	.5	<.5	<.1	6	<.1	.4	.1	40	.01	.024	10	8	.03	74	.007	1	.40	.013	.04	.1	.03	.1	.2	<.05	3	<.5	15
L3E 800S	17.8	36.8	16.7	186	.3	28.1	3.1	60	1.66	19.1	1.4	1.8	.2	22	.2	7.2	.3	228	.01	.061	16	23	.04	264	.007	2	.44	.003	.08	.2	.11	.3	.5	<.05	4	4.1	15
STANDARD DS7	20.4	106.7	68.9	403	.8	53.4	9.2	614	2.34	48.0	4.9																										



SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.3	1.9	2.7	46	<.1	4.7	4.2	483	1.71	<.5	1.8	.6	3.7	50	<.1	<.1	.1	33	.42	.078	6	30	.60	197	.110	1	.91	.057	.48	.1	<.01	1.8	.4	<.05	4	<.5	15
L3E 850S	17.7	42.9	24.5	164	.8	25.3	3.1	59	2.65	29.0	1.2	2.5	.2	28	.4	6.9	.3	193	.01	.096	12	16	.03	374	.004	2	.43	.007	.10	.5	.11	.4	.4	.12	4	5.2	15
L3E 900S	12.3	152.1	19.1	1200	5.7	140.3	4.5	170	2.28	54.8	18.5	15.5	.9	124	12.8	13.1	.3	284	.60	.231	13	46	.13	971	.004	4	.78	.007	.09	.2	11.39	2.8	1.1	.09	2	7.0	15
L3E 950S	9.7	64.5	18.5	305	3.2	56.0	3.5	122	3.70	27.5	3.0	6.1	.7	37	.6	6.3	.3	106	.02	.201	9	21	.05	310	.004	2	.54	.006	.10	.1	.29	.9	.3	.15	2	6.2	15
L3E 1000S	2.4	29.1	6.1	291	1.2	43.7	4.4	119	2.43	5.6	1.1	1.9	.6	5	.2	2.2	.2	48	.01	.075	5	11	.09	218	.006	2	1.09	.008	.06	.1	.07	1.0	.2	<.05	4	.9	15
L3E 1050S	6.1	132.7	19.9	871	.6	117.0	19.7	630	5.70	17.6	3.8	9.9	.9	16	.6	5.6	.4	57	.01	.177	12	13	.08	279	.004	4	.71	.005	.10	.1	.28	2.0	.3	.07	2	3.4	15
L3E 1100S	9.9	102.7	25.8	160	.9	29.8	12.3	659	4.89	32.7	4.0	8.7	.8	34	.4	6.9	.3	91	.03	.188	10	16	.06	298	.005	2	.85	.005	.09	.1	.58	2.0	.3	.10	2	4.6	15
L3E 1150S	7.8	62.8	10.7	182	.3	29.1	3.6	82	2.41	19.6	1.8	5.4	.2	7	.3	4.1	.2	82	.01	.106	7	12	.05	173	.005	2	.65	.012	.06	.1	.16	.5	.3	<.05	3	2.5	15
L3E 1200S	3.5	7.7	1.9	42	.2	6.3	1.2	20	.46	3.0	.4	.8	.1	5	<.1	1.2	.1	43	.01	.026	7	6	.02	80	.005	2	.31	.013	.04	.1	.02	.2	.1	<.05	2	.5	15
L3E 1250S	4.4	16.7	5.2	75	.5	11.6	2.1	57	.89	7.5	1.2	2.4	<.1	9	.2	2.4	.1	67	.02	.067	4	8	.03	159	.005	1	.47	.016	.03	.1	.06	.2	.2	<.05	2	1.5	15
L3E 1300S	12.8	34.0	13.6	152	.4	19.2	2.4	76	1.78	40.2	1.2	1.5	.1	16	.3	5.1	.2	156	.02	.089	11	17	.03	369	.004	3	.43	.008	.08	.2	.06	.3	.3	.06	4	2.5	15
L3E 1350S	.7	4.9	1.7	10	.2	2.2	.7	14	.36	1.2	.2	.7	<.1	8	<.1	.4	<.1	12	.04	.044	1	3	.01	90	.004	<.1	.18	.023	.02	<.1	.02	.2	<.1	<.05	1	<.5	15
L3E 1400S	2.7	51.0	2.6	41	4.7	40.3	1.2	39	.68	6.0	4.7	2.8	<.1	23	1.4	1.2	.1	58	.14	.255	3	12	.04	501	.002	1	.91	.024	.02	<.1	.66	.2	.4	.07	2	3.9	15
L3E 1450S	21.4	153.6	18.1	720	1.4	153.2	6.8	156	3.69	35.2	4.1	3.3	.5	26	.4	10.0	.3	220	.01	.130	15	43	.04	247	.004	2	.68	.004	.06	.1	.10	1.0	.3	<.05	4	11.7	15
L3E 1500S	18.6	164.3	43.7	763	1.8	133.9	17.9	829	7.10	52.0	9.4	14.7	3.9	322	19.1	8.6	.8	171	.38	.370	15	25	.05	503	.004	5	.83	.008	.22	.1	.52	6.2	.5	.39	2	5.7	15
L3E 1550S	19.4	209.4	11.3	189	5.1	37.7	1.3	105	.97	5.8	21.0	5.6	1.7	229	3.0	13.3	.2	972	.34	.296	18	133	.06	1696	.009	6	.61	.004	.10	.2	.75	3.7	1.4	.13	5	30.5	15
L3E 1600S	.3	2.4	.9	7	.2	1.4	.5	12	.25	<.5	.3	<.5	<.1	7	.1	.1	<.1	10	.02	.025	<.1	2	.01	34	.007	<.1	.13	.023	.02	<.1	.03	.1	<.1	<.05	1	.7	15
L3E 1650S	13.5	104.2	16.4	134	6.0	16.1	.9	39	.95	1.7	16.6	4.8	<.1	154	1.9	9.4	.2	530	.08	.220	11	80	.04	1735	.001	4	.60	.005	.12	.2	.85	.2	1.1	.23	4	31.1	15
L3E 1700S	28.1	57.1	16.0	251	2.4	39.2	1.3	31	1.74	9.0	7.2	4.5	.4	180	1.4	17.2	.2	573	.06	.260	14	85	.05	2041	.006	4	.75	.007	.11	.4	.08	.7	1.3	.26	6	33.2	15
L3E 1750S	15.2	50.2	16.4	161	1.2	26.3	1.8	40	1.63	9.8	3.9	2.2	.1	99	.6	8.4	.3	249	.05	.202	11	47	.04	1667	.004	2	.92	.009	.06	.2	.09	.4	.6	.12	6	12.9	15
L3E 1800S	6.5	17.9	8.0	59	.5	6.7	1.0	24	.70	2.8	1.5	1.3	<.1	46	.4	4.5	.1	105	.03	.100	6	18	.02	795	.005	1	.50	.015	.04	.1	.04	.2	.4	.06	3	7.3	15
L3E 1850S	.4	6.1	1.0	5	<.1	1.3	.5	11	.23	<.5	.5	.5	<.1	6	<.1	.2	<.1	10	.02	.030	1	2	.02	46	.011	<.1	.51	.023	.02	<.1	.02	.2	<.1	<.05	2	.5	15
RE L3E 1850S	.4	6.0	1.0	5	<.1	1.3	.5	11	.23	<.5	.5	.5	<.1	6	<.1	.2	<.1	9	.02	.028	1	2	.01	44	.010	<.1	.47	.019	.02	<.1	.02	.3	<.1	<.05	2	.5	15
L3E 1900S	36.8	64.8	20.9	352	3.1	57.6	1.2	22	2.85	24.9	15.5	3.6	.6	362	2.1	28.7	.3	324	.18	.575	12	82	.03	453	.006	1	1.32	.007	.14	.4	.15	1.7	1.4	.40	6	48.5	15
L3E 1950S	12.2	36.1	11.3	160	1.0	23.6	1.3	35	1.41	9.1	5.9	1.7	.2	173	1.2	10.2	.1	210	.21	.283	7	26	.05	726	.005	2	.74	.014	.07	.2	.10	.3	.8	.15	4	17.3	15
L3E 2000S	32.3	73.4	38.8	746	3.8	117.2	4.6	56	4.61	28.3	7.0	7.9	.9	39	1.1	15.0	.6	307	.02	.196	12	50	.04	544	.004	1	.88	.004	.11	.3	.33	1.7	.9	.21	5	21.4	15
L7N 1650N	14.5	98.4	24.1	1161	.9	131.3	10.4	378	2.94	81.4	5.8	6.4	1.5	21	2.0	7.9	1.4	179	.35	.291	14	40	.50	271	.059	2	2.20	.012	.15	.7	.07	2.0	.4	.06	9	6.1	15
L7N 1600N	13.9	56.7	14.5	496	1.2	49.9	4.8	300	1.92	70.5	4.7	16.3	.3	26	3.2	4.6	.4	172	.35	.262	12	20	.14	362	.007	1	1.04	.008	.06	.4	.09	.8	.4	.06	3	6.0	15
L7N 1550N	8.0	103.5	24.2	122	7.6	26.7	2.7	216	7.43	30.8	2.2	11.8	.7	19	.3	30.8	1.1	97	.08	.225	5	101	.97	404	.035	1	2.28	.013	.17	.3	.10	6.1	1.2	.38	11	59.1	15
L7N 1500N	7.7	18.0	17.4	83	.3	9.3	1.6	59	1.33	18.5	1.0	1.9	.1	8	.1	5.7	.5	84	.03	.059	7	11	.06	159	.021	<.1	.56	.012	.04	.3	.02	.3	.2	.06	5	3.7	15
L7N 1450N	17.0	102.2	159.3	214	7.8	18.6	2.7	167	7.40	38.0	5.8	25.1	.5	11	.5	27.3	17.2	140	.07	.245	11	33	.31	708	.017	1	1.34	.009	.09	.9	.19	1.5	.6	.26	10	38.1	15
L7N 1400N	14.1	38.7	32.2	141	1.0	16.5	2.3	100	3.69	42.5	2.2	8.5	.1	11	.2	20.3	.6	169	.03	.143	8	32	.13	265	.011	<.1	1.00	.010	.06	.3	.05	.4	.4	.16	7	13.0	15
L7N 1350N	13.8	31.7	42.8	105	.8	14.2	2.6	111	3.83	38.9	2.4	2.8	.1	17	.1	9.7	.8	190	.03	.174	12	33	.13	297	.009	1	1.13	.007	.06	.3	.04	.3	.5	.12	9	7.1	15
L7N 1300N	7.1	15.6	16.7	87	.6	10.6	1.7	42	1.64	21.6	1.2	2.3	.1	10	.1	6.8	.4	96	.02	.077	8	17	.07	177	.012	<.1	.58	.008	.06	.4	.04	.2	.3	.08	6	3.4	15
L7N 1250N	15.4	40.7	31.5	187	1.2	24.1	2.6	124	4.44	54.2	2.3	6.5	.2	19	.2	15.0	.7	245	.08	.174	13	40	.35	430	.023	1	1.31	.007	.11	.3	.06	.9	.6	.15	9	8.5	15
STANDARD DS7	20.7	109.0	69.9	414	.9	55.5	9.6	627	2.40	49.7	4.8	69.9	4.4	70	6.4	6.1	4.5	85	.94	.080	12	173	1.06	375	.120	38	.96	.077	.45	3.9	.20	2.4	4.2	.22	5	3.4	15

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.





SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppb	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppm	Sc ppm	Tl ppm	S %	Ga ppm	Se ppm	Sample gm
G-1	.4	1.8	3.2	44	<.1	4.5	3.9	510	1.80	<.5	2.0	.9	4.0	61	<.1	<.1	.1	34	.49	.079	8	38	.59	197	.112	2	.98	.064	.46	.1	<.01	2.5	.3	<.05	5	<.5	15.0
L7N 1200N	15.4	47.6	32.3	201	1.4	23.5	2.9	180	4.23	55.7	2.6	8.2	.6	20	.2	15.7	.7	233	.15	.270	15	43	.43	591	.024	2	2.14	.008	.16	.4	.09	1.2	.6	.21	8	10.3	15.0
L7N 1150N	6.2	13.9	20.5	73	.5	8.8	1.6	46	1.63	22.4	1.0	203.5	.1	8	<.1	6.0	1.3	112	.03	.076	7	13	.07	167	.016	2	.72	.015	.05	.9	.04	.2	.4	.07	6	2.3	15.0
L7N 1100N	3.4	7.4	11.0	41	.2	4.9	1.5	29	.99	11.7	.5	9.4	<.1	7	<.1	3.3	.7	63	.03	.052	4	6	.04	91	.012	<.1	.44	.018	.03	.6	.02	.1	.2	<.05	4	1.3	15.0
L7N 1050N	6.0	13.6	20.7	70	.4	8.3	1.9	50	1.69	22.9	1.0	11.1	.1	9	.1	5.9	.9	115	.04	.072	7	13	.09	172	.022	1	.80	.016	.05	.7	.03	.3	.3	<.05	7	2.4	15.0
L7N 1000N	.5	5.2	2.0	10	<.1	1.9	1.4	48	.58	2.1	.3	<.5	<.1	10	<.1	.6	.1	21	.10	.054	2	2	.04	40	.017	<.1	.65	.035	.03	.1	.01	.3	<.1	<.05	3	.8	15.0
L7N 950N	1.0	3.9	3.9	13	.1	2.0	1.3	52	.65	3.0	.3	<.5	<.1	8	.1	1.0	.1	27	.05	.037	2	4	.04	62	.012	<.1	.40	.029	.02	.1	.02	.2	.1	<.05	3	.8	15.0
L7N 900N	9.0	19.8	46.2	86	.4	10.8	1.9	66	2.45	29.7	1.4	1.5	.2	13	.1	7.3	.5	164	.02	.089	15	19	.07	304	.020	1	.87	.008	.08	.2	.04	.5	.6	.07	8	3.6	15.0
L7N 850N	5.9	14.7	22.2	40	.6	6.6	1.6	38	1.63	13.2	1.2	2.1	.1	11	.1	4.5	.3	69	.03	.097	6	12	.07	200	.008	1	.74	.020	.05	.3	.04	.2	.3	.08	5	3.8	15.0
L7N 800N	6.8	12.8	20.4	38	.8	5.5	1.2	32	1.72	13.1	1.1	5.3	.1	21	.1	5.1	.7	86	.05	.103	6	11	.06	392	.008	2	.53	.021	.07	.2	.06	.2	.3	.16	4	6.1	15.0
L7N 750N	2.8	28.6	4.5	25	1.8	8.3	1.4	33	.66	1.9	1.7	.7	.1	11	.9	1.5	.1	28	.07	.134	3	7	.06	160	.004	1	.54	.024	.04	.1	.11	.2	.2	.13	2	3.2	15.0
L7N 700N	.7	3.6	1.7	5	<.1	2.1	.6	16	.36	.6	.4	.5	<.1	8	.1	.2	<.1	14	.05	.031	1	3	.03	23	.011	<.1	.48	.035	.02	.1	.02	.1	<.1	<.05	3	1.1	15.0
L7N 650N	4.4	8.5	8.9	33	<.1	5.3	1.4	32	.82	12.7	.6	.7	.1	9	.1	2.1	.2	69	.03	.030	8	8	.03	84	.008	1	.37	.016	.05	.1	.01	.2	.3	<.05	4	1.6	15.0
L7N 600N	32.3	185.3	32.6	736	2.5	116.9	27.4	1992	5.69	88.6	20.0	2.0	3.3	32	9.4	22.1	.5	201	.18	.184	14	30	.24	260	.028	3	3.25	.012	.13	.8	.48	3.9	.8	.39	4	14.7	7.5
L7N 550N	.1	4.2	.8	3	<.1	.7	.6	16	.25	1.4	.3	<.5	.1	9	<.1	.4	<.1	7	.11	.048	2	1	.03	12	.017	<.1	.42	.033	.02	<.1	<.01	.4	<.1	<.05	1	<.5	15.0
L7N 500N	.6	7.4	2.2	13	<.1	1.6	1.0	26	.37	3.1	.8	<.5	.1	9	<.1	.8	.1	15	.09	.043	2	2	.04	24	.017	<.1	.41	.034	.03	.1	.02	.4	<.1	<.05	1	.5	15.0
L7N 450N	6.7	30.1	11.6	61	.3	7.1	1.8	114	1.19	24.9	2.2	1.0	.1	12	.2	6.0	.2	85	.08	.092	6	10	.09	125	.012	1	.69	.023	.05	.4	.06	.4	.3	<.05	3	2.4	15.0
L7N 400N	3.2	46.1	3.8	201	1.1	61.6	5.0	332	.50	<.5	4.8	3.1	.2	62	26.8	2.7	.1	14	.70	.297	4	4	.14	472	.004	4	.65	.024	.05	.1	.32	1.0	.2	.39	1	12.0	.5
L7N 350N	5.8	70.6	3.3	185	2.1	52.6	4.3	208	.69	1.6	7.5	5.7	.2	50	27.2	4.6	.1	22	.59	.355	7	7	.14	137	.004	3	1.07	.014	.04	.1	.48	1.6	.4	.38	1	9.8	7.5
L7N 300N	8.3	37.0	7.1	285	1.3	36.0	2.3	161	1.84	17.2	3.3	7.8	.5	39	1.5	5.0	.2	197	.31	.117	12	26	.21	433	.009	6	1.14	.018	.15	.2	.31	.9	.5	<.05	5	3.2	15.0
L7N 250N	16.5	58.9	13.7	288	2.3	79.2	14.7	5785	2.09	16.4	5.5	4.8	.3	58	27.4	5.3	.2	93	.50	.278	11	19	.18	689	.005	6	1.30	.013	.12	1.3	.34	.6	.5	.18	4	6.3	.5
L7N 200N	11.7	94.9	18.7	288	1.7	49.3	9.5	337	2.53	30.7	6.7	8.9	.5	45	2.5	8.2	.3	241	.22	.238	16	36	.21	627	.008	8	1.41	.010	.22	.3	.46	.8	.6	.09	5	5.4	15.0
RE L7N 200N	11.9	95.2	18.6	291	1.7	49.6	9.8	342	2.58	31.1	6.7	8.7	.6	46	2.5	8.0	.3	223	.22	.237	16	34	.20	598	.007	7	1.30	.008	.19	.3	.47	1.0	.5	.08	5	5.5	15.0
L7N 150N	8.5	23.2	11.7	105	.1	16.0	3.7	175	1.57	13.4	1.0	34.3	.6	18	.4	3.0	.3	116	.03	.058	14	17	.07	269	.009	2	.68	.010	.12	.2	.01	.4	.3	.06	5	2.0	15.0
L7N 100N	21.0	117.3	19.0	631	1.8	91.0	8.8	259	2.60	39.7	8.5	4.8	.6	21	2.1	12.6	.4	410	.21	.210	15	44	.29	390	.014	7	1.50	.008	.20	.3	.41	1.4	.8	<.05	5	6.0	15.0
L7N 50N	.8	13.8	2.0	16	.2	4.3	.4	17	.14	<.5	1.2	.8	.1	15	1.0	.6	<.1	5	.18	.078	3	2	.04	90	.028	<.1	.54	.033	.02	<.1	.04	.4	.1	<.05	3	10.1	15.0
L7N ON	7.4	48.1	12.8	261	.8	36.6	5.3	322	2.20	21.3	3.8	5.3	.6	28	.9	4.1	.3	188	.17	.147	14	32	.26	451	.009	6	1.60	.006	.18	.4	.23	1.2	.5	<.05	5	3.4	15.0
STANDARD DS7	20.3	109.9	69.0	413	.9	55.8	9.6	643	2.46	49.8	4.9	67.9	4.4	77	6.3	6.1	4.6	85	.97	.079	14	181	1.07	373	.123	38	1.03	.081	.44	4.0	.19	2.6	4.2	.22	5	3.4	15.0

Sample type: SOIL SS80 60C. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.



ASSAY CERTIFICATE



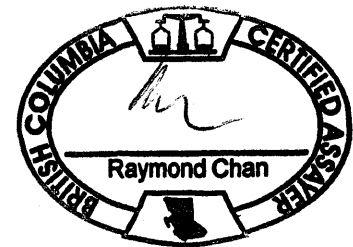
Aurora Geosciences Ltd. (Whitehorse) PROJECT North Canol File # A608826R

108 Gold Road, Whitehorse YT Y1A 2W3 Submitted by: Scott Casselman

SAMPLE#	Zn %	Ag gm/mT
ITSI-RS-12	3.85	14
STANDARD R-3	4.11	202

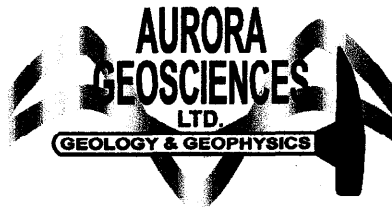
GROUP 7AR - 1.000 GM SAMPLE, AQUA - REGIA (HCL-HNO3-H2O) DIGESTION TO 100 ML, ANALYSED BY ICP-ES.  
- SAMPLE TYPE: ROCK PULP

Data \_\_\_ FA \_\_\_ DATE RECEIVED: DEC 17 2006 DATE REPORT MAILED: ..... **DEC 28 2006**



**APPENDIX III**

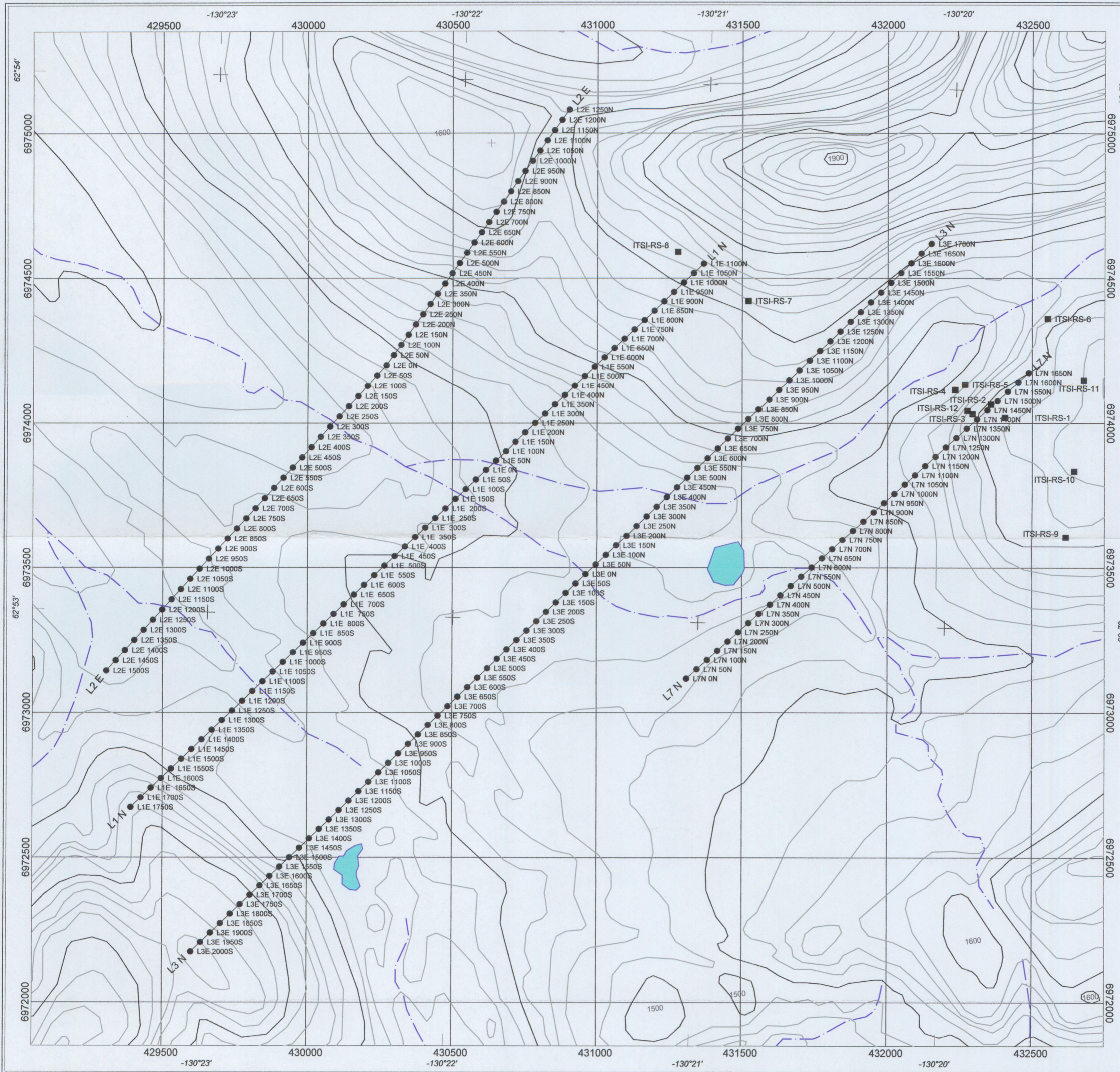
**CREW LOG**



**CREW LOG  
BOOTLEG EXPLORATION INC.  
NORTH CANOL RECONNAISSANCE PROJECT  
September 7 to 17, 2006**

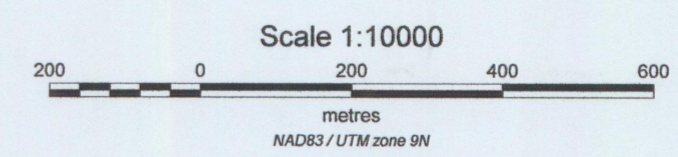
**Crew:** Scott Casselman (Project Manager)  
Casey Adshead (Crew Chief)  
Michael Mark (Field assistant)  
Calvin Delwisch (expediter)

- Thur, Sept 7** Casey Adshead spends 1.5 hours getting gear ready for departure on Saturday.
- Sat, Sept 9** Casey and Michael depart for Ross River at 11:00 am. Crew meets with Brian Parson of Trans North and picks up fuel for next days mob to property.
- Sun, Sept 10** Crew departs Ross River around 7:00 am and drives up North Canol to staging area (approx 4 hour drive). Meet Brian Parsons there and mobilize gear to property and set-up camp.
- Mon, Sept 11** Crew starts prospecting and soil sampling working on line near camp on Line L1 on east side of the valley and L2 on west side of valley.
- Tue, Sept 12** Crew works on L3 area on the east side of the valley, 500 m southeast of L1.
- Wed, Sept 13** Crew works on L4 area 500 m NW of L1.
- Thur, Sept 14** Crew works on L5 area on the western extension of L3.
- Fri, Sept 15** Crew works on L6 area on the western extension of L4.
- Sat, Sept 16** Crew works on L7 area – soil samples both sides of valley.
- Sun, Sept 17** Helicopter arrives at 10:00 am and flies crew and gear to North Canol road. Crew drives back to Whitehorse.

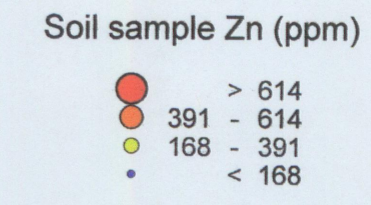
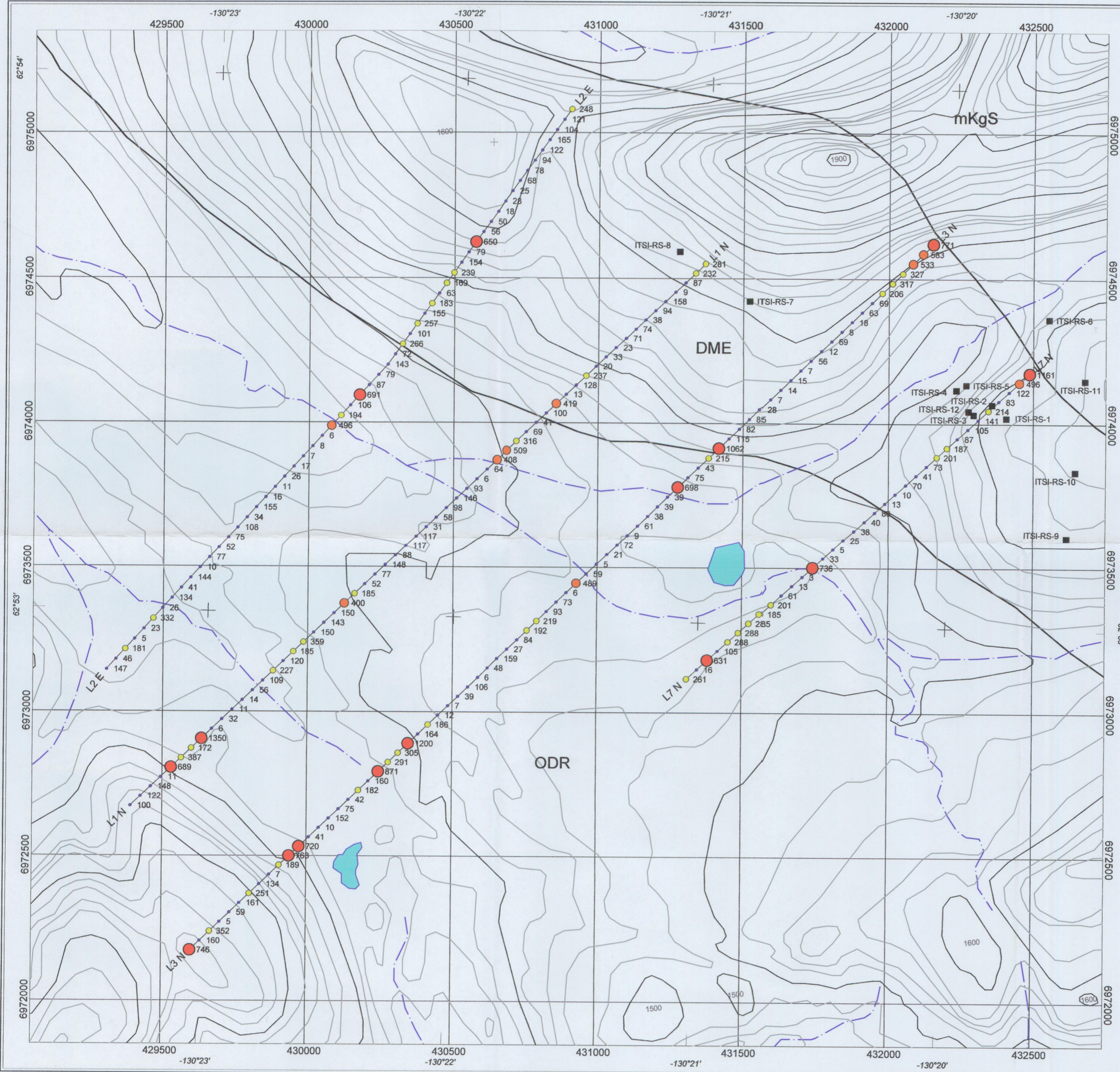


- Soil sample location
- Rock sample location

10 January 2007  
 S. G. CASSELMAN  
 PROFESSIONAL ENGINEER  
 BRITISH COLUMBIA



<b>BOOTLEG EXPLORATION INC.</b>	
<b>NORTH CANOL RECONNAISSANCE PROJECT</b>	
<b>Figure 4 - SAMPLE LOCATION MAP</b>	
NTS: 105J16	Mining District: Watson Lake
Datum: NAD83	Projection: UTM, zone 9
Date: January 3, 2007	Job: BEI-06-03-YT
<b>AURORA GEOSCIENCES LTD</b>	



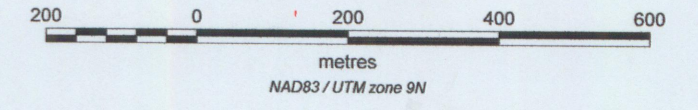
■ Rock sample location

Rock sample geochemistry

Sample	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	Cd (ppm)
ITSI-RS-1	12.03	16.09	112.7	1806	1.4	0.3
ITSI-RS-2	38.97	10.31	320.3	1966	1.6	3.88
ITSI-RS-3	48.23	11.39	96.6	2065	1.8	1.21
ITSI-RS-4	224.84	30.48	35.4	3894	3.7	0.7
ITSI-RS-5	200.9	17.62	498.6	3163	6.1	5.66
ITSI-RS-6	48.37	13.16	60.5	2252	1.3	1.15
ITSI-RS-7	48.68	9.05	686.5	1115	1	1.99
ITSI-RS-8	169.59	5.26	100.1	742	6.4	0.69
ITSI-RS-9	4.31	20.12	40.7	192	3.7	0.15
ITSI-RS-10	76.92	10.71	148.8	688	1.6	0.92
ITSI-RS-11	178.86	2.44	22	2198	2	0.3
ITSI-RS-12	343.04	6.53	38500	12600	32.7	382.63

- mKgS mid Cretaceous Selwyn Suite Intrusion
- DME Devonian to Mississippian Earn Group sediments
- ODR Ordovician to Devonian Road River Group sediments

15 January, 2007  
  
 Scale 1:10000

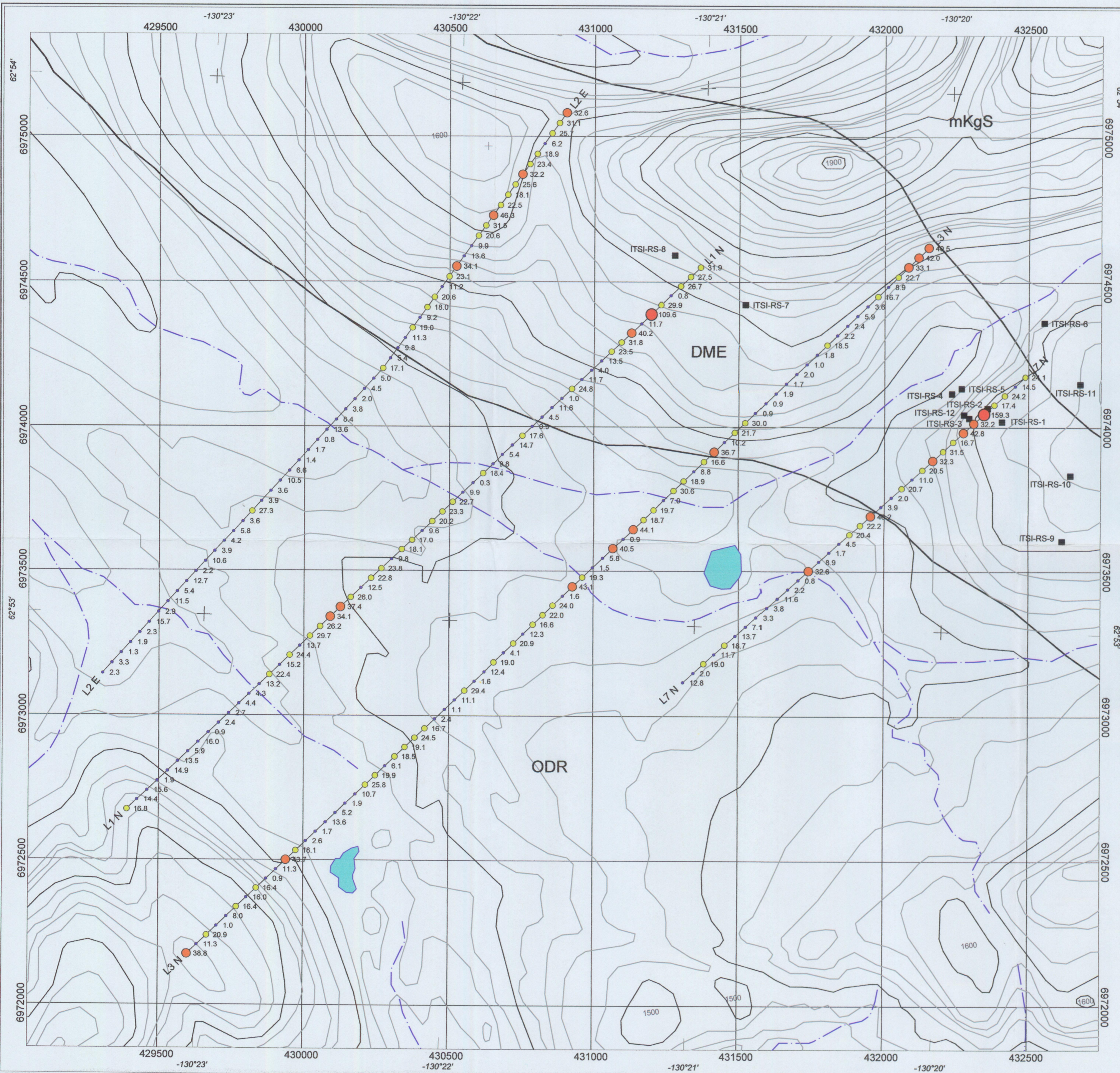


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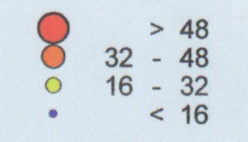
**NORTH CANOL RECONNAISSANCE PROJECT**  
**Figure 5 - SOIL SAMPLE ZINC GEOCHEMISTRY**

NTS: 105J16      Mining District: Watson Lake  
 Datum: NAD83      Projection: UTM, zone 9  
 Date: January 3, 2007      Job: BEI-06-03-YT

**AURORA GEOSCIENCES LTD**



Soil sample Pb (ppm)

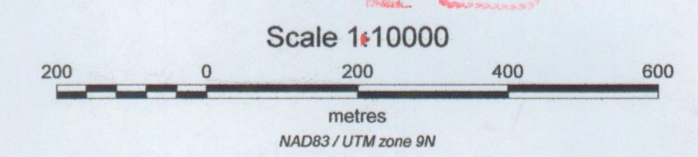


Rock sample location  
Rock sample geochemistry

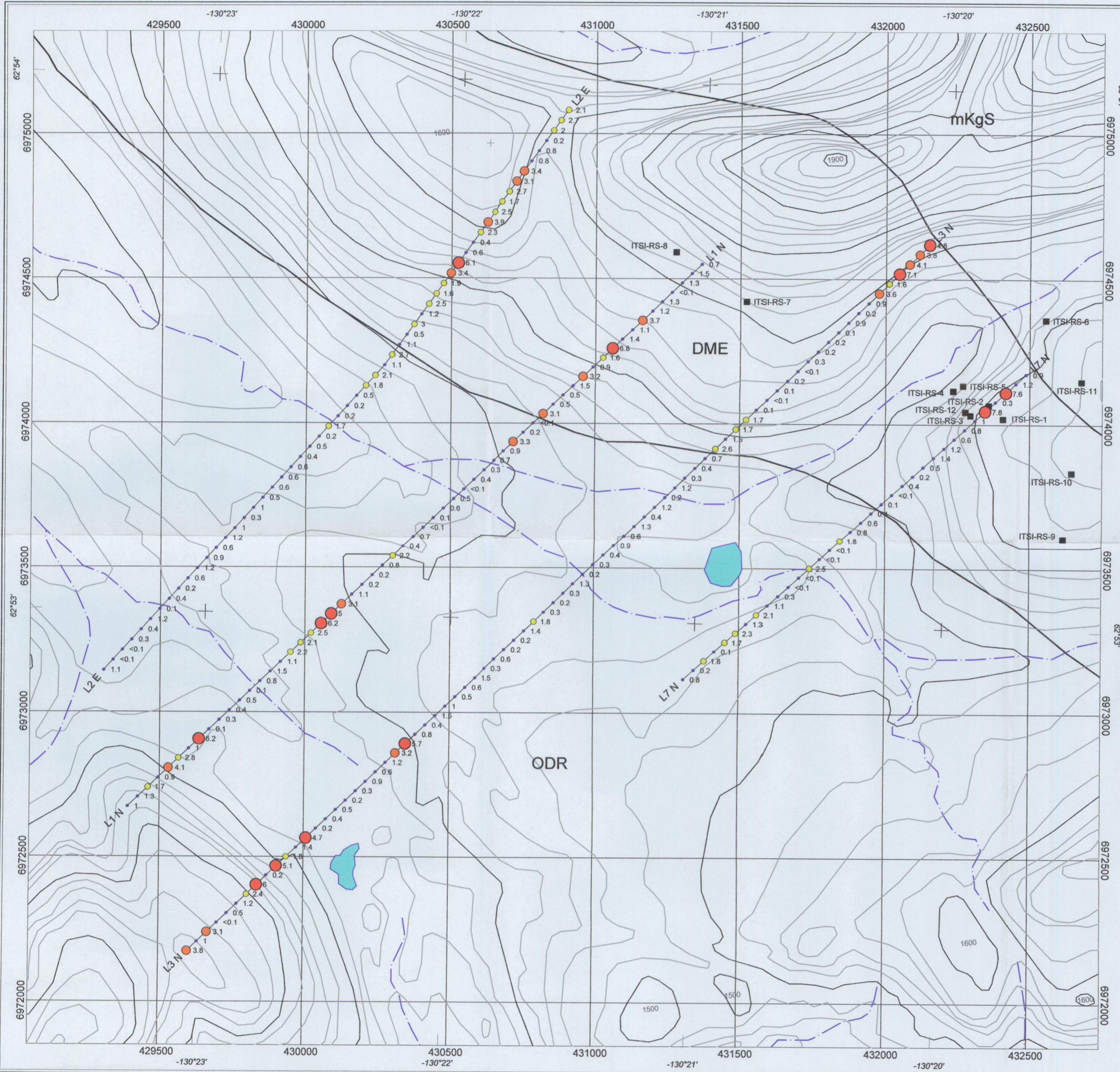
Sample	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	Cd (ppm)
ITSI-RS-1	12.03	16.09	112.7	1806	1.4	0.3
ITSI-RS-2	38.97	10.31	320.3	1966	1.6	3.88
ITSI-RS-3	48.23	11.39	96.6	2065	1.8	1.21
ITSI-RS-4	224.84	30.48	35.4	3894	3.7	0.7
ITSI-RS-5	200.9	17.62	498.6	3163	6.1	5.66
ITSI-RS-6	48.37	13.16	60.5	2252	1.3	1.15
ITSI-RS-7	48.68	9.05	686.5	1115	1	1.99
ITSI-RS-8	169.59	5.26	100.1	742	6.4	0.69
ITSI-RS-9	4.31	20.12	40.7	192	3.7	0.15
ITSI-RS-10	76.92	10.71	148.8	688	1.6	0.92
ITSI-RS-11	178.86	2.44	22	2198	2	0.3
ITSI-RS-12	343.04	6.53	38500	12600	32.7	382.63

- mKgS mid Cretaceous Selwyn Suite Intrusion
- DME Devonian to Mississippian Earn Group sediments
- ODR Ordovician to Devonian Road River Group sediments

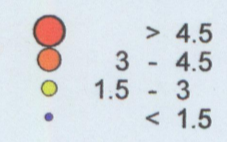
15 January, 2007  
 OF  
 S. G. CASSELMAN  
 BRITISH  
 COLUMBIA



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<b>NORTH CANOL RECONNAISSANCE PROJECT</b>	
<b>Figure 6 - SOIL SAMPLE LEAD GEOCHEMISTRY</b>	
NTS: 105J16	Mining District: Watson Lake
Datum: NAD83	Projection: UTM, zone 9
Date: January 3, 2007	Job: BEI-06-03-YT
<b>AURORA GEOSCIENCES LTD</b>	



Soil sample Silver (ppm)



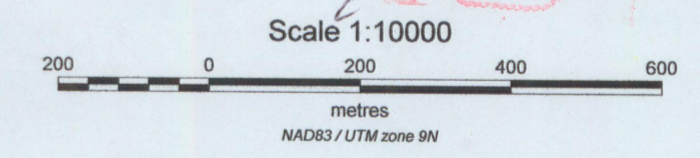
Rock sample location

Rock sample geochemistry

Sample	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	Cd (ppm)
ITSI-RS-1	12.03	16.09	112.7	1806	1.4	0.3
ITSI-RS-2	38.97	10.31	320.3	1966	1.6	3.88
ITSI-RS-3	48.23	11.39	96.6	2065	1.8	1.21
ITSI-RS-4	224.84	30.48	35.4	3894	3.7	0.7
ITSI-RS-5	200.9	17.62	498.6	3163	6.1	5.66
ITSI-RS-6	48.37	13.16	60.5	2252	1.3	1.15
ITSI-RS-7	48.68	9.05	686.5	1115	1	1.99
ITSI-RS-8	169.59	5.26	100.1	742	6.4	0.69
ITSI-RS-9	4.31	20.12	40.7	192	3.7	0.15
ITSI-RS-10	76.92	10.71	148.8	688	1.6	0.92
ITSI-RS-11	178.86	2.44	22	2198	2	0.3
ITSI-RS-12	343.04	6.53	38500	12600	32.7	382.63

- mKgS mid Cretaceous Selwyn Suite Intrusion
- DME Devonian to Mississippian Earn Group sediments
- ODR Ordovician to Devonian Road River Group sediments

15 January 2007  
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 BRITISH COLUMBIA



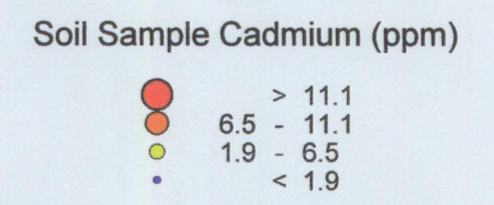
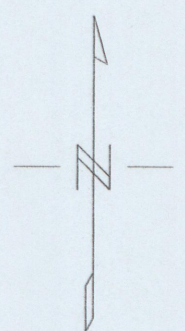
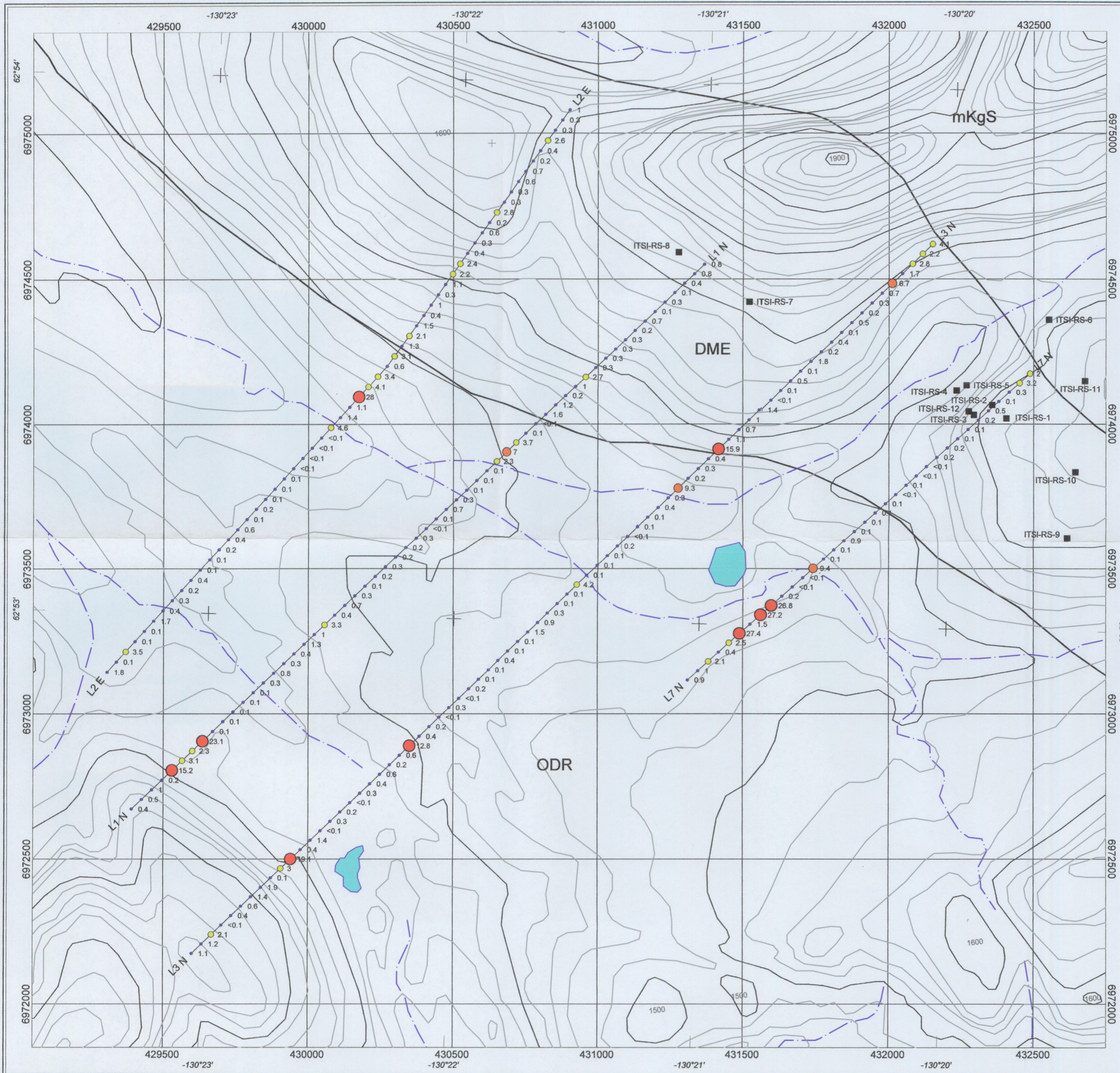
**BOOTLEG EXPLORATION INC.**

**NORTH CANOL RECONNAISSANCE PROJECT**  
**Figure 7 - SOIL SAMPLE SILVER GEOCHEMISTRY**

NTS: 105J16 Mining District: Watson Lake  
 Datum: NAD83 Projection: UTM, zone 9  
 Date: January 3, 2007 Job: BEI-06-03-YT

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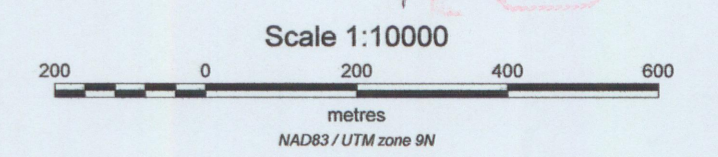


■ Rock sample location  
 Rock sample geochemistry

Sample	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	Cd (ppm)
ITSI-RS-1	12.03	16.09	112.7	1806	1.4	0.3
ITSI-RS-2	38.97	10.31	320.3	1966	1.6	3.88
ITSI-RS-3	48.23	11.39	96.6	2065	1.8	1.21
ITSI-RS-4	224.84	30.48	35.4	3894	3.7	0.7
ITSI-RS-5	200.9	17.62	498.6	3163	6.1	5.66
ITSI-RS-6	48.37	13.16	60.5	2252	1.3	1.15
ITSI-RS-7	48.68	9.05	686.5	1115	1	1.99
ITSI-RS-8	169.59	5.26	100.1	742	6.4	0.69
ITSI-RS-9	4.31	20.12	40.7	192	3.7	0.15
ITSI-RS-10	76.92	10.71	148.8	688	1.6	0.92
ITSI-RS-11	178.86	2.44	22	2198	2	0.3
ITSI-RS-12	343.04	6.53	38500	12600	32.7	382.63

- mKgS mid Cretaceous Selwyn Suite Intrusion
- DME Devonian to Mississippian Earn Group sediments
- ODR Ordovician to Devonian Road River Group sediments

15 January, 2007  
*Stuart*

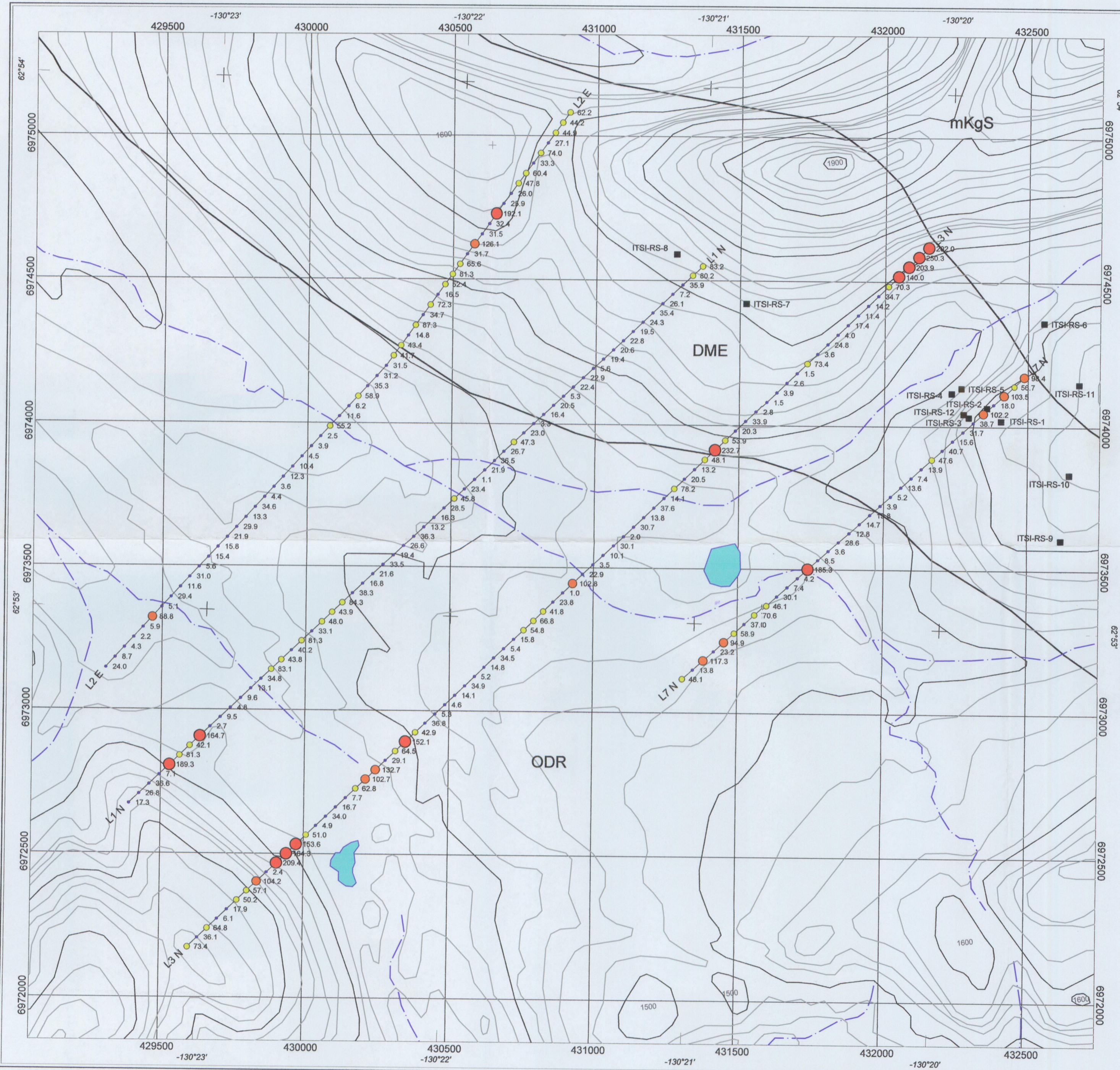


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**NORTH CANOL RECONNAISSANCE PROJECT**  
**Figure 8 - SOIL SAMPLE CADMIUM GEOCHEMISTRY**

NTS: 105J16      Mining District: Watson Lake  
 Datum: NAD83      Projection: UTM, zone 9  
 Date: January 3, 2007      Job: BEI-06-03-YT

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Soil sample Copper (ppm)

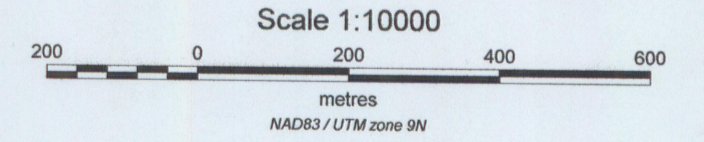
- > 133.4
- 87.5 - 133.4
- 41.6 - 87.5
- < 41.6

Rock sample location  
Rock sample geochemistry

Sample	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	Cd (ppm)
ITSI-RS-1	12.03	16.09	112.7	1806	1.4	0.3
ITSI-RS-2	38.97	10.31	320.3	1966	1.6	3.88
ITSI-RS-3	48.23	11.39	96.6	2065	1.8	1.21
ITSI-RS-4	224.84	30.48	35.4	3894	3.7	0.7
ITSI-RS-5	200.9	17.62	498.6	3163	6.1	5.66
ITSI-RS-6	48.37	13.16	60.5	2252	1.3	1.15
ITSI-RS-7	48.68	9.05	686.5	1115	1	1.99
ITSI-RS-8	169.59	5.26	100.1	742	6.4	0.69
ITSI-RS-9	4.31	20.12	40.7	192	3.7	0.15
ITSI-RS-10	76.92	10.71	148.8	688	1.6	0.92
ITSI-RS-11	178.86	2.44	22	2198	2	0.3
ITSI-RS-12	343.04	6.53	38500	12600	32.7	382.63

- mKgS mid Cretaceous Selwyn Suite Intrusion
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- ODR Ordovician to Devonian Road River Group sediments

15 January 2007  
G. CASSELL  
BRITISH COLUMBIA  
Geological Survey



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**NORTH CANOL RECONNAISSANCE PROJECT**  
**Figure 9 - SOIL SAMPLE COPPER GEOCHEMISTRY**

NTS: 105J16 Mining District: Watson Lake  
 Datum: NAD83 Projection: UTM, zone 9  
 Date: January 3, 2007 Job: BEI-06-03-YT

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